

**AN INTERACTIVE RIVER BASIN  
WATER MANAGEMENT MODEL:  
SYNTHESIS AND APPLICATION**

by

**John M. Shafer**

**August 1979**

**COLORADO WATER RESOURCES**



**RESEARCH INSTITUTE**

**Colorado State University  
Fort Collins, Colorado**

**Technical Report No. 18**

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This research was partially supported by funding provided by the Legislative Council of the Colorado General Assembly and by funds from the U. S. Department of the Interior, Office of Water Research and Technology (authorized under P.L. 95-467). It is the author's doctoral dissertation.

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## ABSTRACT

### AN INTERACTIVE RIVER BASIN WATER MANAGEMENT MODEL: SYNTHESIS AND APPLICATION

A computer model is presented for quantifying the impacts of multi-purpose water management policy. The model is designed for the analysis of water availabilities throughout a river basin over extended time periods. It is capable of simulating the monthly storage, flow, and diversion of water in a complex river basin system. The prototype system is represented in the model by a network of interconnected nodes which characterize the reservoirs, tributary inflow points, and diversion points in the basin. Linkages between nodes represent the conveyance morphology of the basin.

The model, MODSIM, is synthesized from previously existing models. A base or core model is selected from these models, and further modified so as to better conform to the attributes and capabilities considered desirable for the model.

An advantage of the model is its optimizing capability with respect to reservoir operating rules. Also, MODSIM is able to simulate institutional dictates governing water allocation, such as water rights priorities. Conveyance losses and return flows resulting from irrigation practices can also be considered by MODSIM.

MODSIM is interfaced with an interactive conversational data management package. Conversational programming facilitates the rapid analysis of management alternatives, and promotes the successful transfer of

this technology to water planners and managers with little background in computer programming.

Two case studies are presented which demonstrate the utility of MODSIM for aiding in the analysis of impacts of long-term changes in water resource management within a river basin. The Cache la Poudre River Basin in north-central Colorado is used for both case studies. The first case study involves the analysis of opportunities for including recreation in a multipurpose management framework for selected high mountain reservoirs. The second case study addresses the availability of a firm water supply for the proposed Rawhide coal-fired power generation facility.

Model calibration studies are undertaken for both analyses. The calibration studies clearly show the model is capable of accurately simulating the important physical and institutional aspects of water allocation in the basin. The methodologies for evaluating the impacts of the alternative management schemes for each case study are presented, followed by an extensive discussion of the results.

The case studies show that (1) in selected high mountain reservoirs recreation opportunities can be provided by maintaining satisfactory storage levels without causing injury to downstream water users, and (2) sufficient reusable effluent from the City of Fort Collins, Colorado, is available (given the hydrology considered) to meet power plant demand. Together, the case studies represent a viable demonstration of the capabilities of the model.

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CHAPTER I  
INTRODUCTION

Water resources planners and managers are commissioned with the responsibility of developing water policy which provides an atmosphere of consistency and equitability in water administration. During the past decade certain *tools* have become available to the planner/manager which enable him to perform complex analyses of alternate management strategies otherwise impossible within a reasonable time frame. Hopefully, these *tools*, such as computer models and data management systems, provide the means to test the impact of various water resources policies with reasonable accuracy before these policies are actually implemented.

Many computer models exist for evaluating a wide range of water resources problems. Often, too much emphasis is placed on the development of new models, and not enough emphasis on the application of good models already available for actual water resources planning and management. Unfortunately, and for a variety of reasons, many of these models have not been employed to any large degree. Perhaps due to lack of consideration of the requirements and needs of those who will use the model, many efforts of model implementation have failed. However, through modern techniques of interactive conversational computer programming, a new group of potential users may be reached; indeed, a group of users more directly involved in water policy decision-making.

### A. Objectives

There are two principal objectives of this study. The first is the synthesis of a computerized river basin water management model from currently *existing* models. The model is developed in an interactive conversational mode so that familiarity with computer programming is not essential for model usage. Only a rudimentary knowledge of the computer operating system on which the model is implemented is required for successful operation. The intended purpose of this model is to provide State and local water resources planners and managers with a comprehensive and useful tool for evaluating the impacts of alternate water management policies on water availabilities at various critical points in a river basin. Although MODSIM is in reality a long-term water management model, it could be used to evaluate several differing water planning alternatives; however, it has no inherent ability to select the best plan internally.

The second objective of this research is to demonstrate the application of the model through the comprehensive analysis of two specific case studies. The case study approach is an excellent method for introducing the model and its associated advantages and limitations, along with the underlying assumptions concerning its design. The case studies presented in this report are both realistic and varied. They provide potential users with insight into the types of problems that the model can aid in solving, and also, provide users with guidelines concerning problem formulation, data management, and interpretation of results.

### B. Justification

The need for such a model is very much in evidence in many western States of the United States. Though this study will focus on Colorado

water problems, this should by no means detract from the general applicability of the model. Colorado water resources planners and policy makers are facing increasingly challenging problems concerning allocation of the water resources of the State. Water is of critical economic, social, and environmental importance to Colorado. Unfortunately, only a finite raw water supply is made available each year from spring snow-melt in the Colorado Rockies. A portion of this annual supply is captured in a complex network of interconnected storage reservoirs, and then allocated for satisfaction of various competing demands within Colorado, as well as interstate compact agreements for water leaving the State. In years past, when demands placed on raw water supply were lower and the uses less diverse, this system of water collection and distribution was largely self-administering under the Colorado appropriative doctrine.

The Front Range of Colorado, in particular, is experiencing a steadily growing pressure on available water resources. This pressure originates from both direct and indirect influences on demand. For example, expanding urban centers require more water for domestic and industrial uses, which often is obtained through transfer of irrigation water rights. Irrigated agriculture is still the leading water user in Colorado, and greater attention should be focused on more efficient use of water diverted for agriculture. In-stream uses of water resources, as well as water-related recreation, are being given an increasingly higher priority. Finally, the prospect of large-scale energy development in Colorado presents perhaps the greatest challenge when considering some of the projected water requirements for this use. Such energy related endeavors will not only have considerable economic importance



in Colorado, but national implications as well. Rationally, one can only expect that competition for waters originating in Colorado will greatly intensify.

A complex institutional framework has evolved within which this supply/demand cycle operates. Increased demand, however, has led to over-appropriation of waters along the Front Range. Additional diversion of western slope waters is being scrutinized, but this source is limited. In an effort to extend the supply as far as possible, formal arrangements for the reuse or secondary use of water are being pursued, although in practice such a policy has been in existence since the first diversion of water for irrigation purposes. Of the water applied to croplands, a certain portion not consumptively used finds its way back to the stream for subsequent reuse. As the irrigation season progresses, the amount of *return flow* accruing to the river can be significant, as is the case with the Cache la Poudre River Basin in north central Colorado.

W.D. Farr, Chairman of the City of Greeley, Colorado Water and Sewage Board, (1977) stated that:

There is not very much more water that can be developed. The problem is to best manage and utilize our total water supplies not only on a day to day basis, but on a prudent plan for years ahead.

The use of modern systems analysis techniques coupled with high speed digital computers will go a long way in helping achieve effective and efficient water resources planning and management. The use of system analysis techniques in water resources planning and management has gained in acceptance in recent years. Due to the large-scale nature of most physical water resource systems, and the corresponding quantity and

diversity of data, a systematic treatment of problems becomes somewhat mandatory if such problems are to remain tractable. By definition, the systems approach to problem solving specifies an orderly stepwise solution strategy for these complex problems. Such an endeavor aids the planner/manager in pinpointing data requirements and facilitates the rapid analysis of many management schemes. Also, a general modeling framework can be developed that is not basin specific. This allows the planner/manager the flexibility of analyzing problems occurring in different basins using the same model structure. Once this basic model structure has been developed, there is the added advantage of being able to systematically incorporate new data and information as they become available.

#### C. Contribution

This study provides a two-fold contribution to the body of knowledge pertaining to water resources engineering. Generally, the contribution is of both theoretical and practical significance. First, a new computerized water management model is synthesized from previously existing models. This, in itself, is of little practical importance in that new computer models are created with considerable regularity. However, a goodly portion of these new models cannot be used much beyond a small circle of developers and experienced computer programmers. It is the author's firm belief that for a computerized river basin model to have practical, *real world* problem solving potential, it must be capable of being comprehended and employed by those individuals who would benefit most from its use. These individuals are the local and State agency water planners and managers who must actually wrestle with the problems

of water allocation. To this end, MODSIM was developed in an interactive conversational model which allows operation of the model without appreciable computer science training. A theoretically sound model with real practical advantages has been developed. There are few examples of the development and application of interactive river basin water management models, especially those developed in a conversational mode.

The types of problems which the model can be of aid in solving are varied. For instance, upon successful calibration, MODSIM can be used to perform impact analyses and determine sensitivities of:

1. potential critical period hydrologies
2. transfers of water use
3. variations in water rights structure within a river basin
4. changes in water demands
5. new or modified structural facilities such as reservoirs, canals, pipelines, etc.
6. availabilities and/or use of imported water
7. minimum streamflows as dictated by state and federal water quality regulations
8. water conservation and reuse measures.

Finally, it must be noted that computer modeling is an evolutionary process. Most models are in a constant state of flux as new technology becomes available and new theory is tested. As experience is gained through model application, changes are made to better reflect the aspirations of the user. In this way, a constantly improving product results. It is expected that MODSIM will undergo several changes in the future. Ultimately, an accepted and useful tool will emerge which extends the capability of planners and managers beyond that currently realized.

## CHAPTER II

### REVIEW OF SELECTED MODELS

As stated in the introduction, there are a considerable number of river basin computer models currently in existence. These models were developed to aid in the analyses of certain classes of water resource problems. All models are created for a particular purpose. Even within the same class of models (e.g., river basin models) the intended purpose may vary widely. For instance, within a group of river basin simulation models, there may be long-term planning models, real-time operational models, models designed for economic analyses, hydraulic or hydrologic models, surface water models, ground-water models, conjunctive use models, and so forth.

The principal objective of this study is to synthesize from these *existing* models, one model which is better suited for the analysis of water availabilities throughout a river basin resulting from alternate water management policies over long-term planning horizons. This model synthesis is undertaken with a specific user group in mind; State and local governmental water resources planners and managers. However, in order to accomplish this task, the attributes of the most realistically desirable model for the above stated purpose must first be set forth against which the existing models are evaluated and also against which the synthesized model is ultimately judged.

A. Attributes of the Desired River Basin Water Management Model

Basic to the assumption that a desirable model can be perceived is the premise that the model must be capable of simulating the operation of a complex river basin system (by monthly time increments) over a multi-year planning period. Monthly time increments are preferred because they usually provide sufficient accuracy over long time periods and are compatible with available data. Also, monthly time increments enable as detailed as possible analysis of water transfer without the consideration of the necessity for hydrologic routing of flow. In addition, a longer time increment, such as seasonal, does not provide for sufficient temporal resolution required to calibrate MODSIM as accurately as possible. The desirable model should also have the capability of considering the institutional framework within which the physical system functions. This extension beyond typical water accounting models makes it especially useful for studying systems where existing or planned priorities among various beneficial uses of water must be preserved. Also, the model must be *presentable*; that is, it must not be so obscure in methodology and difficult in application to prevent its usage regardless of its ability to analyze the problem.

Thus, a realistic river basin water management model might include the following attributes:

1. An interactive, conversationally programmed input data file to facilitate ease of usage by the planner/manager.
2. Simulation of the water storage, transport, and distribution morphology of the system, including reservoir operation in monthly time increments. The model should have optimizing capability with

respect to reservoir operation and demand satisfaction, since searching among a myriad of possible operating rules can be extremely time consuming.

3. Consideration of non-beneficial consumptive losses such as reservoir evaporation and conveyance losses, though the latter may not actually be lost from the system.
4. Inclusion of the quantifiable aspects of institutional structures governing stream diversion and water storage.
5. Consideration of consumptive water use from municipal and agricultural sectors. Such consideration may range in detail from evapotranspiration prediction using climatic factors, to estimation of demand patterns from historical records.
6. Inclusion of possible imports to the basin from adjacent river basins.
7. Options for including the stochastic nature of inflows, perhaps using rainfall-runoff watershed models to predict virgin streamflows.
8. Flexibility to differentiate between energy consuming pumped pipeline flow and gravity channel flow.
9. Reasonably accurate consideration of irrigation return flows. A high degree of flexibility exists here in appropriate model detail necessary for stream-aquifer interactions within a long-term planning context.
10. Well documented and sufficiently demonstrated modeling procedures. Careful attention must be afforded balancing model detail with available data and study goals.

## B. Selected River Basin Models

By no means was every river basin model in existence considered in the following review. Such a task would be all but impossible due to the large number available and the proprietary nature of some. Rather, the models reviewed in this report represent a cross-section of the types of models available which might prove useful in the synthesis of the desired model. The models selected for consideration along with their reference publication are:

1. POU DRE: R.G. Evans, "Hydrologic budget of the Poudre Valley," M.S. Thesis, Colorado State University, 1971.
2. HEC-3: U.S. Army Corps of Engineers, "HEC-3 reservoir system analysis for conservation--user's manual," Hydrologic Engineering Center, 723-030, July, 1974.
3. NW01: R.W. Ribbens, "Program NW01 river network program--user's manual," U.S. Bureau of Reclamation, Denver, Colorado, July, 1973.
4. MITSIM: R.L. Lenton and K.M. Strzepek, "Theoretical and practical characteristics of the MIT river basin simulation model," Ralph M. Parsons Laboratory, Report No. 225, Massachusetts Institute of Technology, August, 1977.
5. MITSIM-E: R.P. Schreiber, "A digital simulation model for conjunctive groundwater-surface water systems," M.S. Thesis, Massachusetts Institute of Technology, 1976.
6. SIMYLD: Texas Water Development Board, "Economic optimization and simulation techniques for management of regional water resource systems, river basin simulation model SIMYLD-II--

program description," Prepared by Systems Engineering Division, Austin, Texas, July, 1972.

7. WADIST: R.L. Thaemert, "Mathematical model of water allocation methods," Ph.D. Dissertation, Colorado State University, 1976.
8. WRMM: B. Wang, and others, "A water resource management model, Upper Jordan River Drainage, Utah," Utah Water Research Laboratory, Utah State University, March, 1973.
9. SSARR: U.S. Army Corps of Engineers, "Program description and user manual for SSARR model-streamflow synthesis and reservoir regulation," North Pacific Division, Program 724-KS-G0010, September, 1972.

Each model was reviewed with regard to determining its advantages and limitations with respect to those attributes deemed desirable for the synthesized model. All of the models have some similarities. For example, they all are oriented toward water allocation analyses instead of design problems. However, some of the models could be employed to analyze the impact of varying structural designs within a river basin. All are deterministic in the nature of inflow consideration. Monthly time increments are employed by the models except WADIST, which calculates a daily water delivery to irrigation systems throughout the season May through October. All of the surface water quantity aspects of the models use a fundamental mass-balance solution approach.

The above models differ widely in purpose and therefore have varying degrees of sophistication. For instance, NW01 is a surface flow and total dissolved solids accounting model which has limited simulation



ability and considers flows only in 1000 acre-foot units. In comparison, SIMYLD is labeled a quasi-optimization model and provides highly detailed results. The models differ in data requirements and problem formulation. Some develop network configurations of the physical system, while POUFRE considers each canal system independently without preserving the morphology of the system.

While most of the models are designed for general application, some have received only hypothetical test considerations. Others, such as HEC-3, have received broad acceptance and usage throughout the United States. WADIST and POUFRE were developed for the legal system administered in Colorado, and even more specifically, for the Cache la Poudre River Basin, respectively. WRMM is the most hydrologically basic model considered, in that data requirements include temperature, precipitation, and snowmelt characteristics. However, WRMM is less favorable as the core model because it cannot consider water distribution complexities with sufficient detail, and has no optimizing capability. Several of the models (HEC-3, MITSIM, and MITSIM-E) also perform economic analyses as to benefits and costs to be expected from the operation of a system in some specified manner.

MITSIM-E (extended version of MITSIM) includes modeling of stream-aquifer interaction via a discretization of the groundwater basin into a network of irregular polygons. Finite-difference approximations are employed to solve the groundwater flow equations. Although MITSIM-E represents the most sophisticated modeling of groundwater-surface water interactions of these models, it does not have the capability of considering the quantifiable aspects of institutional dictates governing water

distribution. In addition, the data necessary to execute MITSIM-E, such as groundwater head levels, storage coefficients, etc., are not always available on a basin-wide scale.

Some optimizing capability was considered extremely important in selecting the core model from which the synthesized model would evolve. Only SIMYLD offers such a feature. SIMYLD is capable of modeling a multi-reservoir river basin system, including the institutional framework. In the semi-arid western United States, water rights dictate, from a legal viewpoint, amounts of water that can physically be diverted for any purpose. Therefore, in order to realistically simulate the behavior of a river basin in this geographical region the water rights structure must, in some fashion, be included in the modeling effort. POUFRE and WADIST consider the legal framework of water allocation but lack the flexibility of considering the impacts of changes in the legal framework within a particular river basin. SIMYLD, however, through its general quasi-optimization capability allows for priorities or rankings of preferences of water diversion which may reflect the historical legal preferences existing or easily and quickly modified to reflect some new preferential scheme. It should also be noted that since SIMYLD calculates the transfer of water on a monthly volumetric basis and water rights priorities are established as flow (cfs), there has to be a lumping of priorities. Therefore, SIMYLD only approximates the water rights structure present in a river basin.

SIMYLD also provides high resolution of the distributional aspects of a river basin system. However, it does not have the capability of considering conveyance losses or irrigation return flows. Still,

SIMYLD is considered as being the most appropriate base model for which suitable modifications can be added that further enhance its capability in regard to the overall model purpose. It has an optimizing capability which is an extremely important attribute of the desired model, and provides a detailed analysis of the distributional aspects of water transfers within a river basin. Also, SIMYLD can be readily adapted to an interactive, conversational mode. Simulation models must go through a trial and error process in order to determine reservoir releases that will meet downstream demands. The optimizing capability in SIMYLD uses an efficient network algorithm which can find strategies that meet demands, under given priorities, much more rapidly.

Tables II.1 through II.9 contain a complete analysis of each of these river basin models, including limitations of these models in comparison with the desired model. Chapter III further describes SIMYLD and the resulting synthesized model MODSIM.

Table II.1. MODEL: POUFRE

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Model Purpose:	•Adjustment of various water flows throughout a river basin according to a set of weighted data to represent actual conditions in area
Problem Type:	•Hydrologic budget (allocation)
Type of Model:	•Accounting
Problem Formulation	•All inflows and outflows are determined for each canal system
Solution Approach:	•Mass balance on each irrigation portion of basin
Application:	•Specifically designed for Cache la Poudre River Basin, Colorado
Deterministic vs Stochastic:	•Deterministic
Time Period:	•Monthly
Data Requirements:	•Extensive land use inventory •All inflows •Canal diversions •Consumptive loss coefficients •Root zone flows
Output:	•Detailed report of budget (including return flow, consumptive loss, etc.) for each canal system in basin
Major Assumptions:	•Constant crop acreages under each canal •Uniform application and runoff of irrigation water •All errors accumulated in groundwater flows
Advantages:	•Detailed consideration of irrigation sector •Considers mass balance for every irrigation canal in basin •Return flows
Limitations:	•Lacks flexibility of application to other river basins •Not designed for long-term planning studies •No detailed resolution of distributional aspects of river basin •All storage aggregated

Table II.2. MODEL: HEC-3

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Model Purpose:	•Simulation of a multi-reservoir system for conservation purposes, includes economic analysis
Problem Type:	•Allocation
Type of Model:	•Simulation
Problem Formulation:	•Each system component designated as a control point with appropriate characteristics
Solution Approach:	•Mass balance by control point
Application:	•Wide acceptability and usage
Deterministic vs Stochastic:	•Deterministic
Time Period:	•Variable (monthly recommended)
Data Requirements:	•Control point configuration •Reservoir characteristics •Power requirements •Hydrology •Economic factors •Evaporation •Desired diversions •Minimum diversions
Output:	•Detailed monthly conditions at each control point: inflow, outflow, storage, etc. •Results of economic analysis
Major Assumptions:	•All changes in system behavior can be accounted for at control points •Only one diversion per control point
Advantages:	•Hydropower •Economic analysis options •Comprehensive surface water simulation •General model
Limitations:	•No conveyance losses •Complex input format •No optimizing capability •No return flow calculation •No consideration of conditions between control points •Reservoir operating rules based on prescribed storage levels

Table II.3. MODEL: NW01

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Model Purpose:	•Surface flow and TDS accounting model
Problem Type:	•Allocation
Type of Model:	•Accounting
Problem Formulation:	•Network
Solution Approach:	•Mass balance in downstream direction
Application:	•Used for some preliminary studies such as Cache la Poudre River, Colorado
Deterministic vs Stochastic:	•Deterministic
Time Period:	•Monthly
Data Requirements:	•System configuration                   •Evaporation •Reservoir characteristics       •Hydrology •Operating criteria •Imports/Exports •Water use information
Output:	•Monthly conditions at each node--flows, storages, etc.
Major Assumptions:	•Single downstream boundary •Tree type network
Advantages:	•Computes TDS at each node •Network provides detail between nodes •General model
Limitations	•Limited simulation ability •No optimization capability •1000 acre-foot units •No return flow calculation •No conveyance losses •Rough approximation of evaporation •Specified reservoir operating rules allow no flexibility •Only up to 5 reservoirs can be modeled

Table II.4. MODEL: MITSIM

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Model Purpose:	•Hydroeconomic simulation of large-scale river basins
Problem Type:	•Allocation
Type of Model:	•Simulation
Problem Formulation:	•Node-Reach configuration
Solution Approach:	•Mass balance in downstream direction
Application:	•Vadar/Axios River Basin, Greece and Yugoslavia
Deterministic vs Stochastic:	•Deterministic
Time Period:	•Monthly
Data Requirements:	•System configuration •Annual benefits •Loss coefficients •Annual costs •Diversion target flows •Power requirements •Evaporation •Hydrology
Output:	•Mean monthly performance for each node, ex. irrigation node, hydropower node, etc. •Statistical summary •Net economic benefits
Major Assumptions:	•Water allocated to users in upstream to downstream order
Advantages:	•Hydropower •Performs statistical analysis on results •Designed for large-scale long-term planning studies •Economic analysis •General model
Limitations:	•Limited flexibility in reservoir operating rules •No optimization capability •No conveyance losses

Table II.5. MODEL: MITSIM-E

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Model Purpose:	<ul style="list-style-type: none"> <li>•Conjunctive use of surface water and groundwater</li> <li>•Response of both artificial and natural aquifer recharge and discharge</li> </ul>
Problem Type:	<ul style="list-style-type: none"> <li>•Allocation</li> </ul>
Type of Model:	<ul style="list-style-type: none"> <li>•Simulation</li> </ul>
Problem Formulation:	<ul style="list-style-type: none"> <li>•Discretization of groundwater basin into network of irregular polygons</li> </ul>
Solution Approach:	<ul style="list-style-type: none"> <li>•Finite-difference approximation</li> </ul>
Application:	<ul style="list-style-type: none"> <li>•Hypothetical simplified test case</li> </ul>
Deterministic vs Stochastic:	<ul style="list-style-type: none"> <li>•Deterministic</li> </ul>
Time Period:	<ul style="list-style-type: none"> <li>•Monthly</li> </ul>
Data Requirements:	<ul style="list-style-type: none"> <li>•Cellular structure of groundwater basin</li> <li>•Area of cell interfaces</li> <li>•Hydraulic conductivity</li> <li>•Storage coefficients</li> <li>•Initial head levels</li> <li>•Hydrology (infiltration, base flow)</li> </ul>
Output:	<ul style="list-style-type: none"> <li>•Groundwater availability</li> <li>•Distribution of groundwater and surface water contributing to demand</li> </ul>
Major Assumptions:	<ul style="list-style-type: none"> <li>•Constant percentage of applied water at each irrigation area goes to infiltration</li> </ul>
Advantages:	<ul style="list-style-type: none"> <li>•Three stream-aquifer interactions can be modeled:             <ol style="list-style-type: none"> <li>1. base flow</li> <li>2. groundwater recharge</li> <li>3. streamflow infiltration</li> </ol> </li> </ul>
Limitations:	<ul style="list-style-type: none"> <li>•Complex problem formulation</li> <li>•Not compatible with broad planning scope</li> <li>•Data requirements</li> <li>•Cannot consider complex surface water system</li> </ul>



Table II.6. MODEL: SIMYLD

---

Model Purpose:	•Simulation of multi-reservoir river basin system with consideration of institutional framework
Problem Type:	•Allocation
Type of Model:	•Quasi-optimization
Problem Formulation:	•Capacitated Network (circulating)
Solution Approach:	•Out-of-kilter network optimization algorithm which preserves nodal mass balance
Application:	•Limited application on Texas river basins
Deterministic vs Stochastic:	•Deterministic
Time Period:	•Monthly
Data Requirements:	•System configuration •Node characteristics •Operational priorities •Inflows, demands and evaporation rates
Output:	•Highly detailed output by node for each month of simulation •Summary report over entire simulation period
Major Assumptions:	•Unidirectional flow •All linkages bounded from above and below •All inflows, demands, and losses occur at nodes
Advantages:	•Quasi-optimization •High resolution of distributive aspects of river basins •General Model
Limitations:	•No conveyance losses •No return flow calculations

Table II.7. MODEL: WADIST

---

Model Purpose:	•Irrigation demand allocation
Problem Type:	•Allocation
Type of Model:	•Accounting
Problem Formulation:	•Control point concept
Solution Approach:	•Distribution of virgin flow according to prescribed entitlement
Application:	•Designed for Colorado water law •Test case: Poudre River Basin
Deterministic vs Stochastic:	•Deterministic
Time Period:	•Daily
Data Requirements:	•Diversion data •Reservoir data •Daily flow data
Output:	•Summary output of transfers to each canal system including debits and credits and sources of supply
Major Assumptions:	•Constant water requirements •Constant loss factor •Surface return flow has one-day lag
Advantages:	•Conveyance losses considered •Crop water requirements approximated •Return flows calculated
Limitations:	•Distribution criteria must be pre-determined •Cannot readily consider varying water rights structure •Daily time interval not suited for long-term planning studies •Specific to particular river basin •Constant demands for water

Table II.8. MODEL: WRMM

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Model Purpose:	•Watershed hydrology simulation
Problem Type:	•Allocation
Type of Model:	•Watershed simulation with parameter optimization
Problem Formulation:	•Decomposes river system into subbasins with all activity in subbasin aggregated
Solution Approach:	•Mass balance from subbasin to subbasin
Application:	•Upper Jordan River Drainage, Utah
Deterministic vs Stochastic:	•Deterministic
Time Period:	•Monthly
Data Requirements:	•Temperature, precipitation, groundwater inflows, gaged flows, reservoir characteristics, irrigation diversions, imports, exports
Output:	•Storage change, precipitation, snowmelt, and inflow & outflow for each subbasin
Major Assumptions:	•Subbasins are gaged at upstream and downstream boundaries
Advantages:	•Considers basic hydrologic inputs to system •Capable of considering very large river basin systems •Groundwater consideration
Limitations:	•Does not consider distributive complexities with any detail •No optimizing capability •No conveyance losses •Cannot consider complex channel morphology

Table II.9. MODEL: SSARR

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Model Purpose:	•Streamflow synthesis and reservoir regulation model
Problem Type:	•Allocation
Type of Model:	•Mathematical hydrologic model of a river basin system which synthesizes streamflow from snowmelt and rainfall
Problem Formulation:	•Decomposes river basin system into relatively homogeneous hydrologic units. User then specifies upstream to downstream order of all watersheds, reservoirs and river reaches
Solution Approach:	•Modular operating procedure whereby watershed runoff modeling is followed by river system model for streamflow routing combined with reservoir regulation
Application:	•Columbia River Basin through the Cooperative Columbia River Forecasting Unit
Deterministic vs Stochastic:	•Deterministic
Time Period:	•Variable (daily)
Data Requirements	•Description of non-variable physical features •Current conditions of all watershed-runoff indices •Precipitation data, air temperatures, and thermal budget data •Job control and time control data
Output:	•Variable output format which includes listings and/or plotted information concerning simulated system behavior
Major Assumptions:	•Watersheds can be divided into homogeneous units •Linear storage-discharge relationships
Advantages:	•General model •Considers basic hydrologic inputs to system •Streamflow routing •High resolution of channel morphology •English or metric units
Limitations:	•No conveyance losses •No optimizing capability •Not as suitable for long-term management studies (i.e., daily time increments)

## CHAPTER III

### MODEL SYNTHESIS

This chapter describes in detail the synthesized model MODSIM. The core model is first presented followed by a discussion of modifications to the core model, SIMYLD, which result in the synthesized model MODSIM. Included in this chapter is an interpretation of various components of the network constructed and solved by MODSIM. The following chapter, Chapter IV, contains an in-depth user documentation of Program MODSIM.

#### A. The Core Model: SIMYLD

##### A.1 Background to core model selection

Selection of the base or core model, from the specific models reviewed in Chapter II, was contingent upon certain objective criteria including:

1. flexibility in application
2. capability of simulating a large river basin system over a period of several years
3. detail of model output provided
4. input data requirements
5. rapid-access computer core memory requirements
6. central processor time required for a typical run.

In addition to these qualifications, an intuitive feel of those aspects of the core model which would provide a measure of trust for the user was considered. The program methodology must not be so obscure as to

prohibit even a rudimentary understanding of its assumptions, approximations, capabilities, and limitations. Also, the core model selection was, in part, based on a comparison of the capabilities of the reviewed models with the capabilities deemed *desirable* for the model. Of these models, Program SIMYLD (Texas Water Development Board, Systems Engineering Division, 1972) was selected as the most appropriate core model, based on the above discussion.

#### A.2 Program description

The computer program SIMYLD employs the *Out-of-Kilter-Method* (OKM) (Bazaraa and Jarvis, 1977; Clasen, 1968; Durbin and Kroenke, 1967; Ford and Fulkerson, 1962; Fulkerson, 1961) to minimize the total *cost* of flows in a network of interconnected reservoirs, river reaches, pump canals, and gravity flow canals. SIMYLD is capable of indirectly preserving water diversion and storage priorities established by water rights in the basin. This capability is achieved through a ranking procedure which is translated into *pseudo-costs* of water transfer. Using this ranking procedure, SIMYLD apportions available water for storage in various reservoirs and diversion of flow from the river according to their priority. If pump canals are included, the actual energy costs can be used. Otherwise, the costs used in the model are for ranking priorities for water use only. Other more informal institutional structures, such as water exchange agreements (i.e., the diversion of water out of priority as long as downstream senior direct flow rights are satisfied through reservoir releases) can be included.

### A.3 Program methodology

The underlying principle of the operation of SIMYLD is that most physical water resources systems can be represented as capacitated flow networks. The *real* components of the system are represented in the network as nodes (storage and non-storage points) and links (canals, pipelines, river reaches). Reservoirs, demand points, canal diversions, and river confluences are represented as nodes, while river reaches, canals, and closed conduits are node to node linkages. In order to consider demands, inflows, and desired reservoir operating rules, several artificial nodes and linkages must be created. These additional nodes and linkages also insure the circulating nature of the network, which is a necessary condition if the Out-of-Kilter Algorithm is to be employed. A discussion of these artificial arcs is included in the final section of this chapter.

Basic assumptions associated with the core model include:

1. All storage nodes and linkages must be bounded from above and below (i.e., minimum and maximum storages and flows must be given).
2. Each linkage must be unidirectional with respect to flow.
3. All inflows, demands, and losses must occur at nodes.
4. An import node can be designated for water entering the system from across system boundaries.
5. Each reservoir can be designated as a spill node for losses from the system proper.
6. Spills from the system are the most expensive type of water transfer, in the sense that the model seeks to minimize unnecessary spill.

7. Reservoir operating policies are provided by the user as desired in-storage volume for each reservoir at the end of each month throughout the simulation period.

Within the confines of mass balance throughout the network, SIMYLD sequentially solves the following linear optimization problem via the Out-of-Kilter Algorithm.

$$\text{minimize } \sum_{i=1}^N \sum_{j=1}^N w_{ij} q_{ij} \quad (\text{III.1})$$

subject to:

$$\sum_{i=1}^N q_{ij} - \sum_{i=1}^N q_{ji} = 0 \quad ; \quad j=1, \dots, N \quad (\text{III.2})$$

$$l_{ij} \leq q_{ij} \leq u_{ij} \quad ; \quad \text{for } i, j=1, \dots, N \quad (\text{III.3})$$

$$l_{ij} \geq 0$$

where

$q_{ij}$  = integer valued flow from node  $i$  to node  $j$

$w_{ij}$  = weighting or priority factor per unit of flow for node  $i$  to node  $j$

$l_{ij}$  = lower bound on flow in the linkage connecting node  $i$  to node  $j$

$u_{ij}$  = upper bound on flow in the linkage connecting node  $i$  to node  $j$

Equation III.2 insures that the flow into any one node is equal to the flow out of that node. The OKM is an extremely efficient primal-dual simplex algorithm that takes advantage of the special structure of a network-type problem. Appendix A contains an in-depth presentation of



the out-of-kilter method, including an example problem which has been solved using hand calculations.

The reasoning behind labeling SIMYLD and subsequently MODSIM as *quasi-optimization* models stems from the fact that the global optimum is not actively sought. The network flow problem, however, is solved *successively* time period by time period.

#### B. Advantages of Network Approach to River Basin Modeling

There are certain real advantages of employing modern network theory to the solution of large-scale river basin problems. Hamdan (1974) lists these advantages rather succinctly.

1. A network formulation of a system provides a physical picture revealing the morphology of the system, which is readily recognizable.
2. Network optimization techniques (particularly the Out-of-Kilter Algorithm) are efficient solution techniques.
3. If the OKM is used, computation may begin with *any* solution, regardless of feasibility.
4. Extremely large (in terms of network components) problems can be solved.
5. Changes in some system components can be easily incorporated by manipulation of the previously constructed network.

#### C. MODSIM Synthesis

The core model, SIMYLD, was extensively modified so as to better conform to the proposed desired model. This section describes those modifications which resulted in the synthesized river basin planning

model MODSIM. Chapter IV contains the discussion of the interactive, conversational aspects of data file organization which is interfaced with MODSIM.

### C.1 Modifications to core model

The following extended capabilities were added to SIMYLD which resulted in the synthesized model MODSIM being more representative of the desired model.

Target Storage Levels: SIMYLD computes a hydrologic state on a monthly basis by considering current reservoir storage levels and inflows to these reservoirs. Associated with each of these states (average, dry, wet) is a corresponding set of operating rules with ranking priorities. These three hydrologic states are computed by selecting all or some of the reservoirs within the system (user preference) and performing the following analysis:

$$R = \sum_{i=1}^N S_{it} + \sum_{i=1}^N I_{i,t+1} \quad (\text{III.4})$$

$$W = \sum_{i=1}^N S_{imax} \quad (\text{III.5})$$

where:

N = number of reservoirs in the system

t = current month of operation

$S_{it}$  = end of month t storage in reservoir i

$S_{imax}$  = storage capacity for reservoir i, which may be less than the actual maximum capacity due to dam stability and safety considerations.

The user also specifies the upper and lower bounds of the average state as fractions of the total subsystem storage capacity:

$$LB = x_1 W \quad (III.6)$$

$$UB = x_2 W \quad (III.7)$$

where:

LB = lower bound of average state

UB = upper bound of average state

$x_1$  = percentage which defines lower limit of average state

$x_2$  = percentage which defines upper limit of average state

Subsequently, the hydrologic states are defined as:

Dry:  $R < LB$

Average:  $LB \leq R \leq UB$

Wet:  $R > UB$

With the above method of calculating target operating rules, for a long period of analysis, only three target storage levels can be used for any one reservoir. However, the option has been included in MODSIM whereby the user can input separate target storage levels for each reservoir and for each month throughout the *entire* analysis.

Varying Priorities: In the core model, only three differing priorities for any node (storage and/or demand) can be included. Again, these priorities correspond to wet, average, or dry conditions calculated by the model. An additional option has been included which enables the user to input a separate priority for any node for each year of the analysis. This expanded capability means that instead of a maximum of three priorities associated with a wet, average, or dry state, a varying priority can be input for each year of analysis.

Import Nodes: SIMYLD will consider only one import node (i.e., flow originating outside the network). The modified code includes a variable number of possible import nodes.

Area-Capacity Points: Eighteen data points relating reservoir capacity to reservoir surface area are originally required. This means that zero filled entries must be made if, for instance, data are such that only 12 pairs of points are available. This leads to computing inefficiency and increased input time to read the remaining pairs of zeros. The revised code will accept a variable number of area-capacity data points up to a maximum of 18.

Variable Upper Bound on Links: All physical links in the network must be bounded from above. However, as SIMYLD is designed, only one upper bound for each link can be considered in the analysis. For some cases (Case Study #2) this limitation may not be realistic. MODSIM includes the additional capability of allowing the user to input (as originally designed) only one bound per link, or 12 varying monthly maximum flow limits per link.

Flow Through Demand: Demand satisfaction for SIMYLD, as originally designed, does not provide for demands for water which are not terminal; i.e., demands which flow *through* the demand node and remain in the network for subsequent diversion. All water contributing to demand satisfaction in the core model is lost from the network. These are termed *terminal demands*. However, MODSIM will consider both *terminal demands* and *flow-through demands*.

Variable Linkage Cost: The core model prices river reaches to 1 and pump canals to 2, automatically. Once again, for certain problems, this situation may not reflect actual cost variations within the problem. In order to more realistically consider variable water transfer costs throughout a network, MODSIM provides the option of inputting a varying cost for each linkage in the network.

Output Options: The original code outputs results in three reports: (1) echo print of input data, (2) monthly summaries of results for each year of analysis, and (3) a summary report (quite lengthy, for long planning periods) by node and year. The user now has the option of suppressing any or all of these reports according to his computational objectives.

Local File Creation: In order to facilitate additional analyses, all link flows (every link, every month) are read onto a local file which can be saved as a permanent file and read by subsequent user developed programs for further analysis.

Channel Losses: A significant addition to SIMYLD is the capability of including channel losses directly. A loss coefficient for each reach must be included in data input. This coefficient represents the fraction of the total flow in the link that would be lost. For example, some of the earthlined irrigation ditches in the Cache la Poudre River Basin in north central Colorado have estimated loss coefficients from 20 percent to 33 percent of the flow in the ditch. Subroutine CHANLS was added to the code to calculate the expected channel losses for each month. The procedure is as follows: first, network flows are

solved via the Out-of-Kilter Algorithm with no losses. Initially, all flows are set to zero, or the lower bound if greater than zero. The losses in each link are computed by multiplying the loss coefficient by the calculated flows. This loss is established as a demand at the downstream node for each link. The Out-of-Kilter Algorithm is solved again with the increased demand. However, the initial feasible solution is now set equal to the previous optimum solution. New link losses are then computed and the procedure is repeated until acceptable convergence has occurred.

Return Flows: One of the most important modifications to the core model is the inclusion of the capability of determining irrigation return flows. Several options as to the methodology for including return flows in MODSIM were considered. Classical groundwater theory used to develop a finite element or finite difference approach to stream-aquifer interaction was disregarded due to the nature of the purpose of MODSIM. Such an approach would have necessitated extensive data gathering exercises and would not have been compatible with the general context of this planning model. However, for real-time management models, where a smaller (perhaps daily) time increment is employed, such an approach may be required. Also, in many cases, data concerning groundwater head levels, storage coefficients, etc. are not readily available for large-scale river basin studies.

A methodology for including return flows in MODSIM calculations, which would remain consistent with the broad, general nature of a planning model, was developed using an approach similar to one taken by Hodgson (1978). Hodgson (1978) uses multiple linear regression to

simulate groundwater level responses. Since return flows are dependent upon the amount of water applied to irrigation, which is a function of the volume of water diverted to irrigation, the development of a predictive equation for return flows based on ditch diversions also has validity.

The number of monthly lags and the components (independent variables) included in the regression equation must be determined off-line. However, once the regression coefficients have been determined, MODSIM has the capability of considering up to 10 different return flow multiple linear regression equations with up to a maximum six-month lag. The following step-by-step procedure is recommended for use of this option.

1. Determine the number of return flow estimates necessary per month, based on the network design and the nature of the problem.
2. Determine which nodal diversions contribute to each return flow estimate .
3. Determine to which node in the network each monthly return flow estimate will accrue.
4. Using monthly historical data (ditch diversions and return flows), perform statistical correlation studies to determine the appropriate number of monthly lags.
5. Construct multiple linear regression equation based on the results of the above exercise.
6. Solve for regression coefficients for each return flow equation.

According to user input, MODSIM calculates monthly return flows, iterating over demand satisfaction, until acceptable convergence is achieved. Sub-routine RTFLOW has been added to MODSIM for this purpose. A detailed example of the procedure with accompanying results is provided in Chapter VI.

### C.2 MODSIM network interpretation

As previously mentioned, MODSIM solves a capacitated network of real and artificial nodes and arcs. For each real network, a series of artificial nodes and linkages is automatically appended to this network to guarantee circulation and Equation III.1 is solved for the entire network. Therefore, these artificial nodes and arcs are necessary so that ultimately some of the  $q_{ij}$  can be interpreted as demands and storages. This section describes these additional artificial arcs and the calculations of the bounds and costs for these arcs. Figure III.1 displays the total linkage configuration for MODSIM. All of the arcs shown in this diagram are artificial.

Artificial Inflow Arcs: Inflow arcs link each real node (storage and non-storage) with an artificial initial storage and inflow node. The lower bound is set equal to the upper bound which is in turn set equal to the volumetric inflow to each particular real node. In this manner, the model is constrained to accept the particular nodal inflows input. The unit costs ( $w_{ij}$  in Equation III.1) are set equal to zero.

Artificial Demand Arcs: Demand arcs link each real node (storage and non-storage) with an artificial demand node. The lower bound on these arcs is set equal to zero, while the upper bound is set equal to the demand associated with each real node. The cost placed on each artificial demand arc is calculated by the following equation:

$$(w_{i,d})_t = - [1000 - (DEMR_{i,t} \cdot 10)] \quad (III.8)$$

where:

$$(w_{i,d})_t = \text{cost of transporting one unit of water from real node } i \text{ to artificial demand node } d \text{ during month } t$$



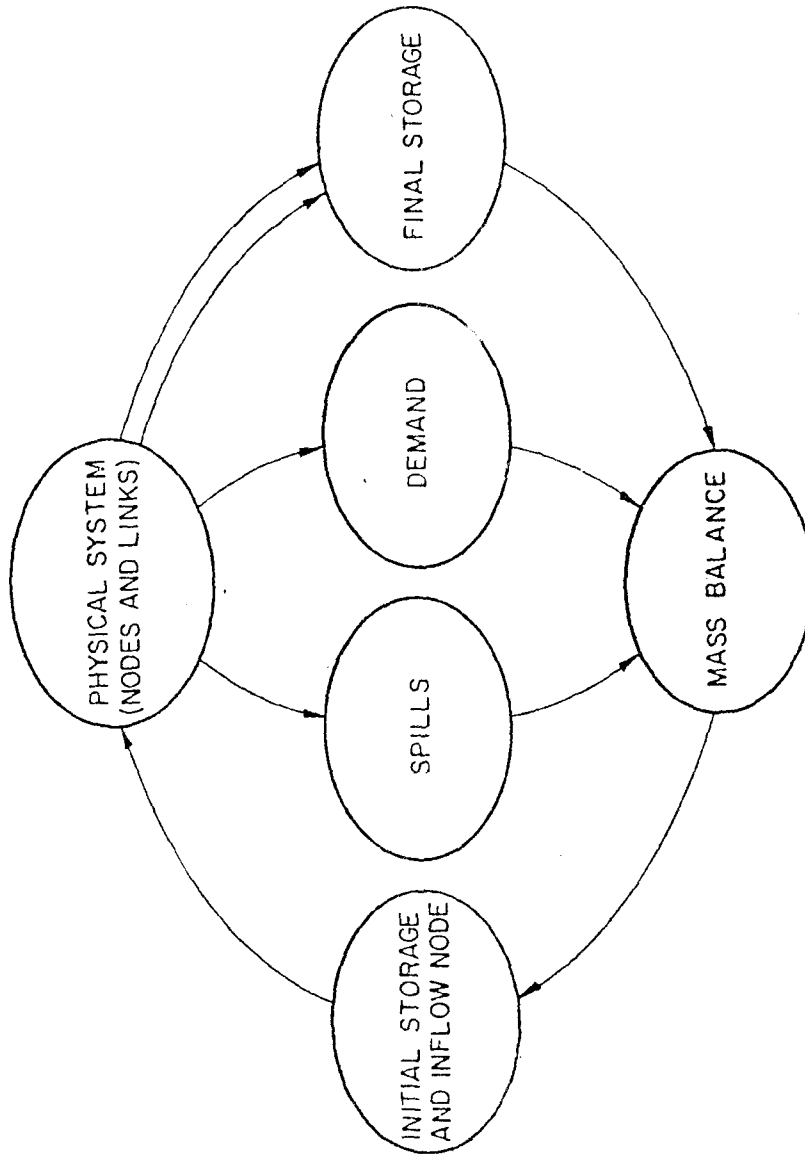


Figure III.1.1. Schematic diagram of linkage configuration for MODSIM.

$DEM_{i,t}$  = user input priority for meeting demand at node  $i$  during month  $t$

$d$  = artificial demand node

$i$  = real node

$t$  = month

As the priority placed on demand satisfaction at node  $i$  ( $DEM_{i,t}$ ) increases, i.e. ( $DEM_{i,t}$  actually *decreases*) the cost of transporting water via the artificial arc ( $i,d$ ) decreases, making the transport of water through this arc more advantageous in relation to other linkages assuming all other costs remain constant. In this manner, the priorities placed on demand satisfaction at each demand node can be used to simulate the institutional framework (water rights priorities) or operational preferences present in all developed river basins in the semi-arid western United States. Again, a lower value of  $DEM_{i,t}$  means a higher priority.

#### Artificial Desired Storage Arcs and Artificial Final Storage Arcs:

In order to provide capacitance in the network, another artificial node is established with linkage to all real nodes. The flows in these linkages or arcs are interpreted as storage volumes in the final results for the current month. For each real node, there are two artificial arcs connecting it with the artificial storage node. One arc is the *desired* storage arc, and the other is the *final* storage arc. The lower bound on desired storage arcs is set at the reservoir minimum capacity plus an estimate of the expected evaporation which would occur if the reservoir went from its current state to the minimum pool. However, if the lower bound of the artificial inflow arc to the reservoir in question is less than the lower bound on the desired storage arc, the lower bound on the desired

storage arc is replaced by the lower bound on the corresponding inflow arc. This condition is necessary to insure network feasibility and subsequently that mass balance is maintained. The upper bound placed on desired storage arcs is the target storage level plus an estimate of the evaporation which would occur if the reservoir went from the current state to the target storage level. The cost associated with transferring one unit of water along the desired storage arc is calculated using an equation identical to Equation III.8 for demand arcs.

$$(w_{i,ds})_t = - [1000 - (OPRP_{i,t} \cdot 10)] \quad (III.9)$$

where:

$(w_{i,ds})_t$  = cost of transporting one unit of water from real node  
i to artificial storage node ds during month t

$OPRP_{i,t}$  = user input priority for meeting the target storage level  
at node i during month t

ds = artificial storage node

i = real node

t = month

The cost  $w_{i,ds}$  is interpreted in exactly the same manner as the previously discussed  $w_{i,d}$  (Equation III.8). Such a procedure gives MODSIM the added advantage of being able to consider preferences among various reservoir storage levels in relation to various demands throughout the network. A final storage arc must also be employed to compensate for situations when (due to the nature of inflows and priorities) the reservoir storage must exceed the target level. The final storage arc connects each reservoir with the artificial storage node in the same manner as the desired storage arc. However, its lower bound equals

zero and its cost equals zero. The upper bound is set equal to the difference between the maximum storage capacity and the target storage level, minus an estimate of evaporation for this case. The *real* node calculated storage volume becomes the sum of the flow in both of these arcs upon solution of the Out-of-Kilter Algorithm.

Artificial Spill Arcs: MODSIM also employs artificial spill arcs which help to maintain feasibility in the network solution. These arcs have the highest unit cost of all arcs associated with them. Each real storage node is linked with the artificial spill node by one artificial arc. The lower bound equals zero while the upper bound equals the total capacity of all reservoirs. The unit cost associated with the transfer of water through a spill arc is 10,000 multiplied by its preferential order.

Mass Balance Arcs: Finally, to assure that a circulating network is constructed, and also to insure mass balance throughout the system, an artificial mass balance node is included with arcs from the artificial demand, storage, and spill nodes leading to it, and one arc from it leading to the artificial inflow node. The costs associated with these mass balance arcs are zero along with the lower bounds (except the lower bound on the inflow mass balance arc), while the upper bounds on these arcs are the summation of the upper bounds on the arcs leading to the particular artificial node (demand, storage, spill).

Figure III.2 shows a simplified network which includes all artificial nodes and arcs as they would be constructed by MODSIM. Only nodes one and two represent the real network. The remaining nodes enhance MODSIM capability according to the above discussion. The user

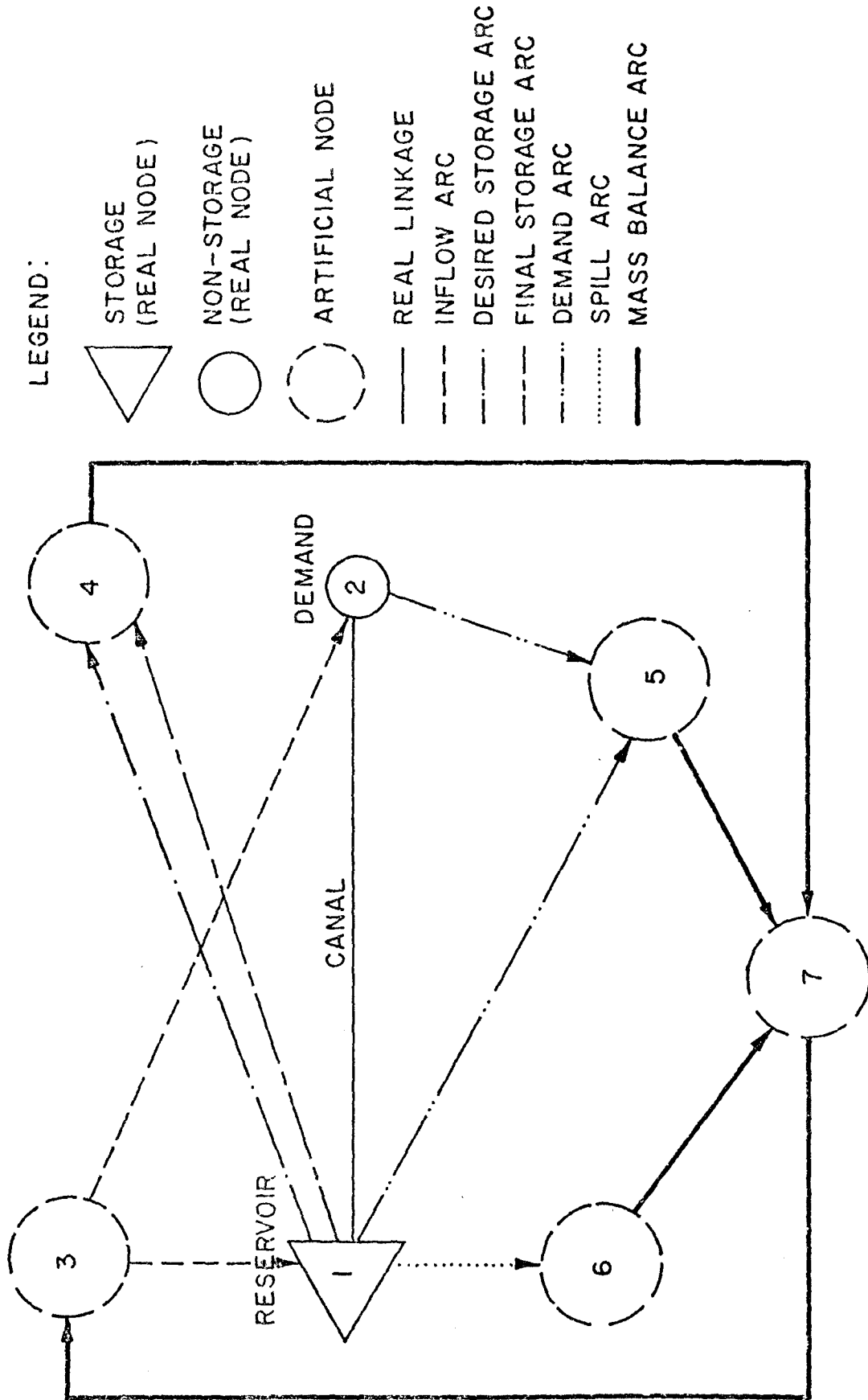


Figure III.2. Simplified network with artificial nodes and arcs included.

should note that, although he need be concerned only with his real network (MODSIM constructs the total network), the true size of his network (the one solved via the OKM) will be considerably larger than the real network. The total number of nodes in the total network will be only five larger than the real network. However, the total number of arcs will be:

$$\#ARCS = N_L + 4N_D + N_S + N_B$$

where

$N_L$  = number of physical links (river reaches, canals, etc.)

$N_D$  = number of nodes (storage and non-storage)

$N_S$  = number of spill nodes

$N_B$  = number of mass balance arcs = 4.

CHAPTER IV  
MODSIM USER DOCUMENTATION

This chapter presents a practical guide for the actual execution of the simulation package. Input requirements are listed and a detailed demonstration of the interactive, conversational mode of data organization is included. Figures displaying the content of output reports are also provided. A complete, but very elementary, example exercise is presented, followed by a discussion of varying approaches by which the model can be used to aid in the analysis of important tradeoffs among in-stream, storage, and consumptive uses of water.

A. Data Requirements

The information necessary to successfully use Program MODSIM includes:

1. physical description of the system to be simulated
2. operational criteria
3. model control parameters
4. monthly unregulated inflows
5. monthly demands
6. monthly evaporation rates.

Two separate files must be created containing the above data. A binary file has to be created which contains monthly unregulated inflows, monthly demands, and monthly evaporation rates. A coded file (card images) contains all network morphology, operational criteria, and model

control parameters. The coded file is divided into several records. The following offers a description of the information required for each record:

Record #1: Control options

1. channel loss option
2. echo print of input data option
3. summary output option
4. priority options (discussed in previous chapter)
5. return flow option

Record #2: Title or heading for simulation

Record #3: Network morphology parameters

1. number of nodes
2. number of reservoirs
3. number of links
4. number of river reaches
5. number of years in simulation
6. number of demand nodes
7. number of spill nodes
8. first calendar year of simulation
9. number of import nodes
10. from-to years for detailed output

Record #4: System nodes (storage nodes must precede all non-storage nodes)

1. node name
2. maximum capacity
3. minimum capacity
4. starting storage



Record #5: Spill reservoirs in order of preference

Record #6: Reservoir area-capacity tables

Record #7: Demand nodes

1. priority or ranking
2. node to which flow through accrues (if necessary)

Record #8: Import nodes

1. annual import
2. monthly distribution as percentage of total amount

Record #9: Calculation of hydrologic states (optional)

Record #10: Conversion factors (optional)

Record #11: Reservoir operational criteria

1. priority or ranking
2. desired storage levels, percentage of maximum capacity

Record #12: System configuration

1. number of variable capacity links
2. origin node for each link
3. termination node for each link
4. minimum capacity
5. maximum capacity
6. linkage loss coefficient
7. linkage unit cost

Record #13: Return flow (optional)

1. number of separate return flow equations
2. number of monthly lags
3. regression coefficients
4. nodes contributing to return flow

5. node accepting return flow
6. observed data for zero minus number of monthly lags

Usually, data files for computer models of this nature are punched on computer cards. This can be an exhausting and frustrating experience, especially if one is not familiar with the particular computer language used and consequently does not completely understand the data formatting. It is the author's opinion that many good simulation models have gone without use for this very reason. Those individuals who would have benefited most from their use did not have the time, patience, and/or computing expertise to follow through with the often long and tedious job of organizing the data in a form suitable for input. However, with Program MODSIM, the capability exists for developing a complete data file, ready for input, without manually punching a single computer card or knowing a single FORTRAN programming statement. This added capability is the result of interactive, conversational programming.

Conversational programming allows the user to execute a FORTRAN code, written in this mode, which queries him concerning the nature of the simulation and, based on his responses, constructs a data file which corresponds exactly to the input format for Program MODSIM. This file is then saved as a system permanent file which is attached to Program MODSIM for execution. Also, the data organization program checks periodically for inconsistencies in the input file which may lead to job abortion.

B. Data Management Program ORGANZ

The program designed to construct the coded data file for Program MODSIM is called ORGANZ. The most appropriate manner in which to present a program of this nature is through demonstration. Figure IV.1 contains a very simple network of four nodes (two reservoirs, two non-storage nodes, three links, and one import node). Node #4 is the demand node, and Reservoir #1 has an unregulated inflow. For the sake of demonstration, it is also assumed that Node #3 has a demand associated with it which only contributes to return flows at Node #4. Capacities and loss coefficients are as displayed. Operational criteria are dependent upon the nature of the problem being analyzed. In demonstrating Program ORGANZ, these criteria will be assumed, however, they are discussed in the section concerning use of program MODSIM to evaluate tradeoffs among varying water uses.

Program ORGANZ must be executed via a *procedure file* which has the form:

CLEAR.	(readies system for new job)
GET,ORGANZ.	(attaches file to job)
FTN,I=ORGANZ,L=0.	(compiles FORTRAN program)
LGO.	(executes program)
REWIND,A.	(writes new job control language)
CALL,A.	(executes new job controls)

The above procedure file is compatible with CDC172 time-sharing software packages. For other time-sharing systems a different (depending on control language) but similar procedure file must be created. Also, depending on the particular FORTRAN compiler used, the free format statements may require modification. The results of the application of Program ORGANZ to the construction of

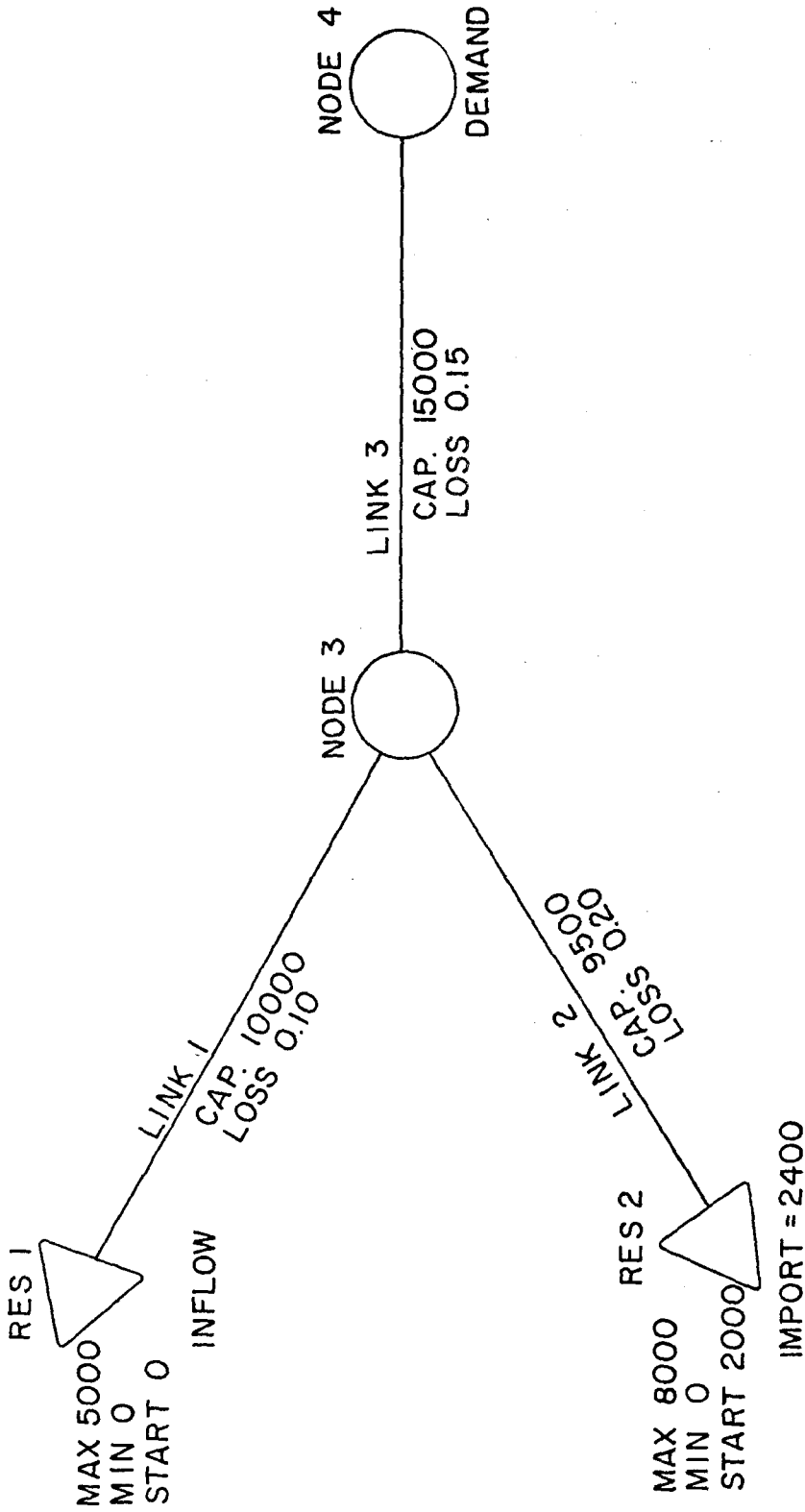


Figure IV.1. Simplified example network.

a data file for the network in Figure IV.1 is displayed in Figure IV.2. Appendix B of this report contains a listing of the FORTRAN IV source listing for Program ORGANZ. Figure IV.3 shows a listing of the resulting coded data file which Program ORGANZ produces for this hypothetical example problem. This file is in exact Program MODSIM format and can either be attached directly to Program MODSIM for execution or sent to system card punching hardware to be punched on 80 column computer cards which can subsequently be read via card reader hardware and executed by Program MODSIM.

### C. Binary Data File Creation

As mentioned previously, it is necessary to create a binary file containing all nodal inflows, demands, and evaporation rates, which also is attached to Program MODSIM prior to execution. To accomplish this task, interactive, conversational Program ADATA was written. Program ADATA is executed in exactly the same manner as Program ORGANZ, from a *procedure file* like (or similar to) the following:

```
CLEAR.  
GET,ADATA.  
FTN,I=ADATA,L=0.  
LGO.  
REWIND,B.  
CALL,B.
```

Figure IV.4 displays an example of the execution of Program ADATA for the demonstration network in Figure IV.1. The binary data file is saved as a permanent file for subsequent attachment to Program MODSIM.

\*\*\*\*\* PROGRAM ORGANIZE \*\*\*\*\*

INTERACTIVE, CONVERSATIONAL DATA ORGANIZATION FOR MODSIM

\*\* BEGIN RECORD 1 \*\*

ARE CHANNEL LOSSES TO BE COMPUTED (YES OR NO) ? YES  
 ECHO PRINT OF INPUT DATA (YES OR NO)? NO  
 SUMMARY OUTPUT (YES OR NO)? NO  
 AVG., WET, DRY STATES TO BE COMPUTED (YES OR NO)? NO  
 IS RETURN FLOW TO BE CALCULATED (YES OR NO) ? YES

\*\* BEGIN RECORD 2 \*\*

ENTER: UP TO 80 CHARACTER TITLE  
 ? EXAMPLE DEMONSTRATION OF PROGRAM ORGANZ

\*\* BEGIN RECORD 3 \*\*

ENTER: NO. OF NETWORK NODES? 4  
 ENTER: TOTAL NO. OF NETWORK LINKS? 3  
 ENTER: NO. OF RESERVOIRS ? 2  
 ENTER: NO. OF RIVER REACHES? 3  
 ENTER: NO. OF DEMAND NODES ? 2  
 ENTER: NO. OF SPILL NODES? 2  
 ENTER: NO. OF IMPORT NODES ? 1  
 ENTER: NO. OF YEARS TO BE SIMULATED? 1  
 ENTER: CALENDAR YEAR BEGINNING SIMULATION? 1979  
 ENTER: FROM-TO YEARS OF DETAILED OUTPUT DESIRED? 1 1  
 IS FIRM YIELD TO BE CALCULATED (YES OR NO)? NO

\*\* BEGIN RECORD 4 \*\*

FOR RESERVOIR NO. 1;  
 ENTER: UP TO 8 CHARACTER NAME? RES 1  
 ENTER: NETWORK NODE NO.? 1  
 ENTER: MAXIMUM CAPACITY? 5000  
 ENTER: MINIMUM CAPACITY? 0  
 ENTER: STARTING VOLUME ? 0  
 FOR RESERVOIR NO. 2;  
 ENTER: UP TO 8 CHARACTER NAME? RES 2  
 ENTER: NETWORK NODE NO.? 2  
 ENTER: MAXIMUM CAPACITY? 8000  
 ENTER: MINIMUM CAPACITY? 0  
 ENTER: STARTING VOLUME ? 2000  
 FOR JUNCTION NO. 3;  
 ENTER: UP TO 8 CHARACTER NAME? NODE 3  
 ENTER: NETWORK NODE NO.? 3  
 FOR JUNCTION NO. 4;  
 ENTER: UP TO 8 CHARACTER NAME? NODE 4  
 ENTER: NETWORK NODE NO.? 4

Figure IV.2. Demonstration of Program ORGANZ for simplified network in Figure IV.1.

\*\* BEGIN RECORD 5 \*\*

ENTER: 2 SPILL NODE(S) IN ORDER OF PREFERENCE? 2 1

\*\* BEGIN RECORD 6 \*\*

ENTER: NO. OF AREA-CAPACITY POINTS PER RES.? 4

FOR RESERVOIR NO. 1;

ENTER: POINT 1 [AREA-CAPACITY] ? 0 0

ENTER: POINT 2 [AREA-CAPACITY] ? 20 1250

ENTER: POINT 3 [AREA-CAPACITY] ? 70 3500

ENTER: POINT 4 [AREA-CAPACITY] ? 100 5000

FOR RESERVOIR NO. 2;

ENTER: POINT 1 [AREA-CAPACITY] ? 0 0

ENTER: POINT 2 [AREA-CAPACITY] ? 70 2000

ENTER: POINT 3 [AREA-CAPACITY] ? 150 5000

ENTER: POINT 4 [AREA-CAPACITY] ? 200 8000

\*\* BEGIN RECORD 7 \*\*

PRIORITY FOR EACH YEAR OF SIMULATION WILL BE INPUT

FOR DEMAND NODE NO. 1;

ENTER: NETWORK NODE NO.? 3

IS THIS A FLOW THRU DEMAND (YES OR NO)? NO

ENTER: PRIORITY FOR SIMULATION YEAR 1? 25

IS MONTHLY DEMAND TO BE INPUT VIA DATA FILE (YES OR NO) ? YES

FOR DEMAND NODE NO. 2;

ENTER: NETWORK NODE NO.? 4

IS THIS A FLOW THRU DEMAND (YES OR NO)? NO

ENTER: PRIORITY FOR SIMULATION YEAR 1? 35

IS MONTHLY DEMAND TO BE INPUT VIA DATA FILE (YES OR NO) ? YES

\*\* BEGIN RECORD 8 \*\*

FOR IMPORT NODE NO. 1;

ENTER: NETWORK NODE NO.? 2

FOR SIMULATION YEAR NO. 1

ENTER: TOTAL ANNUAL IMPORT ? 2400

ENTER: MONTHLY DISTRIBUTION

? .083 .083 .083 .083 .083 .083 .083 .083 .083 .083 .083 .083

\*\* BEGIN RECORD 10 \*\*

ARE CONVERSION FACTORS NECESSARY (YES OR NO)? NO

\*\* BEGIN RECORD 11 \*\*

FOR RESERVOIR NO. 1;

ENTER: PRIORITY FOR SIMULATION YEAR 1? 15

ENTER: MONTHLY DESIRED DISTRIBUTION

? 1 1 1 1 1 1 .8 .6 .4 .6 .8 1

FOR RESERVOIR NO. 2;

ENTER: PRIORITY FOR SIMULATION YEAR 1? 40

ENTER: MONTHLY DESIRED DISTRIBUTION

? 0 0 0 0 0 0 0 .3 .6 .9 1 1

Figure IV.2. Continued.

\*\* BEGIN RECORD 12 \*\*

ENTER: NO. OF LINKS WITH VARIABLE CAPACITY ? 0  
 ENTER REMAINING LINKAGE  
 ENTER: NETWORK LINK NO. ? 1  
     ENTER: MAXIMUM CAPACITY? 10000  
     ENTER: MINIMUM CAPACITY? 0  
     ENTER: ORIGIN NODE NO. ? 1  
     ENTER: TERMINATION NODE NO. ? 3  
     ENTER: LOSS COEFFICIENT? 0.10  
     ENTER: UNIT COST ? 0  
 ENTER: NETWORK LINK NO. ? 2  
     ENTER: MAXIMUM CAPACITY? 9500  
     ENTER: MINIMUM CAPACITY? 0  
     ENTER: ORIGIN NODE NO. ? 2  
     ENTER: TERMINATION NODE NO. ? 3  
     ENTER: LOSS COEFFICIENT? 0.20  
     ENTER: UNIT COST ? 10  
 ENTER: NETWORK LINK NO. ? 3  
     ENTER: MAXIMUM CAPACITY? 15000  
     ENTER: MINIMUM CAPACITY? 0  
     ENTER: ORIGIN NODE NO. ? 3  
     ENTER: TERMINATION NODE NO. ? 4  
     ENTER: LOSS COEFFICIENT? 0.15  
     ENTER: UNIT COST ? 5

\*\* BEGIN RECORD 13 \*\*

ENTER: NO. OF RETURN FLOW EQUATIONS? 1  
 ENTER: NO. OF TIME PERIODS TO BE LAGGED? 1  
 FOR RETURN FLOW EQU. NO. 1;  
     ENTER: NO. OF NODES CONTRIBUTING TO RTFLOW ? 1  
     ENTER: NODE NO. WHERE FLOW RETURNS ? 4  
     ENTER: NODES WHICH CONTRIBUTE TO RTFLOW? 3  
     ENTER: REGRESSION COEF. BEGINNING WITH  
             THE CONSTANT TERM, FOLLOWED BY DITCH  
             DIVERSIONS, FOLLOWED BY RETURN FLOWS  
             EXAMPLE FOR 1 MONTH LAG  
              $A1+A2*D(T)+A3*D(T-1)+A4*R(T-1)$   
 ? 789 .157 .0482 .6589

FOR INITIAL CALCULATIONS ENTER:  
 TOTAL DITCH DIVERSION AND TOTAL RETURN  
 FLOW OBSERVED FOR TIME PERIOD ZERO MINUS  
 1; ? 200 85

SAVE FILE AS PERMANENT FILE (YES OR NO) ? YES  
 ENTER: UP TO 7 CHARACTER FILE NAME ? CODATA  
 IS A LISTING REQUIRED (YES OR NO) ? YES

Figure IV.2. Continued



```

CONTROL OPTIONS      1   0   0   1   1   1
EXAMPLE DEMONSTRATION OF PROGRAM ORGNANZ
PARAMETERS          4   2   3   1   2   1
RES 1                5000  0   0   0   0   10.000
RES 2                8000  0   0   0   0   0
NODE 3               0   0   0   0   0   0
NODE 4               0   0   0   0   0   0
SPILLS              2   1
NO. PAIRS           4
AREA-CAP            1   0   0   20  1250  70   3500
                    100  5000
                    0   0   70  2000  150  5000
                    200  8000
DEMAND 3 0 0 0
RANK      3 25
DEMAND 4 0 0
RANK      4 35
IMPORT    2
YEAR      1
FACTORS   0.000 2400.083.083.083.083.083.083.083.083.083.083.083
ANNUAL OPR 1 0.000 0.000
ANNUAL OPR 2 151.001.001.001.001.001.00 .80 .60 .40 .60 .801.00
NVARLKS   0 400.000.000.000.000.000.000 .30 .60 .901.001.00
LINK      1 1 3 10000 0 .100000000 0
LINK      2 2 3 9500 0 .200000000 10
LINK      3 3 4 15000 0 .150000000 5
NEQU,NLAGS 1 1 .4820E-01 .6589
789.0
EQU       1 4
EQU       3
LAGS      200 85
  
```

Figure IV.3. Example coded data file created by Program ORGNANZ.

\*\*\*\*\* P R O G R A M A D A T A \*\*\*\*\*

BINARY INFLOW, DEMAND, AND EVAP. FILE CREATION FOR MODSIM

ENTER: TOTAL NO. OF NODES? 4  
 ENTER: TOTAL NO. OF RESERVOIRS ? 2  
 ENTER: NO. OF YEARS TO BE SIMULATED? 1

ENTER: NO. OF DEMAND NODES ? 2  
 ENTER: NODE NO. OF EACH DEMAND NODE  
 ? 3 4

ENTER: NO. OF NODES WHERE UNREGULATED INFLOW OCCURS? 1  
 ENTER: NODE NO. OF EACH UNREG. INFLOW NODE  
 ? 1

ENTER: NO. OF RESERVOIRS WITH EVAP. > 0? 2  
 ENTER: NODE NO. OF RESERVOIRS WITH EVAP. > 0  
 ? 1 2

ENTER: MONTHLY INFLOWS FOR NODE 1 YEAR 1  
 ? 1000 2000 2000 2000 750 500 0 0 500 500 1000 1500

ENTER: MONTHLY EVAP. RATES FOR RES. NO. 1 YEAR 1  
 ? -.05 -.02 .01 .04 .14 .22 .27 .35 .28 .17 .06 .01

ENTER: MONTHLY EVAP. RATES FOR RES. NO. 2 YEAR 1  
 ? -.01 -.07 -.10 -.03 .06 .11 .21 .27 .23 .15 .09 .02

ENTER: MONTHLY DEMANDS FOR NODE 3 YEAR 1  
 ? 100 200 300 400 500 500 500 400 300 200 100 100

ENTER: MONTHLY DEMANDS FOR NODE 4 YEAR 1  
 ? 5000 5000 5000 5000 5000 5000 5000 5000 5000 5000 5000 5000

ENTER: UP TO 7 CHARACTER PFN FOR BINARY FILE ? BINDATA  
 SAVE COPY OF CODED DATA FILE ALSO (YES OR NO) ? NO

JOB SUCCESSFULLY COMPLETED.  
 PRINT-OUT OF DATA FILE (YES OR NO)? NO

Figure IV.4. Demonstration of Program ADATA for simplified network in Figure IV.1.

D. Output of Results

The user has the option of obtaining one or more of three possible output reports. These include:

1. an echo of the input data pertaining to the system configuration
2. a detailed *monthly* report providing entire nodal and linkage conditions such as:

- a. Storage node:

initial storage	shortages
unregulated inflows	system loss
upstream spills	water pumped into a node
demand	water pumped from a node
surface area	end-of-month storage (actual)
evaporation loss	end-of-month storage (desired)
downstream spills	

- b. Non-storage demand node:

demand  
shortages

- c. Linkage:

total monthly flow as volume  
loss as volume  
yearly mean flow  
return flow

3. node by node annual summaries for the entire simulation period plus maximum linkage flows and simulation period average flows in each linkage.

Figure IV.5 shows the detailed monthly report for the analysis performed on the example network, as dictated by the data files created by Program ORGANZ and Program ADATA.

#### E. Discussion

In order to properly operate Program MODSIM, a *submit file* must be created which attaches the appropriate files, executes the program, and disposes the output to a line printer. The submit file has the following form for the CDC 172, NOS Operating System:

```

/JOB
<Job Card>
<User Card>
ROUTE,OUTPUT,DC=PR,UN=AD,DEF. (routes output to line printer)
ATTACH,MODSIM.
FTN,I=MODSIM,L=0,OPT.
GET,TAPE5=<coded data file>.
GET,TAPE10=<binary data file>.
LDSET,PRESET=ZERO. (initially sets computer core storage
                    to zero)
LGO,TAPE5,OUTPUT.
/EOF

```

The user should be careful to note that Program MODSIM has been specifically designed to operate with the computer core storage initialized to zero. Also, other system control options may be included in the submit file. The above example represents only the control logic essential to the successful execution of the simulation package.

To this point, no mention has been made of the selection of operating criteria for evaluation by the model. However, the selection

EXAMPLE DEMONSTRATION OF PROGRAM ORANGE

SIMULATION YEAR 1		CALENDAR YEAR 1979												
MONTH	INITIAL STORAGE	RESERVOIR NO 1		RES 2		MAX. SURFACE AREA	CAPACITY EVAP RATE	EVAP LOSS	5000 MIN. DAMPTER SPILLS	OPERATING SHORTAGE	POOL PUMPED INTO	PUMPED OUT	SYSTEM END NO. CONTENT	OPER. RULE
		INFLWS	UPSTN SPILLS	BEHND	BEHND									
1	0	1000	0	0	0	37	-.02	0	0	0	0	0	1000	5000
2	1000	2000	0	0	0	80	-.01	1	0	0	0	0	3000	5000
3	3000	2000	0	0	0	100	-.04	4	1700	0	0	0	4900	5000
4	4000	2000	0	0	0	100	-.14	14	643	0	0	0	5000	5000
5	5000	750	0	0	0	100	-.22	22	431	0	0	0	5000	5000
6	5000	500	0	0	0	100	-.27	27	279	0	0	0	4000	4000
7	5000	0	0	0	0	70	-.35	24	879	0	0	0	3000	3000
8	4000	0	0	0	0	48	-.28	13	1339	0	0	0	2000	2000
9	3000	0	0	0	0	42	-.17	7	0	0	0	0	2493	3000
10	2000	0	0	0	0	50	-.06	4	0	0	0	0	3489	4000
11	2493	1000	0	0	0	55	-.01	1	0	0	0	0	4000	4000
12	3489	1500	0	0	0	55	-.01	1	0	0	0	0	4000	5000
YEAR TOTALS.		11750	0	0	0	114	5587	0	0	0	0	0	0	0

MONTH	INITIAL STORAGE	RESERVOIR NO 2		MAX. SURFACE AREA	CAPACITY EVAP RATE	EVAP LOSS	5000 MIN. DAMPTER SPILLS	OPERATING SHORTAGE	POOL PUMPED INTO	PUMPED OUT	SYSTEM END NO. CONTENT	OPER. RULE
		INFLWS	UPSTN SPILLS									
1	2000	199	0	36	-.07	0	0	1763	0	0	0	0
2	0	199	0	0	-.10	0	0	150	0	0	0	0
3	0	199	0	0	-.03	0	0	150	0	0	0	0
4	0	199	0	0	-.03	0	0	150	0	0	0	0
5	0	199	0	0	-.06	0	0	150	0	0	0	0
6	0	199	0	0	-.11	0	0	150	0	0	0	0
7	0	199	0	0	-.21	0	0	150	0	0	0	0
8	0	199	0	0	-.27	0	0	150	0	0	0	0
9	0	199	0	0	-.23	0	0	150	0	0	0	0
10	0	199	0	0	-.15	0	0	150	0	0	0	0
11	0	199	0	0	-.09	0	0	150	0	0	0	0
12	0	199	0	0	-.02	0	0	150	0	0	0	0
YEAR TOTALS.		2000	0	0	0	0	0	3530	0	0	0	0

Figure IV.5. Example output from Program MODSIM.

DEMAND NODE 3		NODE 3	
MONTH	DEMAND		SHORTAGE
1	100		0
2	200		40
3	300		140
4	400		0
5	500		0
6	500		0
7	500		0
8	400		0
9	300		0
10	200		40
11	100		0
12	100		0
YEAR TOTALS			220

DEMAND NODE 4		NODE 4	
MONTH	DEMAND		SHORTAGE
1	5000		2651
2	5000		3537
3	5000		3208
4	5000		1599
5	5000		2441
6	5000		2503
7	5000		2035
8	5000		1982
9	5000		1408
10	5000		2453
11	5000		2459
12	5000		2493
YEAR TOTALS			28704

Figure IV.5. Continued

3 VOLUMETRIC FLOW IN LINK 3

SEASON LINK NO.	1	2	3	4	5	6	7	8	9	10	11	12	AVERG
1	0	0	0	1786	663	431	879	879	1339	0	0	0	499
LOSS	0.	0.	0.	200.	74.	48.	98.	98.	149.	0.	0.	0.	
2	1700	160	160	160	160	160	160	160	160	160	160	160	293
LOSS	440.	40.	40.	40.	40.	40.	40.	40.	40.	40.	40.	40.	
3	1411	0	0	1323	275	78	459	544	1029	0	51	51	434
LOSS	249.	0.	0.	233.	48.	14.	81.	90.	100.	0.	9.	9.	

RETURN FLOWS CALCULATED

RETURN FLOW EQUATION NO.1 1 RETURNS TO NODE NO.1 4

SEASON	1	2	3	4	5	6	7	8	9	10	11	12
938	1463	1792	2078	2284	2414	2506	2554	2572	2537	2490	2456	2456

Figure IV.5. Continued.

of the appropriate operational criteria is paramount to the success of the particular analysis. Indeed, the right answer to the wrong problem can be potentially more harmful than no answer at all. Specific attention must be afforded the development of operating rules to insure that the problem perceived is the problem analyzed.

The nature and generality of the model provides the user with a high degree of flexibility in the analyses which can be performed. For instance, if instream uses, such as low flow augmentation, are of concern, minimum channel capacities can be established which reflect the desire to maintain appropriate levels of flow. By varying the priorities placed on demands and storages, the critical time periods when it may be difficult to sustain minimum flow levels can be determined. Certain tradeoffs between the sacrifice of water held in storage and the minimum required flow can be determined.

Tradeoffs among more traditional water uses can easily be analyzed; for example, irrigation demands competing with municipal/industrial demands for a limited water supply. By varying the priorities associated with these demands one may test alternate schemes for minimizing the shortage to both sectors, or evaluate management alternatives which distribute expected shortages in some equitable manner. Further, MODSIM is capable of evaluating tradeoffs among in-storage uses of water in differing reservoirs. Flood control pool maintenance versus holding water in storage for recreational usage is a prime



example. The reservoir operating rules input to Program MODSIM may reflect either the desire to maintain storage levels at some point below maximum capacity during certain months (flood control) or maintain levels as high as possible to enhance recreation opportunities. By manipulating the priorities placed on achieving the target storage levels, different operational schemes designed to accomplish these goals can be analyzed over long time periods. Finally, perhaps the greatest advantage of MODSIM is the capability (for large-scale river basins) of simultaneously considering all of the above water usages in a single execution of the code.

## CHAPTER V

### PRESENTATION OF CASE STUDIES

#### A. Introduction

Two case studies were undertaken to fully demonstrate the capability and utility of MODSIM for aiding in the analysis of changes in water resources policy within a river basin. In addition, it is hoped that these case studies will provide the potential user with insight into the formulation of his problem in such a manner that can be readily analyzed by MODSIM. Considerable thought was devoted to the selection of appropriate case studies that were relevant, timely, and provided potential for the actual use of the results. Therefore, several water resources planning and/or management problems currently concerning area (Northern Colorado Front Range) decision-makers were evaluated. These perceived problems were judged according to such factors as complexity, information requirements, potential cost (time and money), urgency as related to other water allocation problems, and the degree of professional interest expected in the study.

The two case studies presented in this report differ completely in objectives; however, they are both located in the same river basin (the Cache la Poudre River Basin) in north-central Colorado (Figure V.1). Even though two entirely different problem formulations are necessary, much of the information requirements remain the same (evaporation rates, gaged inflow records, area-capacity relationships, demands, etc.).

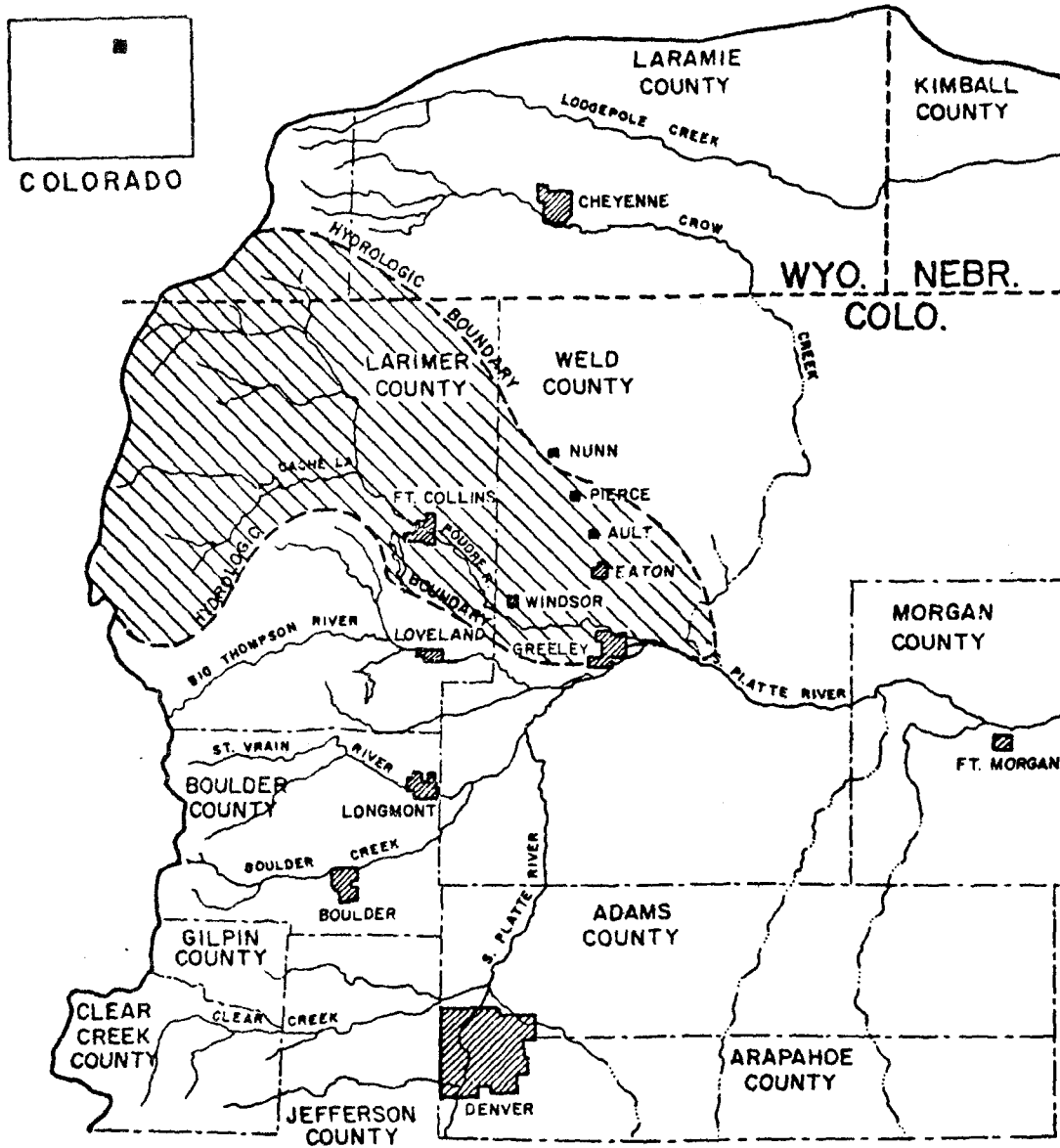


Figure V.1. Location of Cache la Poudre River Basin.

In other words, within the same hydrology and institutional framework many varying problems coexist.

As part of Water Division 1, District 3, the Cache la Poudre River Basin has as complex a system of interrelated water storage and distribution structures and regulations as anywhere along the Front Range. District 3 is also one of the most productive agricultural areas in Colorado. Consequently, irrigated agriculture has dominated the water use in the area. The Cache la Poudre River Basin is also favorable as a study area since there has been much previous modeling work done, although not related to the case studies presented here. However, much information can and has been extracted from these previously completed studies. Also, since water in the Cache la Poudre River on an average annual basis is highly over-appropriated, it affords the challenge of modeling a system in great need of comprehensive planning studies.

## B. Background Information

### B.1 Physical description of the study area

The extremes in elevation in the basin differ by about 7550 vertical feet. The agricultural portion of the valley represents almost 50 percent of the entire basin area and ranges in elevation from roughly 4650 feet above MSL to 5800 feet. The western boundary of the Cache la Poudre River Basin is the Continental Divide, with a maximum elevation of 12,200 feet above MSL (Evans, 1971).

The natural surface water supply is composed of spring snowmelt and direct precipitation. Additional supply is realized from various transbasin diversions. The Colorado-Big Thompson (CBT) Project is the

most significant of these diversion projects and adds substantial flow to lower reaches of the Cache la Poudre River during irrigation seasons. Table V.1 lists sources of water supply to the basin and their corresponding percentage.

Table V.1. Sources of Water Supply for the Cache la Poudre River Basin (Evans, 1971)

SOURCE	Percentage (%)
Natural Inflows (Snowmelt, Precipitation)	44
Pumped Groundwater	33
CBT	17
Other Imported Waters (Transbasin Diversions)	<u>6</u>
	100

Within the Cache la Poudre system there are more than 30 major storage reservoirs located on the plains, plus an additional nine high country reservoirs with significant storage. These reservoirs are owned for the most part by established irrigation companies throughout the basin. For example, the North Poudre Irrigation Company has an elaborate system of canals and interconnected reservoirs and plays an important role in the local economy due to an extensive involvement in an exchange system which has developed in the basin. Figure V.2 displays the major features of the Cache la Poudre River Basin.

As mentioned previously, the average annual natural flow in the Cache la Poudre River has long been over-appropriated. Therefore, to augment this natural supply, a series of transbasin diversions have been established. This importation of western slope water is limited, however, by a number of legally binding obligations. These obligations include the

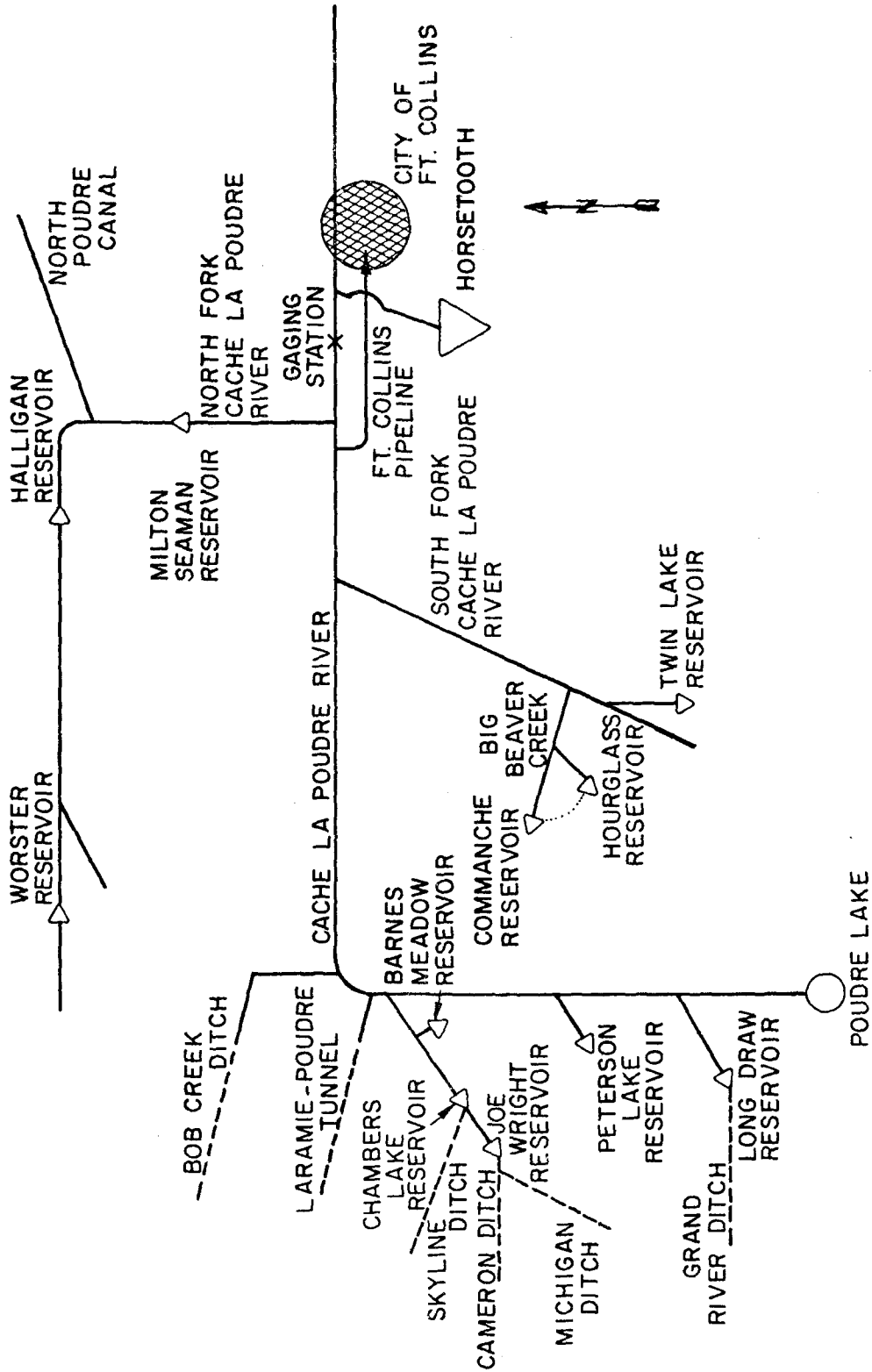


Figure V.2. Schematic diagram of major components of Cache la Poudre River Basin.

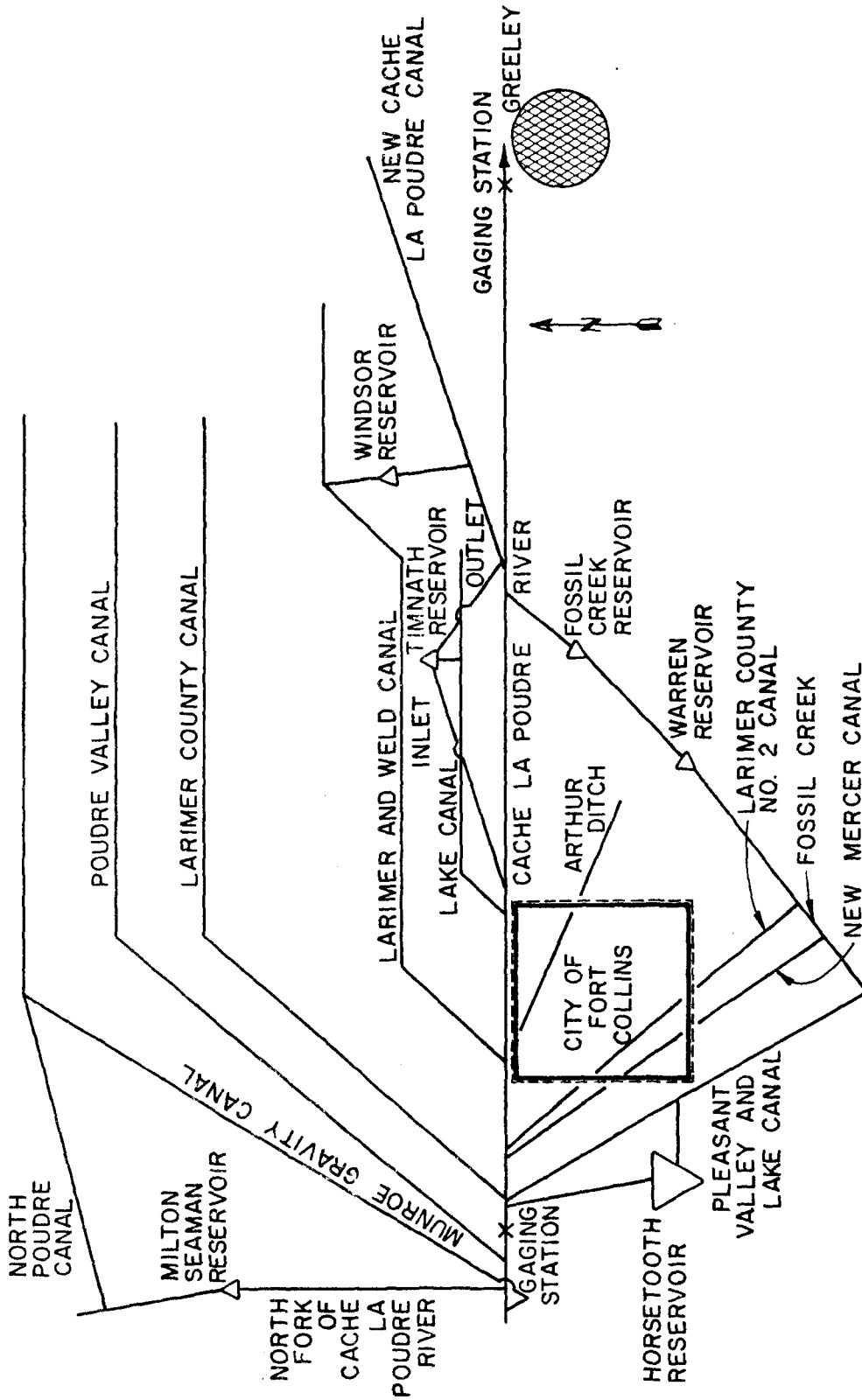


Figure V.2. Continued.

Laramie River Decree, the Colorado River Compact, and the North Platte River Decree. The largest transmountain diversion of water is the CBT Project. Originally, CBT water was intended solely for supplemental irrigation water. Municipalities (including Fort Collins) have subsequently acquired more than 23 percent of CBT water. Historically, high mountain transbasin diversions other than CBT have contributed, on the average, 45,000 acre-feet of water annually to the basin (Evans, 1971).

## B.2 Exchange system

Early in the evolution of the current irrigation scheme in the Poudre Valley, it was realized by the administrators of water in the basin that greater efficiency in water use could be achieved by creating an exchange system. Though Colorado constitutionally supports the appropriation doctrine and senior water right holders must receive their direct flow appropriation first, an exchange system has been developed which allows junior water right holders to receive water through development of additional storage. The important point is that this storage need not be available upstream of their point of diversion.

A maximum mean monthly natural flow of 1769 cfs in the Cache la Poudre River occurs in June. Unfortunately, it can be shown from a review of direct flow rights on the river that most major canals could not operate in June (highest flow month) without the use of some kind of exchange system. Most canals have undergone several expansions, each time filing for an additional decree with a priority date based on the time of the new construction. Through such action, the river has become over-appropriated to the point where as of 1970, for example,



only two years in 35 could the Greeley No. 2 Canal exercise its entire right (priorities 37, 44, 72, 83). The river has approximately 200 formal rights filed for its water. It is unlikely that Larimer and Weld Canal or North Poudre Canal would ever receive any water.

Exchanges of stored and direct flow water between ditch companies occur in conjunction with the reservoirs throughout the basin. Few reservoirs are located such that they can directly service the acreage of the owner. Subsequently, through the exchange system, it is of little significance whether or not a reservoir is located above or below the ditch system of its owner. With the addition of CBT water, which is capable of delivery via the river at any point below the Poudre Valley Canal, the exchange of water throughout the basin becomes even more attractive from an efficiency viewpoint. This system of exchanges has an important bearing on the management strategies which are to be analyzed as part of this case study (for additional information, see Evans, 1971, pp. 115-118).

### B.3 Fort Collins water system

Fort Collins raw water supply is derived from four sources:

(1) CBT water, (2) shares in Water Supply and Storage Company, (3) shares in North Poudre Irrigation Company, and (4) direct flow rights.

Table V.2 lists the annual amounts of these supply sources.

Table V.2. Fort Collins Water Supply (Wengert, 1975)

Source	Mean Annual Supply (acre-feet)
CBT	7,203
Water Supply & Storage Co.	833
North Poudre Irrigation Co.	4,190
Direct Flow	<u>12,293*</u>
	<u>24,519</u>

\*Includes recent acquisitions subsequent to Wengert

The City has two water treatment plants with a combined capacity of approximately 44 mgd. Treatment Plant 1 is located 11 miles northwest of Fort Collins on the Cache la Poudre River and has a capacity of 20 mgd. The second plant is situated at the base of Horsetooth Reservoir Spring Canyon Dam and has a capacity of 24 mgd. The capacity of Plant 2 is scheduled for a 10 mgd expansion by 1980 (Wengert, 1975).

West Fort Collins Water District serves an area to the northwest of Fort Collins. The District purchases treated water from the City and exchanges one acre-foot of CBT water for every unit of treated water the City supplies the District. It is assumed that two percent (2%) of the total gross water supply to the City is diverted to West Fort Collins Water District. Furthermore, no return of this diversion is realized at the City's waste treatment facilities. In other words, Fort Collins does not recover any of the water it supplies West Fort Collins.

M.W. Bittinger and Associates, Inc. (1975) conducted a study in which a detailed analysis of the consumptive use of treated water within the City of Fort Collins was undertaken. Consumptively used water and percentage of adjusted (minus West Fort Collins Water District) total inflow are provided on a monthly basis for 1974. Table V.3 lists the results. The Bittinger report states:

As long as the uses of City water remain in the approximate proportions that existed in 1974, the percentages...should be acceptable for determining the amount of City effluent available for a succession of uses without harming other water rights on the river.

Due to varying microclimatic conditions and changes in land use, these percentages (Table V.3) may fluctuate somewhat.

Table V.3. Consumptive Water Use Fort Collins - 1974  
(Bittinger, 1975)

Month	Adjusted Inflow (acre-feet)	Total Consumptive Use (acre-feet)	Percent
JAN	626.7	6.8	1.1
FEB	577.6	6.8	1.2
MAR	679.5	10.9	1.7
APR	881.8	378.9	42.9
MAY	2029.3	1231.5	60.7
JUN	2251.8	1239.0	55.0
JUL	2855.9	1163.0	45.5
AUG	2353.1	1094.6	46.5
SEP	1541.6	541.7	35.1
OCT	1166.6	254.0	21.8
NOV	844.9	13.6	1.6
DEC	798.0	10.9	1.4

At the wastewater treatment end of the City's system there are two options for treated effluent release. The effluent can either be returned to the river or diverted to Fossil Creek Reservoir.

C. Case Study 1: High Mountain Reservoir Recreation Study

C.1 Problem statement

As stated previously, several high mountain reservoirs are located within the basin boundaries. In the past, these reservoirs have been operated exclusively for the provision of a late season irrigation water supply. Such a policy has often resulted in the complete emptying of these reservoirs toward the end of the irrigation season. Attention has been focused on the inclusion of recreation in a multipurpose framework for some of these reservoirs.

The City of Greeley, Colorado, owns and operates six high mountain reservoirs in the Cache la Poudre River Basin. Of these six reservoirs, water stored in five is sold on a seasonal basis to the North Poudre Irrigation Company and water stored in the sixth (Milton Seaman) is used for exchange purposes and municipal supply. The five high mountain Greeley-owned reservoirs are Peterson, Barnes Meadow, Commanche, Twin Lake, and Big Beaver. These reservoirs, along with the North Poudre Irrigation Company reservoir and canal system, form an autonomous unit in that all water originating in the Greeley reservoirs is delivered to the North Poudre system.

The five high mountain reservoirs were evaluated according to their perceived public recreation potential by outdoor recreation specialists assuming that stable pool elevations could be maintained at or near maximum levels. The analysis included such considerations as fisheries potential, scenic beauty, private versus public ownership of riparian lands, ease of access, etc. The results showed that Barnes Meadow and Twin Lake reservoirs have the highest recreation potential of the five. Commanche Reservoir and Peterson Reservoir were believed to have limited recreation potential while Big Beaver Reservoir was declared to have no recreation potential whatsoever due to private ownership of riparian lands (Aukerman, et al, 1977). The problem in this case study is one of determining if it would be possible, from a hydrologic and legal standpoint, to maintain a stable pool elevation, at or near maximum, in one or more of these reservoirs according to the preferences outlined above. This problem is not as straightforward as it may first appear in that such a change in the operating policy of these reservoirs would,

to some extent, alter the traditional hydrology of the basin. This alteration must occur in such a manner that the North Poudre Irrigation Company demands for Greeley reservoir water are satisfied, no injury to downstream water right holders is incurred, and that appreciable changes in the flow regime of the river do not result.

### C.2 Study objective

The objective of this case study is to investigate opportunities to operate the high mountain reservoirs in such a manner that would allow the maintenance of storages at or near capacity while meeting the North Poudre Irrigation Company demands from other reservoirs owned and operated by the company. The North Poudre Irrigation Company owns and operates many plains reservoirs with storage capacities significantly greater than those of the high mountain reservoirs under consideration. Halligan, Park Creek, and North Poudre No. 15 plains reservoirs have traditionally held large carry-over storages from season to season. These reservoirs have virtually no recreation potential. Therefore, if in the management of the Greeley-North Poudre system as a whole, the severe late season drawdown in the selected high mountain reservoirs could be curtailed while allowing storage levels in the plains reservoirs to more widely fluctuate, enhanced mountain reservoir recreation may be provided.

The approach taken in investigating this problem is to isolate the Greeley high mountain reservoir subsystem and the North Poudre Irrigation Company subsystem. In this manner only water released from the high mountain reservoirs along with other reservoir water controlled by North Poudre needs to be considered. This allows analysis of changes

in the operating policies of the reservoirs without considering direct flow rights along the river or other reservoir water not directly involved with the study.

### C.3 System configuration and decomposition

Due to the interdependence of system components, management of the high mountain reservoirs cannot be analyzed without proper consideration of the demand points for their stored water. However, once the reservoirs to be studied are identified, along with the various distribution and use subsystems to which they contribute water, a spatial decomposition isolates this subsystem of water supply, distribution, and use for further analysis. As long as all sources and sinks of *reservoir* water in the subsystem are considered, a meaningful study of the decomposed system can be conducted even though the entire system is no longer under investigation. This approach allows the problem to remain tractable without great sacrifice in accuracy and detail. Figure V.3 shows the decomposed Greeley-North Poudre subsystem for this case study.

Only the demand for intrabasin high mountain reservoir water is of interest for this problem. Accordingly, imported water is ignored along with direct flow of river water to satisfy irrigation requirements. Since the origin of the reservoir water contributing to demand satisfaction is the only concern, its final destination can be considered a single demand center without introducing any error into the analysis. All of the individual North Poudre Irrigation Company plains reservoirs (N.P. No. 1 and those to the east) provide water to turnouts for application to fields. Of interest to this study is the *total* monthly volume of mountain reservoir water supplied to these plains reservoirs.

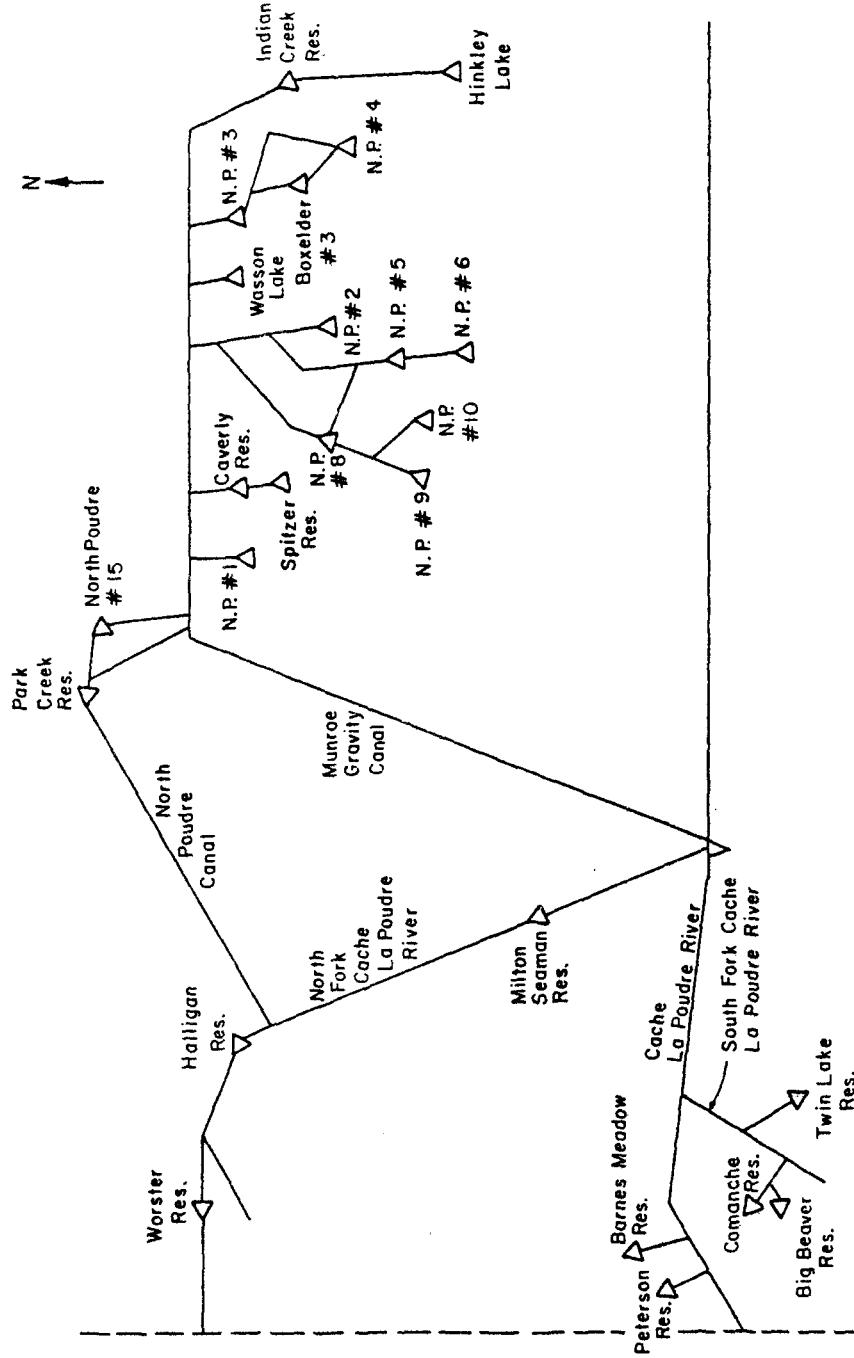


Figure V.3. Decomposed case study reservoir and canal subsystem.

Therefore, the North Poudre plains reservoirs are aggregated into one large plains reservoir whose surface area and storage volume are equal to the sums of the surface acreages and volumes of the individual plains reservoirs. This maneuver allows the total monthly demand for water from the high mountain reservoirs to be lumped together at one demand center (Figure V.4).

Once the physical system has been isolated, and all important components identified, it must be translated into a corresponding graphical network of nodal points and linkages. Care must be exercised during this translation to insure that the essence of the physical system is captured in its entirety. All nodes and links are then labeled numerically. Reservoirs must be labeled first, followed by non-storage nodes. Figure V.5 displays the network configuration for this case study.

#### D. Case Study 2: Rawhide Project

##### D.1 Problem statement

The problem selected for the second case study addresses itself to the availability of water for cooling purposes and other in-plant uses for the proposed *Rawhide Project*. The Rawhide Project is a coal-fired electric generation plant to be located approximately 20 miles north of Fort Collins, Colorado. The project is designed to augment projected power demands of the municipalities of Estes Park, Fort Collins, Longmont, and Loveland, Colorado. The first 230 megawatt unit should be in operation by 1985. Such facilities require adequate supplies of water. The Platte River Power Authority (PRPA) is negotiating with various potential water suppliers, including the City of Fort Collins.



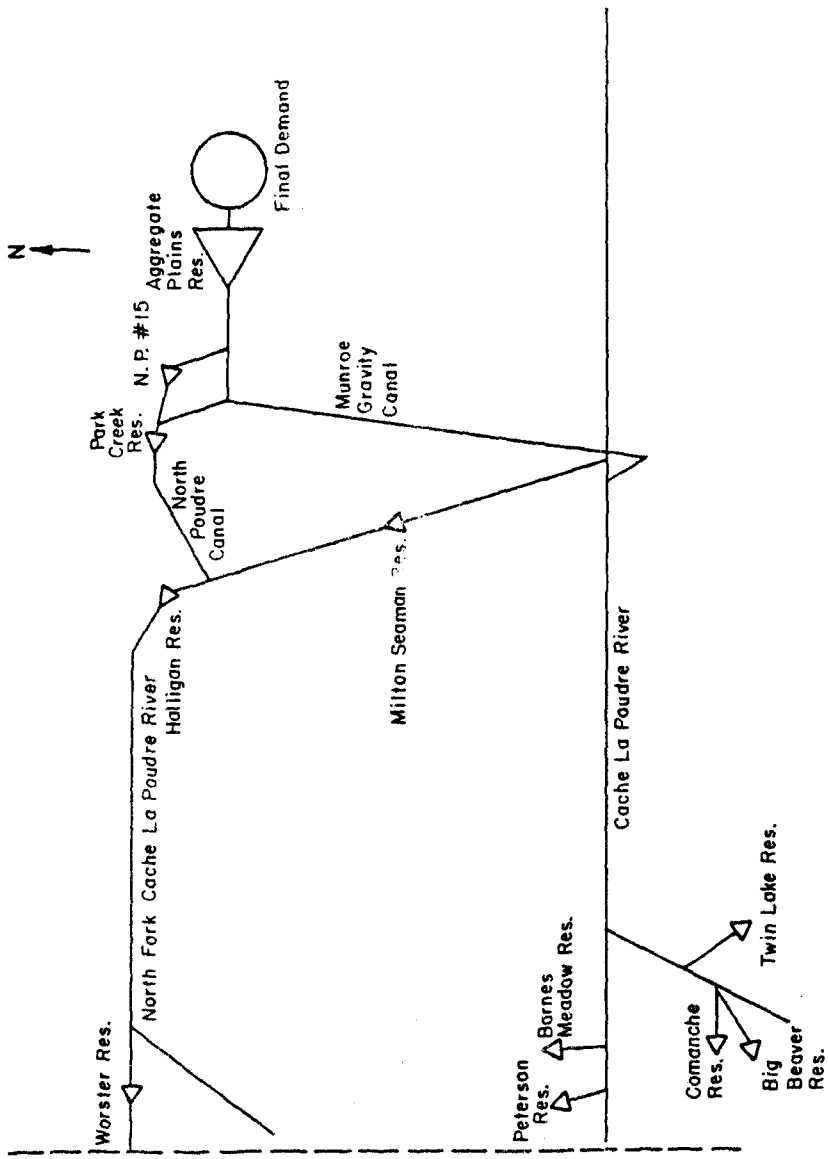


Figure V.4. Decomposed subsystem with aggregated plains reservoirs.

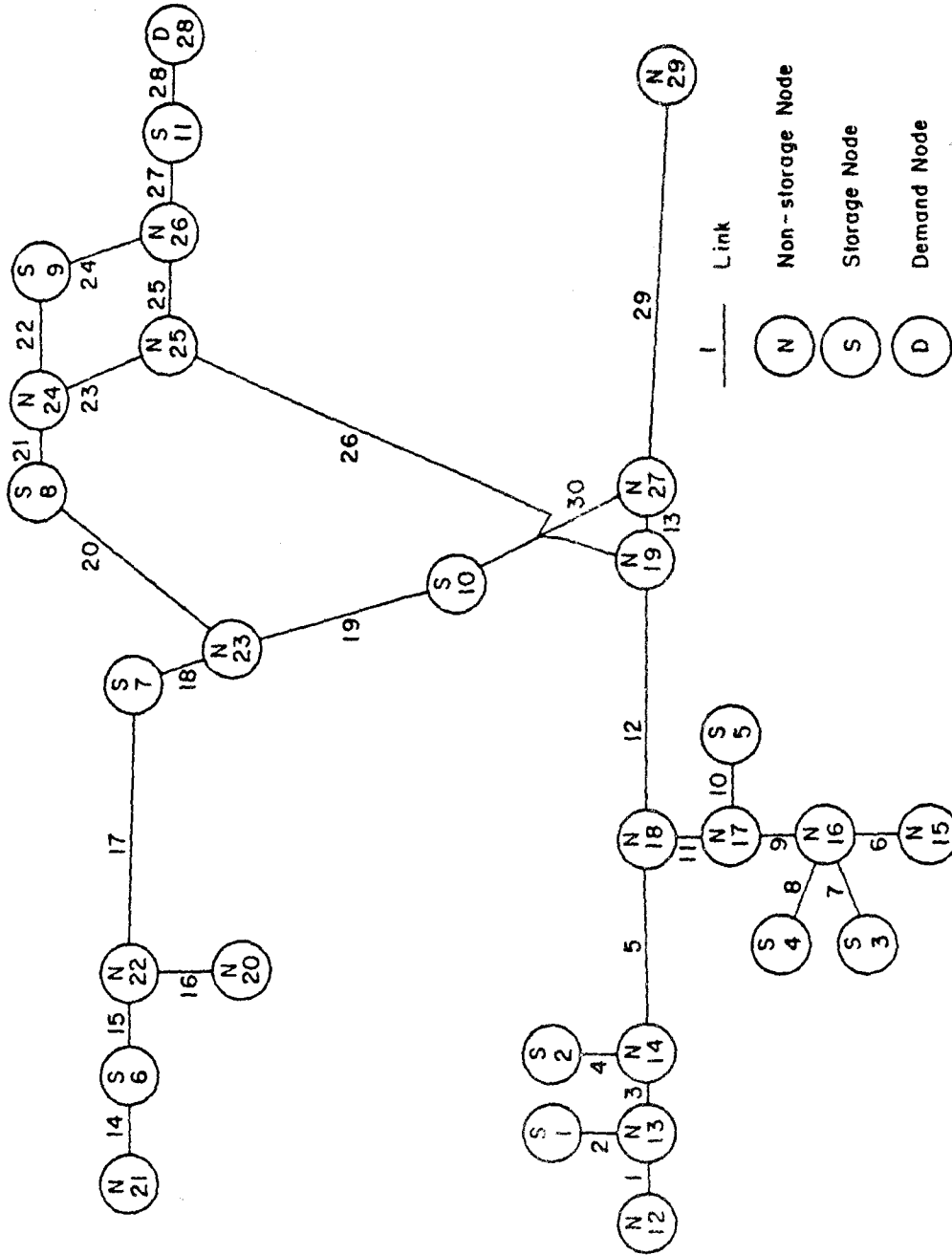


Figure V.5. Network configuration for case study subsystem.

A preliminary contract has been made between Fort Collins, PRPA, and the Water Supply and Storage Irrigation Company outlining a scheme whereby the water requirements of the Rawhide Project could possibly be met. However, before any of the parties enter into a formal agreement, the potential effect of such a scheme on those parties directly and indirectly involved or impacted must be ascertained.

The project calls for the construction of a 13,000 acre-foot reservoir from which waters can be circulated through the power plant for cooling and additional purposes. The Rawhide Project is scheduled for commencement of operation in 1985. However, the Rawhide Reservoir must be full prior to the beginning of power generation. To accomplish this requirement, the agreement between the parties concerned states that filling must begin in 1981. Upon filling the reservoir, the Rawhide Project will require no less than 4200 acre-feet of firm water annually and a stable reservoir elevation within two or three feet.

To accomplish the above tasks, Fort Collins is to provide the Rawhide Project with the opportunity to utilize sewer effluent attributable to newly developed or imported water first used by the City. Imported or foreign water is water which originates outside of the Cache la Poudre River Basin and is diverted from some basin other than the Poudre Basin. The significance of *newly developed* refers to the fact that changing the diversion of the City's effluent attributable to *old* foreign water may result in possible *injury* to those users who have historically come to rely on its availability. In contrast, *new* foreign water is that which only recently or in the future is imported into the Cache la Poudre River Basin in excess of waters which constitute old foreign water.

New foreign waters for Fort Collins originate in the adjacent North Platte River drainage and are diverted across the basin divide via the Michigan Ditch. These waters are then placed in Joe Wright Creek, tributary to the Poudre River. At this point, the water can be used directly or stored in the expanded capacity of Joe Wright Reservoir.

Joe Wright Reservoir is owned and operated by Fort Collins and is being enlarged by the City from 800 acre-feet of water to approximately 8,000 acre-feet. Historic diversions through the Michigan Ditch have been estimated by the parties involved as 1,000 acre-feet per year. Accordingly, the reuse of the first 1,000 acre-feet annually diverted through the Michigan Ditch is, in effect, prohibited. This is not to say that the Rawhide Project cannot divert the effluent from the City's first use of the initial 1,000 acre-feet. However, if such an action takes place, the City must release from other sources the amount of water that would have existed if the 1,000 acre-feet were used by the City and the corresponding return flow was not diverted to the power plant.

New foreign water diverted into the basin via the Grand River Ditch is also available for reuse by the Rawhide Project after first use by Fort Collins. This water can be stored, upon importation, in Long Draw Reservoir which is owned by the Water Supply and Storage Company. However, only 6,000 acre-feet of storage space in this reservoir is to be made available to Fort Collins for storage of Grand River Ditch imports.\*

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\*Maximum capacity of Long Draw Reservoir is approximately 10,500 acre-feet.

### D.2 Study objective

The objective of this case study is to determine, first, if the cooling pond could be filled prior to the beginning of power generation in 1985, and, second, if a minimum of 4,200 acre-feet of reusable water can be provided at a uniform rate thereafter. For this case study all water that becomes available in the basin must be considered. This includes direct flow river water, Colorado-Big Thompson Project water, intrabasin reservoir water, and, of course, the transbasin diversions via Michigan and Grand River ditches. This objective has many ramifications. Injury to water users downstream from the pipeline intake must not occur or must be compensated. A *borrowing* arrangement must be made in order to maintain uniformity in delivery of reused water to the pipeline. A stable pool elevation in the cooling pond must be maintained. The preference of the City's direct flow right over other sources of water must be preserved. Finally, spills from Joe Wright Reservoir and Long Draw Reservoir must be considered. However, as in Case Study #1, the total river basin system can be decomposed into a subsystem of the specific components necessary to analyze this problem.

### D.3 System configuration and decomposition

As previously discussed, the Poudre River system is extremely complex in both composition and operation. Fortunately, the system has two control points situated in advantageous positions. The State of Colorado has two gaging states located on the Poudre River. The upstream gage is situated near the mouth of Poudre Canyon before most of the ditch diversions occur, while the downstream gage is located on the Poudre at the confluence of the South Platte River.

Due to the size of the system (number of interrelated components) it would be all but impossible to model the entire system. Therefore, the complete system is decomposed to a point where the key components of the case study are individually considered, but the remainder of the system is aggregated in various ways. In this manner, the integrity of the system as a whole is preserved while only certain components are *directly* modeled.

The components of the decomposed system pertaining to the Rawhide Project are listed in Table V.4. The system can be defined in this manner as a result of the placement of the aforementioned gaging stations. Flow adjustments are made between gages, as well as from the upstream gage to the headwaters of the Poudre River. The effect of varying diversion schemes on the aggregated systems components can be determined *a posteriori*. Figure V.6 is a schematic diagram depicting the major components of the decomposed system.

Table V.4. Rawhide Project Subsystem Components

Reservoirs	Irrigation Ditches	Other Conveyances
Long Draw	Munroe Gravity Canal	Ft. Collins Pipeline
Joe Wright	Larimer & Weld Canal	Charles Hansen Canal
Chambers Lake	Lake Canal	Timmath Reservoir Inlet
Horsetooth	New Cache la Poudre Canal	Rawhide Pipeline
North Poudre No. 6		
Windsor	<u>Imports</u>	
Timmath	Michigan Ditch	
Fossil Creek	Grand River Ditch	
Rawhide Cooling Pond		

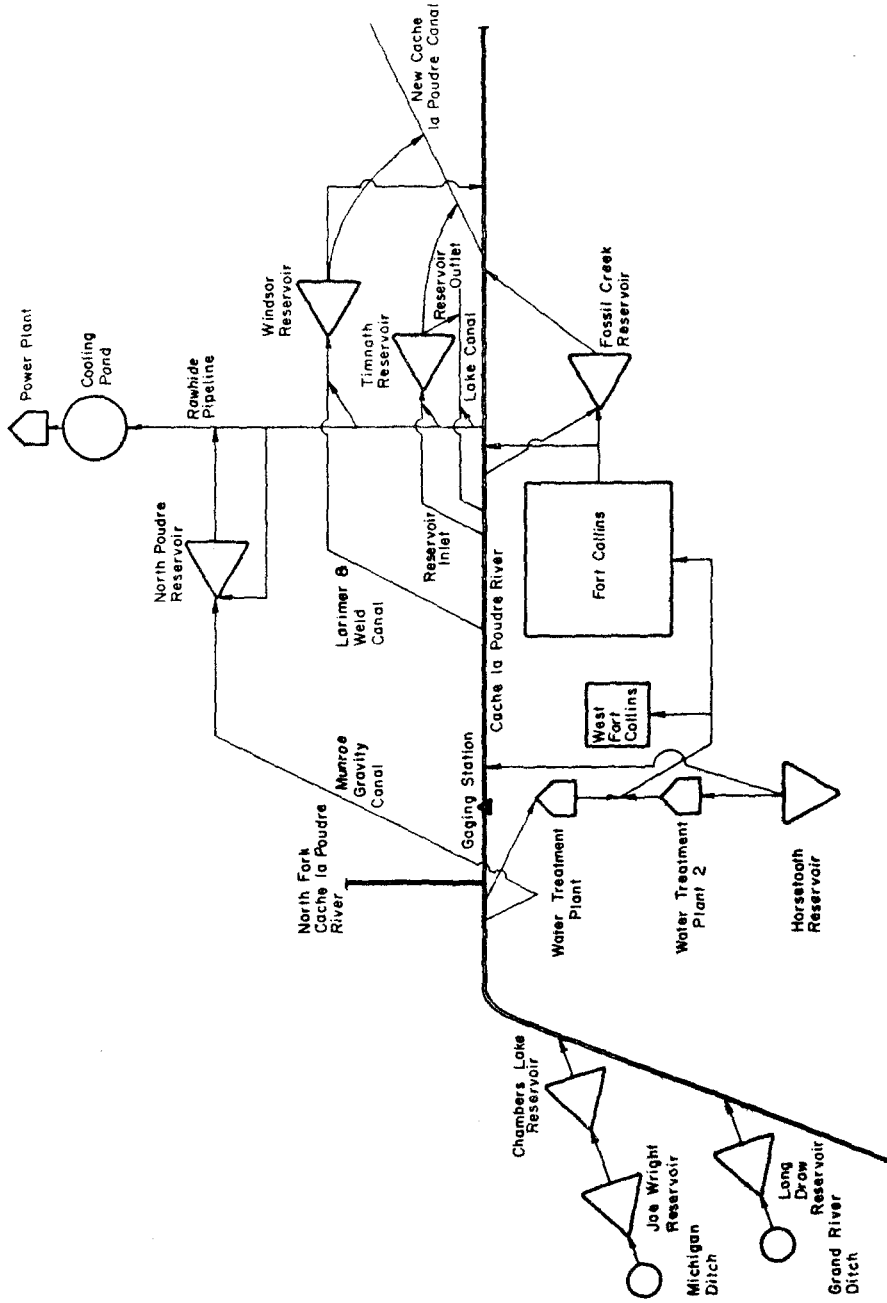


Figure V.6. Major components of decomposed subsystem for Rawhide Project.

Once the physical system to be modeled has been delineated, it must be translated into a node-link network configuration. Particular attention must again be afforded this phase of any study to insure that the essence of the system remains intact. Figure V.7 shows the network system for which the model is calibrated. Table V.5 lists the names of the nodes and the flow capacity of each link. Notice that the Fort Collins water treatment plants have been represented as links instead of nodes. The upper bound on each link corresponds to the respective monthly treatment capacity of each plant. To effectively model the decomposed system, 35 nodes and 47 links are required to represent the physical system, plus additional artificial nodes and arcs.

#### E. Data Organization

Since both case studies involve the same river basin, commonalities in data requirements exist. The same hydrologic, climatic, structural, and institutional characteristics are encountered in each case study. This section identifies the agencies and individuals who have made available the information needed to conduct the case studies. Also, this section contains the method of calculation of the evaporation rates used throughout the analysis. Channel characteristics and reservoir characteristics are also presented, along with other necessary data common to both studies. Information which is specific to one case study is introduced later in the appropriate section of this report. All data must be compatible, therefore, units are selected as follows: (1) flows--acre-feet/month, (2) storage--acre-feet, (3) surface area--acres, (4) net evaporation rate--feet, and (5) demands--acre-feet.



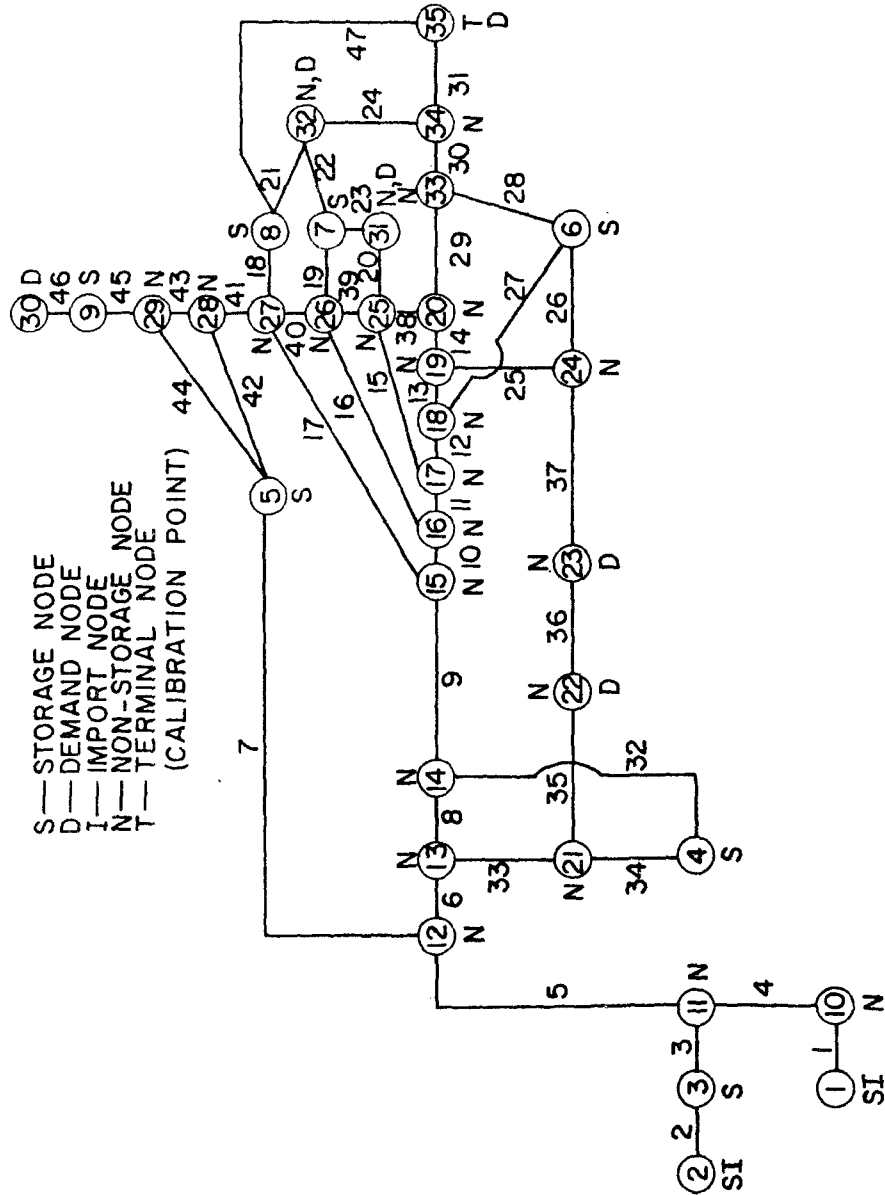


Figure V.7. Network configuration for Rawhide Project.

Table V.5. Rawhide Project Network Components Description

Node #	Name	Node #	Name
1	Long Draw Reservoir	19	Ft. Collins Return Flow
2	Joe Wright Reservoir	20	Rawhide Pipeline Diversion
3	Chambers Lake Reservoir	21	Ft. Collins Inflow
4	Horsetooth Reservoir	22	West Ft. Collins
5	North Poudre No. 6 Reservoir	23	Consumptive Loss
6	Fossil Creek Reservoir	24	Dummy
7	Timmath Reservoir	25	Rawhide Pipeline
8	Windsor Reservoir	26	"
9	Rawhide Cooling Pond	27	"
10	Upper Stem Poudre River	28	"
11	"	29	"
12	Munroe Canal Diversion	30	Rawhide Power Plant
13	Ft. Collins Pipeline Diversion	31	Lake Canal
14	Confluence N. Fork Poudre River	32	New Cache la Poudre Canal
15	Larimer & Weld Canal Diversion	33	Release from Fossil Creek
16	Timmath Reservoir Inlet	34	New Cache la Poudre Canal Diversion
17	Lake Canal Diversion	35	Terminal
18	Fossil Creek Reservoir Inlet		

Link #	Maximum Flow (ac-ft/mo)	Link #	Maximum Flow (ac-ft/mo)
1	15000	25	4026
2	15000	26	4026
3	15000	27	11100
4	300000	28	11100
5	300000	29	300000
6	300000	30	300000
7	15000	31	300000
8	300000	32	91000
9	300000	33	1779
10	300000	34	2247
11	300000	35	4026
12	300000	36	4026
13	300000	37	4026
14	300000	38	0
15	158	39	0
16	10070	40	0
17	60667	41	0
18	60667	42	0
91	10070	43	0
20	158	44	0
21	17689	45	0
22	10070	46	0
23	10070	47	17689
24	35490		

### E.1 Sources of information

Data requirements for performance of the case studies were met from the following sources.

1. The Water Commissioner, District 3, provided data concerning both reservoir and channel characteristics. Also, the commissioner provided valuable assistance in interpreting the water rights structure of the Cache la Poudre River Basin.
2. Information concerning the allocation of Horsetooth Reservoir water via the Colorado-Big Thompson Project was made available by the Northern Colorado Water Conservancy District offices located in Loveland, Colorado.
3. Detailed daily diversion data for all structures in Water District 3 were obtained from the Colorado Water Data Bank through the Division of Water Resources, State Engineer's Office.
4. The United States Bureau of Reclamation, Denver Office, provided information concerning evaporation rates from reservoir surfaces. These data were refined by accounting for precipitation taken from records compiled by the State Climatologist.

### E.2 Evaporation rates

Representative estimates of the expected evaporation rates were difficult to obtain because of a lack of information specific to the area of interest. The rates obtained from the Bureau of Reclamation (USBR) were not oriented toward this particular geographic region. However, the monthly distribution of the annual total was considered acceptable for irrigation years 1973-1975 (Shafer and Labadie, 1977). Two gross evaporation rates were necessary to differentiate between the

plains reservoirs (5000 to 6000 feet above MSL) and the high mountain reservoirs (8000 to 9000+ feet above MSL). An adjustment of the monthly distribution of the total annual value for the mountain reservoirs was made to reflect periods of ice and snow cover on the surface during winter months and differences in vapor pressure and wind velocities during summer. Figure V.8 shows these monthly percentages of the total annual evaporation. Annual summaries of climatological data obtained from the Office of the State Climatologist were used to calculate the net evaporation rates for each month during the three-year period. Mean annual corrected pan evaporation at Grand Lake (elevation 8288 ft) and Fort Collins (elevation 5001 ft) were divided into corresponding monthly values according to the distribution in Figure V.8. The observed monthly precipitation for stations at Red Feather Lakes (elevation 8237 ft) and Fort Collins were subtracted from these gross monthly rates to derive a representative net monthly evaporation rate for the plains reservoirs and high country reservoirs (Figure V.9).

### E.3 Channel characteristics

Since each physical arc must be bounded from above (lower bound equals zero) actual channel capacities were obtained from the CWDB and personal interviews with John W. Neutze, Commissioner, District 3. Typical capacities, along with loss coefficients where appropriate, are provided in Table V.6.

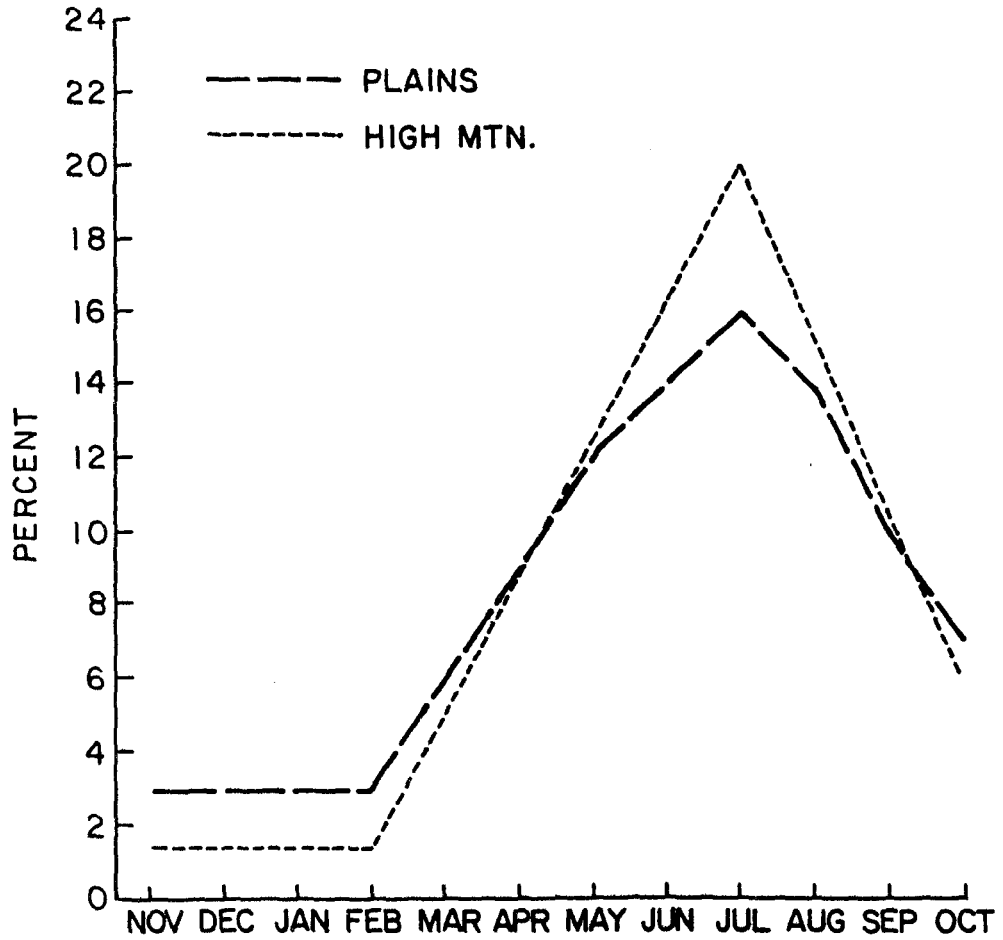


Figure V.8. Monthly distribution of evaporation as percentage of gross annual rate.

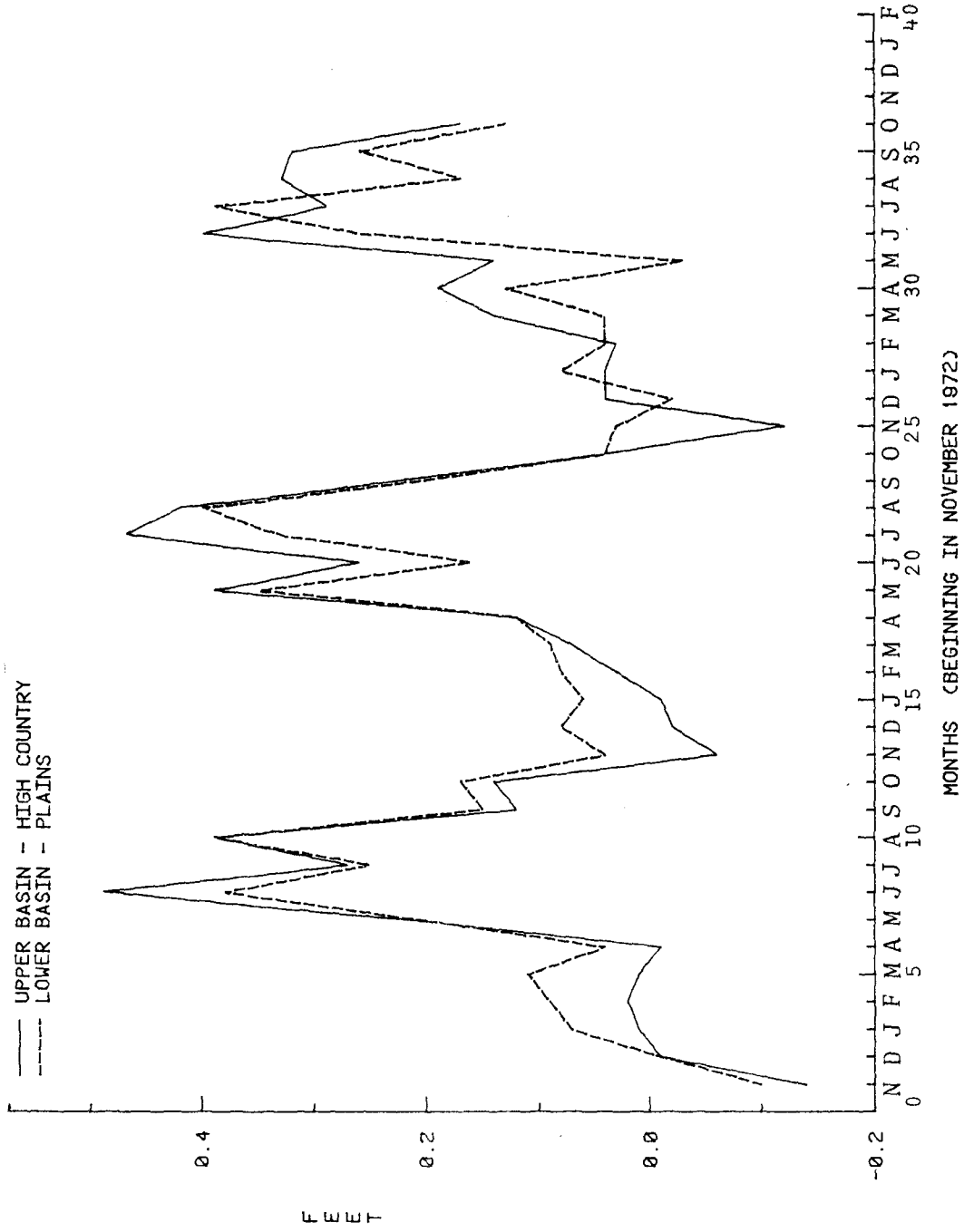


Figure V.9. Net evaporation rate for high country and plains.

Table V.6. Typical Channel Capacities and Loss Coefficients

Capacities	Capacity (acre-feet/month)	Loss (Percentage of Flow)
Mainstream Cache la Poudre	300,000	5.0
Munroe Gravity Canal	15,000	20.0-33.0
Hansen Supply Canal	91,000	---
Larimer and Weld Canal	60,667	20.0-33.0
Timnath Inlet	10,070	20.0-33.0
Lake Canal	9,100	20.0-33.0
New Cache la Poudre Canal	35,297	20.0-33.0

#### E.4 Reservoir characteristics

MODSIM uses a linear interpolation procedure to determine surface area from tables of volume versus surface area points for each reservoir. From an estimate of average surface area during any particular month, the amount of evaporation (net of precipitation) occurring from the water surface can be calculated. The model will accept up to 18 pairs of volume-surface area points for each reservoir. These points were calculated by solving a series of exponential equations relating volume and surface area to gage height (Thaemert, 1976). An interactive conversational computer program was written to calculate these tables, allowing zero or one discontinuity in each curve. Table V.7 contains an example calculation of area-capacity points. Horsetooth Reservoir is not included for reasons which are discussed in the following chapter.

Table V.7. Example Area-Capacity Relationships

Point	Timmath Reservoir			Fossil Creek Reservoir			Long Draw Reservoir		
	Gage Ht (ft)	Area (ac)	Vol. (ac/ft)	Gage Ht (ft)	Area (ac)	Vol. (ac/ft)	Gage Ht (ft)	Area (ac)	Vol. (ac/ft)
1	0.	0	0	0.	0	0	0.	0	0
2	3.778	70	196	4.000	8	40	8.889	69	772
3	5.667	89	345	6.000	28	241	13.333	91	1335
4	6.556	106	517	8.000	54	170	17.778	112	1969
5	9.444	131	776	10.00	80	318	22.222	131	2661
6	11.333	163	1110	12.44	112	530	26.67	149	3403
7	13.222	196	1522	14.00	147	817	31.11	166	4191
8	15.11	230	1988	16.00	188	1188	35.56	182	5019
9	17.00	265	2517	18.00	232	1652	40.00	198	5884
10	18.89	301	3107	20.00	281	2219	44.44	213	6783
11	20.78	337	3760	22.00	333	2897	48.89	228	7715
12	22.67	374	4475	24.00	390	3697	53.33	242	8676
13	24.56	412	5251	26.00	450	4626	57.78	256	9667
14	26.44	451	6090	28.00	515	5692	62.22	270	10519
15	28.33	490	6992	30.00	583	6906			
16	30.22	529	7955	32.00	655	8273			
17	32.11	569	8981	34.00	730	9804			
18	34.00	609	10070	36.00	810	11100			



#### F. Comparison of Case Studies

There are marked differences in these case studies which help to demonstrate the utility of MODSIM for water policy analysis. The high mountain reservoir recreation study is a straightforward analysis of the ability to alter the operating policies of several reservoirs to achieve the same end result as far as demand satisfaction is concerned, while enhancing recreation opportunities on certain reservoirs. Only the water normally contributed to the irrigation system by these reservoirs is important. Once the model has been satisfactorily calibrated, the study becomes a matter of adjusting reservoir priorities in such a manner that allows one to determine the effect of differing operating rules on the decomposed system. No further interpretation of the results produced by MODSIM is necessary, and the outcome of many varying operating policies can be determined quickly. The institutional framework within which the system operates is only marginally involved (by design) in this analysis. As long as the final demand for reservoir water is met, no injury to the North Poudre Irrigation Company will occur. Also, there should be no injury to water users downstream of the Munroe Gravity Canal.

In comparison, the second case study (Rawhide Project) is a much more sophisticated problem. Here, the hydrology is important, but of equal importance is the legal system. For instance, Fort Collins must first exercise its monthly direct flow right before drawing any reservoir water. Since all water in the basin is being considered, as opposed to only reservoir water in the first case study, model calibration must not only include reservoir storages, but also river flows.

There is much more flexibility in system operation due to the added complexity of the second case study. This flexibility must be taken into consideration when adjusting priorities throughout the network.

The primary goal of the high mountain reservoir study is one of determining to what degree the operating policy of the plains reservoirs can be traded with that of the high mountain reservoirs. Demands are given the highest priority and the model does the best it can to achieve target storage levels once the demand has been satisfied. The Rawhide Project, however, not only has certain demands which must be met; but qualifications on how they are met. These qualifications or constraints vary widely from month to month and are dependent upon both the hydrologic and institutional conditions present in any one month. Where the output of results by MODSIM for the first case study is adequate enough to draw particular conclusions about the problem, certain parts of the results provided by MODSIM for the Rawhide Project must be further analyzed to arrive at a conclusion.

CHAPTER VI  
MODEL CALIBRATION

A. Introduction

Model calibration for these case studies is defined as the adjustment of certain model parameters until the model *reasonably duplicates* available historical records for some prescribed time period. Calibration is an extremely important task to be accomplished in river basin studies such as these. Without successful model calibration, there can be no assurance of reliability in subsequent management alternative analyses. *Success* for these cases is defined such that little or no further improvement in model results, in relation to the historical records, can be achieved by continued parameter adjustment. Insufficient data were available at the time of the study for performing a model verification; e.g., splitting the data, calibrating over one portion, and verifying model consistency over the remaining part.

The goal of model calibration is to manipulate the priorities placed on individual reservoir storage and demand satisfaction until:

1. the calculated end-of-month reservoir storage volumes *reasonably duplicate* the historically observed end-of-month storage volumes
2. shortages in calculated water diverted to meet demand are minimized.

Since each case study was calibrated independently, the calibration exercise for each study is discussed separately. However, the same three-year period (1973-1975), and much of the same information is used to calibrate both cases. As mentioned earlier, the Poudre River Basin

is an extremely complex water resource system. Many water exchanges are not documented, since they originate in verbal agreements. Parameters such as channel loss coefficients are only estimates. These values are, however, the best judgements made by persons involved with the river system for many, many years. Also, the Out-of-Kilter Algorithm necessitates the conversion of real values to integer values, which introduces round-off errors. For these reasons, the term *reasonably duplicates* is employed. There is no substitute for good judgement and thorough knowledge of the system when evaluating the results of the calibration phase.

This chapter presents the results of the calibration phase of the two case studies. A brief discussion of the procedure for calibration of MODSIM for the reservoir recreation study is included with the results of this case study. However, a detailed, step by step, outline of the procedure for calibrating MODSIM for the Rawhide Project is provided which not only describes the calibration methodology but also should give potential users insight into data organization for model operation.

#### B. MODSIM Calibration for the High Mountain Reservoir Recreation Study

The approach used to calibrate MODSIM for the subsequent analysis of reservoir recreational potential is straightforward. All inflows which accrue to the decomposed system components are isolated. Evaporation rates are input along with the historical end-of-month reservoir storage volumes. The total monthly demand for reservoir water by the North Poudre Irrigation Company is also input for the three-year period. Finally, appropriate channel loss coefficients are included. An initial set of downstream demand ( $DEM_{i,t}$ ) and reservoir storage ( $OPRP_{i,t}$ ) priorities, from which the values of the  $w_{ij}$  are calculated according

to Equations III.8 and III.9, are selected and the model is operated to determine the distribution of storage based on the degree of demand satisfaction throughout the network. All other parameters, such as evaporation and channel loss coefficients, are fixed. The model results are compared with the historical records for the same three-year period, priority factors are adjusted according to the deviation of model results from historical values, and MODSIM is rerun. The above procedure is repeated until an acceptable deviation is reached or no further improvement can be made. In the latter case, if no further improvement can be made while results remain unacceptable, other model parameters, such as evaporation or channel loss coefficients, must be reviewed, perhaps leading to a redesign of the network or even a reconceptualization of the problem.

A complete summary of MODSIM calibration results for the high country reservoir recreation analysis can be found in Shafer and Labadie (1977; Table 5, pp. 187-189). The mean monthly deviation of calculated storage from historical storage for all the reservoirs (except Milton Seamon Reservoir and the aggregate plains reservoirs) is 2.16 percent. The highest monthly deviation recorded is 100 percent for Twin Lake Reservoir in May, 1975. However, the absolute values of calculated storage versus historical storage for Twin Lake in this month are zero acre-feet and 17 acre-feet, respectively. Even though the deviation is 100 percent, the difference in actual storage levels is not significant. The final storage priorities for the calibration phase are presented in Table VI.1. Decreasing values mean higher priorities, which reflect the implicit priorities that governed the historical management of the system.

Table VI.1. Implicit Historical Reservoir Storage Priorities for High Mountain Reservoir Recreation Study ( $OPRP_{i,t}$ )\*

Reservoir (i)	1973	1974	1975
Peterson	50	50	48
Barnes Meadow	50	55	45
Big Beaver	50	50	59
Commanche	55	50	59
Twin Lake	50	50	59
Worster	70	46	48
Halligan	60	60	48
Park Creek	70	70	48
N.P. #15	80	80	47

\*Referring to Equation III.9, a lower value for  $OPRP_{i,t}$  implies a higher priority since it results in a more negative value for the corresponding  $w_{ij}$ . Because MODSIM performs a minimizing operation, this means that a more negative value would encourage the model to retain more water in storage during a given month  $t$ , i.e., transfer more water to the artificial storage node.

Milton Seamon Reservoir has special consideration in the analysis, in that, although it is owned and operated by the City of Greeley, it does not directly contribute to the North Poudre Irrigation Company system. Also, Seaman Reservoir has little or no recreational potential. This reservoir, however, does contribute slightly to the irrigation system in an indirect fashion through the exchange process. In this analysis, Milton Seaman Reservoir is viewed as an equalizing reservoir and is not allowed to influence the operation of the subsystem. Historically, Seaman Reservoir has a beginning period storage of 2460 acre-feet. This is set equal to zero in the study and no unregulated flows into it were considered. In this manner, Seaman Reservoir cannot unduly influence system performance. The small contribution made by this reservoir toward demand satisfaction for reservoir water is subtracted from the total demand, thereby eliminating the error of overestimating the demand. Finally, its ending storage was allowed to go to zero.

The difference between total historical ending storage volume (excluding Milton Seaman) and total calculated ending storage volume for the calibration exercise is approximately 1875 acre-feet (historical greater than calculated). Although this value is not significant, it does indicate some data inconsistencies. Subsequently, MODSIM was rerun with the above priorities; however, evaporation rates were set equal to zero. For this case, the calculated ending storage was greater than the historically observed ending storage. The above result tends to lend support to the suggestion that evaporative losses are not entirely reflected in the historical records of observed storage in some of the reservoirs. Likewise, it is also true that the evaporation rates used

for these analyses are probably somewhat overestimated, which could explain the lower ending storage. It was suspected that the so-called *observed* storages may not have been observed at all because records showed no change in storage in some cases even though there were no inflows or outflows with evaporation still occurring. In spite of inconsistencies in the observed data and uncertainties with regard to evaporation rates, it was decided that the model could be trusted for purposes of the high mountain recreation analysis.

### C. MODSIM Calibration for the Rawhide Project

#### C.1 Procedure

The following step by step procedure was used to calibrate MODSIM for the Rawhide Project.

1. Set the lower and upper bounds equal to zero for all links representing the Rawhide Pipeline.
2. Set desired monthly ending storage for Joe Wright Reservoir to zero for all months. Joe Wright was inactive during the calibration period.
3. Obtain initial storage volumes (November 1, 1972) (Table VI.2).
4. Set desired or target end-of-month storage values as historically observed end-of-month storage divided by reservoir maximum capacity (except Horsetooth Reservoir) (Table VI.3).
5. Determine unregulated and spurious inflows:
  - i. Inflow to node 14 (confluence of North Fork Cache la Poudre River) equals monthly release from Milton Seaman Reservoir.
  - ii. Inflow to node 10 equals Fort Collins gaged flow plus diversions to Fort Collins Pipeline and Munroe Gravity Canal, minus releases from Chambers Lake, Long Draw Reservoir, and Milton



Table VI.2. Initial Storage Levels  
(November 1, 1972)

Reservoir	Water in Storage (Acre-Feet)
Long Draw	1174
Chambers Lake	2192
North Poudre No. 6	6224
Fossil Creek	5837
Timmath	5455
Windsor	9805
Horsetooth	0

Table VI.3. Storage Targets % of Full

		Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct
<u>1973</u>	CAP												
Long Draw Res.	10519	.112	.128	.128	.126	.129	.134	.000	.000	.000	.000	.000	.000
Chambers Lake	8824	.371	.399	.476	.501	.534	.580	.844	1.00	1.00	.546	.115	.225
No. Poudre #6	9968	.624	.624	.624	.624	.624	.624	.659	.703	.582	.495	.286	.503
Fossil Creek	11100	.652	.765	.759	.791	.843	.927	.797	.935	.892	.573	.658	.658
Tinnath Res.	10070	.612	.774	.774	.774	.808	.928	.910	1.00	.973	.471	.449	.612
Windsor Res.	17689	.659	.680	.708	.734	.791	.888	.781	.697	.847	.466	.493	.500
<u>1974</u>													
No. Poudre #6	9968	.511	.511	.511	.530	.558	.534	.495	.484	.447	.407	.404	.659
Windsor Res.	17689	.550	.573	.607	.629	.646	.776	.720	.857	.421	.417	.236	.504
Tinnath Res.	10070	.715	.715	.715	.741	.830	.836	.887	1.00	.628	.140	0.00	.434
Fossil Creek	11100	.658	.664	.664	.670	.850	.864	.772	.792	.658	.330	.525	.623
Long Draw Res.	10519	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Chambers Lake	8824	.261	.317	.373	.399	.370	4.90	.875	.976	.927	.700	.136	.208
<u>1975</u>													
Long Draw Res.	10519	.018	.018	.018	.018	.018	.018	.062	.993	.993	1.00	.811	.829
Chambers Lake	8824	.257	.293	.369	.369	.401	.440	.297	.962	.962	.281	0.00	.110
No. Poudre #6	9968	.659	.659	.681	.681	.681	.690	.676	.672	.522	.320	.286	.432
Fossil Creek	11100	.676	.685	.595	.595	.700	.617	.374	.857	.687	.353	.056	.079
Tinnath Res.	10070	.662	.662	.662	.662	.662	.662	.436	.678	.569	.152	.271	.273
Windsor Res.	17689	.547	.547	.607	.607	.650	.715	.477	.939	.554	.178	.335	.431

Seaman Reservoir, plus five percent to compensate for channel losses. This result is the gross amount of water available for subsequent diversion in each month from the headwaters of the Poudre River. It is also net of diversions to Poudre Valley Canal and assumes historical operation of high mountain reservoirs not directly modeled.

- iii. For purposes of this study, Horsetooth Reservoir is considered an equalizing reservoir. The reservoir operates on a seasonal basis. In all but a few cases the reservoir only releases water between the first of April and the end of October. Its waters service the entire valley with supplemental irrigation water and also augment the supply of several municipalities, including Fort Collins. To avoid allowing more Horsetooth water to the system than actually is available, the Northern Colorado Water Conservancy District (NCWCD) records were used to delineate only those waters that are delivered to the river and also supplied to the City of Fort Collins. These monthly releases are then summed and entered as inflow to the reservoir in April. The reservoir level is allowed to freely fluctuate except that the storage has to go to zero in October. Evaporation is not deducted from the storage pool due to the fact the adjusted inflow is the net delivery to the City.
- iv. Historical inflows to Long Draw Reservoir and Chambers Lake Reservoir are input monthly.
- v. Additional inflows to certain plains reservoirs are included as a result of ditch transfers that do not originate from diversions on the main stem of the river and non-stream inflows.

Table VI.4 lists the primary inflows to various nodes throughout the system for the calibration period.

6. Net added flow to the river is also calculated. Due to irrigation activity in the valley, there is significant return flow accruing to the Poudre River between Fort Collins and Greeley. Also, tributary inflow, precipitation on the channel, and channel seepage are occurring throughout the year. This net additional inflow to the river can be reasonably estimated. The gaged Poudre River flow at Greeley (confluence with South Platte River), the gaged river flow at Fort Collins, and the monthly diversions and releases between these stations are used to determine the net added flow. Working upstream, diversions and releases to the river are added and subtracted from the gaged record at Greeley. This results in a calculated flow at the Fort Collins gage. Comparing this calculated flow with the observed flow at Fort Collins reveals that in each month the calculated flow at Fort Collins is greater than the observed, as expected. The difference between these values is assumed to be net return flow to the river. Figure VI.1 shows the Fort Collins gaged flow and the net added flow between Fort Collins and Greeley. These monthly values of net added flow are input to the model at node 15. Though the lumping of total return flow at this point is somewhat erroneous, the nature of the aggregated demand for water downstream of the system boundary (as well as other ditches within the system not explicitly included in the model), does not seriously detract from reality.

Table VI.4. Unregulated Inflows (Acre-Feet)

Month	Node 14 Release from Milton Seaman Res.	Node 10 Fort Collins Adjusted Gage Record	Node 4 Horse- tooth Res.	Node 1 Longdraw Res.	Node 3 Chambers Lake Res.
Nov 72	133	3274	0	0	1081
Dec	0	2409	0	150	248
Jan 73	0	2278	0	0	730
Feb	148	2068	0	0	230
Mar	50	2843	114	28	299
Apr	0	4175	66874	53	404
May	3950	92672	0	346	2547
Jun	0	144424	0	0	1584
Jul	184	83659	0	0	0
Aug	1647	26996	0	0	0
Sep	1059	7615	0	0	0
Oct	0	6512	0	0	993
Nov	1879	5576	0	0	345
Dec	154	3719	0	0	493
Jan 74	0	3188	0	0	489
Feb	0	3702	0	0	238
Mar	4	6702	0	0	339
Apr	661	7860	107189	0	461
May	3881	87129	0	0	3396
Jun	400	126667	0	0	1103
Jul	0	54024	0	0	0
Aug	1204	19390	0	0	0
Sep	287	8471	0	0	127
Oct	2208	7298	0	0	630
Nov	28	3715	0	0	434
Dec	170	2106	0	0	319
Jan 75	590	1094	0	0	303
Feb	129	1433	0	0	363
Mar	0	2010	64	0	291
Apr	0	3106	87210	0	343
May	3942	20168	0	1002	449
Jun	0	98256	0	9801	5869
Jul	0	94907	0	0	0
Aug	1449	25328	0	69	0
Sep	1119	10156	0	73	0
Oct	1190	3508	0	194	974

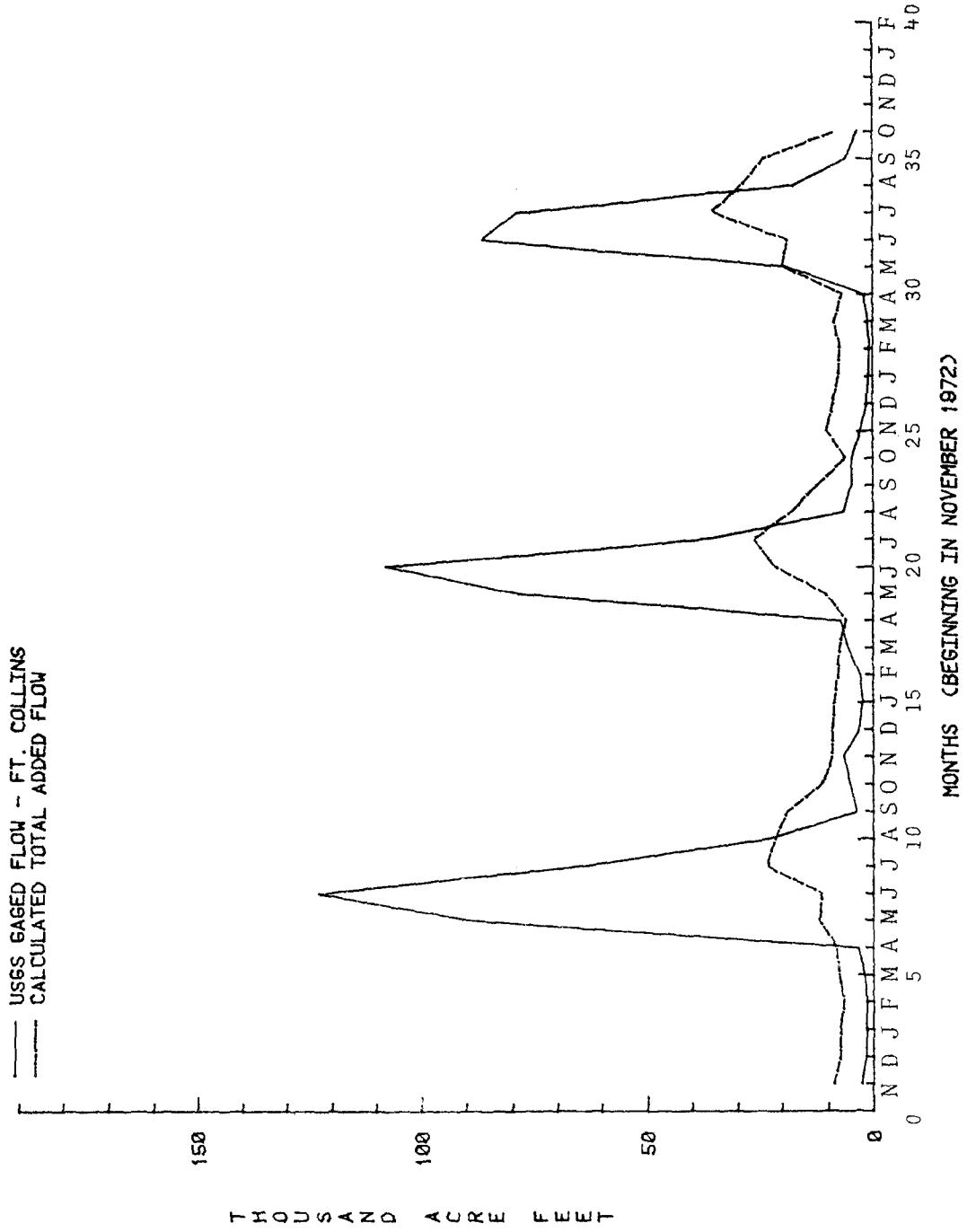


Figure VI.1. Fort Collins gaged flow and net added flow between Fort Collins and Greeley.

7. Determine historical demands:
- i. The demand for raw water by the City of Fort Collins has been discussed previously. Using the aforementioned consumptive loss percentages and a two percent diversion of treated water to West Fort Collins Water District, the resulting estimated losses are specified as model demands. Tables VI.5 through VI.7 display the monthly values for diversions to the Fort Collins treatment plants and associated consumptive losses.
  - ii. The historical river to ditch diversions (including Horsetooth water) as compiled from generated reports from the CWDB are input as demands for the specific canal systems modeled.
  - iii. To insure that the remainder of the system not explicitly modeled is realistically considered, a demand is established at the terminal node which takes into account all ditch diversions not directly analyzed. To do this, the flow normally passing the downstream case study boundary is calculated for the historical period in much the same fashion as the added flow. Beginning with the recorded streamflow of the Greeley gage, canal diversions are added (moving upstream) until the historical flow of the study boundary is calculated. To these monthly values are added the monthly diversions to ditches not directly modeled between the boundary and the Fort Collins stream gage. These total monthly figures are then input as the monthly demand at the terminal node. In this manner, the total historical requirement for river water in this reach is considered (Table VI.8).

Table VI.5. 1973 Demands at Fort Collins (Acre-Feet)

	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Annual
River Diversion to Pipeline	621	704	710	668	708	506	748	1335	1396	1416	1010	920	10,742
Horsetooth					114	280	630	991	569	757	257	90	3,688
TOTAL (Demand at 21)	621	704	710	668	822	786	1378	2326	1965	2173	1267	1010	14,430
2% to West Ft. Collins (Demand at 22)	12	14	14	13	16	16	28	47	39	43	25	20	287
Available at Ft. Collins	609	690	696	655	806	770	1350	2279	1926	2130	1242	990	14,143
% Consumptive Loss	1.6	1.4	1.1	1.2	1.6	42.9	60.7	55.0	46.0	46.5	35.1	21.8	
Consumptive Loss (Demand at 23)	10	10	8	8	13	330	819	1253	886	990	436	216	4,979



Table VI.6. 1974 Demands at Fort Collins (Acre-Feet)

	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Annual
River Diversion to Pipeline	826	796	636	586	587	877	1447	1611	1693	1731	1279	1184	13,353
Horsetooth	36	18	3	3	6	22	623	686	914	669	293	6	3,279
TOTAL (Demand at 21)	862	814	639	589	693	899	2070	2297	2607	2400	1572	1190	16,632
2% to West Ft. Collins (Demand at 22)	17	16	13	12	14	18	41	46	52	48	31	24	332
Available at Ft. Collins	845	798	626	577	679	881	2029	2251	2255	2352	1541	1166	16,300
% Consumptive Loss	1.6	1.4	1.1	1.2	1.6	42.9	60.7	55.0	46.0	46.5	35.1	21.8	
Consumptive Loss (Demand at 23)	14	11	7	7	11	379	1231	1238	1176	1095	542	254	5,965

Table VI.7. 1975 Demands at Fort Collins (Acre-Feet)

	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Annual
River Diversion to Pipeline	776	796	816	750	748	834	1105	966	1196	1178	1034	1028	11,227
	50		6	4	16	26	69			238	109	178	587
							10		65	174	91		340
TOTAL	826	796	822	754	764	858	1184	966	1261	1352	1472	1206	12,263
Horsetooth					64	2	332	528	1077	738	483	173	3,397
TOTAL (Demand at 21)	826	796	822	754	828	860	1516	1494	2338	2090	1955	1379	15,660
2% to West Ft. Collins (Demand at 22)	17	16	16	15	17	17	30	30	47	42	39	28	314
Available at Ft. Collins	809	780	806	739	811	843	1486	1464	2291	2048	1916	1351	15,346
% Consumptive Loss	1.6	1.4	1.1	1.2	1.6	42.9	60.7	55.0	46.0	46.5	35.1	21.8	
Consumptive Loss (Demand at 23)	13	11	9	9	13	362	902	805	1054	952	672	294	5,096

Table VI.8. Calculation of Adjusted Demand at Terminal Node - 1974 (Acre-Feet)

Calculated Flow at Terminal Node	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Annual
	13350	10380	9420	9060	7360	7476	13528	41842	20718	16807	8667	8568	167,176
Ditches Not in Analysis													
Boxelder							1744	1378	2265	1719	659	121	7,886
Chaffee							105	141	125	117			488
Coy						14	283	303	376	297	248	46	1,567
Arthur							1340	1169	1881	729	86		5,205
Larimer Co.#2							3429	3424	1307	1650	555		10,365
New Mercer							2482	1820	1627	1077	240		7,246
Little Cache													
La Poudre		1071	921	832	1154	719	3619	3289	3859	1184	545	89	17,282
Jackson							2170	1934	1632	988	376		7,100
Larimer Co. Canal	362				319	2109	20608	18970	23170	16490	4496	3838	90,362
Pleasant Valley and Lake							4536	4617	3357	3046	2481	818	18,857
Greeley Pipeline	760	719	709	630	739	744	251		1468	1702	1462	1303	10,487
TOTAL	14472	12170	11050	10522	9572	11062	54095	78889	61785	45806	19815	14783	344,021
Seeley Lake Release		125		59		166				311		82	743
Total Adjusted Demand at Terminal Node	14472	12045	11050	10463	9572	10896	54095	78889	61785	45495	19815	14701	343,278

## C.2 Results

The aggregate demand is given the lowest priority among demand nodes to insure that all shortages occur at the terminal node. The water requirement at this node is a conservative estimate of the actual aggregate due to the inclusion of reservoir to reservoir transfers of water that are impossible to separate from the data. Shortages which occur at the boundary should be limited to the non-irrigation months of the year when such transfers take place. This condition is exactly the response one finds from model runs with these data.

The criteria for acceptable model calibration was met after successive adjustment of model priorities. The final priorities or ranks are presented in Table VI.9. Reservoir storages calculated by the model correspond surprisingly well with observed data. In every case (except Windsor Reservoir) the calculated storage identically matches observed, or varies by a few acre-feet. The model calculates storage volumes for Windsor Reservoir in 1975 which are below observed, except for May when the calculated equals observed. This significant deviation may be attributed to an underestimate of either non-stream inflow to Windsor Reservoir or failure to consider transfers within the ditch system itself to the reservoir, or both.

The results of the model calibration are presented in Figures VI.2 through VI.7. Clearly, good correlation between calculated and observed flows at the Fort Collins gage exists. Deviation between the calculated water available at the case study boundary and the historical requirement are only a small percentage of the total requirement, and occur in off-season months. All other demands throughout the system were totally satisfied.

Table VI.9. Final Rankings for Rawhide Project Calibration\*

	Name	Network Node No.	1973	1974	1975
Demand	N. Poudre No. 6 Res.	5	10	10	10
	Munroe Gravity Canal	12	10	10	10
	Larimer & Weld Canal	15	10	28	10
	Fort Collins Pipeline	21	10	40	10
	West Fort Collins	22	10	42	10
	Fort Collins (consumptive loss)	23	10	44	10
	Lake Canal	31	10	48	10
	New Cache la Poudre Canal	32	10	50	10
	System Boundary	35	18	55	15
Storage	Long Draw Res.	1	13	500	13
	Joe Wright Res.	2	500	500	500
	Chambers Lake Res.	3	3	3	3
	Horsetooth Res.	4	50	60	50
	N. Poudre No. 6 Res.	5	1	30	1
	Fossil Creek Res.	6	5	5	5
	Timnath Res.	7	13	3	13
	Windsor Res.	8	17	10	20
	Cooling Pond	9	100	100	100

\*Rankings are translated into *pseudo-costs* of moving a unit of water from storage to demand satisfaction. For example, the rank of 1 in 1973 for holding water in N. Poudre Reservoir No. 6 takes precedence over all other storages and demands in 1973.

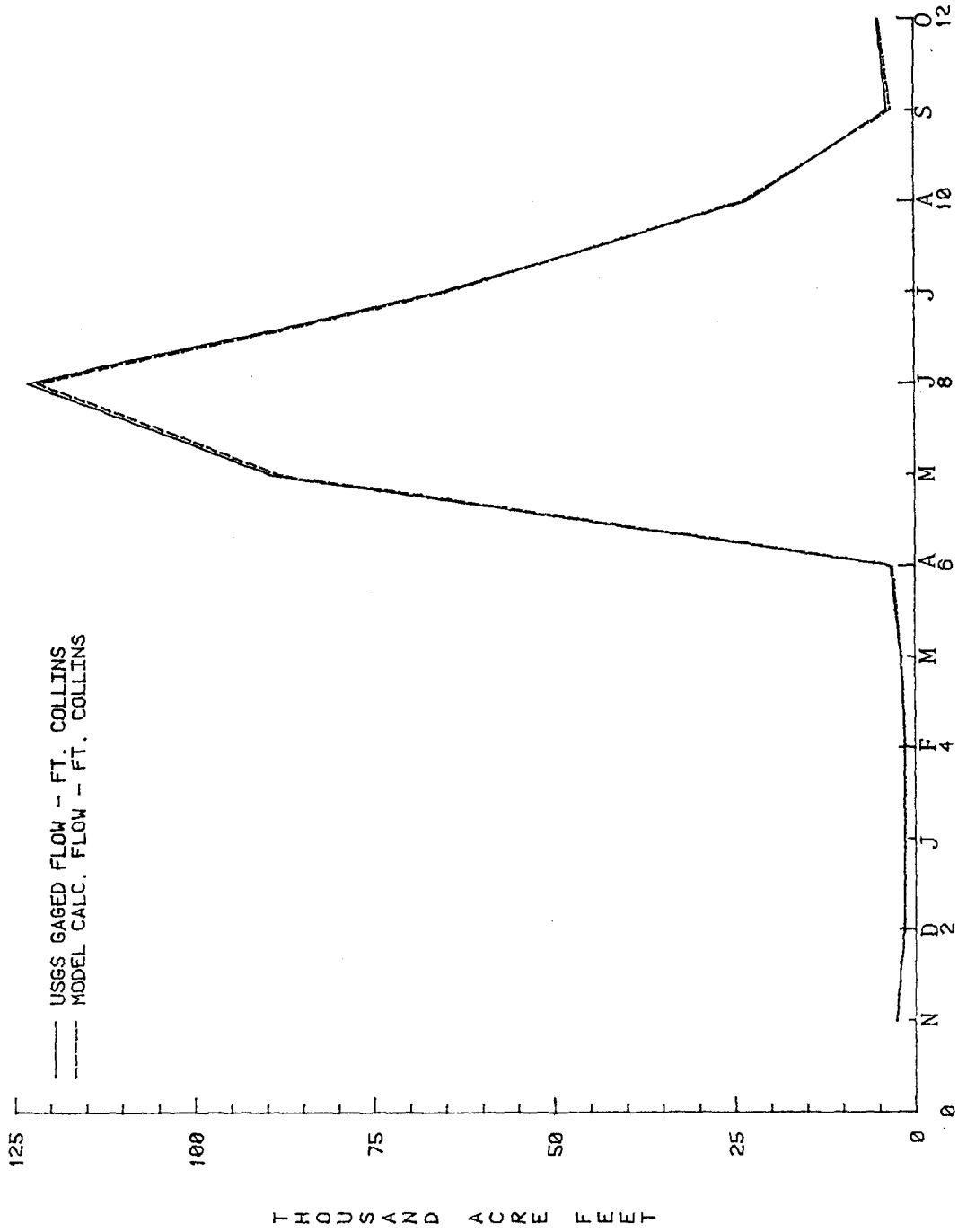


Figure VI.2. Calibration for Rawhide Project irrigation year 1973.

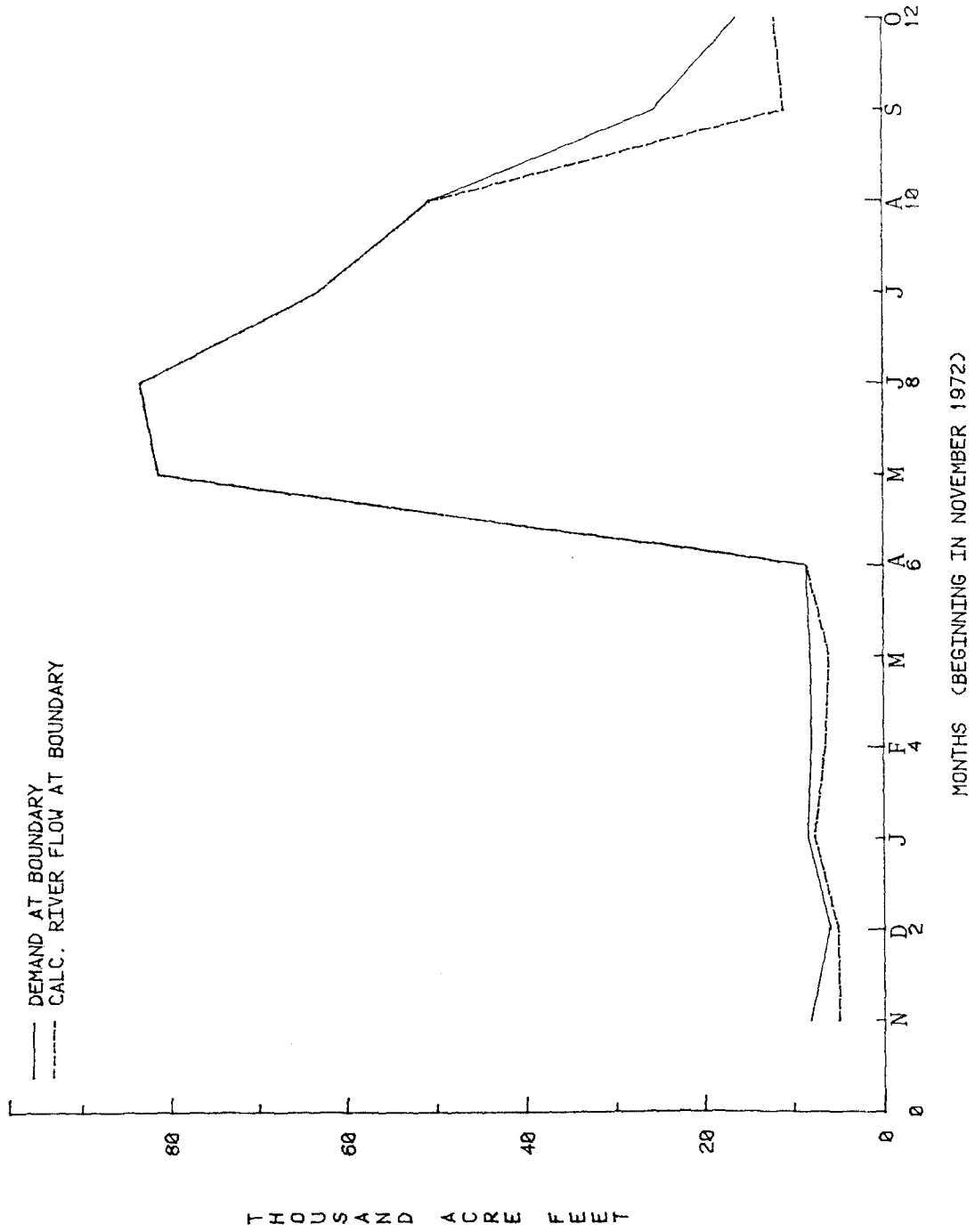


Figure VI.3. Calibration for Rawhide Project irrigation year 1973.

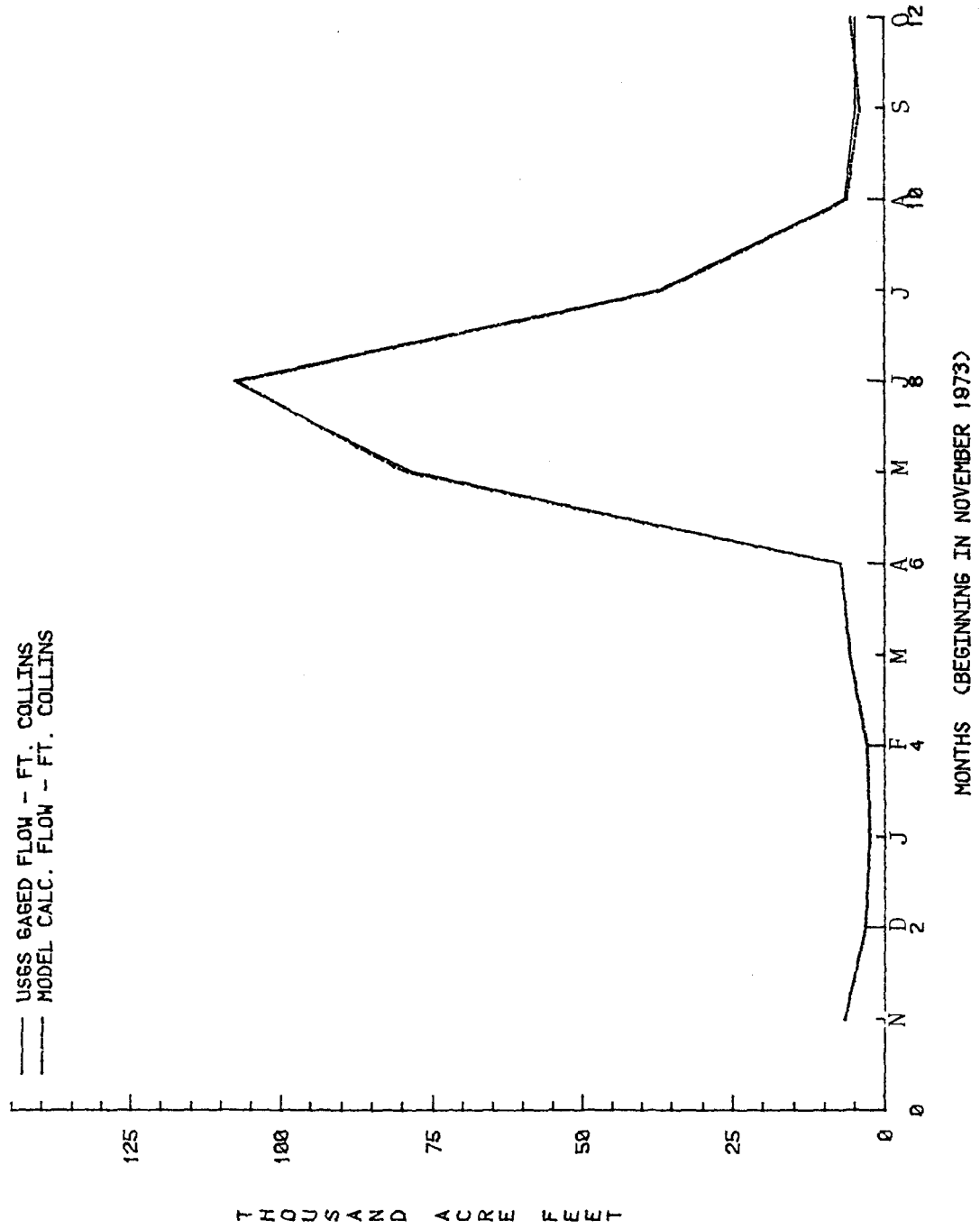
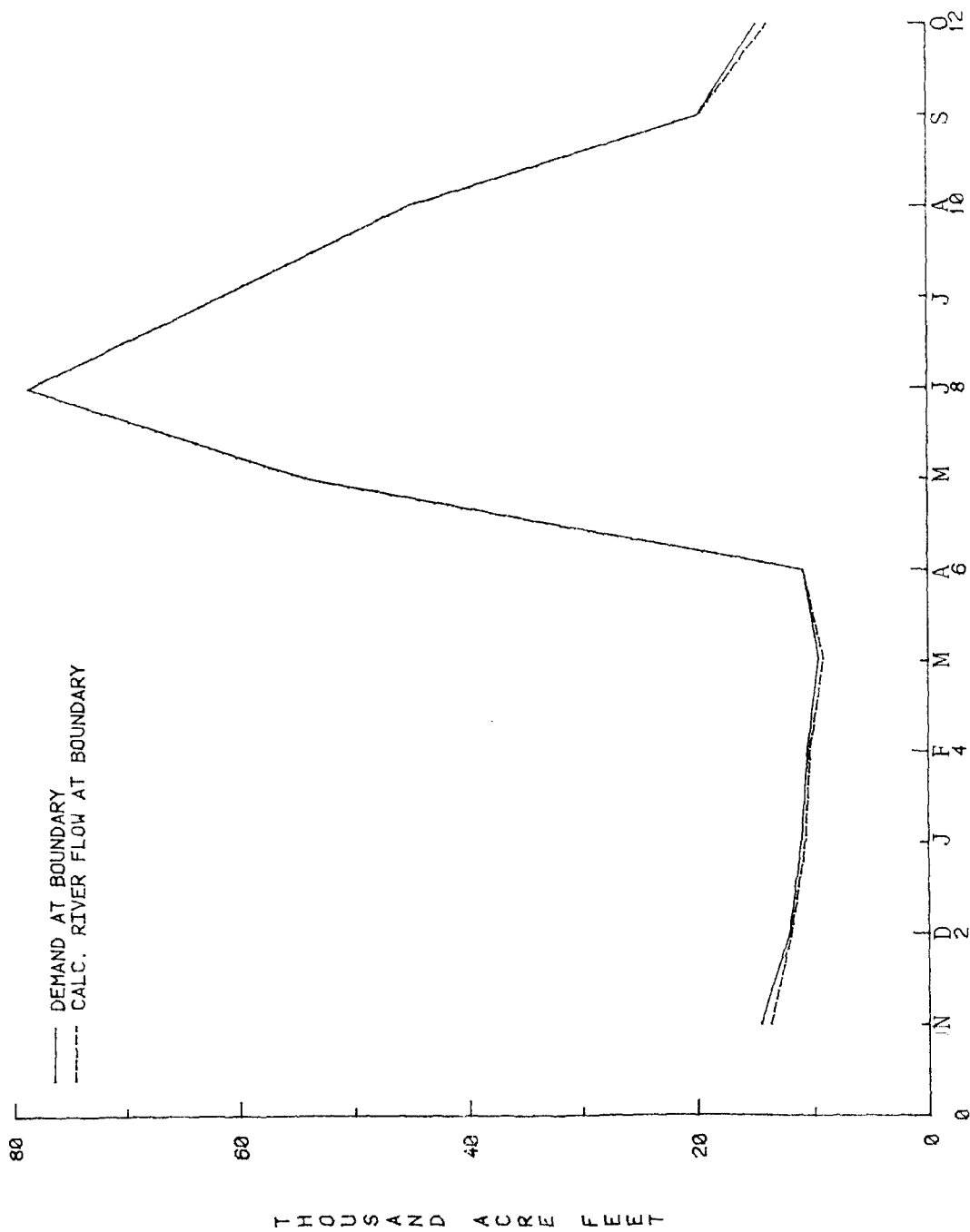


Figure VI.4. Calibration for Rawhide Project irrigation year 1974.





MONTHS (BEGINNING IN NOVEMBER 1973)  
Figure VI.5. Calibration for Rawhide Project irrigation year 1974.

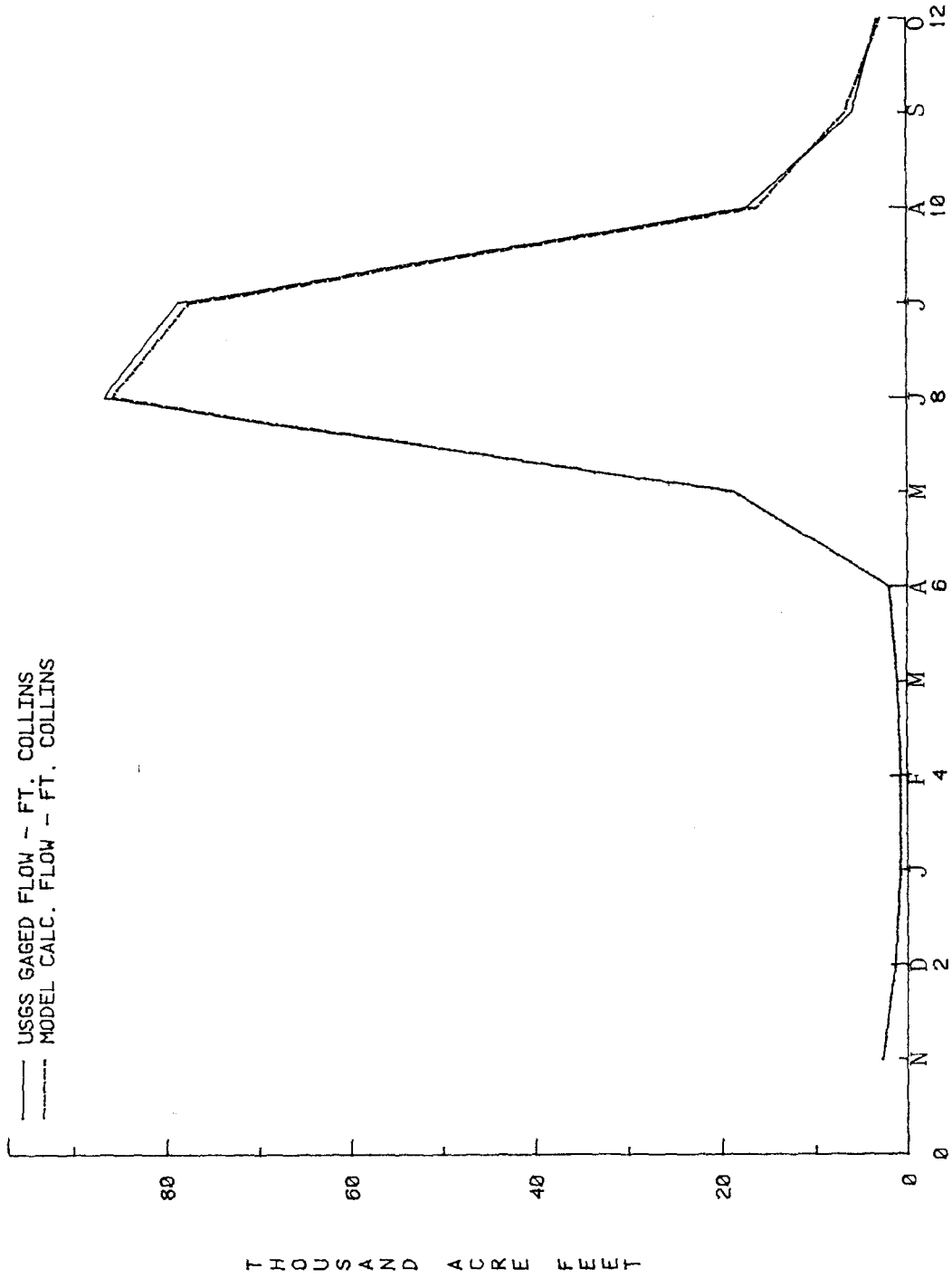


Figure VI.6. Calibration for Rawhide Project irrigation year 1975.

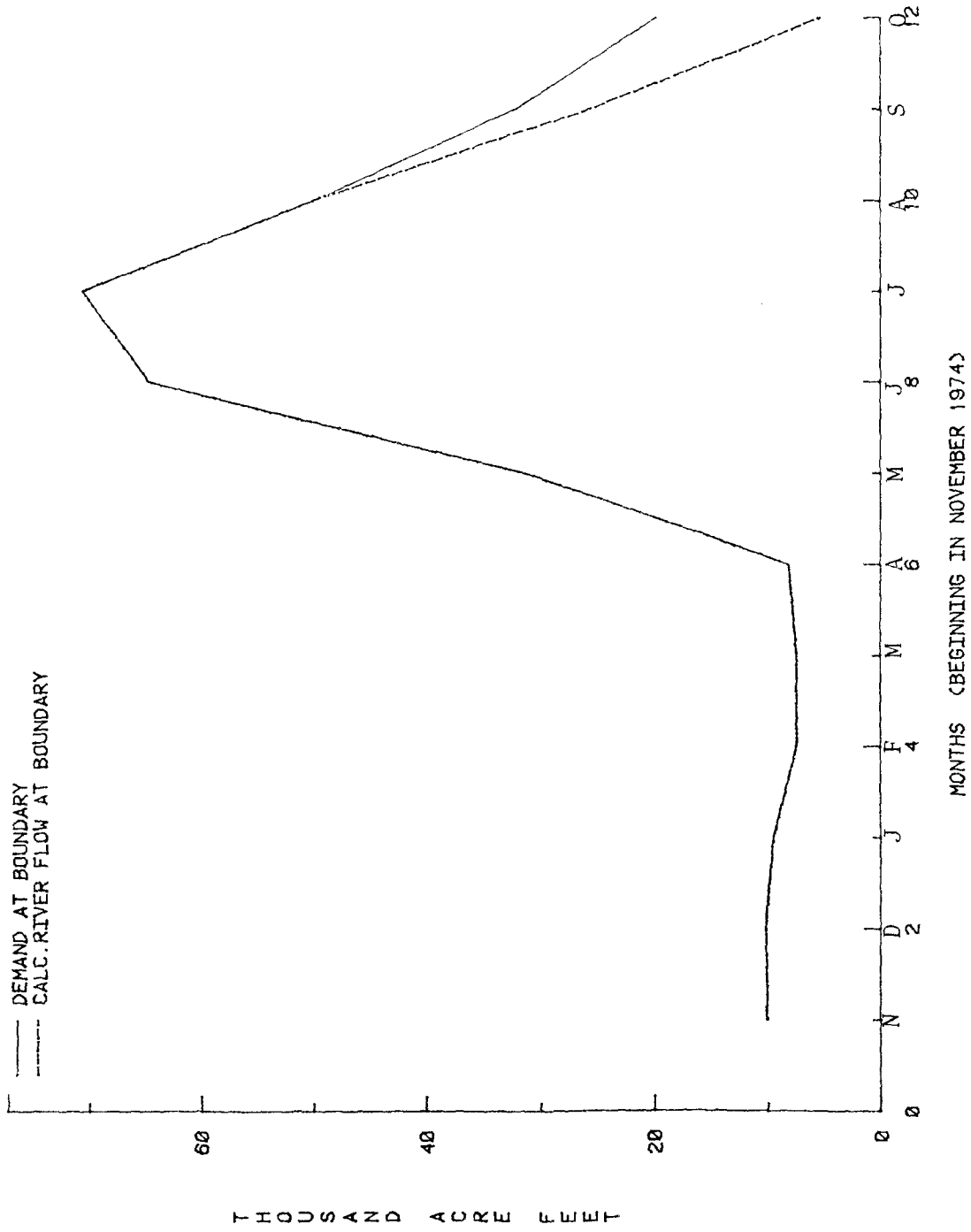


Figure VI.7. Calibration for Rawhide Project irrigation year 1975.

To summarize, the calibration of MODSIM for the Rawhide Project did include the use of some historical data. Historical return flows accruing to the river were input, thus eliminating groundwater considerations from the calibration exercise. As a result, only surface water conditions were attempted to be duplicated during calibration. The  $DEM_{i,t}$  and  $OPRP_{i,t}$  of Equations III.8 and III.9 were adjusted until no better fit of calculated storage volumes, gaged river flows, and demand satisfaction with the historically observed values could be gained.

### C.3 Return flow calculation option

For purposes of this case study, actual monthly return flows (net added flows) are calculated and input to the model. However, as discussed in Chapter III, return flows may be calculated via a multiple linear regression equation whose coefficients are MODSIM input. This section demonstrates the use of this option.

To begin, both a multi-lag autocorrelation of 18 years of monthly return flow values and a multi-lag cross-correlation of ditch diversions with return flows for the same 18 years is performed to determine the significant number of monthly lags to be included in the regression equation. For both correlation exercises a 95 percent confidence interval is used to test for significance of the correlation coefficients. The 18 years of return flow data are calculated in exactly the same manner as the net added flow discussed in the previous section.

The results of the correlation exercises are presented in Tables VI.10 and VI.11.

Table VI.10. Results of Autocorrelation of 18 Years of Monthly Return Flows at 95% Confidence Interval

Lag (K)	Conf. Int. (1)	Correlation R(K)	Conf. Int. (2)
1	- .133	.688	.133
2	- .133	.383	.133
3	- .133	.028	.133

Table VI.11. Results of Cross-Correlation of 18 years of Monthly Ditch Diversions with Return Flows at 95% Confidence Interval

Lag (K)	Conf. Int. (1)	Correlation R(K)	Conf. Int. (2)
0	- .133	.776	.133
1	- .133	.728	.133
2	- .133	.443	.133
3	- .133	.057	.133

From these two tables, the appropriate number of monthly lags which need to be included in the regression equation is determined to be two for both return flows and ditch diversions. Beyond two months there is insignificant (at 95% confidence interval) correlation to warrant expansion of the regression equation to include additional terms.

The confidence interval is used to test for significance of correlation coefficients in the following manner. The hypothesis is formulated which states that all return flow and ditch diversion values are completely independent from all others. The confidence interval (for this case 95%) is the region of acceptance of this hypothesis, i.e., if correlation coefficient  $R(K)$  for lag  $K$  resides within the interval (-.133 to .133) then the hypothesis is accepted and  $R(K)$  is assumed not significantly different from zero. However, if  $R(K)$

resides beyond the confidence interval, then the hypothesis is rejected and a certain dependence according to lag K is assumed to exist among the values.

Once the appropriate number of monthly lags have been determined, a regression analysis can be performed. For this study, the multiple linear regression equation has the form:

$$\hat{R}(t) = a_1 + a_2D(t) + a_3D(t-1) + a_4D(t-2) + a_5\hat{R}(t-1) + a_6\hat{R}(t-2) \quad (\text{VI.1})$$

where:

$\hat{R}(t)$  = dependent variable: return flow for month t

$D(t)$  = independent variable: ditch diversion for month t

$D(t-1)$  = independent variable: ditch diversion for month t-1

$D(t-2)$  = independent variable: ditch diversion for month t-2

$\hat{R}(t-1)$  = independent variable: estimated return flow calculated for month t-1

$\hat{R}(t-2)$  = independent variable: estimated return flow calculated for month t-2

$a_1, a_2, a_3, \dots, a_6$  = regression coefficients.

The same 18 year period used for the correlation coefficients determination is used to calculate the regression coefficients,  $a_i$ . The values of the  $a_i$  are listed in Table VI.12.

Table VI.12. Regression Coefficients for Return Flow Equation

Coefficient	Value
$a_1$	2427.0
$a_2$	0.072633
$a_3$	0.0039629
$a_4$	- 0.024521
$a_5$	0.65021
$a_6$	- 0.031957

These coefficients are used to predict return flows for the calibration period 1973-1975. The results are graphically displayed in Figure VI.8. Although the estimated values and the actual calculated values of return flows differ widely in 1975, based on the large values for ditch diversions and return flows for 1975, in comparison with mean monthly values for the 18 years, 1975 is considered an atypical year. However, the return flows calculated using the regression equation closely conform to the mean monthly values and the overall trends are consistent with both the mean and the three-year period return flows.

For extended planning studies, in which the groundwater basin morphology, water use distributions, and general river basin physiology (e.g. lining of unlined canals) are not subject to a significant level of change, such as the Rawhide Project, one would expect and perhaps

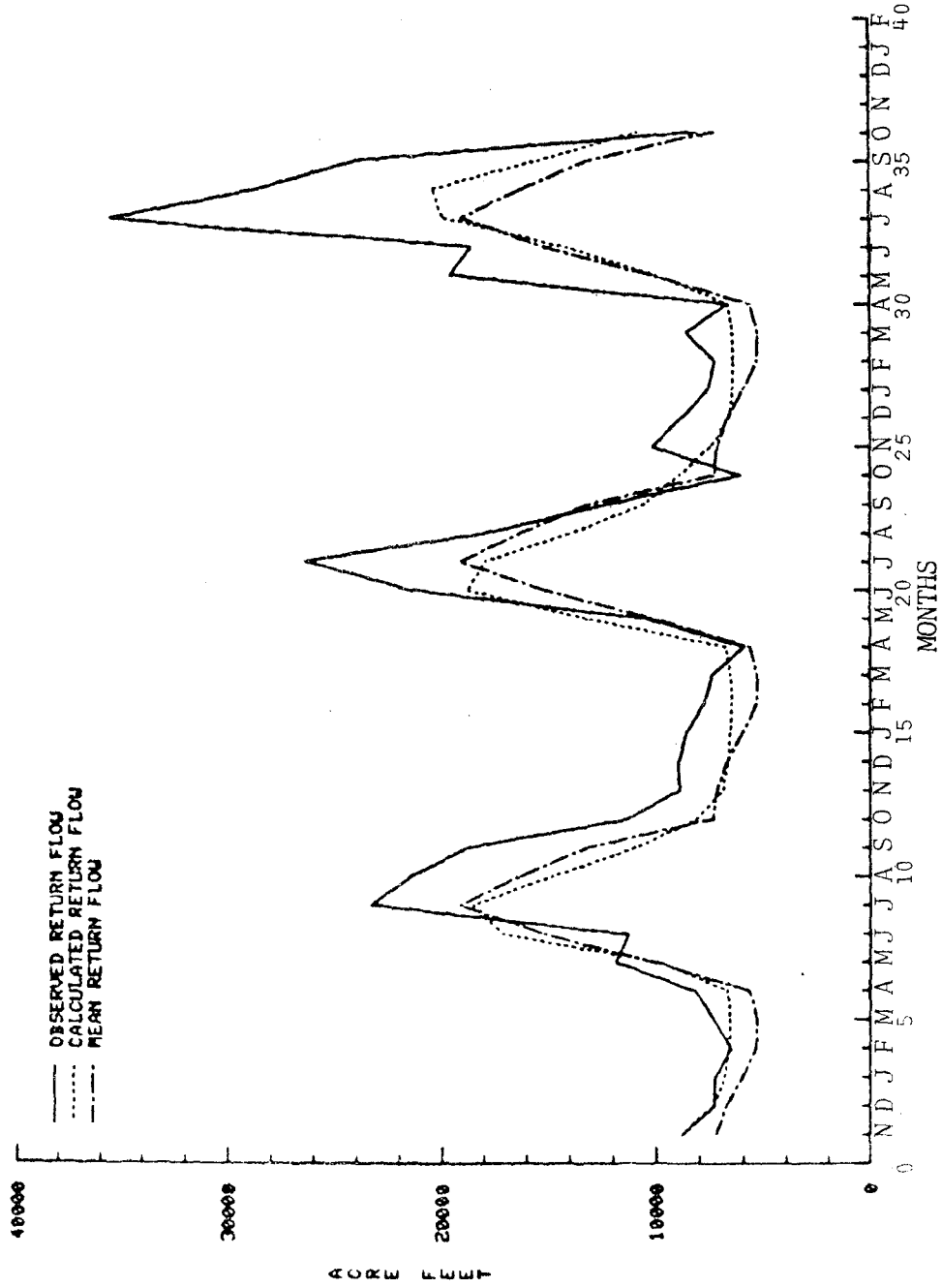


Figure VI.8. Comparison of calculated return flows with observed and mean return flows.



require that return flows fluctuate about the long term mean. This may not be true for short period, real time, operational studies, but for planning studies where one endeavors to determine most probable long range system behavior, based on operational guidelines, such is the case.

It must be noted that the above exercise is conducted off-line. The regression coefficients along with the appropriate monthly lag are input to MODSIM with information concerning the number of nodal demands contributing to return flow and the node to which the return flow accrues. MODSIM constructs the regression equation and iterates over the amount of demand satisfaction for each month, incorporating the return flows in the analysis as specified by the user.

CHAPTER VII  
MANAGEMENT STUDIES

This chapter presents the method of analysis of the proposed water policy changes involved in each of the case studies outlined in Chapter V. The results produced by MODSIM are reported and then the implications of these results are discussed. Since both case studies represent *real world* problems confronting Colorado decision makers, the conclusions drawn from these studies and the associated impacts of these conclusions on the Cache la Poudre River system are important, and explained in detail.

A. Case Study #1

A.1 Method of analysis

The management strategy developed for this case study centers around the creation of a recreational reservoir out of Barnes Meadow and a recreational reservoir out of Twin Lake. As previously mentioned, these two reservoirs are considered to have the highest recreation potential of the five Greeley high mountain reservoirs. The management of these reservoirs with recreation included in a multipurpose framework is in marked contrast to the traditional operating policy demonstrated during the calibration phase.

The same simulation period used for model calibration is also used to perform the management study. Irrigation years 1973-75 are

deemed acceptable for the analysis since they do represent a wet to dry cycle in the basin and complete information concerning the decomposed system is available. Also, during these years the high mountain reservoirs were emptied at the end of each year which is in conflict with stated management objectives.

The goal of this management study is to determine *what if*, for the three years in question, the high mountain reservoirs were operated in such a fashion that would provide for suitable water related recreation. The desired monthly storage levels for all five reservoirs are set at the maximum capacity of each reservoir. Desired storage levels for the remaining non-recreational reservoirs are set at zero for each month, thereby allowing these storage levels to freely fluctuate, based on the operation of the five high mountain reservoirs. The priorities assigned to each reservoir reflect the ordered preference of meeting the new management operating rules. Table VII.1 lists all the reservoirs and their corresponding priorities. Determination of these priority factors requires successive approximation. A set of initial priorities are selected. MODSIM computes storage levels based on these values. These storage levels are then compared to the desired levels for recreation enhancement, and the priority factors adjusted appropriately. It must also be remembered that throughout this analysis the priority established on demands is significantly higher than any reservoir storage priority to insure satisfaction of the demands for reservoir water.

It can be seen from these priorities that Barnes Meadow and Twin Lake reservoirs are given equally the highest consideration for storage maintenance, followed in order by Peterson, Commanche, and Big Beaver

Table VII.1. Storage Preferences for High Mountain Reservoir Management Analysis [ $OPRP_{i,t}$ ]

Reservoir (i)	Priority Factors*		
	1972-1973	1973-1974	1974-1975
Peterson	50	50	50
Barnes Meadow	40	40	40
Big Beaver	80	80	80
Commanche	60	60	60
Twin Lake	40	40	40
Worster	75	75	75
Halligan	85	85	85
Park Creek	90	90	90
North Poudre #15	115	115	115
Milton Seaman	200	200	200
Aggregate	150	150	150

\*A lower value is interpreted as a higher priority.

reservoirs. Priorities for the remaining non-recreational reservoirs reflect a desire to maintain water as high as possible in the system for added flexibility.

#### A.2 Results of analysis

Figures VII.1 thru VII.8 graphically display the results of this management analysis. Both the historical and the calculated monthly ending storage values are plotted over the 36 month simulation period. Keeping in mind that the same demand for reservoir water is met in each instance, and based on admittedly conservative evaporation rates, the alternative management strategy is clearly *hydrologically* viable. Upon initial filling, Barnes Meadow and Twin Lake reservoirs maintain near capacity storage levels throughout the simulation period, as expected. Also, Peterson Reservoir, which has the next greatest recreation potential (reflected by its priority in relation to Barnes Meadow and Twin Lake reservoirs) remains filled near capacity. Commanche and Big Beaver reservoirs are drawn empty in late 1975, which is acceptable. The remainder of the reservoirs fluctuate between zero storage and their maximum capacity as dictated by the demand pattern.

Carry-over storage at the end of the three-year period should be reasonably consistent with that calculated during calibration. A value of 6053 acre-feet of total carry-over storage was obtained from MODSIM calibration. This compares to a value of 4709 acre-feet of total carry-over storage for the new management scheme. A difference is expected due to changes in the distribution of the carry-over storage and variations in channel losses between calibration and management study results.

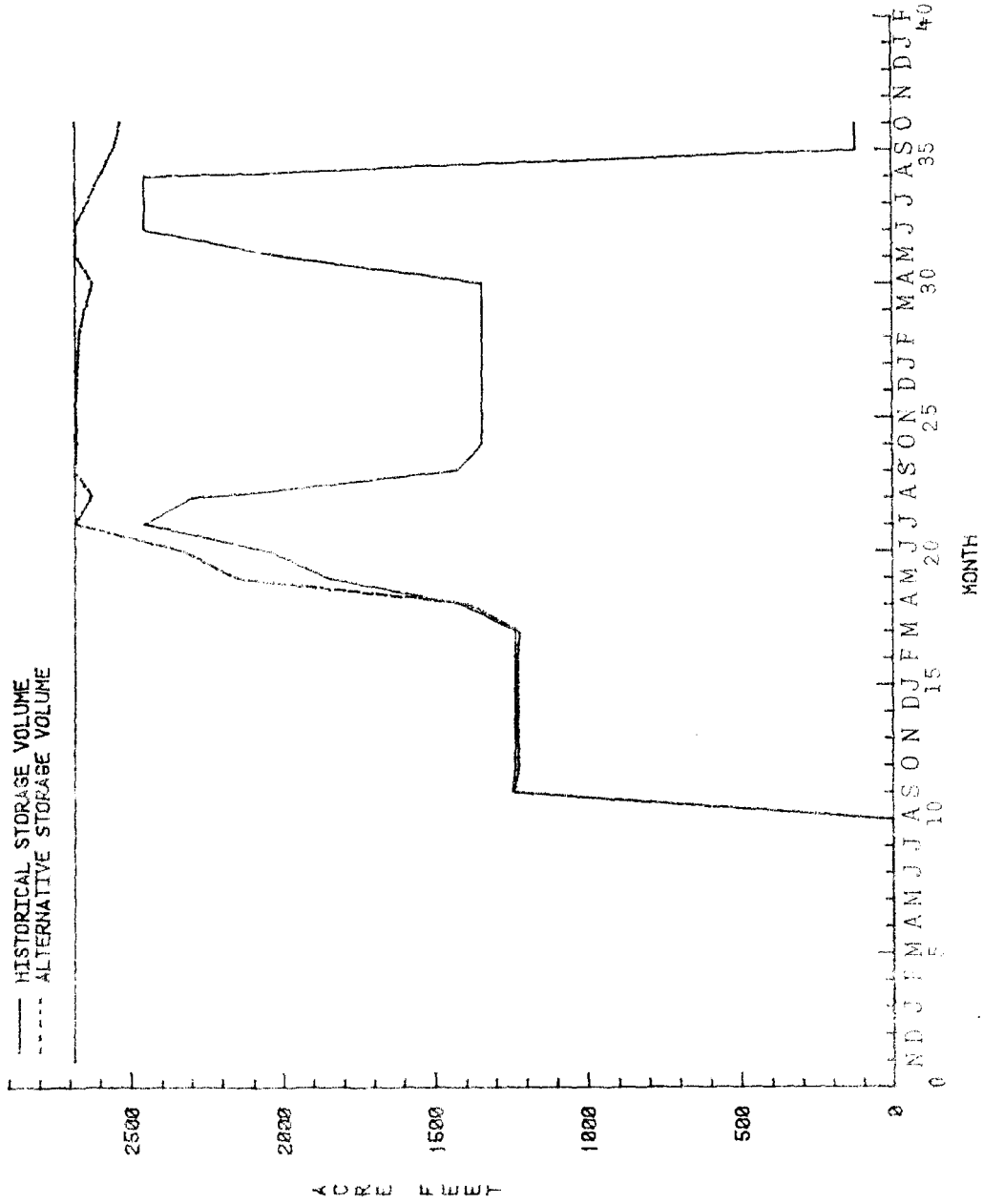


Figure VII.1. Barnes Meadow Reservoir.

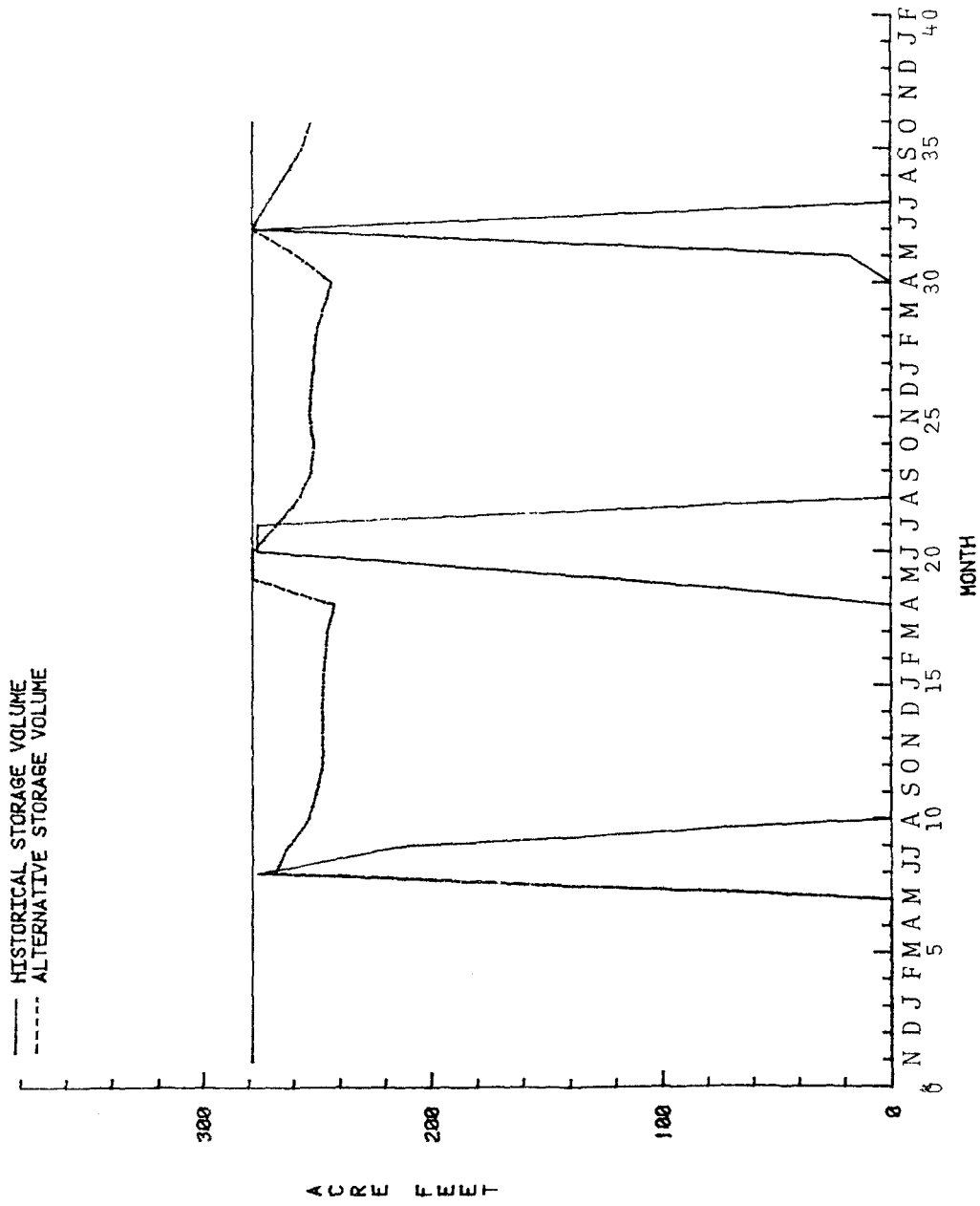


Figure VII.2. Twin Lake Reservoir.

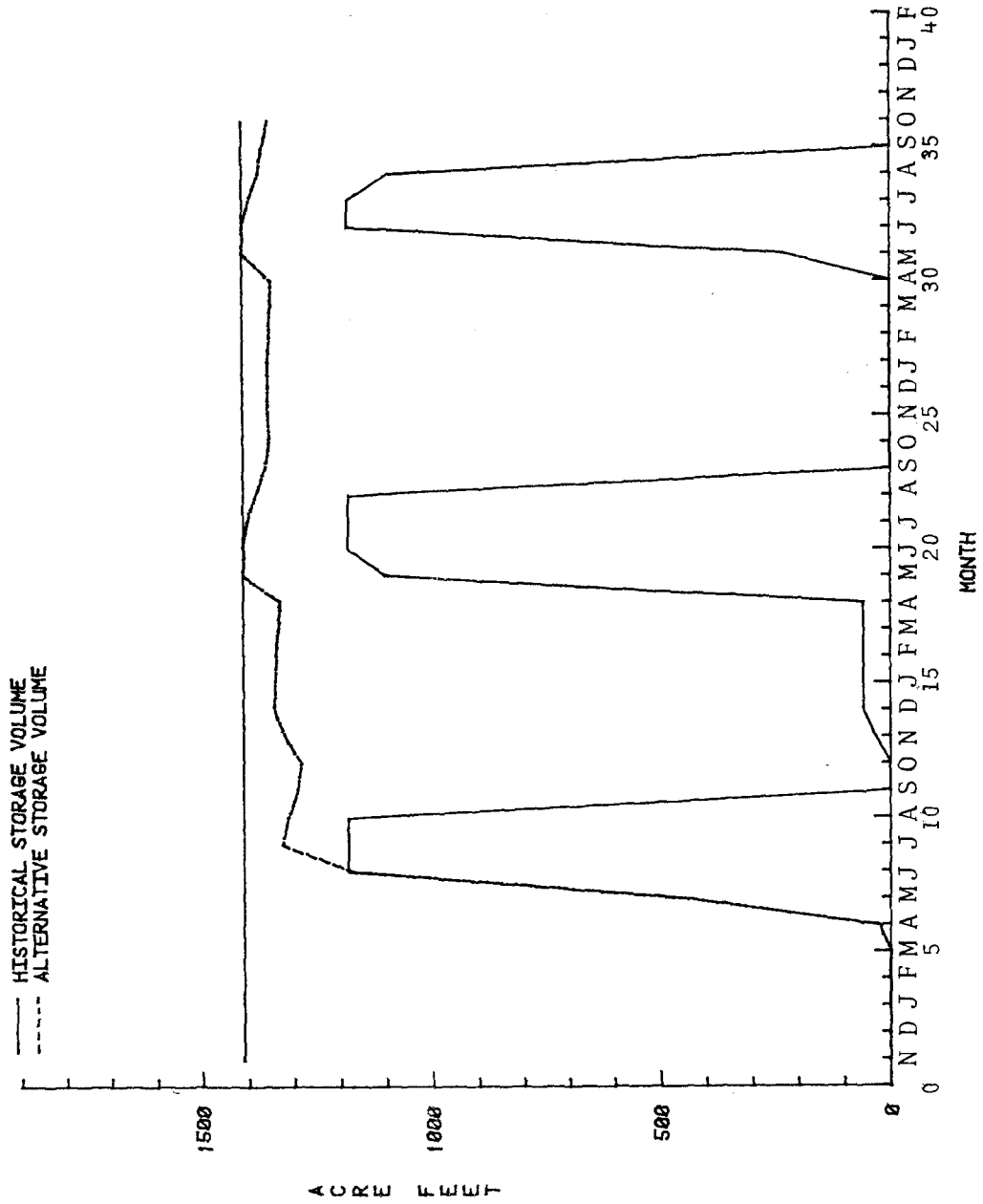


Figure VII.3. Peterson Lake Reservoir.



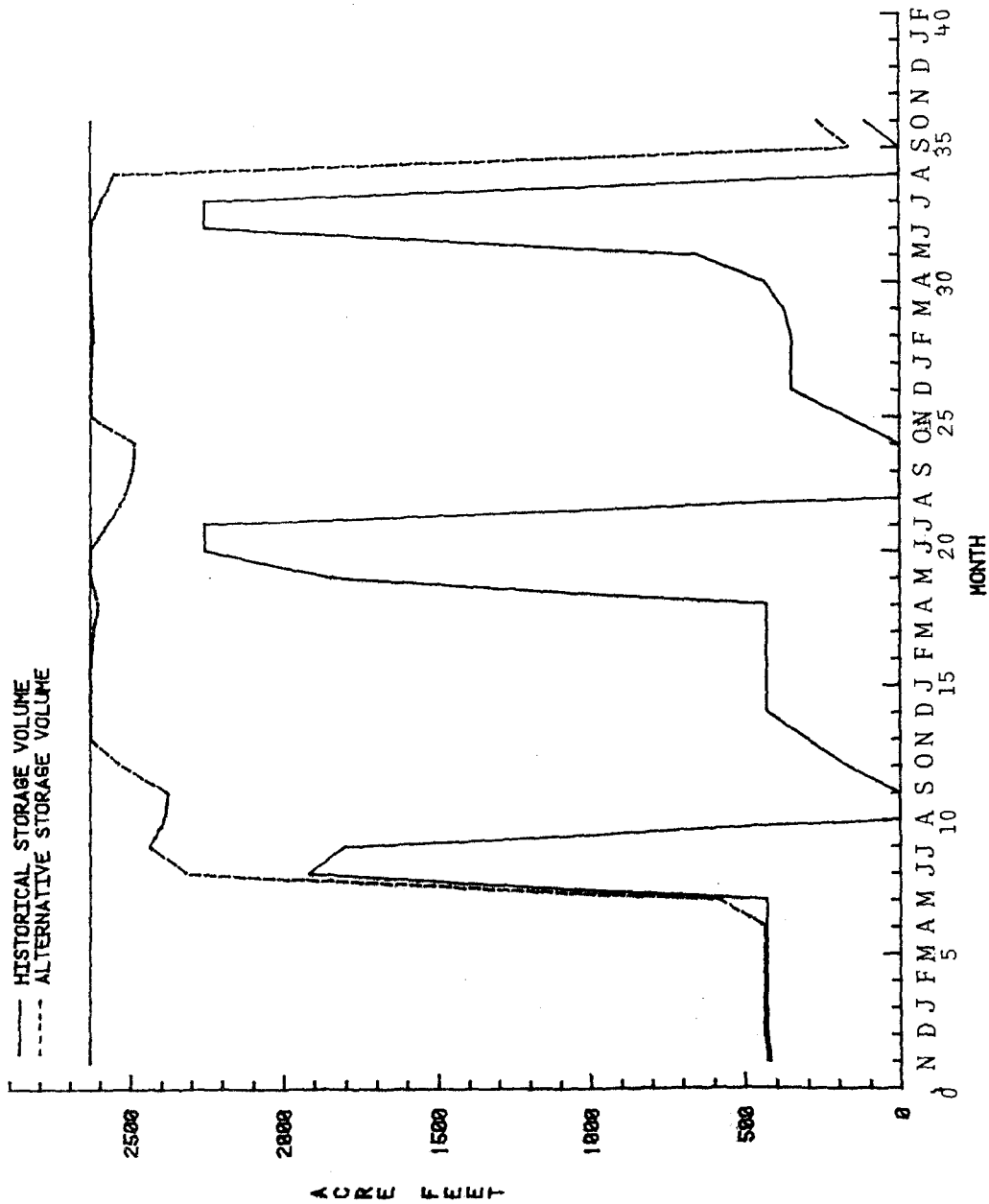


Figure VII.4. Commanche Reservoir.

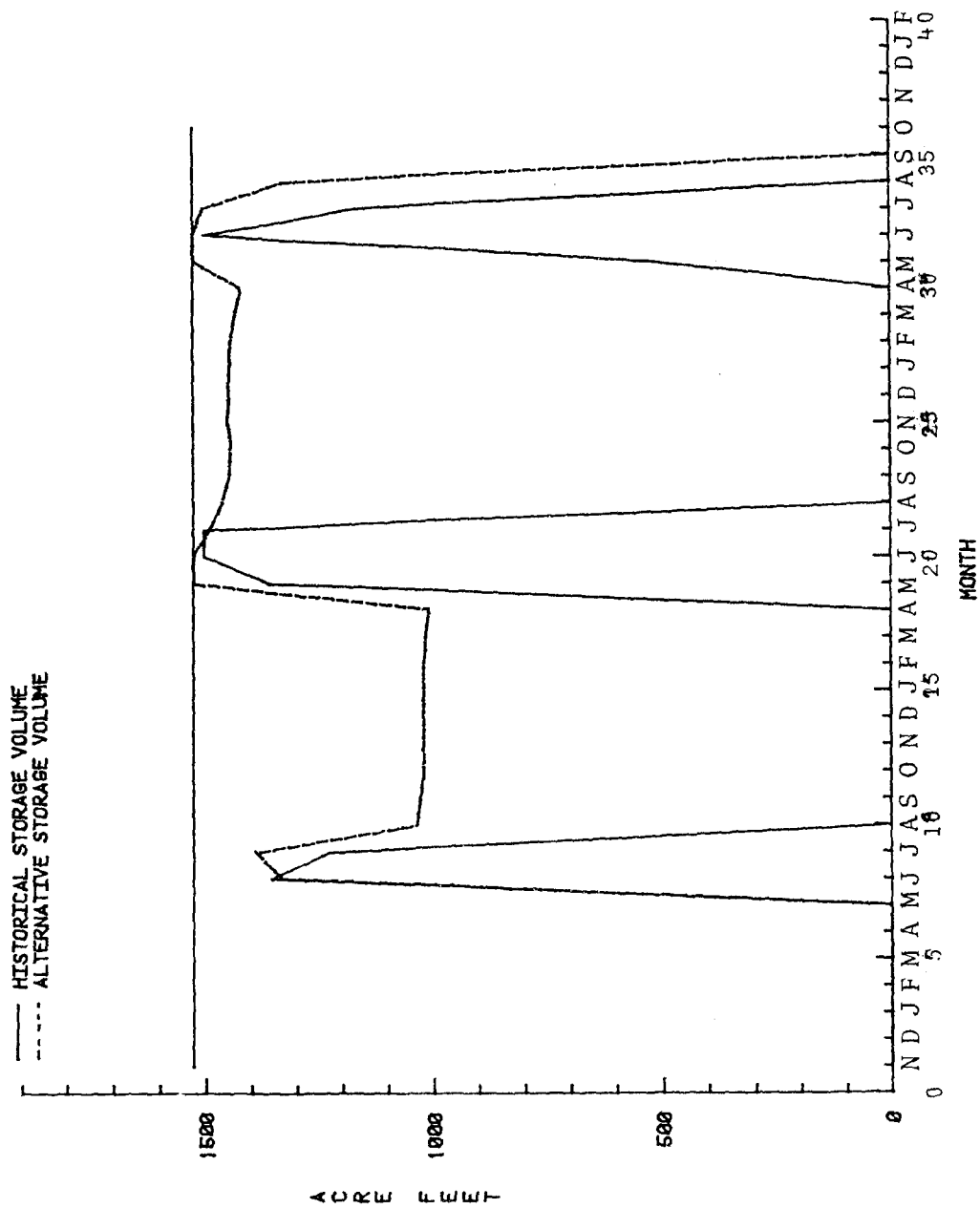


Figure VII.5. Big Beaver Reservoir.

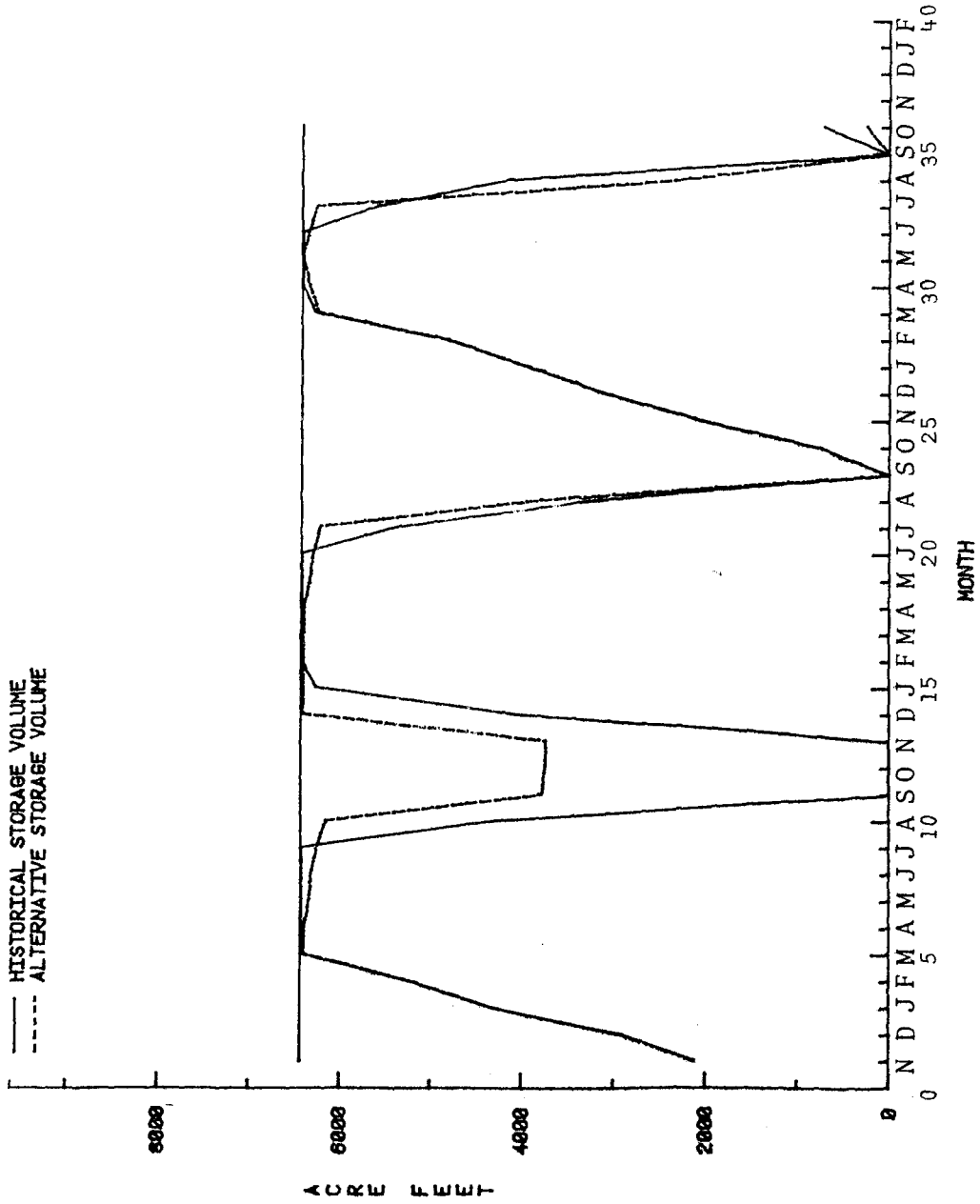


Figure VII.6. Halligan Reservoir.

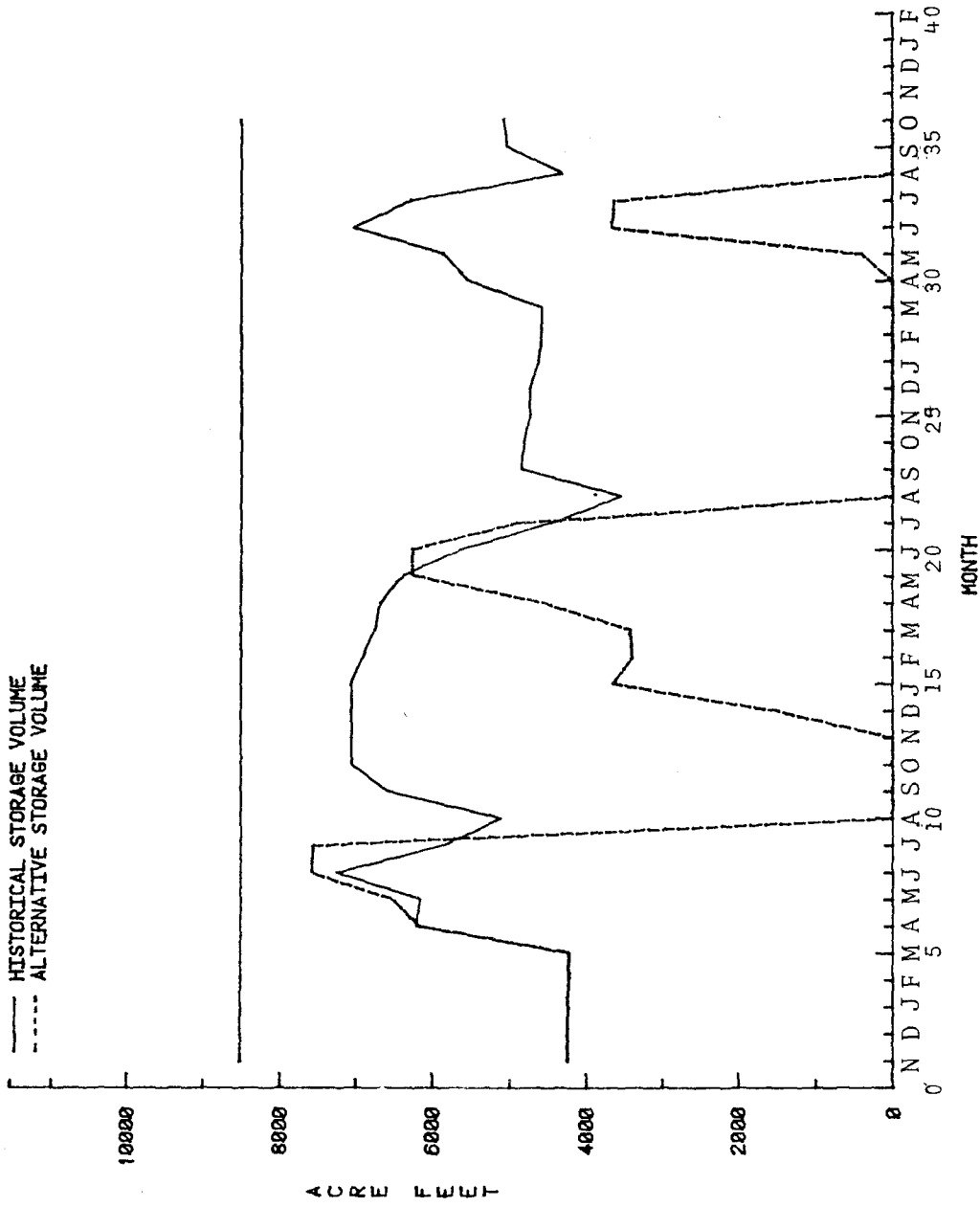


Figure VII.7. Park Creek Reservoir.

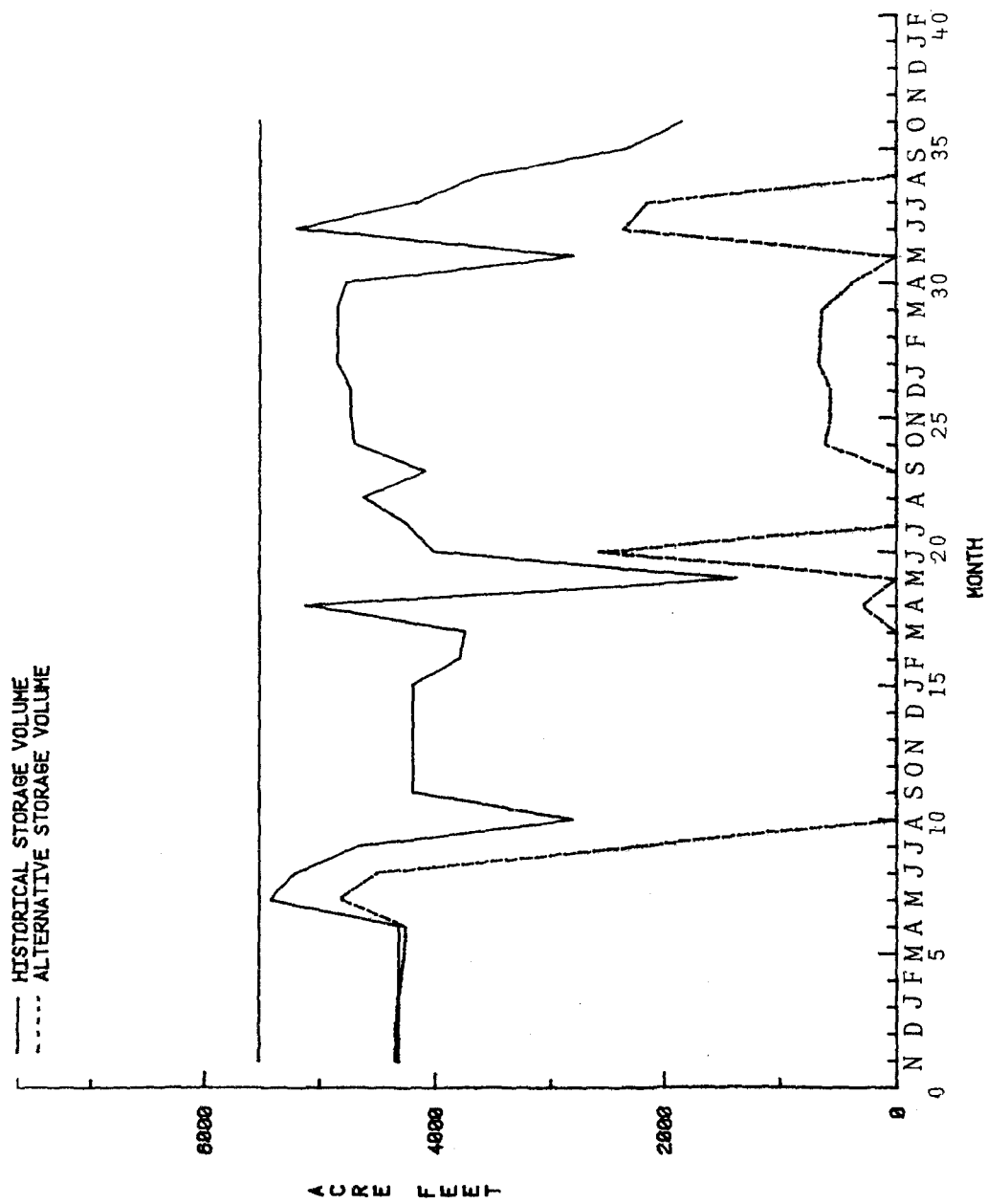


Figure VII.8. North Poudre Reservoir #15.

Consequently, a difference of 1344 acre-feet is not considered significant when the entire storage capacity of the subsystem is over 30,000 acre-feet.

### A.3 Discussion of results

It is clear from Figures VII.1 thru VII.8 that the proposed management strategy simply specifies a shifting of stored water from reservoirs not conducive to recreation to those high country reservoirs with greater recreation potential. Large conservation pool levels are able to be maintained in three out of five high country reservoirs. Commanche Reservoir, however, must be emptied along with Big Beaver Reservoir which has no recreation potential whatsoever. For the three-year period considered in this study, it is evident that enough water is available in the subsystem to maintain storage levels in certain selected high country reservoirs, while still meeting the historical demand for water from all the reservoirs under investigation. This is partly due to the large difference in storage volume between the plains reservoirs and the high mountain reservoirs. The total combined storage volume for Twin Lake, Commanche, Peterson, and Barnes Meadow reservoirs is approximately 7000 acre-feet, while the combined storage of the non-recreational reservoirs is over 25,000 acre-feet, not including Milton Seaman Reservoir or the aggregated reservoirs.

The simulated operation of Halligan Reservoir is very near that which took place historically, except MODSIM produces slightly less draw-down at the end of 1973. For 1974 and 1975, the historical and simulated operation of the reservoir is identical. Significant operational changes in plains reservoirs occur in Park Creek Reservoir and North Poudre

Reservoir #15. From the figures, it is readily evident that a highly fluctuating, intraseasonal storage and release policy has been replaced by a more regular filling and emptying policy not unlike the operating policy historically observed for the high country reservoirs. Also, it should be noted that the ending storage in Worster Reservoir is the same for the new management scheme as the ending storage historically recorded, insuring that no additional water was obtained from this source. It is included in the analysis because Halligan Reservoir is on-line downstream from it, therefore, releases from Worster Reservoir contribute to the total inflow to Halligan Reservoir. To insure that no double accounting takes place, the initial storage in the aggregate reservoir is set equal to zero. Thereby, not allowing additional water from this source to be allocated toward the satisfaction of its own demand. The ending storage in the aggregate reservoir is also zero, which means that no water was taken from the other reservoirs unnecessarily.

There are many *legal* issues which also must be dealt with before attempting to actually implement this type of management practice. Such a strategy involves the storing of water out of legal priority. However, stored water is merely being transferred to other portions of the system, and overall demands should continue to be satisfactorily met. The exchange program is specifically designed for such an action.

The release or storage of water in the Greeley high mountain reservoirs would have no impact downstream of the turnout to the Munroe Canal. Fortunately, since the Munroe Canal is the highest (most upstream) diversion for irrigation water in the system, changing the operating

policy of the high mountain reservoirs would have zero impact (positive or negative) on the remaining water use structure within the basin. It is true, however, that flow levels in the Cache la Poudre River above the Munroe Gravity Canal will be affected by changes in the operating policies of the high mountain reservoirs. Historically, releases from these reservoirs during late summer help to augment the natural flow in the river, which is low during this time. In recognition of this fact, the effect of the new management strategy on river flow levels is determined. Traditionally, the split between high mountain reservoir water delivered to the Munroe and North Poudre canal system and other reservoir water delivered to the system is approximately 35% and 65%, respectively. The new management scheme results in a split in delivery of roughly 2% and 98% between high country and plains reservoirs. This change in percentage of the prospective sources of reservoir water is most critical in the first year when the mountain reservoirs are filling and release no water.

Subsequent to filling, only that portion of the annual inflow necessary to maintain the storage pool is held while the remainder is released downstream. Calculated river flows vary from historical values only during the months of May through September (the typical operating period for high country reservoirs). Table VII.2 shows the percentage decrease in total river flow above the Munroe Canal and the resultant adjusted flow for 1973, the most critical year, for the new management system.

The minimum monthly flow occurs in February and is 1301 acre-feet. This flow is unaffected by the change in operating policy of the high mountain reservoirs. A decrease in flow volume begins in May and increases, as expected, to a maximum of approximately 87% of the



Table VII.2. Change in River Flow Above Munroe Canal - 1973

Month	% Decrease in Total River Flow Above Munroe Canal	Calculated Adjusted River Flow Above Munroe Canal - Acre-feet
NOV	0	2,497
DEC	0	1,590
JAN	0	1,460
FEB	0	1,301
MAR	0	2,000
APR	0	3,470
MAY	0.18	89,310
JUN	0.33	132,976
JUL	0.68	76,035
AUG	9.56	25,541
SEP	12.95	7,534
OCT	0	5,210

historical flow in September. However, the adjusted flow in September (7,534 acre-feet) is still above the minimum flow of six out of the twelve months. Based on this analysis, it is concluded that the new management strategy will not seriously alter volumetric flow levels in the river. However, a tradeoff analysis could easily be performed by running MODSIM for various increased minimum flow levels in the river.

In case of severe drought conditions, water could still be taken from the high country reservoirs to meet pressing downstream agricultural, industrial, and municipal water needs. Such emergency releases could be conducted in ways which would distribute the drawdown proportionally to the capacity of each reservoir in order to minimize the destruction of the fishery of any one particular reservoir. Since, by definition, the high mountain reservoirs are at higher elevations, there is much greater flexibility in meeting downstream water demands as a result of the new management approach. A small release from several of these reservoirs would serve the same purpose as a large release from a single reservoir. It should be noted that structural weaknesses in the dams of some of these reservoirs may prevent the maintenance of maximum pool year around. In these cases, appropriate upper bounds can easily be placed in MODSIM. Also, lower bounds on flow in some of the canals may need to be increased in order to maintain proper heads at turnouts and equalize the system hydraulically.

## B. Case Study #2

### B.1 Method of analysis

The goal of this case study is to determine if, using that portion of effluent from Fort Collins attributable to new foreign water, the

Rawhide Project cooling pond could be filled by 1985 and if, from the same source, a minimum of 4200 acre-feet can be supplied the power plant annually. To pursue this goal using MODSIM, the network for which the model was calibrated must be revised to better account for the proportions of new foreign water delivered to the City and new foreign water spilled downstream (Figure VII.9). Also, the interaction between the river and the Rawhide Pipeline is eliminated so that no direct flow may enter the pipeline. However, the network is adjusted in such a manner that still allows the City to divert effluent directly to the river as well as to the pipeline and Fossil Creek Reservoir. Long Draw Reservoir is decomposed into two reservoirs (dashed line) to reflect the fact that only 6000 acre-feet are available for storage of imported water. All imports to Long Draw Reservoir occur at node 10 with a storage capacity of 6000 acre-feet, while intrabasin inflows to Long Draw Reservoir are restricted to node 1 with a storage capacity of 4400 acre-feet. The combined capacity of the reservoir is the true 10,400 acre-feet. Linkages directly connecting Joe Wright Reservoir and Long Draw Reservoir with Fort Collins (links 2 and 4, respectively) were included in order to differentiate between these sources and the exercise of the direct flow rights of the City. These reservoirs also remain linked (directly or indirectly) to the river. Such a change allows the model to account for spills of water downstream that are not diverted to the City. Appropriate channel losses are considered in both branches for each reservoir.

Although the model was calibrated for the three-year historical period 1973 to 1975, the required management study planning horizon is

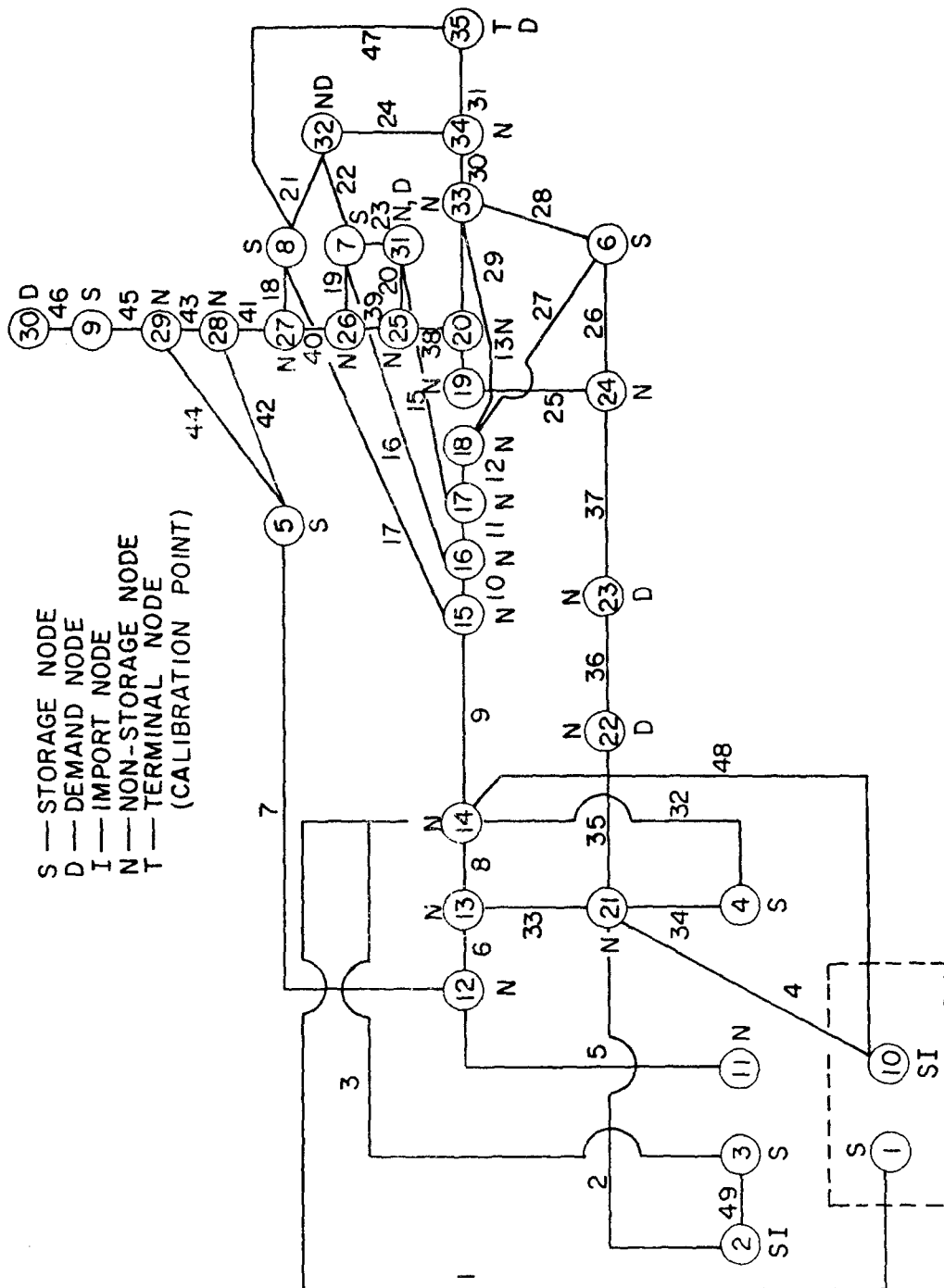


Figure VII.9. Revised network for Case Study #2.

19 years, from 1981 to 1999. This period is chosen in accordance with contract specifications which state that the filling of the cooling pond is to be initiated in 1981; the operation of the first generating unit is to begin in 1985; and the Windy Gap Project is to assume responsibility for meeting Rawhide Project demands in the year 2000. This extended 19 year period is consistent with the calibration phase since the river is over-appropriated which means that the water rights structure should not change appreciably. It is also assumed that the direct flow rights the City holds for Cache la Poudre River water will remain constant over this period. Table VII.3 lists the total monthly direct flow right exercised by Fort Collins. Each month throughout the analysis the appropriate direct flow must be totally diverted by the City before any reservoir water, including Horsetooth Reservoir water, can be delivered to the City. This constraint on the operation of the system is satisfied by setting the upper bound for the link connecting the City with the river at the City's direct flow right for each month and giving the link a very low cost as compared to all other links. In this manner, the most attractive transfer (from an optimization viewpoint) of water in the network is via this link (#33), and when feasible, flow should be at the upper bound.

The total annual demand for water by Fort Collins had to be estimated for the period 1981 to 1999. This was accomplished by fitting an exponential curve to the values forecast for years 1980, 1990, and 2000 by the Water Utilities Department, City of Fort Collins (1977). The projected annual Fort Collins demand over the period of analysis is presented in Figure VII.4. The same monthly distribution of the annual demand is employed for the management study as is for the calibration phase.

Table VII.3. Fort Collins Monthly Total Direct Flow Right

Month	Acre-Feet
NOV	864
DEC	893
JAN	893
FEB	807
MAR	893
APR	1054
MAY	1186
JUN	1148
JUL	1186
AUG	1186
SEP	1148
OCT	1035
TOTAL	12293

Table VII.4. Projected Annual Fort Collins Demand

Year	Acre-Feet	Year	Acre-Feet
1981	19451	1991	26074
1982	20334	1992	26773
1983	21097	1993	27494
1984	21661	1994	28229
1985	22244	1995	28987
1986	22839	1996	29769
1987	23454	1997	30565
1988	24082	1998	31385
1989	24729	1999	32227
1990	25245		

However, the monthly consumptive loss percentages of the City were modified slightly to better conform to normal conditions. These modified values are listed in Table VII.5. These values are used to determine what portion of the total monthly diversion of water by the City is available as effluent. It must be remembered, however, that under the contract, only the effluent attributable to new foreign water can be diverted to the pipeline. Again, the sequential preference of source of supply for Fort Collins is: (1) direct flow river water, (2) new foreign water (Joe Wright and Long Draw reservoirs), and (3) Horsetooth Reservoir water. Once, in any given month, the City has fully exercised its direct flow right, it can start to pull the transmountain water (if available) of which the resulting effluent can be diverted to the pipeline.

It was necessary to generate monthly data for both sources of foreign water (Michigan Ditch and Grand River Ditch) over the period of analysis. Resource Consultants, Inc. (1978) generated these data by determining the similarity of runoff potential of the watersheds which provide water for the Michigan Ditch and Grand River Ditch systems. Four years (1974 through 1977) of monthly data pertaining to the potential reusable water from the Michigan Ditch was correlated with the historical yield of the North Fork of the Michigan River to obtain 19 years of generated diversions via the Michigan Ditch. Table VII.6 contains these estimates of Michigan Ditch diversions. These data are input to MODSIM as annual values with appropriate monthly distributions. Estimates of Grand River Ditch diversions were generated in much the same manner and are reported in Table VII.7.

Table VII.5. Modified Consumptive Loss Percentages of the City of Fort Collins (Resource Consultants, Inc., 1978)

Month	Consumptive Loss (%)
NOV	1.5
DEC	1.5
JAN	1.5
FEB	1.5
MAR	1.5
APR	25.8
MAY	27.5
JUN	51.4
JUL	60.1
AUG	57.6
SEP	47.3
OCT	29.4

Figure VII.6. Generated Monthly Estimates of Michigan Ditch Diversions to Joe Wright Reservoir (acre-feet)

<u>Year</u>	<u>May</u>	<u>June</u>	<u>July</u>	<u>Aug.</u>	<u>Sept.</u>	<u>Total</u>
1981	152	1848	1123	334	30	3487
1982	237	2651	1262	315	39	4504
1983	199	2280	1061	266	33	3839
1984	151	1841	1120	333	30	3475
1985	211	2424	1125	281	35	4076
1986	204	2346	1089	272	34	3945
1987	241	2694	1288	322	40	4585
1988	144	744	341	52	0	1311
1989	147	1787	1092	325	29	3380
1990	209	2412	1118	279	35	4053
1991	190	1165	832	143	48	2378
1992	199	2287	1064	266	32	3848
1993	208	2386	1105	276	34	4009
1994	199	2281	1062	265	33	3840
1995	212	2434	1131	283	35	4095
1996	219	2497	1170	292	37	4215
1997	151	1847	1123	333	30	3484
1998	214	2430	1130	283	35	4092
1999	209	2407	1115	278	34	4043



Table VII.7. Generated Monthly Estimates of Grand Ditch Diversions to Long Draw Reservoir (acre-feet)

<u>Year</u>	<u>May</u>	<u>June</u>	<u>July</u>	<u>Aug.</u>	<u>Sept.</u>	<u>Total</u>
1981	308	1679	644	168	0	2799
1982	305	3763	4475	1322	305	10170
1983	555	3202	1786	493	123	6160
1984	219	1263	704	194	49	2429
1985	366	1993	764	199	0	3322
1986	406	2683	3740	1138	163	8130
1987	223	2753	3274	967	223	7440
1988	97	642	894	272	39	1944
1989	112	740	1032	314	45	2243
1990	916	4997	1916	500	0	8329
1991	85	557	777	236	34	1689
1992	779	4501	2510	693	173	8656
1993	282	1633	911	251	63	3140
1994	261	1504	840	232	58	2895
1995	1032	5632	2159	563	0	9386
1996	937	5109	1958	511	0	8515
1997	227	1312	732	202	50	2523
1998	599	3462	1931	533	133	6658
1999	158	1043	1454	443	63	3161

In Figure VII.10 the generated total imports of water from the Michigan Ditch and Grand River Ditch are plotted for each year. These values are then separated into three distinct groups; with the limitation that for any one year both imports must be in the same category. These groups are then interpreted as wet (1973), intermediate (1974), and dry (1975) according to the results of the calibration phase. Therefore, for each year a complete and representative hydrology is obtained for input to the model. For example, for 1985 the generated transmountain diversions are coupled with the 1985 projected Fort Collins demand. Historical adjusted inflows and demands along with the estimated return flows for 1974 are then combined with the 1985 projections to form a complete and consistent hydrological sequence for 1985. This approach is justifiable because the river is vastly over-appropriated. Most likely no additional water will be allocated to the various demand centers without significant changes in the character of the basin, which are not expected over the planning period. Also, dry years in relation to the volume of import should be associated with dry years in relation to unregulated inflows originating within the basin, and the amount of demand satisfaction realized in any year is directly proportional to the water available from snowmelt. This is the reason that, for this example, 1974 demands and return flows remain coupled with 1974 inflows. Likewise, it is doubtful that, for this limited area, great differences (relative to the size of the basin) in snowpacks would occur. Finally, it can be shown from the historical record that very rarely are there more than two dry years in succession, or for that matter two wet years. This observation influenced the placement of the imports into their respective

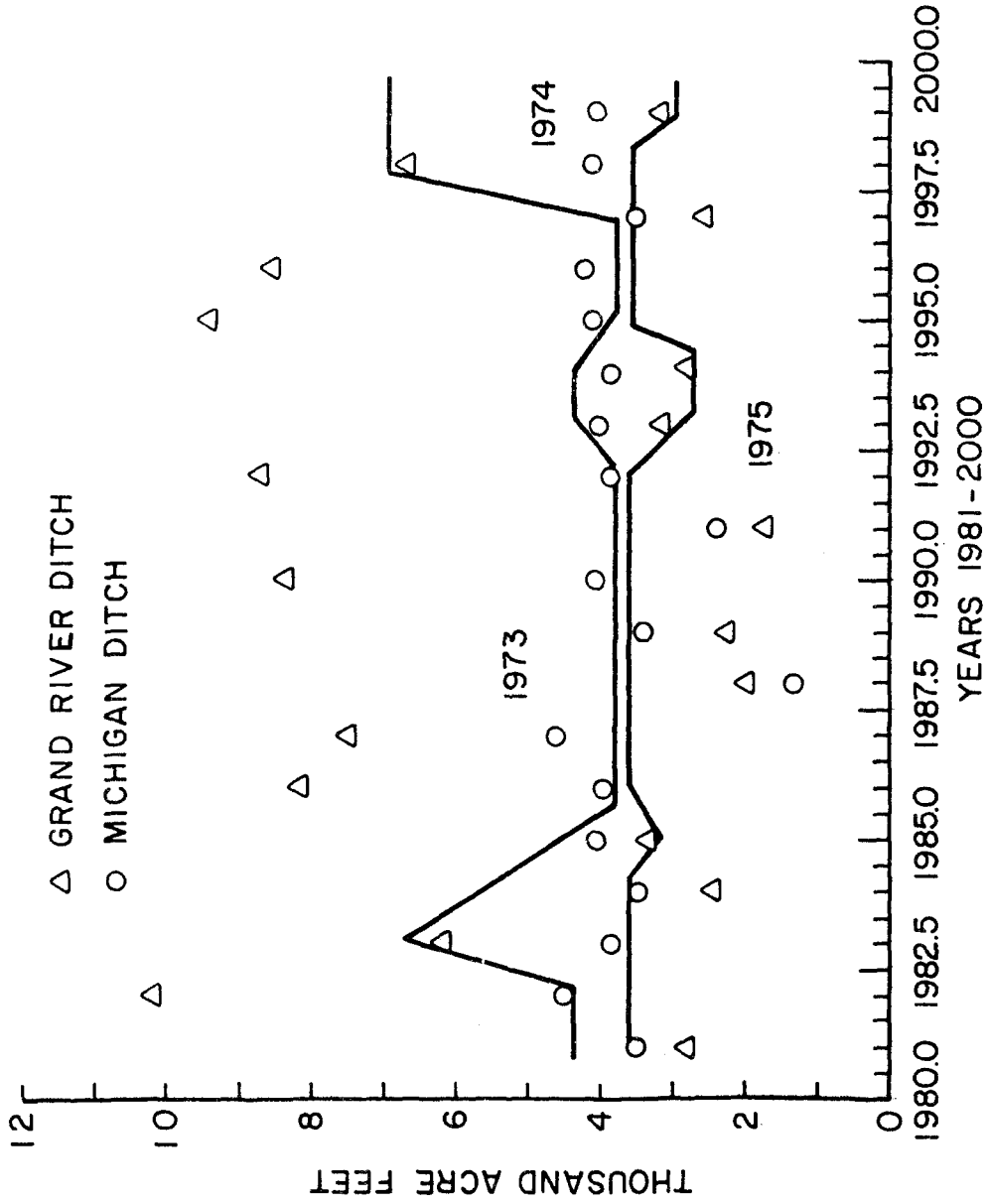


Figure VII.10. Estimated Grand River Ditch and Michigan Ditch imports.

categories. The hydrologic situation for each year of the analysis is constructed in the above fashion.

The 19 years of data were programmed and an initial set of priorities were chosen. MODSIM computed the transfers of water throughout the network based on these priorities. The results were analyzed by a supplemental computer program which takes the linkage flows calculated by MODSIM and tabulates the reusable effluent attributable to Joe Wright and Long Draw reservoir releases delivered to Fort Collins. The priorities (of storage versus release in the reservoirs) were then adjusted in such a manner as to converge on a value of 4200 acre-feet or more annual reusable water from these two reservoirs. A discussion of the method of adjustment of these priorities is included in the final section of this chapter. Fifteen successive adjustments of these priorities were necessary before a reasonable conclusion was obtained.

## B.2 Results of analysis

First, the projected demand for water by Fort Collins is satisfied, without exception, in every year throughout the simulation period. Also, Fort Collins direct flow right is fully exercised in every month of the analysis, as required. Figure VII.11 shows the proportions of the supply (direct flow, Horsetooth Reservoir, Long Draw Reservoir, and Joe Wright Reservoir) contributing to each year's projected demand. It is interesting to note that the amount of Horsetooth Reservoir water required, according to the final scheme, steadily increases while the amount of Joe Wright and Long Draw reservoir water remains fairly constant.

In Figure VII.12 the amount of reusable effluent resulting from Joe Wright Reservoir and Long Draw Reservoir releases to the City is displayed.

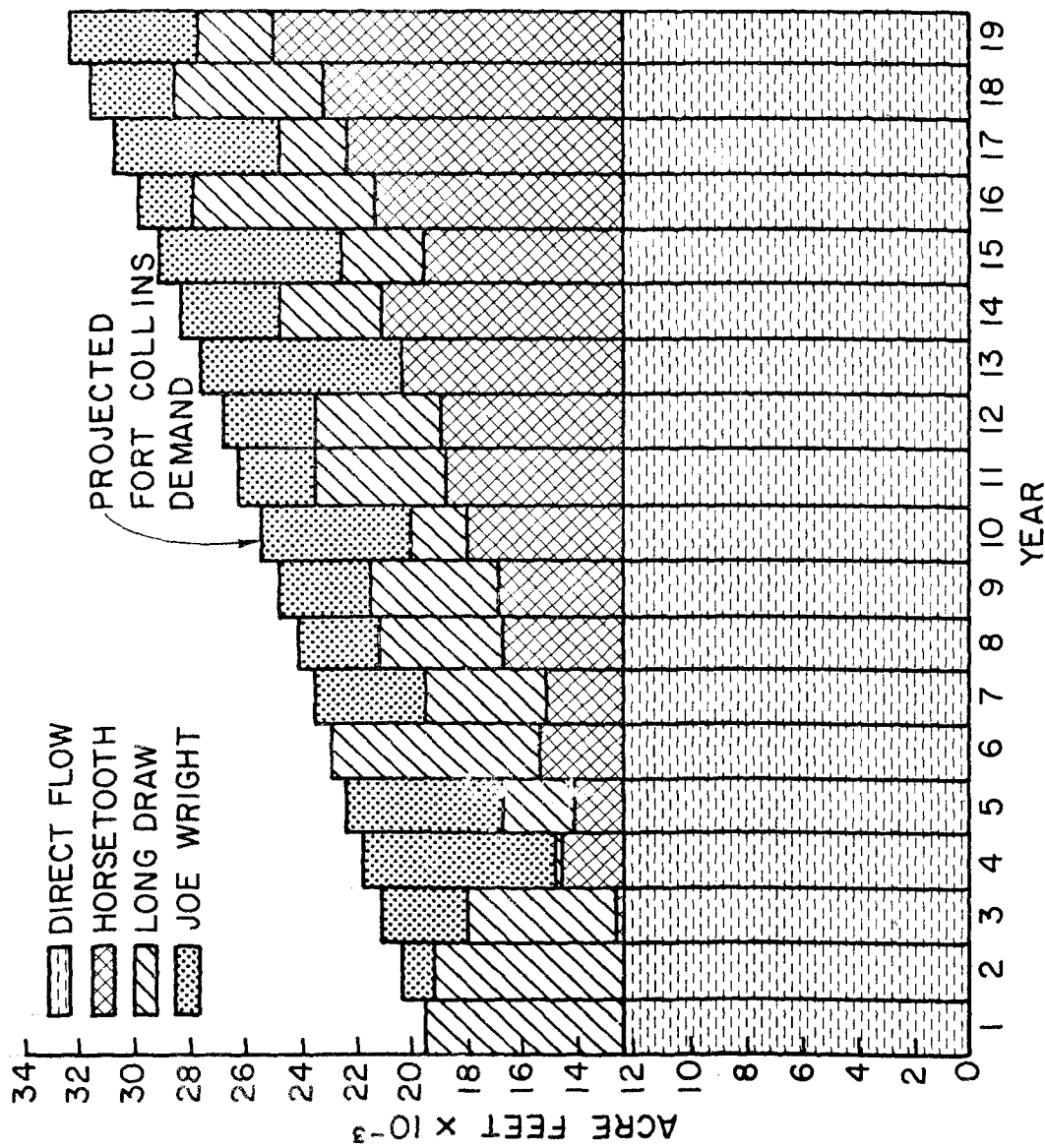


Figure VII.11. Proportion of Fort Collins demand met by various sources of supply.

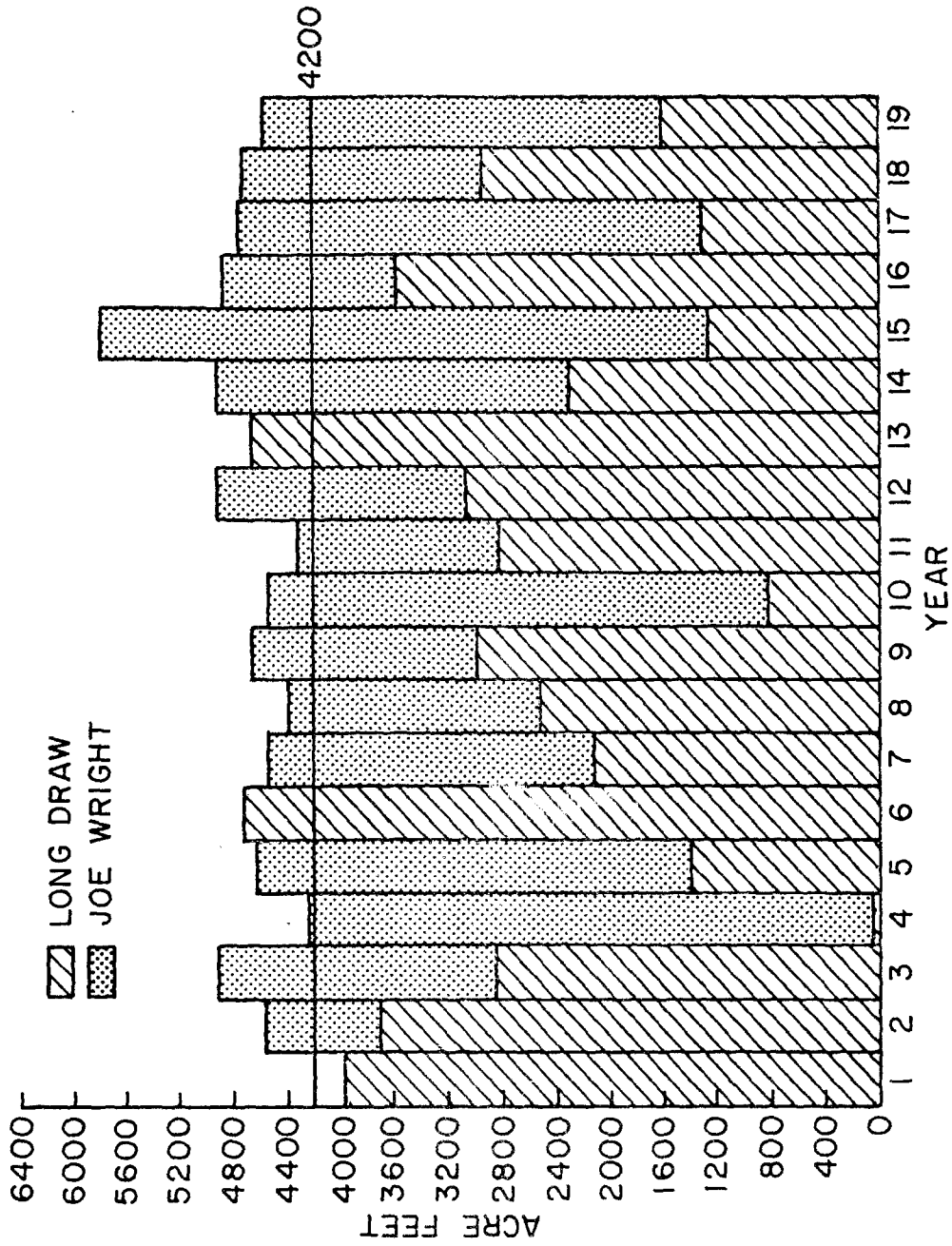


Figure VII.12. Reusable effluent deliverable to Rawhide pipeline.

Only in the first year (1981) is the return flow less than the 4200 acre-foot target. This is because the projected Fort Collins demand for 1981 is too small to allow enough water from the reservoirs to be used to obtain 4200 acre-feet of reusable effluent. However, in all the remaining years this target is exceeded. Excluding the first year, the mean annual deliverable effluent to Rawhide Pipeline is 4662 acre-feet, and for the entire 19 year period a surplus of 8776 acre-feet above the annual 4200 acre-feet required is calculated. Also, during several high flow years (importation of relatively large amounts of foreign water) spills from these two reservoirs occur. The total amount of spills calculated by the model equals 4075 acre-feet; 336 acre-feet from Joe Wright Reservoir and 3739 acre-feet from Long Draw Reservoir.

As noted earlier, the first four years of the analysis is designated as a filling period for the cooling pond. From the results obtained from MODSIM, there are 17,651 acre-feet of reusable water available for filling the pond during this period. A uniform rate of delivery is not essential to the filling, therefore, no borrowing or exchange program needs to be invoked. For the first four years, water is delivered to the pond as available. The capacity of the pond is estimated at 13,000 acre-feet, which means that about 4650 acre-feet of excess water is available for evaporative losses during filling. MODSIM calculates an evaporation loss during filling of 2239 acre-feet. This leaves an additional 2411 acre-feet for contingencies. The implications of these results are discussed in the next section.

### B.3 Discussion of results

The amount of carry-over storage provided in both Joe Wright and Long Draw reservoirs from year to year is of critical importance to the ability of these reservoirs to meet the demand for reusable effluent. Figure VII.13 shows the combined and individual carry-over storage for these reservoirs throughout the period. However, to avoid spills as much as possible the reservoirs must be evacuated early in the year to allow storage space for the incoming transmountain diversions. This is particularly true during high flow years. The most realistic case is tested for this management study, in that the initial storage in Long Draw Reservoir is 6000 acre-feet while Joe Wright Reservoir begins empty. Ending storages are also 6000 acre-feet and zero, respectively.

From the manipulation of the storage priorities for Long Draw Reservoir and Joe Wright Reservoir certain insight into operational guidelines can be gained. The priorities selected for a particular simulation are based on the results obtained from the previous run. This means, that past the initial run, a certain degree of foreknowledge or forecasting is employed by the user in determining the adjustments of the priorities to better conform with his mental notion of how the system should function. This is not unrealistic, in that, the true operation of these reservoirs will not be performed in a vacuum. As experience is gained, a better understanding of system response will be acquired. Estimates of snowpack conditions will provide information concerning the hydrology for the upcoming season which in turn will allow for preliminary formulation of operational guidelines. There is also added realism since the model does the best it possibly can, given flexibility



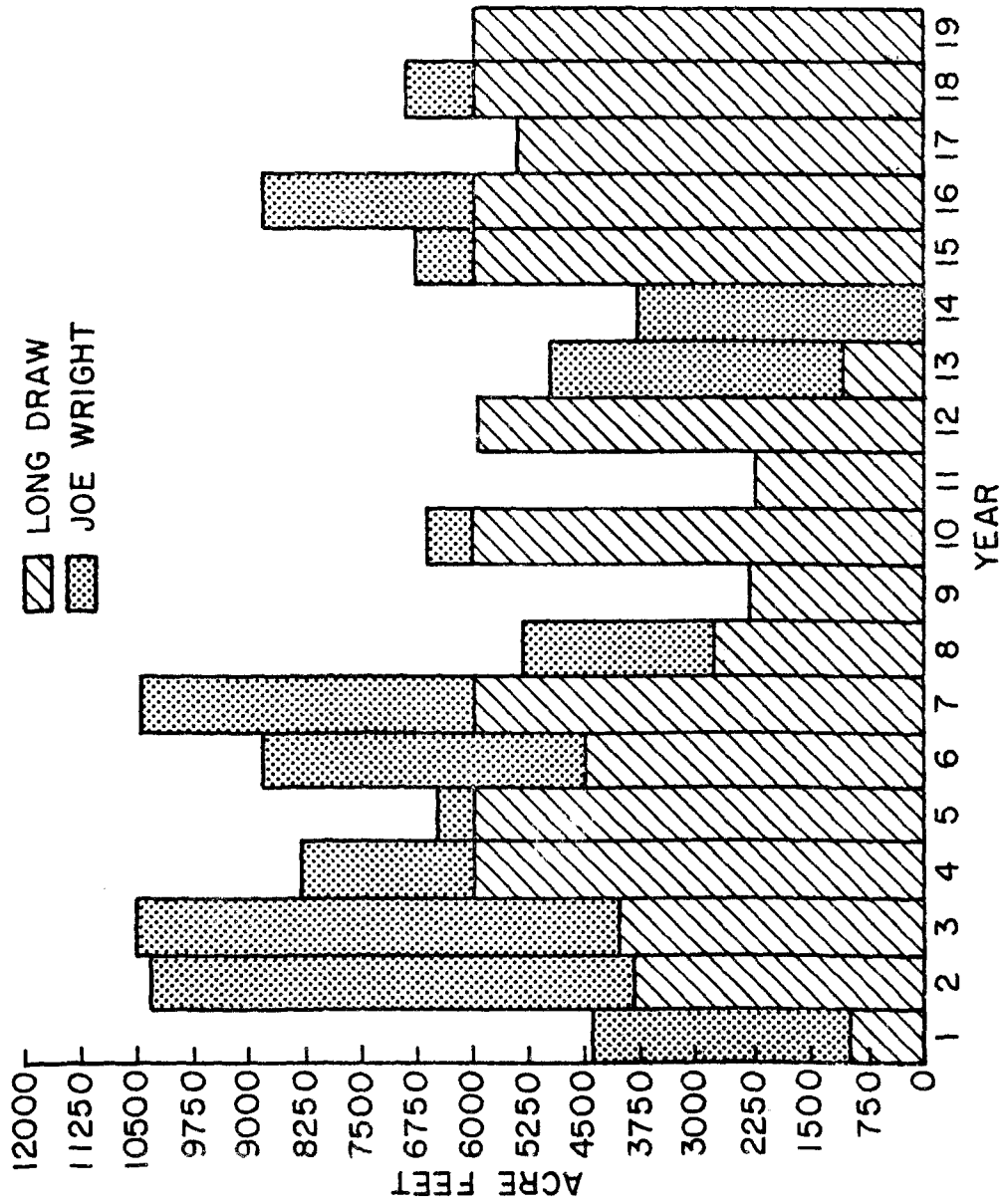


Figure VII.13. Individual and total carry-over storage for Joe Wright and Long Draw Reservoirs.

in the system, to apportion water to the various demand and storage centers on a month to month basis. It does not consider what happened last month or anticipate what will take place next month. However, it does select the optimum operating policy for the current month. The *user* must adjust the priorities placed on the transfer of water throughout the network to consider previous conditions and anticipate future developments.

An example of the above discussion is shown in Figures VII.14 and VII.15 which display the sensitivity of storage priorities for Joe Wright and Long Draw reservoirs in determining carry-over storage. In both cases, for simulation #2, carry-over storage was minimal beyond 10 years; resulting in severe deficiencies in reaching the 4200 acre-foot target in many of these years. However, through successive adjustment of the priorities, adequate carry-over storage was achieved (simulation #15). *Adequate* refers to the fact that through the provision of carry-over storage, 4200 acre-feet, or more, of reusable effluent could be realized from these reservoirs even during dry years. The relationship between storage priority and carry-over storage is not linear, however. Physical feasibilities are also active in determining carry-over storage as well as the demand structure and variability of monthly consumptive loss rates. From Figures VII.14 and VII.15 it is evident that in the first five years or so of the analysis, the change in the priorities between the two simulation runs for both reservoirs has very little impact on carry-over storage. Therefore, there is no basic scheme in changing priorities other than gaining experience with the model. However, after a few model runs, the effect of changing the relative and absolute values of the priorities can be anticipated with greater and greater confidence.

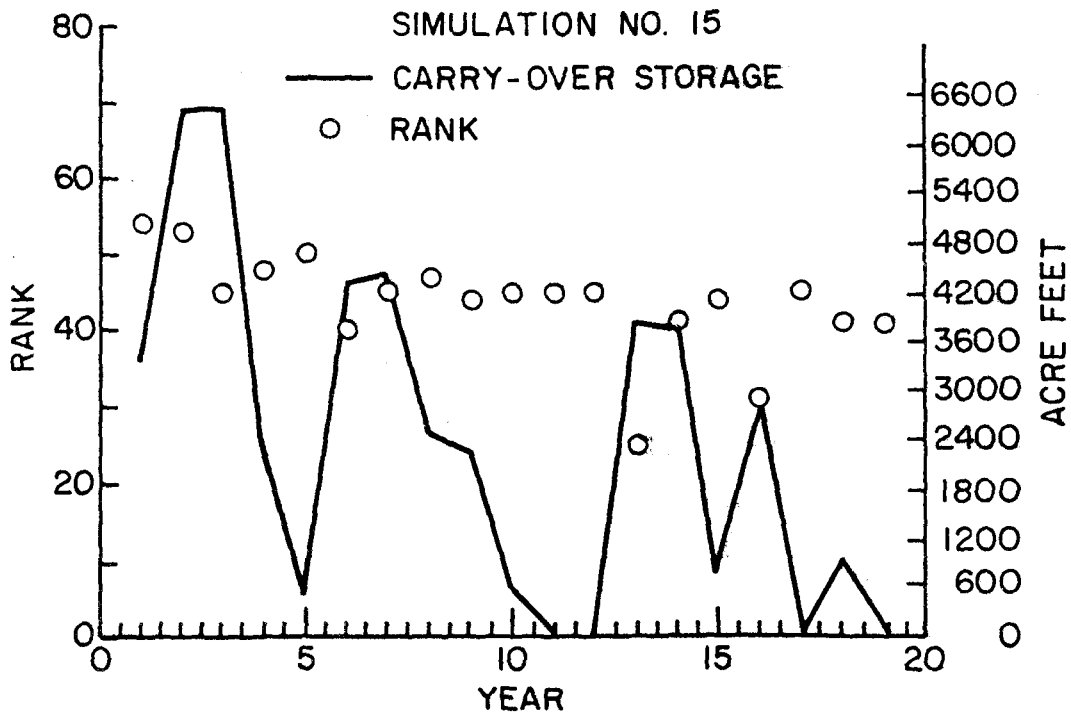
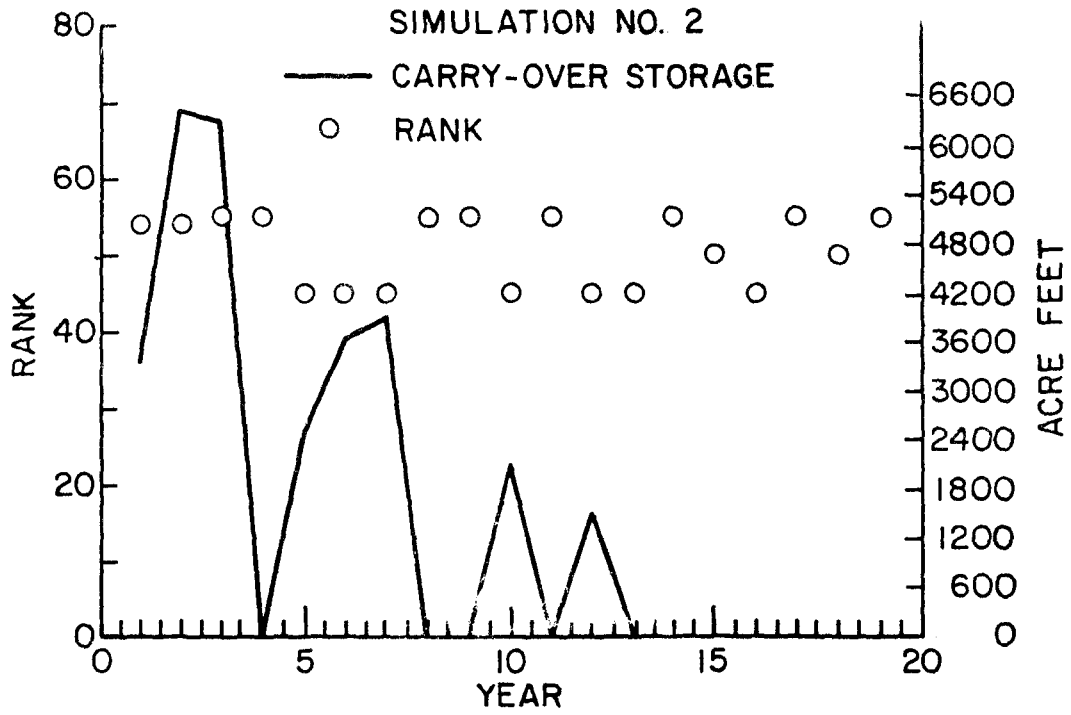


Figure VII.14. Sensitivity of storage priority vs carry-over storage for Joe Wright Reservoir.

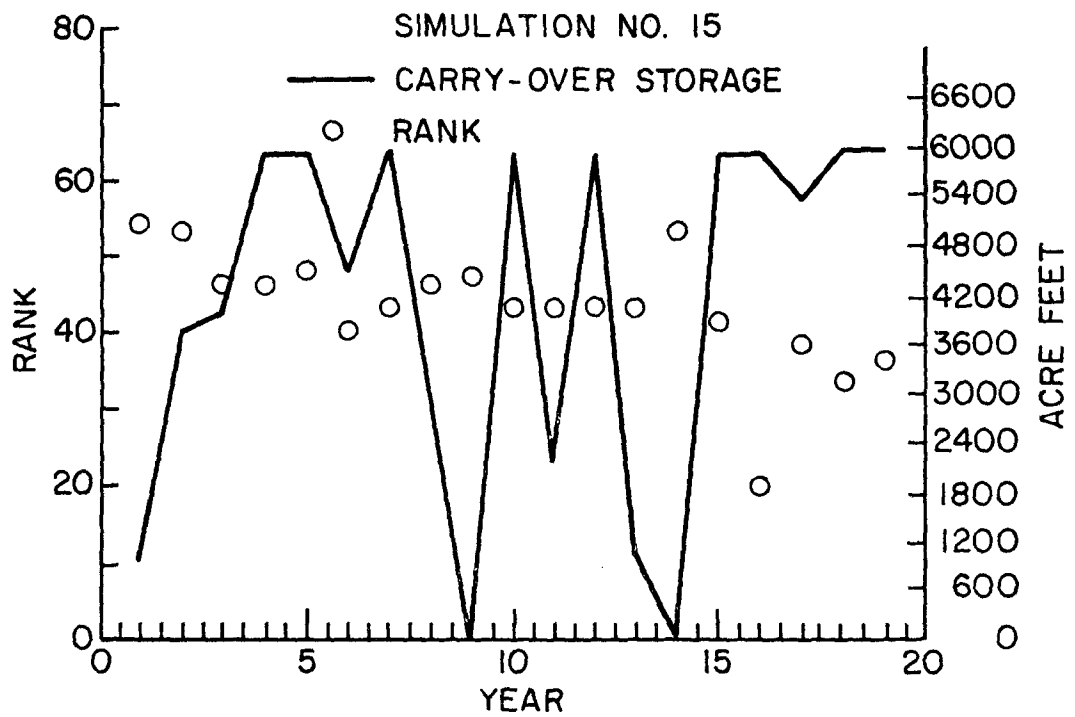
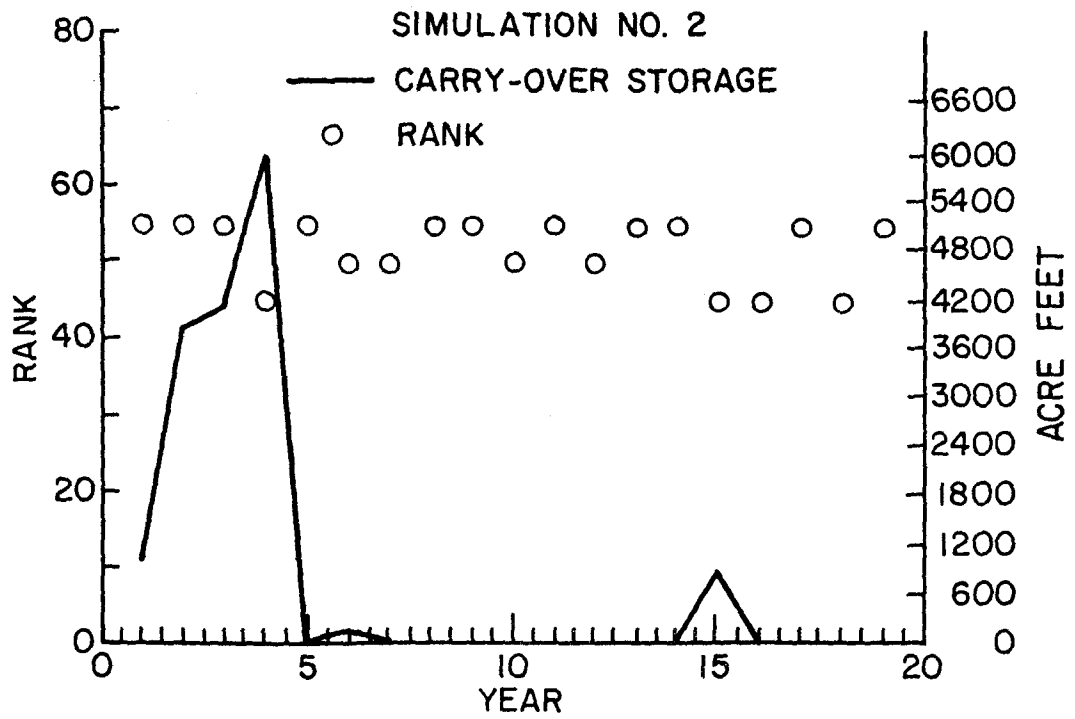


Figure VII.15. Sensitivity of storage priority vs carry-over storage for Long Draw Reservoir.

Along with the determination of the priorities to be placed on water transfers throughout the system, target storage levels must also be determined. Initially, the desired monthly ending storage levels for Long Draw and Joe Wright reservoirs were established at maximum capacity. Subsequently, it was discovered that such a policy leads to a greater amount of spills (water lost from first use opportunity by the City) than necessary. For this reason, in the first years of the analysis target storage levels were set below maximum capacities in order to evacuate part of the reservoirs to allow for the storage of anticipated large inflows later in the season. Figures VII.16 and VII.17 display the target monthly ending storage and the calculated monthly ending storage throughout the 19 year period for each reservoir. During the later part of the period, storage levels in Joe Wright Reservoir approach the maximum capacity but do not reach it, while Long Draw Reservoir storage levels remain at or near capacity during the final months. This scheme does not totally eliminate spills but it does reduce them considerably. Also, foreknowledge of the magnitude of transbasin diversions coupled with the variable consumptive loss rates characteristic of the return flow of the City, can be used to minimize spills. During high flow years, it is advantageous to transfer a large amount of foreign water to the City during the high consumptive loss months; while conversely, it is of benefit to transfer more foreign water to the City in low flow years during the low consumptive loss months.

Demand shortages throughout the remainder of the system are aggregated at the terminal node, and are reasonably consistent with the demand shortages occurring during the calibration phase of this study.

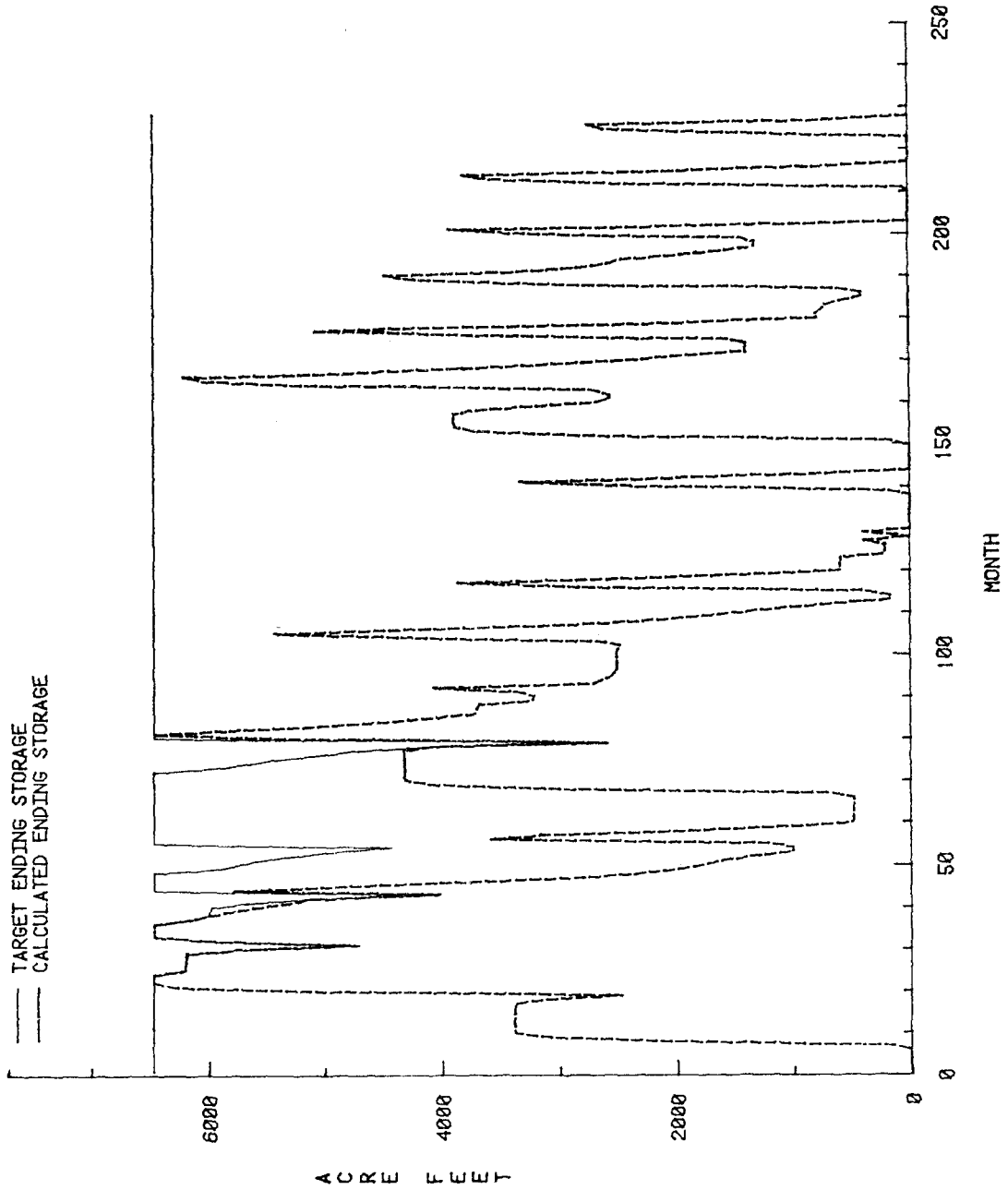


Figure VII.16. Target vs calculated end of month storage for Joe Wright Reservoir.

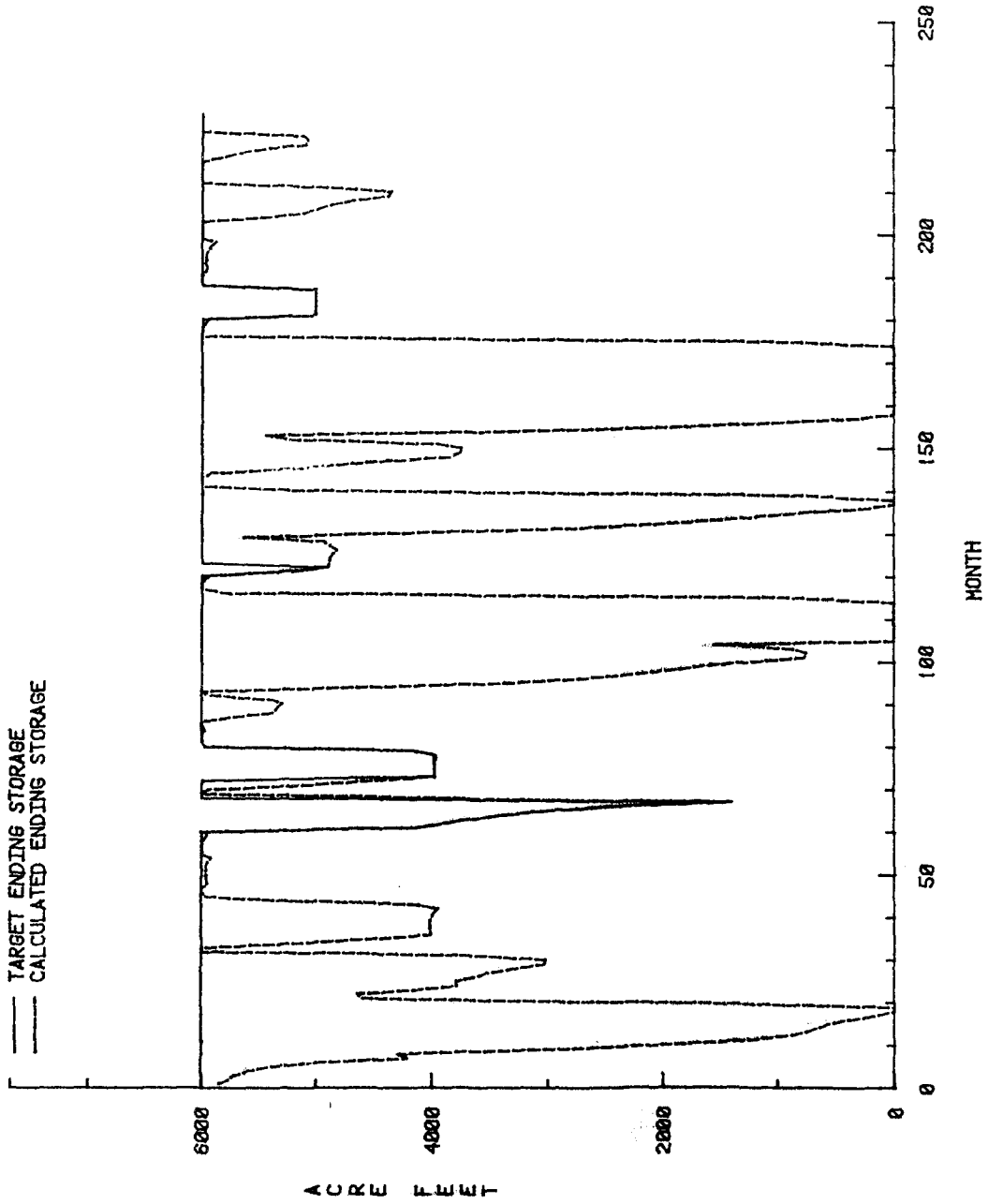


Figure VII.17. Target vs calculated end of month storage for Long Draw Reservoir.

An underestimate of the availability of Horsetooth Reservoir water to meet this demand is possibly part of the cause for the shortage. As Fort Collins draws increasing amounts of Horsetooth Reservoir water to meet projected demands, an increasing portion of this water becomes unavailable for downstream demand satisfaction. However, the shortages remain uniformly low (Figure VII.18), and most likely will be satisfied from additional Colorado-Big Thompson water imported to the basin. The simulated operating policy of the other reservoirs in the system is closely aligned with historical storage and release patterns in that they fill and empty on a seasonal basis during the period of analysis.

Finally, as mentioned in Chapter V, a *borrowing* agreement must be made between North Poudre Irrigation Company (owner of Fossil Creek Reservoir) and Fort Collins in order to provide a more desirable uniform rate of delivery of reusable effluent to the power plant. Such an arrangement would commence in 1985 and would consist of the borrowing by Rawhide Project, via the pipeline from Fossil Creek Reservoir, enough water to compensate for the difference between the reusable effluent and the desired pipeline diversion during months when the reusable effluent is less than the desired diversion. Otherwise, Rawhide Project will repay Fossil Creek Reservoir when the amount of reusable effluent exceeds the desired pipeline flow during any one month. Such an agreement is advantageous to both parties since the Rawhide Project will benefit from a uniform pumping rate and Fossil Creek Reservoir will receive additional water (reusable effluent exceeds 4200 acre-feet each year) to its storage decree and usually during low flow months. Also, the borrowing arrangement should have no impact on the direct flow rights structure along the river, since the pipeline would be borrowing



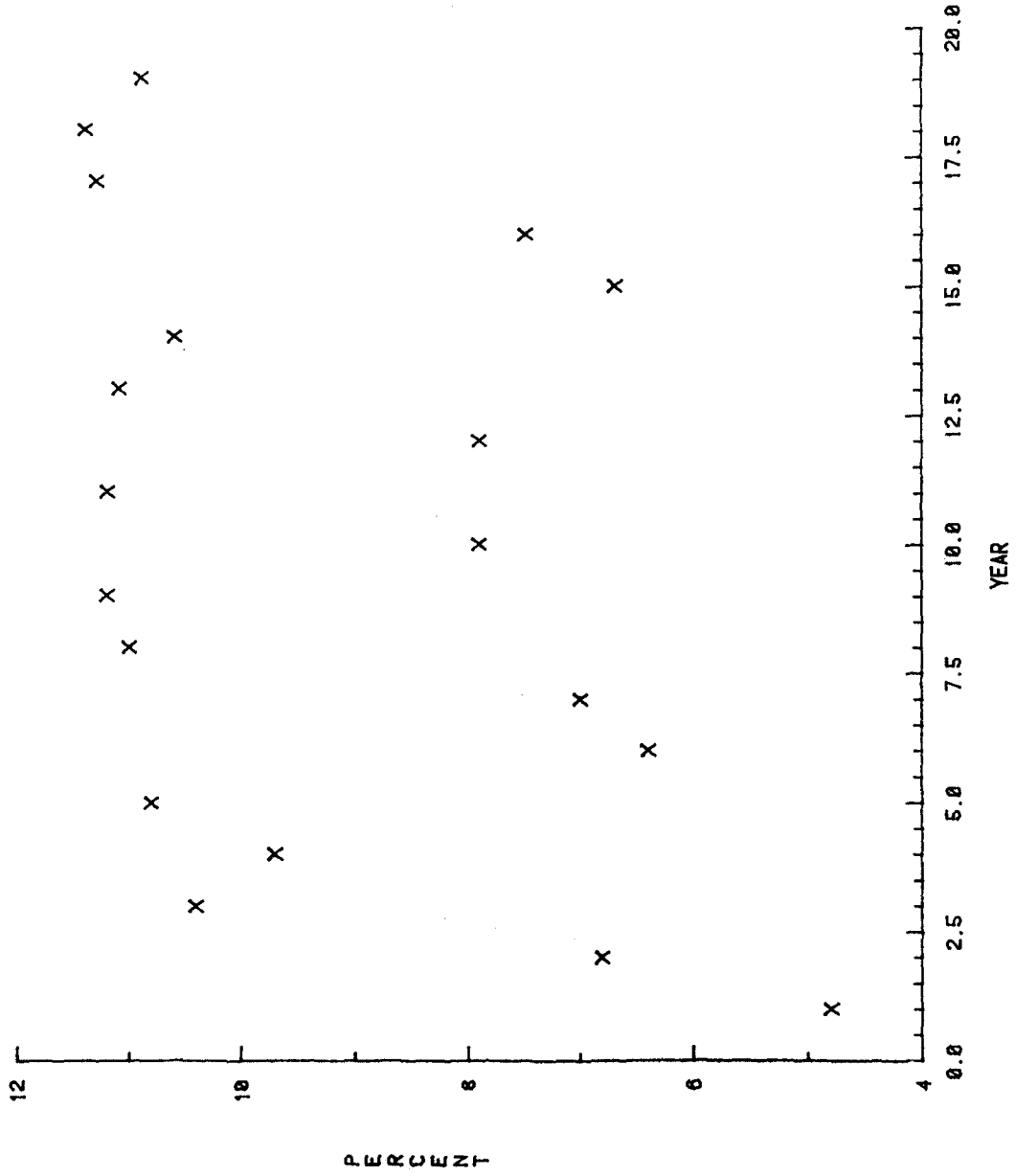


Figure VII.18. Annual percentage of shortage at terminal node.

only on the reservoir storage rights. Table VII.8 contains two examples of how this arrangement would function. The first year (1985) of power generation and 1991, the year the lowest level of reusable effluent is expected. Even for the worst year, the repayment is over 100 acre-feet greater than the amount borrowed.

Table VII.8. Example Borrowing Arrangement Between Pipeline and Fossil Creek Reservoir

Year	Month	Exchange with Fossil Creek Reservoir		Pipeline-Reservoir Exchange	
		Reusable Effluent	Desired Pipeline Diversion	Borrow From Fossil Creek	Repay Fossil Creek
1985	NOV	312	345	33	
	DEC	197	357	160	
	JAN	171	357	186	
	FEB	256	322	66	
	MAR	303	357	54	
	APR	0	345	345	
	MAY	145	356	211	
	JUN	882	345		537
	JUL	833	357		476
	AUG	639	356		283
	SEP	485	345		140
	OCT	<u>339</u>	<u>357</u>	<u>18</u>	
		4562	4200	1073	1436
-----					
1991	NOV	512	345		167
	DEC	337	357	20	
	JAN	0	357	357	
	FEB	362	322		40
	MAR	0	357	357	
	APR	0	345	345	
	MAY	0	356	356	
	JUN	913	345		568
	JUL	160	357	197	
	AUG	835	356		479
	SEP	674	345		329
OCT	<u>522</u>	<u>357</u>		<u>165</u>	
	4315	4200	1632	1748	

## CHAPTER VIII

### SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

#### A. Summary

A river basin water management planning model is synthesized from currently existing river basin models. MODSIM is specifically designed for the analysis of water availabilities throughout a complex river basin system according to preselected allocative priorities. The underlying principle of the operation of the model is that most physical river basin systems can be represented as capacitated flow networks. MODSIM employs the Out-of-Kilter Algorithm to minimize the total cost of flows in this graphical network of interconnected reservoirs, river reaches, pump canals, and gravity flow canals.

In addition to the consideration of the physical aspects of a river basin system, MODSIM is capable of simulating the storage and distributional preferences resulting from the institutional framework existing in a basin. This capability is achieved through a ranking procedure which is translated into pseudo-costs of water transfer. Using this ranking procedure, MODSIM apportions the available water for storage in various reservoirs and diversion of flow from the river according to preferences established by the user.

A methodology is also included which allows MODSIM to estimate return flows occurring from irrigated agriculture. Multiple linear regression is used to develop a predictive equation for return flows

based on canal diversions and previously calculated return flows. This methodology is consistent with the general planning nature of MODSIM and produces results compatible with this modeling level.

The execution of the simulation package is accomplished in an interactive, conversational programming mode. This advantage adds great utility to the model since no appreciable knowledge of computer programming is necessary for the successful operation of MODSIM. Two conversational data organization programs are interfaced with MODSIM which query the user concerning the nature of the simulation and, based on his responses, construct a complete and executable data file.

Two case studies are undertaken to fully demonstrate the capability of MODSIM in aiding in the analysis of changes in water resources policy within a river basin. The first case study concerns the inclusion of recreation in a multipurpose management framework for certain high mountain reservoirs in the Cache la Poudre River Basin. Traditionally, these reservoirs have been operated exclusively for the provision of a late season irrigation water supply, often resulting in complete emptying of the reservoirs toward the end of the irrigation season. These reservoirs were previously evaluated according to their perceived recreation potential. Based on the conclusions concerning the recreation potential of these reservoirs, the case study addresses the question of the hydrologic and legal feasibility of maintaining stable pool elevations, at or near maximum, in two of these reservoirs.

The second case study analyzes the availability and opportunity of providing water for cooling purposes for the proposed Rawhide Project. By contract, the City of Fort Collins, Colorado is to provide the Rawhide Project with the opportunity to utilize sewer effluent attributable to

newly developed or imported water first used by the City. Joe Wright Reservoir and Long Draw Reservoir are to be used as temporary storage facilities for the imported water which is subsequently to be released to Fort Collins. The project calls for the development, at the site, of a 13,000 acre-foot reservoir which must be filled prior to initial operation of the power plant, scheduled for 1985. Upon filling of the reservoir, the Rawhide Project will require no less than 4200 acre-feet of firm water annually.

MODSIM is calibrated for both case studies for the years 1973-1975 before the management alternative analyses are performed. Detailed calibration methodology is presented, followed by the results obtained from the calibration phase of the investigations. Acceptable duplication of historical records is achieved by successively adjusting model priorities placed on the transfer of water throughout the networks. An example of the use of the return flow calculation option is also included.

Upon successful MODSIM calibration, the model is used to analyze the feasibilities of both case studies management alternatives. The priorities placed on water transfers throughout the networks which are obtained from model calibration are adjusted to reflect the objectives of the alternate management policies. Complete data necessary for each analysis is presented along with the methodology for each case study. Finally, the results obtained from MODSIM are discussed along with their implications.

## B. Conclusions and Recommendations

The conclusions drawn from this study pertain to three general areas: (1) conclusions concerning the model MODSIM and its utility, (2) conclusions concerning the two case studies, and (3) conclusions concerning the general nature of this study. From a consideration of conclusions, recommendations for improvements (both theoretical and practical) emerge, and are also discussed in this section.

### B.1 The model

In relation to the desired river basin water management model set forth in Chapter II, synthesized MODSIM is more closely aligned than any of the models selected for review. Perhaps the most important aspect of the simulation package is the enhanced user capability provided by the interactive, conversational programming nature of the model. MODSIM is specifically designed as a *friendly* modeling package, in that, it is particularly oriented toward the analysis of complex river basin water management problems by those individuals who are most closely associated with these problems, the actual state and local planners and managers of our water resources. Even though MODSIM is a long-term water management model, it still could be used to evaluate the impact of several different planning options, although it will not select a plan.

MODSIM is capable of simulating the water storage, transport, and distribution morphology of a river basin system to a very high level of resolution, depending on the problem. However, it is not able to consider the inclusion of hydropower production in river basins. Since

energy production is fast becoming one of the most important political and economic issues in the United States, and also since hydropower is relatively inexpensive and extremely clean in relation to other sources of energy, the inclusion of a hydropower production analysis option is recommended for future refinements of MODSIM.

The model is able to consider non-beneficial consumptive losses such as evaporation and conveyance losses. However, MODSIM, as it currently exists, can only consider beneficial consumptive losses as they relate to volumetric monthly demands. It is recommended that future efforts be devoted to the study of the possibility of expanding the irrigation sector of the model to include crop water requirements, perhaps based on evapotranspiration prediction. Nevertheless, it must be remembered that MODSIM is a long-term management model and care must be taken to insure that the model does not become unwieldy.

Another feature unique to MODSIM is its quasi-optimizing capability which enables it to include, very satisfactorily, the quantifiable aspects of institutional structures governing stream diversion, water storage, and exchange. This capability is a necessity if the model is to be used for planning purposes, whereby the existing institutional structure of a river basin may be modified slightly to reflect an alternate future allocative scheme.

Research is currently being conducted at Colorado State University on options for including the stochastic nature of inflows in the model. It is recommended that such an option be developed independently of MODSIM with the capability of being directly interfaced with the model. A modularized package has certain advantages in computer core storage savings and execution time minimization.



Since irrigation return flows are a significant aspect of the hydrology of an agriculturally productive river basin, such as the Cache la Poudre River Basin, the inclusion of a return flow consideration in the model is imperative. However, there is a wide range of methodology for this inclusion. An attempt is made to accurately model return flows (in a planning context) without making the model overly cumbersome. Nevertheless, it would be possible to include a stream-aquifer interaction model, similar to MITSIM-E, in a modularized package for studies where the current method of calculating return flows proves too unreliable.

## B.2 The case studies

The two case studies are intended for the demonstration of the capability and utility of MODSIM. As such, the specific conclusions drawn from these studies offer initial guidelines for the management of the Cache la Poudre River Basin to achieve the stated goals of the case studies. However, further analysis may be required before actual implementation of results. For instance, dam safety investigations should be undertaken before any attempt is made to maintain storage levels near maximum in any of the high country reservoirs. Nevertheless, the results of the case study do show that, based on the hydrology considered, it would be possible to provide some level of recreational opportunity in these reservoirs without causing injury to other water users in the basin.

Similarly for the Rawhide Project, based on the hydrologic sequence considered, a firm annual water supply of 4200 acre-feet of reusable effluent from the City of Fort Collins could be provided. Although the

synthetically generated transbasin diversions input to MODSIM do contain dry periods, many simulations of the system, varying both the sequence and severity of dry periods, would be necessary before any firm conclusions could be drawn.

Certain general conclusions from these studies, in relation to the model, also need to be addressed. The problem formulation, data gathering, and data organization phase of studies, such as in this report, is the single most important aspect of an investigation. Extreme care must be taken in developing a network that preserves those attributes of the real system which are being analyzed. The adage "what comes out is no better than what goes in" never had more relevance than to river basin modeling.

The calibration phase should be conducted with as much prior knowledge of system behavior as possible. There is no substitute for a thorough working knowledge of the river basin being modeled. With such information, insight into expected model outcome can be gained which helps to determine correct diversion priority adjustments necessary for acceptable calibration. These case studies, although requiring the preferential consideration of storage and demand, do not entirely illustrate the use of water rights priorities by MODSIM. Again, it is noted that there must be aggregation of priorities due to the volumetric transfer of water monthly by MODSIM. As such, only an approximation of these priorities is possible.

These two case studies represent actual *real world* problems which are analyzed by MODSIM. In this respect, they represent a true demonstration of the capability and application of MODSIM. Also, such being the case, they offer a guide to prospective model users concerning the types of information required, the design and construction of the

network, and the subsequent input of data and execution of MODSIM. Finally, considerable detail is afforded the interpretation of results obtained from MODSIM.

### B.3 The report

This report is specifically written for a broad audience. It is intended to provide sufficient user documentation for the application of MODSIM to river basin water management problems by planner/managers. Also, it provides an in-depth presentation of the underlying methodology employed by the model, including a complete discussion and demonstration of the Out-of-Kilter Algorithm (Appendix A). Hopefully, this report also provides the reader with a feel for the types of problems which can be readily solved by MODSIM. Every model is created for a specific purpose and no model can realistically be applied to all problems.

It must be reiterated that river basin modeling is an evolutionary process. As new theory is tested and operational life is put on the model, continued improvements are made. Finally, a model, such as MODSIM, is nothing more than a tool. And, as any tool, its utility is closely related to the skill of the user.

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APPENDIX A  
OUT-OF-KILTER ALGORITHM

APPENDIX A

OUT-OF-KILTER ALGORITHM

The Out-of-Kilter Algorithm determines minimum cost flows in branching type *circulating* networks. The general format for these problems is:

$$\text{minimize } \sum_{i=1}^N \sum_{j=1}^N c_{ij} x_{ij} \quad (\text{A.1})$$

subject to:

$$\sum_{j=1}^N x_{ij} - \sum_{j=1}^N x_{ji} = 0 \quad \forall_i \quad (\text{A.2})$$

$$x_{ij} \leq u_{ij} \quad \forall_{ij} \quad (\text{A.3})$$

$$x_{ij} \geq \ell_{ij} \quad \forall_{ij} \quad (\text{A.4})$$

where:

$c_{ij}$  = cost of moving one unit of commodity  $x$  along arc  $i,j$  from node  $i$  to node  $j$

$x_{ij}$  = amount of homogeneous commodity moving along arc  $i,j$

$u_{ij}$  = maximum capacity for arc  $i,j$

$\ell_{ij}$  = minimum requirement for arc  $i,j$ .

The Out-of-Kilter Algorithm solves this problem via an efficient primal-dual simplex technique. Associating a dual variable,  $w_i$ , with each node conservation equation (A.2), dual variable  $h_{ij}$  with each upper bound constraint (A.3), and dual variable  $v_{ij}$  with each lower bound constraint (A.4), the dual problem is:

$$\text{maximize } \sum_{i=1}^N \sum_{j=1}^N \ell_{ij} v_{ij} - \sum_{i=1}^N \sum_{j=1}^N u_{ij} h_{ij} \quad (\text{A.5})$$

subject to:

$$w_i - w_j + v_{ij} - h_{ij} = c_{ij} \quad \psi_{ij} \quad (\text{A.6})$$

$$h_{ij} \geq 0 \quad \psi_{ij} \quad (\text{A.7})$$

$$v_{ij} \geq 0 \quad \psi_{ij} \quad (\text{A.8})$$

$$-\infty \leq w_i \leq +\infty$$

Rearranging the terms of Equation A.6:

$$v_{ij} - h_{ij} = c_{ij} - w_i + w_j \quad (\text{A.10})$$

The  $w_i$  can be considered as a "commodity price" at node  $i$ . Therefore,  $c_{ij} - w_i + w_j$  is the net arc cost, considering both shipment cost and the price of nodes terminating the arc. Thus, the net arc cost equals the shipment cost plus the difference in prices,  $w_i$ , at the terminating nodes.

If  $v_{ij}$  and  $h_{ij}$  are defined as:

$$v_{ij} = \max \{0, c_{ij} - w_i + w_j\} \quad (\text{A.11})$$

$$h_{ij} = \max \{0, -(c_{ij} - w_i + w_j)\} \quad (\text{A.12})$$

given any  $w_i$ 's, the dual problem always remains feasible. By further defining:

$$\bar{c}_{ij} = w_i - w_j - c_{ij} \quad (\text{A.13})$$

and applying the complementary slackness conditions, the optimality criteria can be determined as:

$$\text{If: } \bar{c}_{ij} < 0; \quad \text{then } x_{ij} = \ell_{ij} \quad (\text{A.14})$$

$$\bar{c}_{ij} > 0; \quad \text{then } x_{ij} = u_{ij} \quad (\text{A.15})$$

$$\bar{c}_{ij} = 0; \quad \text{then } \ell_{ij} \leq x_{ij} \leq u_{ij} \quad (\text{A.16})$$

Condition A.14 states that if a loss is incurred in shipping commodity from  $i$  to  $j$ , the flow should be as low as possible. Conversely, condition A.15 states that if it is profitable to send commodity from  $i$  to  $j$  then the flow should be as large as possible. Finally, if the net arc cost equals zero, indifference occurs as long as bounds are not violated. Any arc which satisfies one of the above conditions is termed *in-kilter*. Arcs which do not satisfy the above conditions are *out-of-kilter*. The Out-of-Kilter Algorithm systematically searches over conserving flows  $x_{ij}$  (primal) and values of  $w_i$  (dual) until each arc satisfies the optimality conditions. Possible *kilter states* for an arc are:

	$\bar{c}_{ij} < 0$	$\bar{c}_{ij} = 0$	$\bar{c}_{ij} > 0$
$x_{ij} > u_{ij}$	out	out	out
$x_{ij} = u_{ij}$	out	in	in
$l_{ij} < x_{ij} < u_{ij}$	out	in	out
$x_{ij} = l_{ij}$	in	in	out
$x_{ij} < l_{ij}$	out	out	out

Along with kilter states, *kilter numbers* are also defined. The kilter number of an arc is the minimal change in flow over that particular arc necessary to bring it to an in-kilter state. Arc kilter numbers are determined as:

	$\bar{c}_{ij} < 0$	$\bar{c}_{ij} = 0$	$\bar{c}_{ij} > 0$
$x_{ij} > u_{ij}$	$ x_{ij} - l_{ij} $	$ x_{ij} - u_{ij} $	$ x_{ij} - u_{ij} $
$x_{ij} = u_{ij}$	$ x_{ij} - l_{ij} $	0	0
$l_{ij} < x_{ij} < u_{ij}$	$ x_{ij} - l_{ij} $	0	$ x_{ij} - u_{ij} $
$x = l_{ij}$	0	0	$ x_{ij} - u_{ij} $
$x < l_{ij}$	$ x_{ij} - l_{ij} $	$ x_{ij} - l_{ij} $	$ x_{ij} - u_{ij} $

The following general steps list the strategy of the Out-of-Kilter Algorithm:

1. Begin with conserving flow (not necessarily feasible),  $x_{ij}=0$ , and a feasible solution to the dual,  $w_i=0$ . Determine kilter state of each arc and corresponding kilter number.
  2. If network has an out-of-kilter arc, conduct the primal of the algorithm. Out-of-Kilter arc is selected and an attempt is made to construct a new conserving flow in such a way that the kilter number of no arc is worsened and that of the selected arc is improved.
  3. When no improving flow can be constructed, the algorithm finds a new dual solution in such a way that no kilter number is worsened. Step #2 is repeated.
  4. Iterating between steps #2 and #3, the algorithm either finds an optimal solution or determines that no feasible solution exists.
- If an optimal solution exists, finite convergence is assured because there is a finite number of arcs and the kilter number of any arc is never allowed to increase. However, the kilter number of some arc is reduced at finite intervals (integer).

A labeling procedure has been developed for the solution of network problems via the Out-of-Kilter Algorithm. The following step-by-step process describes this node labeling solution technique.

1. Select a conserving flow;  $x_{ij}=0$ , and set dual variables  $w_i=0$ .
2. If all arcs are in-kilter, the optimal solution has been found, otherwise:
  - a. select an out-of-kilter arc  $(p,q)$ . If  $(p,q)$  is in a state where a flow increase,  $\Delta_{pq}$  is required, then set  $s=q$ ,  $t=p$  and label for node equals  $L(s)=(+t, \Delta_{pq})$
  - b. If  $(p,q)$  is in a state where a flow decrease,  $\Delta_{pq}$  is required, then set  $s=p$ ,  $t=q$  and  $L(s)=(-t, \Delta_{pq})$ .
3. If node  $i$  has a label, node  $j$  has no label, and flow may be increased by amount  $\Delta_{ij}$ ; assign node  $j$  label  $L(j)=(+i, \Delta_j)$  where  $\Delta_j = \text{minimum}\{\Delta_i, \Delta_{ij}\}$ . If node  $i$  has a label, and node  $j$  has no label and flow may be decreased by  $\Delta_{ji}$  along arc  $(j,i)$ , then give node  $j$  label  $L(j)=(-i, \Delta_j)$  where  $\Delta_j = \text{minimum}\{\Delta_i, \Delta_{ji}\}$ .

Repeat Step #3 until either node  $t$  is labeled (circulation), called *breakthrough* or no more nodes can be labeled, called *nonbreakthrough*.

If breakthrough, go to Step #4; if nonbreakthrough, go to step #5.

4. Flow change: let  $\Delta = \Delta_t$  and begin at node  $t$ . If  $L(t)=(+k,y)$ , then add  $\Delta$  to  $x_{kt}$ ; if  $L(t)=(-k,y)$ , then subtract  $\Delta$  from  $x_{ky}$ . Backtrack through cycle until node  $t$  is reached again.

Go to Step #2.

5. Dual phase: Divide labeled nodes and unlabeled nodes into sets  $X$  and  $\bar{X}$ , respectively.

a. Define  $S_1 = \{(i, j)\}$

where:

$i$  is an element of  $X$

$j$  is an element of  $\bar{X}$

$$\bar{c}_{ij} < 0$$

$$x_{ij} \leq u_{ij}$$

b. Define  $S_2 = \{(i, j)\}$

where:

$i$  is an element of  $\bar{X}$

$j$  is an element of  $X$

$$\bar{c}_{ij} > 0$$

$$x_{ij} \geq l_{ij}$$

If  $S_1 \cap S_2 = \emptyset$  (null set), stop; no feasible solution exists,

otherwise: let  $\theta = \text{minimum}\{|\bar{c}_{ij}|, \infty\}$  considering all  $(i, j)$  in

$S_1 \cap S_2$ .

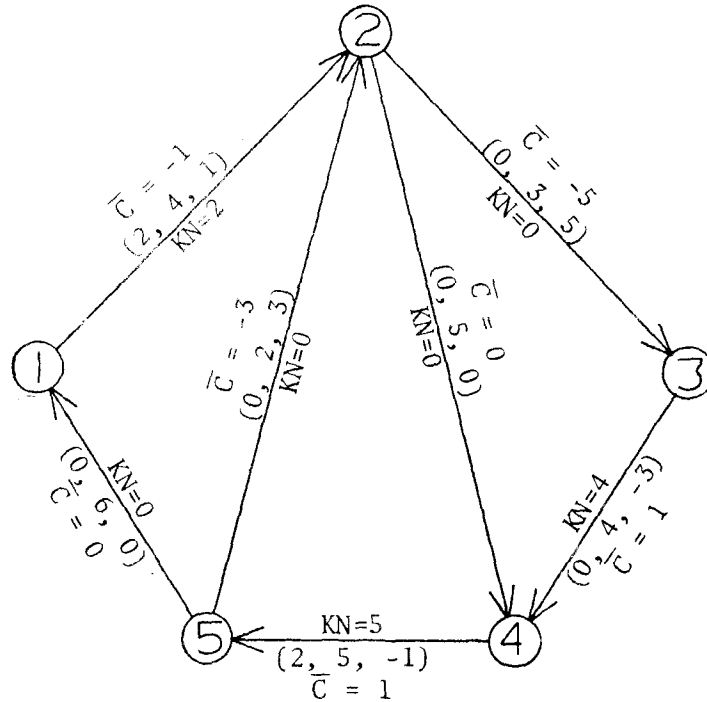
Change  $w_i$  according to:

$$w_i = \begin{cases} w_i + \theta & \text{if } i \in X \\ w_i & \text{if } i \in \bar{X} \end{cases}$$

Go to Step #2

Example hand calculation of solution to a network problem using the Out-of-Kilter Algorithm follows. The notation used for each arc;  $(l, u, c)$ , relates to the lower bound, upper bound, and arc cost. KN refers to kilter number.

EXAMPLE SOLUTION USING OUT-OF-KILTER ALGORITHM



STEP 1:  $\bar{c}_{ij} = w_i - w_j - c_{ij}$

$x_{ij} = 0$   
 $w_i = 0$  Initial solution

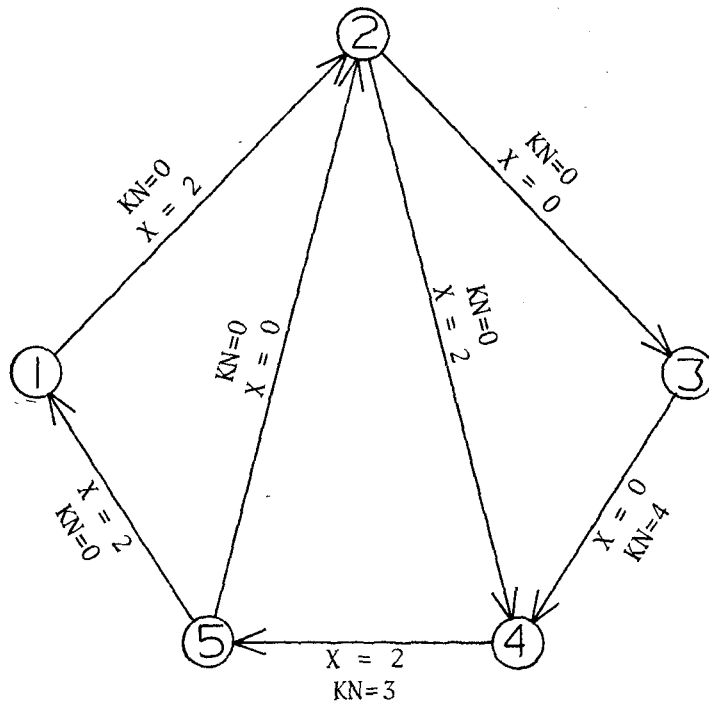
STEP 2: •  $(p, q) = (1, 2); s=2, t=1; L(2) = (+1, 2)$

STEP 3: •  $(i, j) = (2, 4); \Delta_{ij}=5; \text{Min}\{\Delta_i, \Delta_{ij}\} = \Delta_j = 2; L(4) = (+2, 2)$   
 •  $(i, j) = (4, 5); \Delta_{ij}=5; \text{Min}\{\Delta_i, \Delta_{ij}\} = \Delta_j = 2; L(5) = (+4, 2)$   
 •  $(i, j) = (5, 1); \Delta_{ij}=6; \text{Min}\{\Delta_i, \Delta_{ij}\} = \Delta_j = 2; L(1) = (+5, 2)$

BREAKTHROUGH

STEP 4: •  $\Delta_t = 2 = \Delta$   
 •  $x'_{51} = x_{51} + \Delta = 0 + 2 = 2$   
 •  $x'_{45} = x_{34} + \Delta = 0 + 2 = 2$   
 •  $x'_{24} = x_{24} + \Delta = 0 + 2 = 2$   
 •  $x'_{12} = x_{12} + \Delta = 0 + 2 = 2$





STEP 2:  $(p, q) = (3, 4)$ ;  $s=4$ ,  $t=3$ ;  $L(4) = (+3, 4)$

STEP 3:  $(i, j) = (4, 5)$ ;  $L(5) = (+4, 3)$

$(i, j) = (5, 1)$ ;  $L(1) = (+5, 3)$

$(i, j) = (4, 2)$ ; Added Reverse Flow;  $L(2) = (-4, 2)$

NON-BREAKTHROUGH, COULD NOT GET TO NODE 3

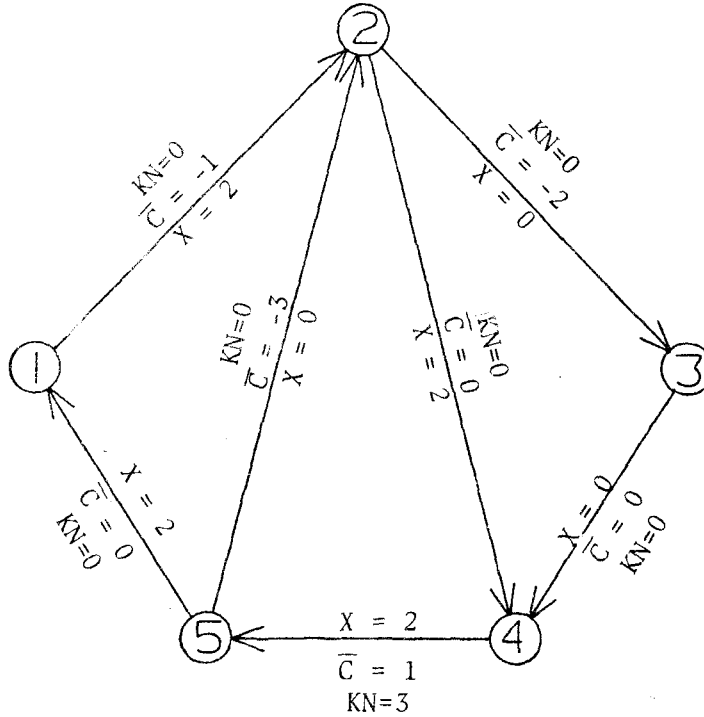
STEP 5:  $X = \{1, 2, 4, 5\}$   $\bar{X} = \{3\}$

$S_1 = \{(2, 3)\}$ ,  $S_2 = \{3, 4\}$

$\theta_1 = 5$ ,  $\theta_2 = 3$

$\theta = 3$

$w_1 = 3$ ;  $w_2 = 3$ ;  $w_3 = 0$ ;  $w_4 = 3$ ;  $w_5 = 3$



Compute new  $\bar{C}_{ij}$

STEP 2: •  $(p, q) = (4, 5)$ ;  $s=5$ ,  $t=4$ ;  $L(5) = (+4, 3)$

STEP 3: •  $L(1) = (+5, 3)$

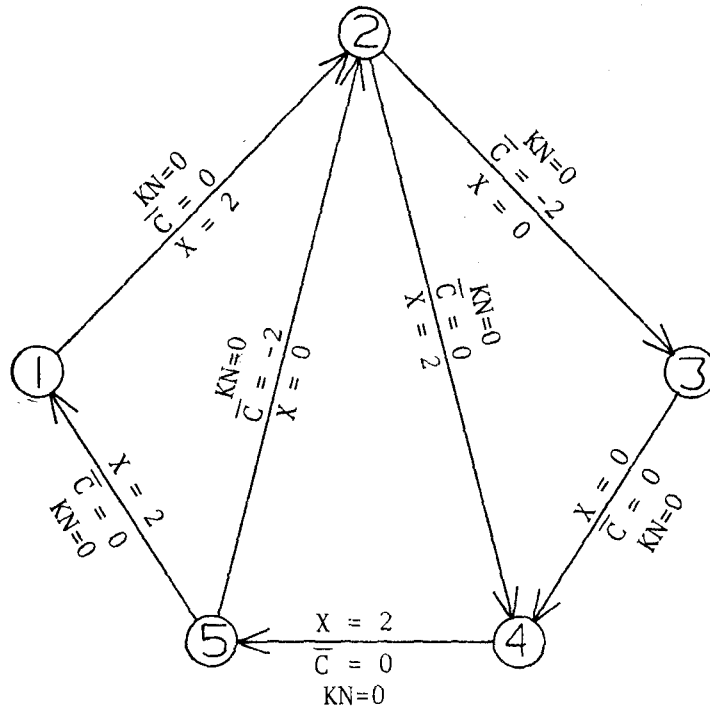
NON-BREAKTHROUGH

STEP 5:  $X = \{5, 1\}$ ,  $\bar{X} = \{2, 3, 4\}$

$S_1 = \{(5, 2), (1, 2)\}$ ,  $\theta_1 = 1$   $\theta = 1$

$S_2 = \{(4, 5)\}$ ,  $\theta_2 = 1$

$w_1 = 4$ ;  $w_2 = 3$ ;  $w_3 = 0$ ;  $w_4 = 3$ ;  $w_5 = 4$



- Compute new  $\bar{C}_{ij}$
- ALL ARCS ARE IN-KILTER, OPTIMAL SOLUTION HAS BEEN FOUND

APPENDIX B

SOURCE LISTING: PROGRAM ORGANZ

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PROGRAM ORGANIZ (INPUT, OUTPUT, TAPES, A, TAPE1-A)
DIMENSION TITLE(20), SP(30), RNAME(2), ACTAB(12,2), DEMR(12),
X DEMD(12), DIMP(12), JESVOL(30), OPRP(10), OPRR(12),
X CRAXU(12), ACTI(15), IDIVL(15), IRTL(15), IRTFF(15)
X INTEGER RCAP, RMIN, FSTART, SP, ACTAB, DEM, DEMR, OPRP, CMAX, CRIM, COST,
X CRAXU
PRINT 5
5 FORMAT (/24(1HX),32H P R O G R A M O R G A N I Z E .24(1HX)/)
PRINT 6
6 FORMAT (12X,5GHINTERACTIVE, CONVERSATIONAL DATA ORGANIZATION FOR M
XODSIN,/)
11 PRINT 12
12 FORMAT (1X,20HX BEGIN RECORD 1 XX,/)
15 FORMAT (4I)
C
C
C
      BEGIN RECORD 1
REIND 8
PRINTI, ARE CHANNEL LOSSES TO BE COMPUTED (YES OR NO)",
READ 15, ANS1
IF (ANS1.EQ.1HY) GO TO 40
LOPT=0
GO TO 45
40 LOPT=1
45 PRINTI, ECHO PRINT OF INPUT DATA (YES OR NO)",
READ 15, ANS2
IF (ANS2.EQ.1HY) GO TO 50
IOTT=0
GO TO 55
50 IOTT=1
55 PRINTI, SUMMARY OUTPUT (YES OR NO)",
READ 15, ANS3
ISUM=0
IF (ANS3.EQ.1HY) ISUM=1
IALLY=0
PRINTI, AVG., NET, DRY STATES TO BE COMPUTED (YES OR NO)",
READ 15, ANS35
IF (ANS35.EQ.1HY) IALLY=1
IRTN=0
PRINTI, IS RETURN FLOW TO BE CALCULATED (YES OR NO)",
READ 15, ANS36
IF (ANS36.EQ.1HY) IRTN=1
WRITE(8,60) LOPT, IOTT, ISUM, IALLY, IRTN
60 FORMAT('CONTROL OPTIONS',5I5)
PRINT 61
61 FORMAT (/1X,20HX BEGIN RECORD 2 XX,/)
C
C
C
      BEGIN RECORD 2
PRINTI, ENTER: UP TO 80 CHARACTER TITLE"
READ 62, (TITLE(I),I=1,20)
WRITE(8,62) (TITLE(I),I=1,20)
62 FORMAT (20A4)
PRINT 64
64 FORMAT (/1X,20HX BEGIN RECORD 3 XX,/)
C
C
C
      BEGIN RECORD 3

```



```

85 FORMAT (2A4)      ENTER: NETWORK NODE NO.'',
PRINTS, J
READS, J
IF (J.LE.NJ) GO TO 86
PRINTS, 'xERROR: MAXIMUM NO. OF NODES - ', NJ
GO TO 84
86 PRINTS, '      ENTER: MAXIMUM CAPACITY'',
READS, RCAP
PRINTS, '      ENTER: MINIMUM CAPACITY'',
READS, RMIN
PRINTS, '      ENTER: STARTING VOLUME'',
READS, FSTART
IF (FSTART.GE.RMIN.AND.FSTART.LE.RCAP) GO TO 84
PRINTS, 'xERROR: STARTING VOLUME IS OUTSIDE OF BOUNDS'
GO TO 86
94 WRITE(8,95) (RNAME(L),L=1,2),J,RCAP,RMIN,FSTART
95 FORMAT (2A4,2X,I5,3I10)
GO TO 129
100 PRINTS, 'FOR JUNCTION NO. ', I, ' ',
PRINTS, '      ENTER: UP TO 8 CHARACTER NAME'',
READ 85, (RNAME(L),L=1,2)
PRINTS, '      ENTER: NETWORK NODE NO.'',
READS, J
IF (J.LE.NJ) GO TO 110
PRINTS, 'xERROR: MAXIMUM NO. OF NODES - ', NJ
GO TO 100
110 RCAP=0
RMIN=0
FSTART=0
WRITE(8,95) (RNAME(L),L=1,2),J,RCAP,RMIN,FSTART
120 CONTINUE
121 PRINT 122
122 FORMAT (/1X,20H11 BEGIN RECORD 5 11,/)
C
C
C
      B E G I N   R E C O R D   5
PRINTS, 'ENTER: ', NS, ' SPILL NODE(S) IN ORDER OF PREFERENCE'',
READS, (SP(I),I=1,NS)
WRITE(8,130) (SP(I),I=1,NS)
130 FORMAT ('SPILLS',4X,I2I5)
131 PRINT 132
132 FORMAT (/1X,20H11 BEGIN RECORD 6 11,/)
C
C
C
      B E G I N   R E C O R D   6
PRINTS, 'ENTER: NO. OF AREA-CAPACITY POINTS PER RES.'',
READS, NPAIRS
IF (NPAIRS.LE.18) GO TO 133
PRINTS, 'xERROR: MAXIMUM NO. OF POINTS - 18'
GO TO 131
133 WRITE(8,134) NPAIRS
134 FORMAT ('NO. PAIRS',1X,I5)
DO 145 I=1,NPAIRS
PRINTS, 'FOR RESERVOIR NO. ', I, ' ',
DO 138 JJ=1,NPAIRS
PRINTS, '      ENTER: POINT ', JJ, ' [AREA-CAPACITY]'',
READS, (ACTAB(JJ,L),L=1,2)

```

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138 CONTINUE
140 WRITE(8,140) I,((ACTAB(K,L),L=1,2),K=1,NPAIRS)
140 FORMAT('AREA-CAP',2X,15,6110/(15X,6110))
145 CONTINUE
146 PRINT 147
147 FORMAT ('//1X,20H** BEGIN RECORD 7 **/')

C
C
C      B E G I N   R E C O R D   7

IF (IALLY.EQ.1) GO TO 190
PRINTX,'AUG., WET, AND DRY HYDROLOGIC STATES WILL BE COMPUTED.'
DO 185 I=1,ND
150 PRINTX,'FOR DEMAND NODE NO. ',I,'.'
PRINTX,'ENTER: NETWORK NODE NO.',
READI,MODED
PRINTX,' IS THIS A FLOW THRU DEMAND (YES OR NO)',
READ I5, ANS45
IDSTRM=0
IF (ANS45.EQ.14H) GO TO 151
PRINTX,'ENTER: NODE WHERE DEMAND ACCRUES',
READI, IDSTRM
151 PRINTX,'ENTER: PRIORITY FOR AVG. HYDROLOGIC STATE',
PRINTX,'ENTER: PRIORITY FOR DRY HYDROLOGIC STATE',
READI,DEMR(2)
PRINTX,'ENTER: PRIORITY FOR WET HYDROLOGIC STATE',
READI,DEMR(3)
PRINTX,' IS MONTHLY DEMAND TO BE INPUT VIA DATA FILE (YES OR
      * NO)',
READ I5, ANS5
IF (ANS5.EQ.14H) GO TO 170
PRINTX,'ENTER: TOTAL ANNUAL DEMAND',
READI,DEM
PRINTX,'ENTER: MONTHLY DISTRIBUTION',
READI,(DEMD(J),J=1,12)
170 DEM=0
DO 171 J=1,12
DEMD(J)=0.0
171 CONTINUE
178 WRITE(8,180) NODED, IDSTRM, DEM, (DEMR(K),K=1,3), (DEMD(J),J=1,12)
180 FORMAT ('DEMAND',1X,213,18,313,12F4.2)
185 CONTINUE
GO TO 230
190 PRINTX,'PRIORITY FOR EACH YEAR OF SIMULATION WILL BE INPUT'
DO 227 I=1,ND
195 PRINTX,'FOR DEMAND NODE NO. ',I,'.'
PRINTX,'ENTER: NETWORK NODE NO.',
READI,MODED
PRINTX,' IS THIS A FLOW THRU DEMAND (YES OR NO)',
READ I5, ANS46
IDSTRM=0
IF (ANS46.EQ.14H) GO TO 193
PRINTX,'ENTER: NODE NO. WHERE DEMAND ACCRUES',
READI, IDSTRM
193 DO 196 J=1,NYEAR
PRINTX,'ENTER: PRIORITY FOR SIMULATION YEAR ',J,
READI,DEMR(J)

```



```

196 CONTINUE
PRINTX, ' IS MONTHLY DEMAND TO BE INPUT VIA DATA FILE (YES OR
      NO) '
READ 15 ANSS
IF (ANSS.EQ.1MY) GO TO 210
PRINTX, ' ENTER: TOTAL ANNUAL DEMAND '
READI,DEM
PRINTX, ' ENTER: MONTHLY DISTRIBUTION '
READI,(DEMD(J),J=1,12)
210 DEM=0
DO 213 J=1,12
DEMD(J)=0.0
213 CONTINUE
215 WRITE(8,217) NODED,IDISTRN,DEM,(DEMD(J),J=1,12)
217 FORMAT ('DEMAND',1X,213,18,9X,12F4.2)
219 WRITE(8,219) NODED,(DEMD(J),J=1,12)
219 FORMAT ('RANK',6X,11I5)
227 CONTINUE
230 IF (1MY.EQ.0) GO TO 246
231 PRINT 232
232 FORMAT ('//1X,20H## BEGIN RECORD 8 ##,/')
      C
      C
      C BEGIN RECORD 8
DO 245 I=1,1MN
PRINTX, 'FOR IMPORT NODE NO. ',I,' '
PRINTX, ' ENTER: NETWORK NODE NO. ',
READI,IMP
WRITE(8,233) IMP
233 FORMAT ('IMPORT',4X,15)
DO 2455 N=1,MYEAR
PRINTX, 'FOR SIMULATION YEAR NO. ',N
PRINTX, ' ENTER: TOTAL ANNUAL IMPORT ',
READI,IMPRT
PRINTX, ' ENTER: MONTHLY DISTRIBUTION '
READI,(DIMP(J),J=1,12)
240 WRITE(8,240) N,IMPRT,(DIMP(J),J=1,12)
240 FORMAT ('YEAR',2X,12,12X,110,12F4.3)
245 CONTINUE
GO TO 248
246 WRITE(8,247)
247 FORMAT ('IMPORT',8X,0')
248 IF (1ALLY.EQ.1) GO TO 260
249 PRINT 2495
2495 FORMAT ('//1X,20H## BEGIN RECORD 9 ##,/')
      C
      C
      C BEGIN RECORD 9
PRINTX, 'ENTER: NO. OF RESERVOIRS IN SUBSYSTEM',
READI,NSRS
PRINTX, 'ENTER: NETWORK NODE NO. OF RESERVOIRS IN SUBSYSTEM',
READI,(RESVOL(I),I=1,NSRS)
PRINTX, 'ENTER: FRACTION FOR AVERAGE LOW AND AVERAGE HIGH',
READI,AUGLO,AUGHI
250 WRITE(8,250) NSRS,(RESVOL(J),J=1,NSRS)
250 FORMAT ('SUBSYSTEM',1X,14I5)

```

```

WRITE(8,255) AUGLO,AUGHI
FORMAT ('AVERAGE ST',2(SX,F5.3))
260 PRINT 262
262 FORMAT (/1X,21H33 BEGIN RECORD 10 11,/)
C
C
      B E G I N   R E C O R D 10
PRINT*,ARE CONVERSION FACTORS NECESSARY (YES OR NO)*,
READ 15,AMS7
IF (AMS7.EQ.11H) GO TO 265
CONINF=0.0
CONDEM=0.0
CONFLO=0.0
GO TO 270
265 PRINT*,ENTER: CONVERSION FOR LINK CAPACITIES TO STORAGE UNITS*,
READ1,CONFLO
PRINT*,ENTER: CONVERSION FOR INFLOWS TO STORAGE UNITS*,
READ1,CONINF
PRINT*,ENTER: CONVERSION FOR DEMANDS TO STORAGE UNITS*,
READ1,CONDEM
270 WRITE(8,275) CONFLO,CONINF,CONDEM
275 FORMAT ('FACTORS',3X,3(SX,F5.3))
276 PRINT 277
277 FORMAT (/1X,21H33 BEGIN RECORD 11 11,/)
C
C
      B E G I N   R E C O R D 11
IF (IALLY.EQ.1) GO TO 315
DO 310 I=1,NRES
PRINT*,FOR RESERVOIR NO. ',I,',
PRINT*,ENTER: PRIORITY FOR AUG. HYDROLOGIC STATE*,
READ1,OPRR(1)
PRINT*,ENTER: DESIRED MONTHLY DISTRIBUTION*
READ1,(OPRR(J),J=1,12)
WRITE(8,285) I,OPRR(1),(OPRR(J),J=1,12)
285 FORMAT(: RESERVOIR',15,10X,15,12F4.2)
PRINT*,ENTER: PRIORITY FOR DRY HYDROLOGIC STATE*,
READ1,OPRR(2)
PRINT*,ENTER: DESIRED MONTHLY DISTRIBUTION*
READ1,(OPRR(J),J=1,12)
WRITE(8,295) I,OPRR(2),(OPRR(J),J=1,12)
295 FORMAT(: OPERATING',15,10X,15,12F4.2)
PRINT*,ENTER: PRIORITY FOR WET HYDROLOGIC STATE*,
READ1,OPRR(3)
PRINT*,ENTER: DESIRED MONTHLY DISTRIBUTION*
READ1,(OPRR(J),J=1,12)
WRITE(8,305) I,OPRR(3),(OPRR(J),J=1,12)
305 FORMAT(: RULES ',15,10X,15,12F4.2)
310 CONTINUE
GO TO 336
315 DO 335 I=1,NRES
PRINT*,FOR RESERVOIR NO. ',I,',
DO 330 J=1,MYEAR
PRINT*,ENTER: PRIORITY FOR SIMULATION YEAR ',J',
READ1,OPRR(J)
PRINT*,ENTER: MONTHLY DESIRED DISTRIBUTION*
READ1,(OPRR(L),L=1,12)

```

```

335 WRITE(8,325) I,OPPR(J),(OPPR(L),L=1,12)
336 FORMAT('ANNUAL OPR',15,10X,15,12F4.2)
339 CONTINUE
335 CONTINUE
336 PRINT 337
337 FORMAT ('//1X,21HEX BEGIN RECORD 12 XX,/')
C
C
C
      B E G I N   R E C O R D   12
PRINT*,ENTER: NO. OF LINKS WITH VARIABLE CAPACITY*.
READS,NUMAKL
WRITE(8,338) NUMAKL
338 FORMAT('NUMAKLS',3X,15)
IF (NUMAKL) 339,347,339
339 DO 345 I=1,NUMAKL
PRINT*,FOR VARIABLE CAPACITY LINK NO. ',I,';'
PRINT*,ENTER: NETWORK LINK NO.,'
READS,LINK
PRINT*,LINK
ENTER: MINIMUM CAPACITY*.
READS,CRIN
PRINT*,CRIN
ENTER: ORIGIN NODE NO.,'
READS,LF
PRINT*,LF
ENTER: TERMINATION NODE NO.,'
READS,LT
XLCF=0.0
IF (LOPT) 341,342,341
341 PRINT*,ENTER: LOSS COEFFICIENT',
READS,XLCF
342 PRINT*,ENTER: UNIT COST',
READS,COST
PRINT*,ENTER: MAXIMUM CAPACITY FOR EACH MONTH'
READS,CMAX(J),J=1,12)
WRITE(8,344) LINK,NUMAKL,CRIN,XLCF,COST
344 FORMAT ('LINK',6X,315,10X,F10.8,15)
WRITE(8,345) (CMAX(J),J=1,12)
345 FORMAT ('CMAXU',3X,12I6)
346 CONTINUE
347 NULL=NULL-NUMAKL
IF (NULL.EQ.0) GO TO 361
PRINT*,ENTER: REMAINING LINKAGE CONFIGURATION*
DO 350 I=1,NULL
PRINT*,ENTER: NETWORK LINK NO.,'
READS,LINK
PRINT*,LINK
ENTER: MAXIMUM CAPACITY*,
READS,CMAX
PRINT*,CMAX
ENTER: MINIMUM CAPACITY*,
READS,CRIN
PRINT*,CRIN
ENTER: ORIGIN NODE NO.,'
READS,LF
PRINT*,LF
ENTER: TERMINATION NODE NO.,'
READS,LT
IF (LOPT.EQ.1) GO TO 349
XLCF=0.0
GO TO 350
349 PRINT*,ENTER: LOSS COEFFICIENT',
READS,XLCF
350 PRINT*,ENTER: UNIT COST',

```

```

READI,COST
WRITE(8,355) LINK,LF,LT,CMAX,CHIN,XLCF,COST
355 FORMAT('LINK',6X,315,210,F10.8,15)
360 CONTINUE
361 IF (IRTH.EQ.0) GO TO 397
C
C
C      B E G I N   R E C O R D   13
362 PRINT 362
FORMAT (//1X,21HX BEGIN RECORD 13 //,/)
PRINTI,ENTER: NO. OF RETURN FLOW EQUATIONS*,
READI,NEQU
PRINTI,ENTER: NO. OF TIME PERIODS TO BE LAGGED*,
READI,NLAGS
WRITE(8,363) NEQU,NLAGS
363 FORMAT ('NEQU,NLAGS',215)
LAGS=24NLAGS*2
DO 385 I=1,NEQU
PRINTI,FOR RETURN FLOW EQU. NO. 'I',
PRINTI,ENTER: NO. OF NODES CONTRIBUTING TO RTFLOW*,
READI,NDNEQU
PRINTI,ENTER: NODE NO. WHERE FLOW RETURNS*,
READI,JRTFT
PRINTI,ENTER: NODES WHICH CONTRIBUTE TO RTFLOW*,
READI,(IRTF(J),J=1,NDNEQU)
PRINTI,ENTER: REGRESSION COEF. BEGINNING WITH*,
PRINTI,THE CONSTANT TERM, FOLLOWED BY DITCH*,
PRINTI,DIVERSIONS, FOLLOWED BY RETURN FLOWS*,
PRINTI,EXAMPLE FOR 1 MONTH LAG*,
PRINTI,A1+2RD(T)+3RD(T-1)+44RD(T-1)
READI,(A(J),J=1,LAGS)
WRITE(8,365) (A(J),J=1,LAGS)
365 FORMAT (8G10.4)
WRITE(8,366) NDNEQU,JRTFT
366 FORMAT ('EQU',2X,215)
367 FORMAT ('EQU',2X,1515)
367 PRINT 369
369 FORMAT (/)
PRINTI,FOR INITIAL CALCULATIONS ENTER:
DO 370 K=1,NLAGS
PRINTI,TOTAL DITCH DIVERSION AND TOTAL RETURN*
PRINTI,FLOW OBSERVED FOR TIME PERIOD ZERO MINUS*,
PRINTI,K,
READI,IDIUL(K),IRTL(K)
370 CONTINUE
WRITE(8,371) ((IDIUL(K),IRTL(K)),K=1,NLAGS)
371 FORMAT ('LAGS',1X,1216)
385 CONTINUE
C
C
C      F I L E   N A M E
397 REWIND 8
398 PRINT 398
398 FORMAT (//)
399 REWIND 1
399 PRINTI,SAVE FILE AS PERMANENT FILE (YES OR NO)*,

```

```
READ 15, ANS8
IF (ANS8.EQ.IHM) GO TO 999
PRINTX, 'ENTER: UP TO 7 CHARACTER FILE NAME'.
READ 400, FILM
FORMAT (A7)
WRITE (1,410) FILM
410 FORMAT ('COPY TAPES',A7,')
WRITE (1,420) FILM
420 FORMAT ('REWIND',A7,')
WRITE (1,430) FILM
430 FORMAT ('REPLACE',A7,')
PRINTX, 'IS A LISTING REQUIRED (YES OR NO)'.
READ 15, ANS9
IF (ANS9.EQ.IHM) GO TO 999
WRITE (1,440) FILM
440 FORMAT ('COPY',A7, '.OUTPUT.').
999 STOP
END
```

APPENDIX C

SOURCE LISTING: PROGRAM ADATA

```

PROGRAM ADATA (INPUT-65,OUTPUT,TAPE10,TAPE11,B,TAPE2-B)
DIMENSION IDEM(40),IFLO(40),IEUAP(40)
DIMENSION FLOW(20,40,12),DEMD(20,40,12),EUAP(20,20,12)
DATA FLOW/360000.0/,DEMD/360000.0/,EUAP/480000.0/
REWIND 10
REWIND 11
PRINT 1
1 FORMAT (/,27(1H2),26H P R O G R A M A D A T A ,27(1H2),//)
PRINT 2
2 FORMAT (10X,57HINARY INFLOW, DEMAND, AND EUAP. FILE CREATION FOR
XMODSIM,/)
PRINTX,ENTER: TOTAL NO. OF NODES',
READX,NJ
PRINTX,ENTER: TOTAL NO. OF RESERVOIRS',
READX,NRES
PRINTX,ENTER: NO. OF YEARS TO BE SIMULATED',
READX,NYEAR
PRINTX,
PRINTX,ENTER: NO. OF DEMAND NODES',
READX,NDEM
PRINTX,ENTER: MODE NO. OF EACH DEMAND NODE'
READX,(IDEM(J),J=1,NDEM)
PRINTX,
PRINTX,ENTER: NO. OF NODES WHERE UNREGULATED INFLOW OCCURS',
READX,NUREG
PRINTX,ENTER: MODE NO. OF EACH UNREG. INFLOW NODE'
READX,(IFLO(J),J=1,NUREG)
PRINTX,
PRINTX,ENTER: NO. OF RESERVOIRS WITH EUAP. > 0',
READX,NEUAP
PRINTX,ENTER: MODE NO. OF RESERVOIRS WITH EUAP. > 0'
READX,(IEUAP(J),J=1,NEUAP)
10 DO 100 IY=1,NYEAR
DO 90 JU=1,NJ
IF (NUREG.EQ.0) GO TO 20
DO 15 KK=1,NUREG
IF (JU.NE.IFLO(KK)) GO TO 15
PRINTX,ENTER: MONTHLY INFLOWS FOR NODE ',JU,' YEAR ',IY
READX,(FLOW(IY,JU,K),K=1,12)
PRINTX,
15 CONTINUE
20 IF (NDEM.EQ.0) GO TO 30
DO 25 KK=1,NDEM
IF (JU.NE.IDEM(KK)) GO TO 25
PRINTX,ENTER: MONTHLY DEMANDS FOR NODE ',JU,' YEAR ',IY
READX,(DEMD(IY,JU,K),K=1,12)
PRINTX,
25 CONTINUE
30 IF (NEUAP.EQ.0) GO TO 90
DO 35 KK=1,NEUAP
IF (JU.NE.IEUAP(KK)) GO TO 35
PRINTX,ENTER: MONTHLY EUAP. RATES FOR RES. NO. ',JU,' YEAR ',IY
READX,(EUAP(IY,JU,K),K=1,12)
PRINTX,
35 CONTINUE
90 CONTINUE

```

```

WRITE(10) ((FLOW(I,J,K),K-1,12),J-1,NJ),
* ((DEMD(I,J,K),K-1,12),J-1,NJ),
* ((LEUP(I,J,K),K-1,12),J-1,NRES)
WRITE(11,115) ((FLOW(I,J,K),K-1,12),J-1,NJ),
* ((DEMD(I,J,K),K-1,12),J-1,NJ)
115 FORMAT (6F12.0)
WRITE(11,116) ((LEUP(I,J,K),K-1,12),J-1,NRES)
116 FORMAT (6F12.4)
100 CONTINUE
REWIND 10
REWIND 11
PRINT*,ENTER: UP TO 7 CHARACTER PFN FOR BINARY FILE*,
READ 101, INAM
101 FORMAT (A7)
WRITE(2,102) INAM
102 FORMAT ('REPLACE,TAPE10-',A7,'.')
PRINT*,SAVE COPY OF CODED DATA FILE ALSO (YES OR NO)*,
READ 130, ANS0
IF (ANS0.EQ.1HN) GO TO 119
PRINT*,ENTER: UP TO 7 CHARACTER PFN FOR CODED FILE*,
READ 107, INAM
107 FORMAT (A7)
WRITE(2,108) INAM
108 FORMAT ('REPLACE,TAPE11-',A7,'.')
119 REWIND 2
PRINT 120
120 FORMAT ('//IX,27HJOB SUCCESSFULLY COMPLETED.')
PRINT*,PRINT-OUT OF DATA FILE (YES OR NO)*,
READ 130, ANS
130 FORMAT (A1)
IF (ANS.EQ.1HN) GO TO 999
PRINT 140
140 FORMAT ('//IX,4HFLOU,/')
PRINT 145, ((FLOW(I,J,K),K-1,12),J-1,NJ),I-1,NYEAR)
145 FORMAT (2X,I3,5X,12F7.0)
PRINT 150
150 FORMAT ('//IX,6HDEMAND,/')
PRINT 145, ((J,DEMD(I,J,K),K-1,12),J-1,NJ),I-1,NYEAR)
PRINT 160
160 FORMAT ('//IX,11HEVAPORATION,/')
PRINT 165, ((J,LEUP(I,J,K),K-1,12),J-1,NRES),I-1,NYEAR)
165 FORMAT (2X,I3,5X,12F7.3)
999 STOP
END

```



APPENDIX D

SOURCE LISTING: PROGRAM MODSIM

```

1  PROGRAM MODSIM
   1(INPUT-65,OUTPUT-65,TAPES-INPUT,TAPES-OUTPUT,TAPE10,TAPE15)
   C
   C
5  *****
   C
   C
10  PROGRAM MODSIM - RIVER BASIN SIMULATION PACKAGE
   C ORIGINAL DEVELOPMENT - CARLOS FLEKTES
   C SYSTEMS ENGINEERING DIVISION, TEXAS WATER DEVELOPMENT BOARD
   C MARCH 1972
   C MODIFICATIONS - JOHN R. SHAFER
   C COLORADO STATE UNIVERSITY
   C 1978-1979
   C
15  *****
   C
   C COMMON /CONTROL/ KIN , KOUT , KAPE1 ,
   C KAPE4
   C
   C COMMON /IPRINT/ IPRINT , IYLD , ITOY ,
   C IFRON
   C
20  COMMON /LDATA/ XLCF(50) , XCLL(50,12) , LOFT ,
   C TOL , IALLY , IRTN
   C
   C DATA KIN,KOUT,KAPE1,KAPE4/5.6,10.15/
   C
25  REWIND KAPE4
   C
   C CONTROL OPTIONS:
   C IF: LOFT-1, CHANNEL LOSSES WILL BE CONSIDERED
   C IOTT-1, ECHO PRINT OF INPUT DATA
   C ISUM-1, SUMMARY OUTPUT
   C IALLY-1, INPUT PRIORITY FOR EACH YEAR
   C IRTN-1, RETURN FLOW WILL BE CALCULATED
35  READ (KIN,100) LOFT,IOTT,ISUM,ially,IRTN
   C
   C 100 FORMAT (15X,5I5)
   C
   C STEP 02
   C CALL INPUT AND OUTPUT SUBROUTINES
   C TO READ AND PRINT INPUT VARIABLES
40  CALL CARDS
   C IF (IOTT.EQ.1) CALL OUTI
   C
   C STEP 03
   C BUILD NETWORK AND OPERATE SYSTER
45  CALL SETNET
   C CALL OPRTATE
   C
   C STEP 04
   C CALL SUMMARIES PRINT ROUTINES
50  *****
   C
   C

```

```

MOD 0010
MOD 0020
MOD 0030
MOD 0040
MOD 0050
MOD 0060
MOD 0070
MOD 0080
MOD 0090
MOD 0100
MOD 0110
MOD 0120
MOD 0130
MOD 0140
MOD 0150
MOD 0160
MOD 0170
MOD 0180
MOD 0190
MOD 0200
MOD 0210
MOD 0220
MOD 0230
MOD 0240
MOD 0250
MOD 0260
MOD 0270
MOD 0280
MOD 0290
MOD 0300
MOD 0310
MOD 0320
MOD 0330
MOD 0340
MOD 0350
MOD 0360
MOD 0370
MOD 0380
MOD 0390
MOD 0400
MOD 0410
MOD 0420
MOD 0430
MOD 0440
MOD 0450
MOD 0460
MOD 0470
MOD 0480
MOD 0490
MOD 0500
MOD 0510
MOD 0520
MOD 0530
MOD 0540

```

```

55      C      IF (ISUM.EQ.1) CALL OUT3
56      C      REJIND KAPE4
57      C      END
58      C      SUBROUTINE ADJUST 73/73 OPT-2 TRACE
59      C      FTM 4.6+452
60      C      79/05/10. 13.11.59
61      C
62      C      SUBROUTINE ADJUST (IV,IQUIT,ICNT)
63      C      INTEGER
64      C      RCAP
65      C      ,ACTAB
66      C      ,SP
67      C      ,KIN
68      C      ,KOUT
69      C      ,IVLD
70      C      ,IPRNT
71      C      ,NJ
72      C      ,MRES
73      C      ,NYEAR
74      C      ,INM
75      C      ,RYIN
76      C      ,DENR
77      C      ,KAPE1
78      C      ,ITOV
79      C      ,NJUNC
80      C      ,ND
81      C      ,TITLE(20)
82      C      ,TOTLS(40,20,12)
83      C      ,RYIN(40)
84      C      ,OPRR(20,10,12)
85      C      ,DEMR(40,12)
86      C      ,DIRP(2,12,20)
87      C      ,ICAP(40,12,13)
88      C      ,RYARE(40,2)
89      C      ,RCAP(40)
90      C      ,ACTAB(10,18,2)
91      C      ,SP(10)
92      C      ,DENR(40)
93      C      ,UI(40,12)
94      C      ,IMP(2)
95      C      ,INPR(2,20)
96      C      ,AURGLD
97      C      ,AURCHI
98      C      ,CONFLD
99      C      ,CONFIN
100     C      ,CPCT
101     C      ,JESVLD(10)
102     C      ,LRULE
103     C      ,KOUT(100)
104     C      ,TITLE,IYLD,RYARE(IYLD,I),I = 1,2
105     C      ,ADJ 0230
106     C      100 FORMAT (1H1//20X,20A4//10X,3A0) DETERMINE FIRM YIELD OF RESERVOIR ,ADJ 0240
107     C      12,2X,2A4//10X,9H ITERATION,2X,4MYEAR,2X,10HOLD DEMAND,2X,10H SHORTADJ 0250
108     C      PAGE,2X,10HNEW DEMAND,2X,20HSHORT./DEMAND RATIO )
109     C      ISHTA = 0
110     C      JN = IYLD
111     C      IYD = 1
112     C
113     C      PCT = 0.0
114     C      DO 110 IKY = 1,MYEAR
115     C      ITSHT = 0
116     C      ITSHT = TOTLS(JN,IKY,8)
117     C      IF (ISHTA.GT.ITSHT) GO TO 110
118     C      IYD = IKY
119     C      ISHTA = ITSHT
120     C
121     C      STEP 01
122     C      DETERMINE GREATEST YEARLY SHORTAGE
123     C      AND YEAR INCURRED
124     C
125     C      STEP 02
126     C      IF SHORTAGE IS ZERO INCREMENT DEMAND
127     C      BY 10 PERCENT
128     C
129     C      110 CONTINUE
130     C      IF (ISHTA.EQ.0) NUMRD = FLOAT(DEN(JN)) * 1.1
131     C
132     C      MOD 0550
133     C      MOD 0560
134     C      MOD 0570
135     C      MOD 0580
136     C      MOD 0590
137     C      79/05/10. 13.11.59
138     C      ADJ 0010
139     C      ADJ 0020
140     C      ADJ 0030
141     C      ADJ 0040
142     C      ADJ 0050
143     C      ADJ 0060
144     C      ADJ 0070
145     C      ADJ 0080
146     C      ADJ 0090
147     C      ADJ 0100
148     C      ADJ 0110
149     C      ADJ 0120
150     C      ADJ 0130
151     C      ADJ 0140
152     C      ADJ 0150
153     C      ADJ 0160
154     C      ADJ 0170
155     C      ADJ 0180
156     C      ADJ 0190
157     C      ADJ 0200
158     C      ADJ 0210
159     C      ADJ 0220
160     C      ADJ 0230
161     C      ADJ 0240
162     C      ADJ 0250
163     C      ADJ 0260
164     C      ADJ 0270
165     C      ADJ 0280
166     C      ADJ 0290
167     C      ADJ 0300
168     C      ADJ 0310
169     C      ADJ 0320
170     C      ADJ 0330
171     C      ADJ 0340
172     C      ADJ 0350
173     C      ADJ 0360
174     C      ADJ 0370
175     C      ADJ 0380
176     C      ADJ 0390
177     C      ADJ 0400
178     C      ADJ 0410
179     C      ADJ 0420
180     C      ADJ 0430
181     C      ADJ 0440
182     C      ADJ 0450
183     C      ADJ 0460
184     C      ADJ 0470
185     C      ADJ 0480
186     C      ADJ 0490
187     C      ADJ 0500

```

```

50 C STEP 03 ADJ 0500
    C IF SHORTAGE GREATER THAN 0, DECREASE
    C ANNUAL DEMAND BY THE RATIO SHORTAGES/YEAR ADJ 0510
    C ADJ 0520
    C ADJ 0530
    C ADJ 0540
    C ADJ 0550
    C ADJ 0560
    C ADJ 0570
    C ADJ 0580
    C ADJ 0590
    C ADJ 0600

    IF (ISHTA.EQ.0) GO TO 120
    PCT = FLOAT(ISHTA)/FLOAT(DEM(JN))
    IF (PCT.LE.CPCT) IQUIT = 0
    IF (PCT.LE.0.01) IQUIT = 0
    NUDDMD = DEM(JN) - (ISHTA * PCT * 100.0)/IVD
    NUDDMD = DEM(JN) - ISHTA/IVD

60 C

    STEP 04 ADJ 0610
    C IF ITERATIONS GREATER THAN 20 OR SHORTAGE
    C LESS THAN CPCT - QUIT- ADJ 0620
    C ADJ 0630
    C ADJ 0640
    C ADJ 0650
    C ADJ 0660
    C ADJ 0670
    C ADJ 0680
    C ADJ 0690
    C ADJ 0700
    C ADJ 0710
    C ADJ 0720
    C ADJ 0730
    C FTN 4.6+452 79/05/10. 13.11.59

65 C 120 CONTINUE
    ICNT = ICNT + 1
    IF (ICNT.GT.20) IQUIT = 0
    WRITE (KOUT,130) ICNT,IVD,DEM(JN),ISHTA,NUDDMD,PCT
130 FORMAT (14X,12,6X,13,3I12,F12.3)
    DEM(JN) = NUDDMD
    RETURN

70 C

SUBROUTINE AREA 73/73 OPT=2 TRACE FTN 4.6+452

1 1 SUBROUTINE AREA (X,Y,J) ARE 0010
  1 INTEGER CMAXV RCAP ARE 0020
  2 OPKP ARE 0030
  2 OPKP OPKP SP ARE 0040
  1 INTEGER UREG START ISHTA USE ARE 0050
  2 EUPT APMX ARE 0060
  1 INTEGER /CONTRL/ X KOUT Y ARE 0070
  1 COMMON /KAP4/ KIN ARE 0080
  1 COMMON /IPRNT/ IPRNT ARE 0090
  1 COMMON /PARR/ NJ ARE 0100
  2 ML NC ARE 0110
  2 NS IYEAR ARE 0120
  3 NR NPAIRS ARE 0130
  1 COMMON /RESU/ RNAME(40,2) RCAP(40) ARE 0140
  2 FSTART(40) ACTAB(10,10,2) ARE 0150
  1 OPKP(20,10) SP(10) DER(40) ARE 0160
  3 EUWP(10,12) U(40,12) IMP(2) ARE 0170
  4 DEPR(40,20) IMPRT(2,20) ARE 0180
  1 COMMON /WRKD/ START(40) STEND(40) USE(40) ARE 0190
  2 UREG(40) ISHTA(40,13) ISPIL(40,13) AREAX(40) ARE 0200
  2 EUPT(40) APMX(40) ANIN(40) IAREA(40) ARE 0210
  2 ROFF = .499 ARE 0220
  2 ARE 0230
  2 ARE 0240
  2 ARE 0250
  2 ARE 0260
  2 ARE 0270
  2 ARE 0280

    STEP 01
    BASED ON RES UOL DETERMINE AREA

```



```

35      LNKFL0(L,MON) = FLOW(L)/CONFLO
        XCLL(L,MON) = FLOAT(LNKFL0(L,MON)) * XLCF(L)
        NN = LMODE(L,2)
        IUSE(NN) = IUSE(NN) + IFIX(XCLL(L,MON))
        TLOSS1 = TLOSS1 + XCLL(L,MON)
110     CONTINUE
        DO 120 J = 1,NJ
            IUSE(J) = IUSE(J) + USE(J)
120     CONTINUE
        TDIFF = ABS(TLOSS1 - TLOSS2)
        IF (TDIFF.LE.TOL) GO TO 160
        IF (ITER.GE.ITERMX) GO TO 140
        TLOSS2 = TLOSS1
        MAXD = 0
        DO 130 L = L7,L8
            JN = NF(L)
            HI(L) = IUSE(JN)
            MAXD = MAXD + HI(L)
130     CONTINUE
        GO TO 170
140     WRITE (KOUT,150) MON,IV
150     FORMAT (140,7#E15.5,2#CHANNEL LOSS FUNCTION WOULD NOT CONVERGE TO
        15#SPECIFIED TOLERANCE,2X,7#MONTH -,12,2X,6#YEAR -,13)
160     IDONE = 1
170     DO 180 L = 1,ML
        LNKFL0(L,MON) = 0
180     CONTINUE

```

CHN 0340  
 CHN 0350  
 CHN 0360  
 CHN 0370  
 CHN 0380  
 CHN 0390  
 CHN 0400  
 CHN 0410  
 CHN 0420  
 CHN 0430  
 CHN 0440  
 CHN 0450  
 CHN 0460  
 CHN 0470  
 CHN 0480  
 CHN 0490  
 CHN 0500  
 CHN 0510  
 CHN 0520  
 CHN 0530  
 CHN 0540  
 CHN 0550  
 CHN 0560  
 CHN 0570  
 CHN 0580  
 CHN 0590  
 CHN 0600

```

RETURN
END
SUBROUTINE CARDS 73/73 OPT=2 TRACE FTN 4.6+452 79/05/10. 13.11.59
1      SUBROUTINE CARDS
    INTEGER
1      CRAXU
2      OPREP
3      COST
    COMMON /CONTROL/
1      KAPE4
    COMMON /IPRINT/
1      IPRINT
    COMMON /PHARM/
1      MS
2      NS
3      NR
    COMMON /RESU/
1      FSTART(40)
2      ACTAB(10,18,2)
3      EUMP(10,12)
4      BCTR(40,20)
    COMMON /LINE/
    COMMON /CONF AC/
1      AURGL0
2      LABLE
    COMMON /LDATE/
        RCAP
        ACTAB
        SP
        KIN
        IPRNT
        NJ
        NC
        IYEAR
        NPAIRS
        RNAME(40,2)
        ACTAB(10,18,2)
        SP(10)
        U(40,12)
        IIMP(2)
        IPRNT(2,20)
        LMODE(50,2)
        AURGL0
        CONINE
        JESVOL(10)
        XLCF(50)
        RRIN
        DEN
        CRAN
        KOUT
        IYLD
        NRES
        MYEAR
        IIN
        RCAP(40)
        DEN(40)
        IIMP(2)
        CRAX(50)
        AURGH1
        CPCT
        XCLL(50,12)
        FSTART
        DENR
        CRIN
        KAPE1
        ITOY
        NJUNC
        MD
        TITLE(20)
        RRIN(40)
        OPREP(20,10,12)
        DEN(40)
        IIMP(2,12,20)
        CRIN(50)
        CONFLO
        MSRS
        LOPT

```

CHN 0610  
 CHN 0620  
 CHN 0630  
 CHN 0640  
 CHN 0650  
 CHN 0660  
 CHN 0670  
 CHN 0680  
 CHN 0690  
 CHN 0700  
 CHN 0710  
 CHN 0720  
 CHN 0730  
 CHN 0740  
 CHN 0750  
 CHN 0760  
 CHN 0770  
 CHN 0780  
 CHN 0790

```

25      TOL      , IALLY      , IRTH      , A(10,15)
      /RI/      , MEQU      , NLAGS     , INTF(10,240)
      NDNEQU(10), IRTF(10,15), IRTH(10), INTF(10,240)
2  IDIUL(10,15), IRTH(10,15)
      /D/      , MOND(40)  , ITHRU(40)
1  NPARL      , LUAR(50)  , CHANU(50,12)
      /ADATA/  , NPARC     , NMAX
      /ADATA/  , MT(500)   , FESIBL
2  LO(500)   , FLOU(500) , HI(500)
DO 110 J = 1, NJ
DO 100 K = 1, 20
DEPR(J,K) = 99
OPRP(K,J) = 99
100 CONTINUE
110 IDSTR(J) = 0
C
C          STEP 01
C          READ FILE A CARDS
C
45      READ (KIN,120) (TITLE(I), I = 1,20)
      IF (EOF(KIN)) 500,130,500
120 FORMAT (20A4)
C
130 READ (KIN,140) NJ, NRES, PL, IS, MYEAR, MO, MS, IYEAR, IPR, IVLD, IFRM, I700,
      I800, I900
C
140 FORMAT (19X,12I5,4X,1I,5F,9)
      IF (CPCT.LE.0.0) CPCT = 0.10
C
      IFRM = IFRM
      NC = NL - NR
C
C          STEP 02
C          READ FILE B CARDS
C
      DO 150 I = 1, NJ
150 READ (KIN,160) J, (RNAME(J,K), K = 1,2), RCOMP(J), RPTIM(J), FSTART(J)
SUBROUTINE CARDS
      160 FORMAT (T11,I5,T1,20A4,T16,3I10)
C
C          STEP 03
C          READ FILE C CARDS
C
      READ (KIN,170) (SP(I), I = 1, NS)
170 FORMAT (10X,12I5)
C
C          STEP 04
C          READ FILE D CARDS
C
      READ (KIN,180) NPAIRS
180 FORMAT (10X,15)
      DO 190 I = 1, NRES
190 READ (KIN,200) J, ((ACTAB(J,K,L), L = 1,2), K = 1, NPAIRS)
200 FORMAT (10X,15,6I10/15X,6I10)
C

```

79/05/10. 13.11.50

CRD 0240  
CRD 0250  
CRD 0260  
CRD 0270  
CRD 0280  
CRD 0290  
CRD 0300  
CRD 0310  
CRD 0320  
CRD 0330  
CRD 0340  
CRD 0350  
CRD 0360  
CRD 0370  
CRD 0380  
CRD 0390  
CRD 0400  
CRD 0410  
CRD 0420  
CRD 0430  
CRD 0440  
CRD 0450  
CRD 0460  
CRD 0470  
CRD 0480  
CRD 0490  
CRD 0500  
CRD 0510  
CRD 0520  
CRD 0530  
CRD 0540  
CRD 0550  
CRD 0560  
CRD 0570  
CRD 0580  
CRD 0590  
CRD 0600  
CRD 0610  
CRD 0620  
CRD 0630  
CRD 0640  
CRD 0650  
CRD 0660  
CRD 0670  
CRD 0680  
CRD 0690  
CRD 0700  
CRD 0710  
CRD 0720  
CRD 0730  
CRD 0740  
CRD 0750  
CRD 0760  
CRD 0770

```

80 C C C STEP 05
    READ FILE E CARDS
    DO 230 I = 1,ND
      READ (KIN,210) J, IDSTRM(J), DER(J), (DEMR(J,K),K = 1,3), (DEMD(J,K),K = 1,12)
      J, K = 1, 12
    210 FORMAT (7X, 213, 18, 313, 12F4.0)
    IF (IALLY.GT.0) READ (KIN,220) J, (DEMR(J,K),K = 1,MYEAR)
    220 FORMAT (10X, 1115)
    NORD(I) = J
    230 CONTINUE

90 C C C STEP 06
    READ FILE F CARD
    DO 270 I = 1,IMN
      READ (KIN,240) IMP(I)
    240 FORMAT (10X, 115)
    DO 260 K = 1,MYEAR
      READ (KIN,250) IMPRT(I,K), (DIMP(I,J,K),J = 1,12)
    250 FORMAT (20X, 110, 12F4.0)
    260 CONTINUE
    270 CONTINUE

100 C C C STEP 06
    READ FILE G CARDS
    IF (IALLY.GT.0) GO TO 300
    READ (KIN,280) NSRS, (JESVOL(I),I = 1,NSRS)
    280 FORMAT (10X, 1415)
    READ (KIN,290) AVRGLO, AURCHI
    290 FORMAT (10X, 2F10.0)

110 C C C STEP 07
    READ FILE H CARD
    300 READ (KIN,310) CONFLO, CONINF, CONDEM
    310 FORMAT (10X, 2F10.0)
    IF (CONINF.LE.0.0) CONINF = 1.0
    IF (CONDEM.LE.0.0) CONDEM = 1.0
    IF (CONFLO.LE.0.0) CONFLO = 1.0

115 C C C SUBROUTINE CARDS 73/73 OPT=2 TRACE FTN 4.6+452
    120 SUBROUTINE CARDS 73/05/10. 13.11.59

125 C C C STEP 08
    READ FILE I CARDS
    IF (IALLY) 320, 320, 350
    320 DO 330 K = 1, NRES
    330 READ (KIN, 340) (J, OPRP(L,J), I = 1, 12), L = 1, 3)
    340 FORMAT (10X, 15, 10X, 15, 12F4.0)

130 C C C GO TO 370
    350 DO 360 K = 1, NRES

```

CRD 0780  
 CRD 0790  
 CRD 0800  
 CRD 0810  
 CRD 0820  
 CRD 0830  
 CRD 0840  
 CRD 0850  
 CRD 0860  
 CRD 0870  
 CRD 0880  
 CRD 0890  
 CRD 0900  
 CRD 0910  
 CRD 0920  
 CRD 0930  
 CRD 0940  
 CRD 0950  
 CRD 0960  
 CRD 0970  
 CRD 0980  
 CRD 0990  
 CRD 1000  
 CRD 1010  
 CRD 1020  
 CRD 1030  
 CRD 1040  
 CRD 1050  
 CRD 1060  
 CRD 1070  
 CRD 1080  
 CRD 1090  
 CRD 1100  
 CRD 1110  
 CRD 1120  
 CRD 1130  
 CRD 1140  
 CRD 1150  
 CRD 1160  
 CRD 1170  
 CRD 1180  
 CRD 1190  
 CRD 1200  
 CRD 1210  
 CRD 1220  
 CRD 1230  
 CRD 1240  
 CRD 1250  
 CRD 1260  
 CRD 1270  
 CRD 1280  
 CRD 1290  
 CRD 1300  
 CRD 1310



```

135 DO 360 I = 1, NYEAR
      READ (KIN,340) J,OPRR(I,J),(OPRR(I,J,L),L = 1,12)
      360 CONTINUE
      C
      C
      C
140 STEP 09
      READ FILE J CARDS
      370 READ (KIN,380) NUARL
      380 FORMAT (10X,15)
      IF (NUARL.EQ.0) GO TO 420
      DO 410 LL = 1, NUARL
        READ (KIN,390) L,(LNODE(L,I),I = 1,2),CRIN(L),XLCF(L),COST(L)
        390 FORMAT (10X,315,10X,110,F10.0,15)
        LUAR(LL) = L
      READ (KIN,400) (CMAKU(L,I),I = 1,12)
      400 FORMAT (8X,1216)
      410 CONTINUE
      420 LRI = NL - NUARL
      IF (LRI.EQ.0) GO TO 450
      DO 440 LL = 1, LRI
        READ (KIN,430) L,(LNODE(L,I),I = 1,2),CMAK(L),CRIN(L),XLCF(L),COST(L)
        430 FORMAT (10X,315,2110,F10.0,15)
        440 CONTINUE
      450 IF (LRI.NE.0) RETURN
      READ (KIN,460) MEQU,MLAGS
      460 FORMAT (10X,215)
      LAGS = 2 * MLAGS + 2
      DO 510 I = 1,MEQU
        READ (KIN,470) (M(I),J = 1,LAGS)
        470 FORMAT (8F10.0)
      READ (KIN,480) MNEQU(I),JPTFF(I)
      480 FORMAT (5X,215)
      IDLNB = MNEQU(I)
      490 READ (KIN,490) (INTFF(I,J),J = 1,IDLNB)
      490 FORMAT (5X,1515)
      500 READ (KIN,500) ((IDIUL(I,J),INTL(I,J)),J = 1,MLAGS)
      500 FORMAT (5X,1216)
      510 CONTINUE
      520 CALL EXIT
      STOP
      C
175 SUBROUTINE DATA1 73/73 OPT=2 TRACE FTM 4.6+452 78/05/10. 13.11.59
      1 SUBROUTINE DATA1
      INTEGER CMAKU
      1 CMAKU
      2 CMAK
      5 INTEGER /CONTR/
      COMMON /CONTR/ KAPE4
      1 COMMON /IPRNT/ IPRNT
      1 COMMON /PARA/ NU
      RCAP
      ACTAB
      SP
      START
      KIN
      IPRNT
      NU
      RMIN
      DEN
      CMAK
      UREG
      KOUT
      IYLD
      MRES
      FSTART
      DENDR
      CRIN
      KAPE1
      ITOY
      NJLNC
      DAT 0010
      DAT 0020
      DAT 0030
      DAT 0040
      DAT 0050
      DAT 0060
      DAT 0070
      DAT 0080
      DAT 0090
      DAT 0100

```



```

65      C      ARG-1,DRY-2,NET-3
      C
70      LRULE = 1
      XMAX = TSUBRX X AURGHI
      XMIN = TSUBRX X AURGLO
      IF (UTRSYS.LT.XMIN) LRULE = 2
      IF (UTRSYS.GT.XMAX) LRULE = 3
      IF (AURGLO.LE.0.0) LRULE = 1
      IF (AURGHI.LE.0.0) LRULE = 1
      RETURN
75      C
      SUBROUTINE OPRATE 73/73 OPT=2 TRACE
      END
      FTN 4.6+452
      79/05/10. 13.11.59

1      SUBROUTINE OPRATE
      LOGICAL FESIBL
      INTEGER
      INTEGER
      1      UREG
      2      EUPT
      1      CRAYU
      2      OPRP
      COMMON /CONTR/
      1      KAPE4
      1      IPRINT
      1      IFRON
      1      PPARH/
      1      NL
      2      MS
      3      MR
      COMMON /PRINT/
      1      UREG(40)
      2      EUPT(40)
      COMMON /RESU/
      1      FSTART(40)
      2      OPRP(20,10)
      3      EVAP(10,12)
      4      DEPR(40,20)
      COMMON /LINK/
      1      LNKFLU/
      2      LNKFLU(50,13)
      COMMON /ADATA/
      1      NTINE
      2      LO(500)
      COMMON /CONFAC/
      1      CONDEN
      2      LRULE
      COMMON /DEMON/
      1      TOL
      2      DEMOU(10)
      1      IRTF(10,15)
      2      IDIUL(10,15), IRTL(10,15)

      TOTLS
      HI
      STARY
      ISHTP
      AFAX
      RCAP
      ACIAB
      SP
      KIM
      IYLD
      MRES
      MYEAR
      INN
      ICAP(40,12,13)
      START(40)
      ISHTP(40,13)
      IPRINT(40)
      AMAX(40)
      RNAME(40,2)
      ACTAB(10,18,2)
      SP(10)
      U(40,12)
      IMPRT(2,20)
      LNKFLU(50,13)
      MARG
      NT(500)
      FLOW(500)
      AURGLO
      CONING
      JESVOL(10)
      XLCF(50)
      DEMON(40,13)
      IALLY
      MEGU
      IRTF(10,15), IRTL(10,15)

      STUG
      COST
      STEND
      ISPIL
      AMIN
      DEN
      CRAX
      KOUT
      MRES
      MYEAR
      INN
      TOTLS(40,20,12)
      USE(40)
      AREAX(40)
      IAREA(40)
      AMIN(40)
      RCAP(40)
      DER(40)
      IMP(2)
      CRAX(50)
      NMAX
      NF(500)
      COST(500)
      AURGHI
      CPCT
      XCELL(50,12)
      IRTN
      MLAGS
      JRTFT(10)
      A(10,15)
      IRTF(10,240)

      STEPP
      FLOW
      USE
      AREAX
      FSTART
      DEMR
      CRAX
      KAPE1
      ITOY
      MUNG
      MO
      TITLE(20)
      TOTLS(40,20,12)
      USE(40)
      AREAX(40)
      IAREA(40)
      AMIN(40)
      RCAP(40)
      OPRP(20,10,12)
      DEPR(40,12)
      DIMP(12,12,20)
      CRIM(50)
      LNKAPL(50,13)
      FESIBL
      NI(500)
      CONFLO
      NSRS
      LOPT
      A(10,15)
      IRTF(10,240)

```

```

DAT 0650
DAT 0650
DAT 0670
DAT 0680
DAT 0690
DAT 0700
DAT 0710
DAT 0720
DAT 0730
DAT 0740
DAT 0750
DAT 0760
79/05/10. 13.11.59
OPR 0010
OPR 0020
OPR 0030
OPR 0040
OPR 0050
OPR 0060
OPR 0070
OPR 0080
OPR 0090
OPR 0100
OPR 0110
OPR 0120
OPR 0130
OPR 0140
OPR 0150
OPR 0160
OPR 0170
OPR 0180
OPR 0190
OPR 0200
OPR 0210
OPR 0220
OPR 0230
OPR 0240
OPR 0250
OPR 0260
OPR 0270
OPR 0280
OPR 0290
OPR 0300
OPR 0310
OPR 0320
OPR 0330
OPR 0340
OPR 0350
OPR 0360
OPR 0370
OPR 0380
OPR 0390
OPR 0400
OPR 0410
OPR 0420

```

```

C C COMMON /D/ NDRD(40) ; IDSTRM(40) ; ITHRU(40)
45 C 1, LUAR(50) ; CHAXU(50,12)
C C DIMENSION IA(70) ; IB(70) ; IC(70)
50 C C
C C STEP 01
C C ZERO OUT ARRAYS AND INITIALIZE
C C VARIABLES
55 C 100 NR = ML - NC
C ROFF = 0.499
C ITOT = 0
C IQUIT = 0
C DO 110 L = 1, ML
60 SUBROUTINE OPRATE 73/73 OPT=2 TRACE FTN 4.6+452
C DO 110 I = 1,13
C LNKFL(L,I) = 0
C LNKAF(L,I) = 0
C LNKAX(L,I) = 0
65 110 CONTINUE
C DO 120 J = 1, NJ
C STEND(J) = 0
C ITOT = ITOT + RCAP(J)
70 120 N = 1,12
C ISHTR(J,N) = 0
C ISPIL(J,N) = 0
120 CONTINUE
C C
C C SET LIMITS ON ARCS
75 C C
C C L1 = ML + 1
C L2 = ML + NJ
80 C C L3 = L2 + 1
C L4 = L2 + NJ
C L5 = L4 + 1
C L6 = L4 + NJ
85 C C L7 = L6 + 1
C L8 = L6 + NJ
C L9 = L8 + 1
C LA = L8 + NRES
C LB = NR + 1
90 C DO 130 L = 1, NARC
C HI(L) = 0
C LO(L) = 0
C FLOW(L) = 0
95 C 130 CONTINUE

```

```

OPR 0430
OPR 0440
OPR 0450
OPR 0460
OPR 0470
OPR 0480
OPR 0490
OPR 0500
OPR 0510
OPR 0520
OPR 0530
OPR 0540
OPR 0550
OPR 0560
OPR 0570
OPR 0580
OPR 0590
OPR 0600
79/05/10. 13.11.59

OPR 0610
OPR 0620
OPR 0630
OPR 0640
OPR 0650
OPR 0660
OPR 0670
OPR 0680
OPR 0690
OPR 0700
OPR 0710
OPR 0720
OPR 0730
OPR 0740
OPR 0750
OPR 0760
OPR 0770
OPR 0780
OPR 0790
OPR 0800
OPR 0810
OPR 0820
OPR 0830
OPR 0840
OPR 0850
OPR 0860
OPR 0870
OPR 0880
OPR 0890
OPR 0900
OPR 0910
OPR 0920
OPR 0930
OPR 0940
OPR 0950
OPR 0960

```

```

100 C      SET HI + LO ON LINKS
      DO 140 L = 1,ML
      LO(L) = CRIN(L) * CONFLO
      IF (NUARL.EQ.0) HI(L) = CRAX(L) * CONFLO
140  CONTINUE
C
C
C
105 C      STEP 03
      PRICE RIVER REACHES TO 1 AND CANALS TO 2
C
C
110 C      DO 150 L = 1,ML
      IF (COST(L).NE.0) GO TO 150
      COST(L) = 1
      IF (L.GT.NR) COST(L) = 2
150  CONTINUE
C
C
115 C      STEP 04
      IF FIRM YIELD RUN - SET SWITCH
C
C
120 C      SET SWITCHES AND CONTROL FOR YIELD RUN
      IF (IVLD.EQ.0) GO TO 160
      SUBROUTINE OPRATE 73/73 OPT-2 TRACE FTH 4.6+452
      IQUIT = 1
160  REWIND KAPE1
C
125 C      ISTRT = 1
      MYR = MYEAR
C
C
130 C      STEP 06
      NTIME-1 FOR FIRST SOLUTION
      BEGIN YEARLY LOOP
C
C
135 C      START YEARLY LOOP
      IV = ISTRT
170  IF (LOPT) 200,200,180
180  DO 190 L = 1,ML
      DO 190 N = 1,12
      XCLL(L,N) = 0.0
190  CONTINUE
200  CONTINUE
      DO 210 J = 1,NJ
      DO 210 I = 1,12
      TOTLS(J,IV,I) = 0
210  CONTINUE
C
C
145 C      STEP 07
      READ MONTHLY DATA FOR ONE YEAR
C
C
150 C

```

```

OPR 0970
OPR 0980
OPR 0990
OPR 1000
OPR 1010
OPR 1020
OPR 1030
OPR 1040
OPR 1050
OPR 1060
OPR 1070
OPR 1080
OPR 1090
OPR 1100
OPR 1110
OPR 1120
OPR 1130
OPR 1140
OPR 1150
OPR 1160
OPR 1170
OPR 1180
OPR 1190
OPR 1200
79/05/10. 13.11.59
OPR 1210
OPR 1220
OPR 1230
OPR 1240
OPR 1250
OPR 1260
OPR 1270
OPR 1280
OPR 1290
OPR 1300
OPR 1310
OPR 1320
OPR 1330
OPR 1340
OPR 1350
OPR 1360
OPR 1370
OPR 1380
OPR 1390
OPR 1400
OPR 1410
OPR 1420
OPR 1430
OPR 1440
OPR 1450
OPR 1460
OPR 1470
OPR 1480
OPR 1490
OPR 1500

```

```

155 C CALL DATA2
      JFLAG = 0
      DO 220 J = 1, NJ
      IF (IDSTRT(J).EQ.0) GO TO 220
      JFLAG = 1
220 CONTINUE
      C
      C
      C STEP 08
      C SET BEGIN STORGES TO STARTING
      C
      C
      C IF (IV.GT.1) GO TO 240
      C DO 230 J = 1, NRES
      C STEND(J) = FSTART(J)
230 CONTINUE
      C
      C ENTER SEASONAL LOOP
      C STEP 09
      C BEGIN MONTHLY LOOP
      C
      C 240 DO 750 MON = 1, 12
      C JMONY = ((IV - 1) * 12) + MON
      C IF (MMARL.EQ.0) GO TO 280
      C DO 270 I = 1, NI
      C DO 250 LL = 1, MMARL
      C IF (LVAR(LL).EQ.L) GO TO 250
      C GO TO 260
      C MI(L) = CMAXU(L, MON) * COMFLO
      C GO TO 270
      C OPT=2 TRACE
180 SUBROUTINE OPRAE 73/73 OPT=2 TRACE FTN 4.6+452
      C
      C 260 CONTINUE
      C MI(L) = CMAX(L) * COMFLO
270 CONTINUE
280 IDONE = 1
      C ITERI = 0
      C MTIME = 1
      C ICONU = 0
      C FLAG2 = 1
290 ITER = 0
      C DO 300 J = 1, NJ
      C USE(J) = 0
      C EUP(T(J)) = 0
      C UREG(J) = 0
      C START(J) = 0
      C DO 300 I = 1, 13
      C ICAP(J, MON, I) = 0
300 CONTINUE
      C DO 310 I = 1, MMARL
      C FLOW(L) = 0
310 CONTINUE
      C
      C
      C STEP 10
      C SET INFLOWS AND DEMANDS - IF A TOTAL
      C YEARLY DEMAND IS GIVEN USE IT X DISTRIB.
1510 OPR
1520 OPR
1530 OPR
1540 OPR
1550 OPR
1560 OPR
1570 OPR
1580 OPR
1590 OPR
1600 OPR
1610 OPR
1620 OPR
1630 OPR
1640 OPR
1650 OPR
1660 OPR
1670 OPR
1680 OPR
1690 OPR
1700 OPR
1710 OPR
1720 OPR
1730 OPR
1740 OPR
1750 OPR
1760 OPR
1770 OPR
1780 OPR
1790 OPR
1800 OPR
79/05/10. 13.11.59
1810 OPR
1820 OPR
1830 OPR
1840 OPR
1850 OPR
1860 OPR
1870 OPR
1880 OPR
1890 OPR
1900 OPR
1910 OPR
1920 OPR
1930 OPR
1940 OPR
1950 OPR
1960 OPR
1970 OPR
1980 OPR
1990 OPR
2000 OPR
2010 OPR
2020 OPR
2030 OPR
2040 OPR

```



```

260           IF (RCAP(JN).EQ.0) GO TO 410
C
C
C
C
265           STEP 14
ESTIMATE EWAP FOR MONTH
STUG = 0.5 * (START(JN) + RCAP(JN))
CALL AREA (STUG,ISURA,JN)
IA(JN) = ISURA * EWAP(JN,MON) + ROFF
STUG = 0.5 * (START(JN) + RMIN(JN))
CALL AREA (STUG,ISURA,JN)
IB(JN) = ISURA * EWAP(JN,MON) + ROFF
STUG = 0.5 * (START(JN) + OPRR(LRULE,JN,MON) * RCAP(JN))
CALL AREA (STUG,ISURA,JN)
IC(JN) = ISURA * EWAP(JN,MON) + ROFF

270
C
C
C
C
275           STEP 15
SET UP BOUNDS FOR DESIRED STORAGE ARCS
BASED ON RULES - PRICE ARCS FROM RANK
INPUT - CALCULATE BOUNDS FOR FINAL STORAGE
ARCS
IAT = IAT + IA(JN)
RMINPOL = RMIN(JN)
LO(NP) = IB(JN) + RMINPOL
IF (LO(L).LT.LO(NP)) LO(NP) = LO(L)
IF (LO(NP).LT.0) LO(NP) = 0
LO(MN) = 0
HI(NP) = OPRR(LRULE,JN,MON) * RCAP(JN) + IC(JN)
COST(NP) = - (1000 - OPRR(LRULE,JN) * 10)
HI(MN) = (1.0 - OPRR(LRULE,JN,MON)) * RCAP(JN) + IA(JN) - ICOPR 2800
(JN)
IF (HI(MN).LT.0) HI(MN) = 0
IF (HI(NP).GT.LO(NP)) GO TO 410
HI(NP) = LO(NP)
HI(MN) = RCAP(JN) - HI(NP)
IF (HI(MN).LT.0) HI(MN) = 0
CONTINUE
FLOU(MN) = FLOU(L)
LO(MARC - 3) = LO(MARC - 3) + LO(NP)
CONTINUE

300 SUBROUTINE OPRATE 73/73 OPT=2 TRACE STEP 16 FTN 4.6+452
C
C
C
C
305           SET UP BOUNDS IN PASS BALANCE ARCS
FLOU(MARC - 3) = ISUM
HI(MARC - 3) = ITOT + IAT
FLOU(MARC) = ISUM
HI(MARC) = FLOU(MARC)
LO(MARC) = FLOU(MARC)

310           STEP 17
SET UP DEMAND ARCS AND PRICE
ACCORDING TO RANK
SET LIMITS ON DEMAND ARCS

```

OPR 2500  
 OPR 2600  
 OPR 2610  
 OPR 2620  
 OPR 2630  
 OPR 2640  
 OPR 2650  
 OPR 2660  
 OPR 2670  
 OPR 2680  
 OPR 2700  
 OPR 2710  
 OPR 2720  
 OPR 2730  
 OPR 2740  
 OPR 2750  
 OPR 2760  
 OPR 2770  
 OPR 2780  
 OPR 2790  
 OPR 2800  
 OPR 2810  
 OPR 2820  
 OPR 2830  
 OPR 2840  
 OPR 2850  
 OPR 2860  
 OPR 2870  
 OPR 2880  
 OPR 2890  
 OPR 2900  
 OPR 2910  
 OPR 2920  
 OPR 2930  
 OPR 2940  
 OPR 2950  
 OPR 2960  
 OPR 2970  
 OPR 2980  
 OPR 2990  
 OPR 3000  
 78/05/10. 13.11.59  
 OPR 3010  
 OPR 3020  
 OPR 3030  
 OPR 3040  
 OPR 3050  
 OPR 3060  
 OPR 3070  
 OPR 3080  
 OPR 3090  
 OPR 3100  
 OPR 3110  
 OPR 3120



```

315 C          MAXD = 0
          DO 430 L = L7, L8
              JN = NF(L)
              HI(L) = USE(JN)
              COST(L) = -(1000 - DEPR(JN, LRULE) * 10)
              MAXD = MAXD + HI(L)
          CONTINUE
320 C          CONTINUE
          440 CONTINUE
          HI(NARC - 1) = MAXD
          IF (LOPT.EQ.1.AND.ITER.GE.1) GO TO 480

325 C          STEP 18
          SET UP SPILL ARCS AND PRICE
          ACCORDING TO ORDER

330 C          SET LIMITS ON SPILL ARCS

          MAXS = 0
          DO 470 L = L9, LA
              JN = NF(L)
              MTX = 0

335 C          DO 450 K = 1, MS
              IF (JN.EQ.SP(K).AND.MS.NE.0) MTX = 1
              IF (MTX.EQ.1) GO TO 460
              CONTINUE
              K = 0

340 C          KS = K
              HI(L) = ITOT * 10 * MTX
              COST(L) = MTX * 10000 * (1 + KS)
              MAXS = MAXS + HI(L)
          CONTINUE
345 C          HI(NARC - 2) = MAXS

          C          CONTINUE

350 C          STEP 19
          CALL NETWORK FLOW ALGORITHM

355 C          CALL SUPERK
          IF (.NOT.FESIBL) GO TO 770
          MTIME = 2

          C          IF (LOPT.EQ.1) CALL CHANLS (NON, ITER, IDONE, L7, L8, MAXD, IV)
          IF (IDONE.EQ.0) GO TO 440

360 C          SUBROUTINE OPRATE
          DO 490 L = 1, ML
              73/73 OPT=2 TRACE          FTM 4.6+452

          490 FLOW(L) = FLOW(L) - INT(XCELL(L, NON))
          CONTINUE
          IF (JFLAG.EQ.0) GO TO 530
          DO 500 J = 1, NJ
              ITHRU(J) = 0
          CONTINUE

365 C          500 CONTINUE
    
```

OPR 3130  
 OPR 3140  
 OPR 3150  
 OPR 3160  
 OPR 3170  
 OPR 3180  
 OPR 3190  
 OPR 3200  
 OPR 3210  
 OPR 3220  
 OPR 3230  
 OPR 3240  
 OPR 3250  
 OPR 3260  
 OPR 3270  
 OPR 3280  
 OPR 3290  
 OPR 3300  
 OPR 3310  
 OPR 3320  
 OPR 3330  
 OPR 3340  
 OPR 3350  
 OPR 3360  
 OPR 3370  
 OPR 3380  
 OPR 3390  
 OPR 3400  
 OPR 3410  
 OPR 3420  
 OPR 3430  
 OPR 3440  
 OPR 3450  
 OPR 3460  
 OPR 3470  
 OPR 3480  
 OPR 3490  
 OPR 3500  
 OPR 3510  
 OPR 3520  
 OPR 3530  
 OPR 3540  
 OPR 3550  
 OPR 3560  
 OPR 3570  
 OPR 3580  
 OPR 3590  
 OPR 3600  
 OPR 3610  
 OPR 3620  
 OPR 3630  
 OPR 3640  
 OPR 3650  
 OPR 3660

73/66/18. 13.11.59

```

370 DO 520 L = 1,NL
      DO 510 J = 1,NJ
        IF (IDSTRM(J).EQ.0) GO TO 510
        IF (LNODE(L,2).EQ.J) ITHRU(IDSTRM(J)) = ITHRU(IDSTRM(J))
        + FLOW(L)
        CONTINUE
510 CONTINUE
520 IF ((JFLAG.EQ.1).AND.(IRTN.EQ.0)) GO TO 540
      ITER1 = 1
530 IF (IRTN.EQ.0) GO TO 550
      CALL RTFLOW (MON,IV,JFLAG2,ICOMU,JROWV,L7,L8)
      IF (JFLAG2.EQ.0) GO TO 200
      GO TO 550
540 IF (ITER1.NE.0) GO TO 550
      ITER1 = 1
      GO TO 200
      C
      C
      C
385 STEP 20
      BUILD SHORTAGE ARRAY
      C
      C
550 DO 560 L = L7,L8
      JN = NF(L)
      ISHTM(JN,MON) = MI(L) - FLOW(L)
      CONTINUE
      C
      C
      C
395 STEP 21
      BUILD SPILL ARRAY
      C
      C
      C
      C
400 DO 570 L = L9,L4
      JN = NF(L)
      ISPI(L,JN,MON) = FLOW(L)
      CONTINUE
      C
      C
      C
      C
      C
405 STEP 22
      CALCULATE FINAL RES STORAGE
      AND SET MONTHLY EVAP ESTIMATE
      C
      C
      C
      C
      C
410 DO 580 L = L3,L4
      JN = NF(L)
      LN = L + NJ
      STEND(JN) = FLOW(L) + FLOW(LN)
      EUPT(JN) = IA(JN)
      IF (FLOW(L).EQ.0) EUPT(JN) = IB(JN)
      IF (FLOW(LN).EQ.0) EUPT(JN) = IC(JN)
      IF (STEND(JN).LT.0) STEND(JN) = 0
      CONTINUE
      C
      C
      C
415 STEP 23
      CALCULATE MONTHLY EVAP. AND DETERMINE
      RES. ENDING STORAGE
      C
      C
      C
      C
420 SUBROUTINE OPRATE DO 650 L = L3,L4
      73/73 OPT=2 TRACE FTH 4.0+452

```

```

425      ICHK = 0
         JN = NF(L)
         IF (RCAP(JN).LE.0) GO TO 650
         EUP = EUPT(JN)
         STEMP = STEND(JN)
         IF (STEMP.GT.RCAP(JN)) STEMP = RCAP(JN)
         STUG = (STEMP + START(JN)) * 0.5
         CALL AREA (STUG,ISURA,JN)
         ETEMP = 0.0
         IAREA(JN) = ISURA
         IF (EUAP(JN,MON)) 600,640,600
         ETEMP = ISURA * EUAP(JN,MON) + ROFF
         IF (ABS(ETEMP - EUP).LT.5.0) GO TO 640
         ICHK = ICHK + 1
         IF (ICLK.LE.100) GO TO 630
         WRITE (KOUT,610) JN,ETEMP,EUP,ISURA,START(JN),STEND(JN)
         610 FORMAT (5X,3HJN=,13,5X,6HETEMP=,F12.4,5X,4HEUP=,F10.4,5X,6HISURA=,
         1110,7HSTART =,110,8HSTEND =,110)
         620 FORMAT (//3110)
         WRITE (KOUT,620) IY,MON,STEMP
         CALL EXIT
         630 CONTINUE
         EUP = ETEMP
         STEMP = STEND(JN) - EUP
         IF (STEMP.LT.0) STEMP = 0
         GO TO 590
         640 STEMP = ETEMP
         STEND(JN) = STEND(JN) - STEMP
         IF (STEND(JN).LT.0) STEND(JN) = 0
         IF (STEND(JN).GT.RCAP(JN)) STEND(JN) = RCAP(JN)
         EUPT(JN) = STEMP
         650 CONTINUE
C
C
C
C
STEP 25
BUILD PRINT-ARRAY WITH MONTHY DATA
DO 700 J = 1,NRES
ICAP(J,MON,1) = START(J)
ICAP(J,MON,2) = UREG(J)
ICAP(J,MON,4) = USE(J)
ICAP(J,MON,5) = IAREA(J) + ROFF
ICAP(J,MON,6) = EUPT(J)
ICAP(J,MON,8) = ISHTR(J,MON)
ICAP(J,MON,11) = ISPIL(J,MON)
ICAP(J,MON,12) = STEND(J)
ICAP(J,MON,13) = OPRR(LNULE,J,MON) * RCAP(J) + ROFF
IDM = 0
IUP = 0
IPI = 0
IPO = 0
700 CONTINUE
C
C
C
STEP 26
SET UP UPSTREAM AND DOWNSTREAM FLOWS
IF (NR.EQ.0) GO TO 670

```

OPR 4210  
 OPR 4220  
 OPR 4230  
 OPR 4240  
 OPR 4250  
 OPR 4260  
 OPR 4270  
 OPR 4280  
 OPR 4290  
 OPR 4300  
 OPR 4310  
 OPR 4320  
 OPR 4330  
 OPR 4340  
 OPR 4350  
 OPR 4360  
 OPR 4370  
 OPR 4380  
 OPR 4390  
 OPR 4400  
 OPR 4410  
 OPR 4420  
 OPR 4430  
 OPR 4440  
 OPR 4450  
 OPR 4460  
 OPR 4470  
 OPR 4480  
 OPR 4490  
 OPR 4500  
 OPR 4510  
 OPR 4520  
 OPR 4530  
 OPR 4540  
 OPR 4550  
 OPR 4560  
 OPR 4570  
 OPR 4580  
 OPR 4590  
 OPR 4600  
 OPR 4610  
 OPR 4620  
 OPR 4630  
 OPR 4640  
 OPR 4650  
 OPR 4660  
 OPR 4670  
 OPR 4680  
 OPR 4690  
 OPR 4700  
 OPR 4710  
 OPR 4720  
 OPR 4730  
 OPR 4740  
 OPR 4750  
 OPR 4760

```

480 SUBROUTINE OPRATE
      DO 660 L = 1, NR
        LNKFLO(L, MON) = FLOW(L)/CONFLO
        IF (LMODE(L, 1).EQ.1) IDN = IDN + FLOW(L)
        IF (LMODE(L, 2).EQ.2) IUP = IUP + FLOW(L)
        FTR, 4.6+452
        OPT=2 TRACE
      660 CONTINUE
      ICAP(J, MON, 3) = IUP
      ICAP(J, MON, 7) = IDN
485
      DO 670 L = 1, NR
        IF (MCON.EQ.0) GO TO 690
        LNKFLO(L, MON) = FLOW(L)/CONFLO
        IF (LMODE(L, 1).EQ.1) IPO = IPO + FLOW(L)
        IF (LMODE(L, 2).EQ.2) IPI = IPI + FLOW(L)
690 CONTINUE
695 ICAP(J, MON, 8) = IPI
      ICAP(J, MON, 10) = IPO
495
      STEP 27
      CALCULATE AVER. AND MAX FLOWS
500
      CONTINUE
      DO 710 L = 1, NR
        LNKAFL(L, MON) = LNKAFL(L, MON) + LNKFLO(L, MON)/MYEAR
        IF (LNKFLO(L, MON).GT.LNKAFL(L, MON)) LNKAFL(L, MON) = LNKFLO(L, MON)
710 CONTINUE
505
      NDS = NJ - NRES
      IF (NDS.EQ.0) GO TO 730
      DO 720 J = 1, NDS
        JN = J + NRES
        ICAP(JN, MON, 2) = USREG(JN)
        ICAP(JN, MON, 4) = USSE(JN)
        ICAP(JN, MON, 8) = ISATRI(JN, MON)
720 CONTINUE
730 CONTINUE
515
      STEP 28
      ADD MONTHLY AMOUNTS FOR YEAR TOTALS
520
      DO 740 JN = 1, NJ
        IF (MON.EQ.1) TOTLS(JN, IV, 1) = START(JN)
        IF (MON.EQ.12) TOTLS(JN, IV, 12) = STEND(JN)
      740 I = 2, 11
        TOTLS(JN, IV, I) = TOTLS(JN, IV, I) + ICAP(JN, MON, I)
740 CONTINUE
750 CONTINUE
530
      STEP 29
  
```

OPR 4770  
 OPR 4780  
 OPR 4790  
 OPR 4800  
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 OPR 4810  
 OPR 4820  
 OPR 4830  
 OPR 4840  
 OPR 4850  
 OPR 4860  
 OPR 4870  
 OPR 4880  
 OPR 4890  
 OPR 4900  
 OPR 4910  
 OPR 4920  
 OPR 4930  
 OPR 4940  
 OPR 4950  
 OPR 4960  
 OPR 4970  
 OPR 4980  
 OPR 4990  
 OPR 5000  
 OPR 5010  
 OPR 5020  
 OPR 5030  
 OPR 5040  
 OPR 5050  
 OPR 5060  
 OPR 5070  
 OPR 5080  
 OPR 5090  
 OPR 5100  
 OPR 5110  
 OPR 5120  
 OPR 5130  
 OPR 5140  
 OPR 5150  
 OPR 5160  
 OPR 5170  
 OPR 5180  
 OPR 5190  
 OPR 5200  
 OPR 5210  
 OPR 5220  
 OPR 5230  
 OPR 5240  
 OPR 5250  
 OPR 5260  
 OPR 5270  
 OPR 5280  
 OPR 5290  
 OPR 5300

```

IF ONE PASS OR CONVERGENCE AND PRINT
YEAR-CALL YEARLY PRINT ROUTINE
535 KEY = 1
CALL OUT2 (IV)
IV = IV + 1
IF (IV.LE.MYEAR) GO TO 170
540 SUBROUTINE OPRTATE 73/73 OPT=2 TRACE FTN 4.6+452
STEP 30
CALL ROUTINE TO ADJUST ANNUAL DEMAND
AT YIELD NODE IF NECESSARY
545 IF (IQUIT.EQ.0) GO TO 760
CALL ADJUST (IV,IQUIT,ICHT)
GO TO 160
550 CONTINUE
STEP 31
PRINT ARC DUMP IF SOLUTION INFEASIBLE
555 RETURN
770 WRITE (KOUT,780) IV,NOM,(L,NF(L),NT(L),LO(L),HI(L),FLOU(L),COST(L))
1,L = 1,NARC)
780 FORMAT (1H1/20X,20HSOLUTION INFEASIBLE .5H YEAR,13,7H MONTH,13/60PR 5570
10H LINK FROM TO LO HI FLOW COST /((30PR 5580
215,4110))
560 RETURN
END 73/73 OPT=2 TRACE FTN 4.6+452
SUBROUTINE OUT1
SUBROUTINE OUT1
INTEGER RCAP , RRIN , FSTART
1 CRAXU , ACTAB , DEN , DENR
2 CRAP , SP , CRAX , CRIN
1 KAPEL , KOUT , KAPE1
1 IPRINT , IYLD , ITOY
1 COMMON /PARM/ NJ , NRES , NJUNC
2 NL , NYEAR , MO , TITLE(20)
3 NR , NPAIRS , RCAP(40)
1 FSTART(40) , ACTAB(10,18,2) , RRIN(40)
2 OPRP(20,18) , SP(10) , DEN(40)
3 EUPR(10,12) , U(40,12) , IPR(2)
4 DEMR(40,20) , IPRINT(8,20) , CRAX(50)
COMMON /LINK/ UNODE(50,2) , SAURCH1
COMMON /CONFAC/ AURGLD , CONFL0
COMMON /CONDEN/ , CONINF , , MSRS
1
SUBROUTINE OUT1
INTEGER RCAP , RRIN , FSTART
1 CRAXU , ACTAB , DEN , DENR
2 CRAP , SP , CRAX , CRIN
1 KAPEL , KOUT , KAPE1
1 IPRINT , IYLD , ITOY
1 COMMON /PARM/ NJ , NRES , NJUNC
2 NL , NYEAR , MO , TITLE(20)
3 NR , NPAIRS , RCAP(40)
1 FSTART(40) , ACTAB(10,18,2) , RRIN(40)
2 OPRP(20,18) , SP(10) , DEN(40)
3 EUPR(10,12) , U(40,12) , IPR(2)
4 DEMR(40,20) , IPRINT(8,20) , CRAX(50)
COMMON /LINK/ UNODE(50,2) , SAURCH1
COMMON /CONFAC/ AURGLD , CONFL0
COMMON /CONDEN/ , CONINF , , MSRS
1
SUBROUTINE OUT1
INTEGER RCAP , RRIN , FSTART
1 CRAXU , ACTAB , DEN , DENR
2 CRAP , SP , CRAX , CRIN
1 KAPEL , KOUT , KAPE1
1 IPRINT , IYLD , ITOY
1 COMMON /PARM/ NJ , NRES , NJUNC
2 NL , NYEAR , MO , TITLE(20)
3 NR , NPAIRS , RCAP(40)
1 FSTART(40) , ACTAB(10,18,2) , RRIN(40)
2 OPRP(20,18) , SP(10) , DEN(40)
3 EUPR(10,12) , U(40,12) , IPR(2)
4 DEMR(40,20) , IPRINT(8,20) , CRAX(50)
COMMON /LINK/ UNODE(50,2) , SAURCH1
COMMON /CONFAC/ AURGLD , CONFL0
COMMON /CONDEN/ , CONINF , , MSRS
1

```

OPR 5310  
OPR 5320  
OPR 5330  
OPR 5340  
OPR 5350  
OPR 5360  
OPR 5370  
OPR 5380  
OPR 5390  
OPR 5400  
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OPR 5410  
OPR 5420  
OPR 5430  
OPR 5440  
OPR 5450  
OPR 5460  
OPR 5470  
OPR 5480  
OPR 5490  
OPR 5500  
OPR 5510  
OPR 5520  
OPR 5530  
OPR 5540  
OPR 5550  
OPR 5560  
OPR 5570  
OPR 5580  
OPR 5590  
OPR 5600  
OPR 5610  
OPR 5620  
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OTI 0010  
OTI 0020  
OTI 0030  
OTI 0040  
OTI 0050  
OTI 0060  
OTI 0070  
OTI 0080  
OTI 0090  
OTI 0100  
OTI 0110  
OTI 0120  
OTI 0130  
OTI 0140  
OTI 0150  
OTI 0160  
OTI 0170  
OTI 0180  
OTI 0190  
OTI 0200

```

25 COMMON /ADATA/      JESVOL(10)      NMAX      FESIBL      071 0210
    1 MARC             NT(500)          NK(500)    MI(500)      071 0220
    2 FLOW(500)        COST(500)   IDSTRM(40) ITHRU(40)   071 0230
    1 NUMRL           LVAR(50)          CHANV(50,12) ITHRU(40)   071 0240
    1 /LDATA/         XCLL(50,12)  IRTM       071 0250
    1 /RI/            NEQU             NLAGS      A(10,15)   071 0260
    2 NMEQU(10)       IRTF(10,15), IRTF(10)  IRTF(10,240) 071 0270
    1 IDIUL(10,15),  IRTL(10,15)  LOUT(2)     071 0280
DIMENSION             COND(3)
DATA COND/4*NRG,4*DRY ,4*MET /
DATA LOU/8H ULL ,8*UILL NOT/

35 STEP 01
    PRINT OUT ALL INPUT INFORMATION

40 I111 = 2
    WRITE (KOUT,100) TITLE
100 FORMAT (1H//10X,75*RIUER BASIN SIMULATION PACKAGE: ,10X,42*PROOT) 0410
1GRAM MODSIN - COLORADO STATE UNIVERSITY,720X,2004) 071 0420
    WRITE (KOUT,110) NJ,NRES,NL,NR,1YEAR,NYEAR,MD,MS,1YLD,IRN 071 0430
110 FORMAT (/10X,15X,17*NUMBER OF NODES = 15,7X,7X,25*NUMBER OF RESERT) 0440
    1UOIRS = 13/10X,15X,17*NUMBER OF LINES = 15,7X,4X,25*NUMBER OF RIUOT) 0450
2ER REACHES = 13/10X,32*CALENDAR YEAR OPERATION STARTS = 15,7X,20*RI 0460
4 = 15,7X,6X,23*NUMBER OF SPILL NODES = 13/10X,8X,24*NUMBER OF DEFS) 0470
57X,5X,24*NUMBER OF IMPORT NODES = 13/30X,12*YIELD NODES = 15,071 0480
    IF (LOPT.EQ.1) I111 = 1 071 0490
    WRITE (KOUT,120) LOU(I111) 071 0500
120 FORMAT (/10X,15*CHANNEL LOSSES ,AS,14H BE CONSIDERED) 071 0510
130 FORMAT (1H ,18X,11*TOLERANCE = ,F8.3,/) 071 0520
    I111 = 2 071 0530
    IF (IRTN.EQ.1) I111 = 1 071 0540
    WRITE (KOUT,140) LOU(I111) 071 0550
140 FORMAT (/10X,13*RETURN FLOWS ,AS,14H BE CALCULATED) 071 0560
    WRITE (KOUT,150) 071 0570
150 FORMAT (/10X,8*NODE NO.,3X,8*NODE NAME,4X,9(1H-),12H CAPACITIES 071 0580
    73/73 OPT-2 TRACE FTN 4.6+452 79/05/10. 13.11.59
SUBROUTINE OUT1
19(1H-),5X,6*YEARLY/10X,25X,28*MAXIMUM MINIMUM STARTING,5X,6*DE 0610
2*AND) 071 0620
DO 160 J = 1,NJ 071 0630
    IF (MOD(J,20).NE.0) GO TO 160 071 0640
    WRITE (KOUT,100) TITLE 071 0650
    WRITE (KOUT,150) 071 0660
160 WRITE (KOUT,170) J, (RNAME(J,1),1 = 1,2),RCAP(J),RIR(J),FSTART(J), 071 0670
    1DEFL(J) 071 0680
170 FORMAT (/10X,13,8X,20X,4X,2110,1X,110,3X,18) 071 0690
    WRITE (KOUT,180) 071 0700
180 FORMAT (/10X,20*SYSTEM CONFIGURATION/10X,8*LINK NO.,4X,8*FROM 071 0710
    1DE,5X,7*TO NODE,5X,13*MAX. CAPACITY,4X,13*MIN. CAPACITY,5X,10*LOSS) 0720
    2 COEFFICIENT,11X,4*COST) 0730
    0740

```

```

75 DO 250 L = 1, NL
   IF (MOD(L,20).NE.0) GO TO 190
   WRITE (KOUT,100) TITLE
   WRITE (KOUT,180)
   IF (NVARL.EQ.0) GO TO 230
   DO 220 LL = 1, NVARL
     IF (LVAR(LL).EQ.L) GO TO 200
     GO TO 220
   WRITE (KOUT,210) L, (LNODE(L,1), I = 1,2), CRIN(L), XLCF(L), COSTOT1
210 FORMAT (/10X,2X,12,12X,12,12X,12,5X,14#ARRIES MONTHLY,7X,110,16X,F01
15.3,10X,15)
   GO TO 250
220 CONTINUE
230 WRITE (KOUT,240) L, (LNODE(L,1), I = 1,2), CRAX(L), CRIN(L), XLCF(L)
240 FORMAT (/10X,2X,12,12X,12,12X,12,9X,110,7X,110,16X,F5.3,10X,15)
250 CONTINUE
   WRITE (KOUT,260) (SP(I), I = 1, NS)
260 FORMAT (///10X,27#LIST OF SPILL RESERVOIRS - .1415//)
   IF (INP.EQ.0) GO TO 300
   WRITE (KOUT,100) TITLE
   DO 290 I = 1, INP
     DO 280 K = 1, NYEAR
       WRITE (KOUT,270) IMP(I), IMPRT(I,K), (DIRP(I,J,K), J = 1,12)
270 FORMAT (/10X,5#MODE NO. ,12,5X,16#YEARLY IMPORT - ,18,26X,25#MONTHLY
1LY IMPORT DISTRIBUTION: ,12F5.2)
     DO 280 CONTINUE
280 CONTINUE
290 IF (IALLY.GT.0) GO TO 330
   WRITE (KOUT,310) (JESU(I), I = 1, NERS)
310 FORMAT (//10X,25#SUB-SYSTEM OF RESERVOIRS ,1415)
   AULO = AURGL0 * 100.
   AUHI = AURCHI * 100.
   WRITE (KOUT,320) AULO, AUHI
320 FORMAT (//10X,2#AVERAGE: DEFINED AS BETWEEN,FB.1,5# ,AND,FB.1,250T1
1# PERCENT FULL OF SUBSYSTEM)
   GO TO 360
330 WRITE (KOUT,340)
340 FORMAT (//10X,5#AVERAGE, MET, AND DRY STATES WILL NOT BE CALCUL
1ATED #)
   WRITE (KOUT,350)
350 FORMAT (/10X,5#H DESIRED OPERATING LEVELS WILL BE INPUT FOR EACHOT1
1 YEAR)
360 WRITE (KOUT,370) CONFL0, CONIF, CONDER
370 FORMAT (//10X,7#FACTORS//15X,2#MULTIPLY LINK CAPACITIES BY ,FB.30T1
73/73 OPT-2 TRACE
SUBROUTINE OUT1
1//15X,2#MULTIPLY INFLOWS BY ..... ,FB.2//15X,2#MULTIPLY DEMANDOT1
25 BY ..... ,FB.2)
   WRITE (KOUT,100) TITLE
   IF (IALLY.GT.0) GO TO 430
   WRITE (KOUT,380)
380 FORMAT (//10X,30# ,27#MONTHLY DEMAND DISTRIBUTION//10X,5#MODE NO.6X,OT1
14X,4# 1 .3X,4# 2 .3X,4# 3 .3X,4# 4 .3X,4# 5 .3X,4# 6 .3X,4# 7 .3X,4#
2 7 .3X,4# 8 .3X,4# 9 .3X,4# 10 .3X,4# 11 .3X,4# 12 .3X,4#13
120 SUBROUTINE OUT1
79/05/10. 13.11.50

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79/05/10. 13.11.50

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130 37) WRITE (KOUT,300)
      FORMAT (11X,11HAG DRY YET)
      DO 429 J = 1,NJ
      DO 428 INJ = 1,ND
      IF (J - MOD(INJ)) 429,400,420
      WRITE (KOUT,410) J,(DEPR(J,K),K = 1,12),(DEPR(J,I),I = 1,3)
      FORMAT (10X,2X,12,10X,12F7.4,3X,314)
      CONTINUE
      GO TO 500
135 430 WRITE (KOUT,440)
      FORMAT (/10X,31HANNUAL RANKING FOR DEMAND MODES)
      DO 439 J = 1,NJ
      DO 438 INJ = 1,ND
      IF (J - MOD(INJ)) 439,450,430
      WRITE (KOUT,460)
      FORMAT (/)
      DO 470 I = 1,NYEAR
      WRITE (KOUT,480) J,I,DEPR(J,I)
      FORMAT (15X,9HNOE NO. ,12,3X,4HYEAR,13,3X,7HRANK = ,13)
      CONTINUE
145 490 WRITE (KOUT,100) TITLE
      WRITE (KOUT,510)
      FORMAT (/10X,30X,45HDESIGNED MONTHLY STORAGE LEVEL (PERCENT FULL)
      130X,4HRANK/10X,13HRESERVOIR NO.)
      IF (1ALLY,GT.0) GO TO 540
      DO 520 J = 1,MRES
      IF (MOD(J,8).EQ.0) WRITE (KOUT,100) TITLE
      WRITE (KOUT,530) J,(COND(L),OPRR(L,J),I = 1,12),OPRR(L,J),L = 1,3)
150 530 FORMAT (/10X,2X,12,3X,44,3X,12F7.4,5X,14/(17X,A4,3X,12F7.4,5X,14)X)
      GO TO 590
      DO 580 J = 1,MRES
      WRITE (KOUT,550)
      FORMAT (/)
      IF (MOD(J,5).EQ.0) WRITE (KOUT,100) TITLE
      DO 560 L = 1,NYEAR
      WRITE (KOUT,570) J,L,(OPRR(L,J),I = 1,12),OPRR(L,J)
      FORMAT (11X,12,3X,4HYEAR,12,2X,12F7.4,5X,14)
      CONTINUE
      WRITE (KOUT,600)
      FORMAT (/40X,33HRESERVOIRS AREA - CAPACITY TABLES//)
      K = 0
      M2 = 0
160 610 K = K + 1
      M1 = M2 + 1
      M2 = K + 6
      IF (M1.GT.MRES) M1 = 0
      IF (M2.GT.MRES) M2 = MRES
      IF (M1.EQ.0) GO TO 650
      IF (K.GT.1) WRITE (KOUT,100) TITLE
      SUBROUTINE OUT1
      OPT=2 TRACE
      FTR 4,6+452
      78/85/10. 13.11.58
170 620 WRITE (KOUT,620) (CRS,KRS = M1,M2)
      620 FORMAT (10X,614X,13HRESERVOIR NO.,13/3X,8HPOINT,2X,6(5X,4HYEAR,1X)11

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185 1.2X,8HCAPACITY))
      DO 630 NPT = 1, NPAIRS
      630 WRITE (KOUT,640) NPT, ((ACTAB(JN,NPT,KKK),KKK - 1,2),JN = M1,M2)
      640 FORMAT (3X,12.5X,6(19,1X,110))
      GO TO 610
      650 CONTINUE
      IF (IRTN.EQ.0) RETURN
      WRITE (KOUT,100) TITLE
      LAGS = 2 * NLAGS + 2
      DO 700 I = 1, NEQU
      IDUMB = MDNEQU(I)
      660 FORMAT (/10X,25#F0 RETURN FLOW EQUATION:,13,14# NO. OF LAGS *,13071 1950
      1.2# FLOW RETURNS TO NODE1,13)
      WRITE (KOUT,670) (IRTF(I,J),J = 1,IDLUM)
      670 FORMAT (/10X,41#NODE DEMANDS CONTRIBUTING TO RETURN FLOW:,1513)
      DO 690 J = 1, LAGS
      680 WRITE (KOUT,680) I,J,A(I,J)
      690 FORMAT (/10X,2#A(,12,1H,,12,2#)-,1X,G12.5)
      700 CONTINUE
      RETURN
205 C
      END 73/73 OPT=2 TRACE FTM 4.6+452 79/05/10. 13.11.59

SUBROUTINE OUT2
1 SUBROUTINE OUT2 (IY)
  INTEGER
  INTEGER
  1 CRAXU , P
  2 OPRP , RMH
  1 CONTROL/ , DEF
  1 KAPE4 , KIN , KOUT
  1 IPRINT , IYLD
  1 NL , NRES
  2 MS , NREAR
  3 NR , INN
  1 COMMON /PRINT/ , NPAIRS
  1 COMMON /RESU/ , ICAP(40,12,13)
  2 FSTART(40) , RMARE(40,2) , RCAP(40)
  3 OPRP(20,10) , ACTAB(10,18,2) , SP(10) , DEF(40)
  4 DEWR(40,20) , U(40,12) , IMP(2)
  1 COMMON /LKFLL/ , IMP(2,20)
  1 COMMON /LWPK(10,13) , LKFLO(50,13)
  1 COMMON /D/ , NORD(40) , IDSTRM(40)
  1 COMMON /LWML/ , LWML(50) , CHXRU(50,12)
  1 COMMON /LDATA/ , XLCF(50) , XCLL(50,12) , LOPT
  1 COMMON /R1/ , IALLY , IRTN
  1 MDNEQU(10) , NEQU , NLAGS
  2 IDIVL(10,15) , IRTFF(10,15) , JRTFF(10) ; IRTFF(10,240);
  STEP 01
20 C

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C          C          PRINT OUT MONTHLY DATA FOR YEAR
C          C          P = 1
C          C          ICALYR = IYEAR - 1 + IY
C          C          KTD = 0
C          C          DO 160 J = 1, NRES
C          C          IF (MOD(P,3).EQ.1.OR.J.EQ.1) WRITE (KOUT,100) TITLE,IV,ICALYR
C          C          100 FORMAT (1H1,20X,20A4//3X,15H SIMULATION YEAR,13,5X,13H CALENDAR YEAR,072
C          C          1,15)
C          C          WRITE (KOUT,110) J, (RNAME(J,1), I = 1,2), RCAP(J), RRIN(J)
C          C          110 FORMAT (/21X,12H RESERVOIR NO.13,2X,2A4,4X,13H MAX. CAPACITY,18,2X,1072
C          C          19H MIN. OPERATING POOL,18)
C          C          WRITE (KOUT,120)
C          C          120 FORMAT (1H0,9X,7H INITIAL,5X,4H REG,3X,6H UNSTR,12X,7H SURFACE,2X,4H 072
C          C          1EUMP,4X,4H EUMP,2X,7H UNSTR,12X,6H UNSTR,4X,6H UNSTR,1072
C          C          2X,7H END NO.,4X,5H OPER,13X,12X MONTH STORAGE INF LOSS SPILLS
C          C          3 DEMAND AREA RATE LOSS SPILLS SHORTAGE INTO OUT,072
C          C          4 LOSS CONTENT RULE)
C          C          DO 130 MON = 1,12
C          C          130 WRITE (KOUT,140) MON, (ICAP(J,MON,1), I = 1,5), EUMP(J,MON), (ICAP
C          C          1 J,MON,1), I = 6,13)
C          C          140 FORMAT (4X,12,2X,519,2X,16,219,18,419)
C          C          WRITE (KOUT,150) (TOTLS(J,IV,1), I = 2,4), (TOTLS(J,IV,1), I = 6,
C          C          1)
C          C          150 FORMAT (/1X,4X,12H YEAR TOTALS,219,15X,219,18,419)
C          C          P = P + 1
C          C          SUBROUTINE OUTE P = 73/73 OPT=2 TRACE PTH 40-400 79/05/10 13:31.59
C          C          160 CONTINUE
C          C          I1 = NRES + 1
C          C          DO 220 J = 11,NJ
C          C          220 INJ = 1,ND
C          C          IF (J = NORD(INJ)) 229,170,229
C          C          170 IF (MOD(P,3).EQ.1) WRITE (KOUT,100) TITLE,IV,ICALYR
C          C          WRITE (KOUT,180) J, (RNAME(J,1), I = 1,2)
C          C          180 FORMAT (/21X,11H DEMAND NODE,13,2X,2A4//21X,5H UNSTR,9X,6H DEMAND,5X,
C          C          110H SHORTAGE)
C          C          DO 190 MON = 1,12
C          C          190 WRITE (KOUT,200) MON,ICAP(J,MON,4),ICAP(J,MON,8)
C          C          200 FORMAT (21X,13,7X,110,5X,110)
C          C          WRITE (KOUT,210) TOTLS(J,IV,4),TOTLS(J,IV,8)
C          C          210 FORMAT (20X,11H YEAR TOTALS,2110,5X)
C          C          P = P + 1
C          C          220 CONTINUE
C          C          DO 230 L = 1,ML
C          C          IF (L.NE.1) GO TO 260
C          C          IF (MOD(P,2).EQ.1) GO TO 230
C          C          WRITE (KOUT,100) TITLE,IV,ICALYR
C          C          230 WRITE (KOUT,240)
C          C          240 FORMAT (/1X,48X,27H3 VOLUMETRIC FLOW IN LINE 1)

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85      WRITE (KOUT,250) (I,I - 1,12)
250  FORMAT (1X,6HSEASON,BX,12(12,7X),5HMERG/1X,5HLINK NO.)
260  LNKFL0(L,13) = 0
      X = 0.0
      DO 270 I = 1,12
270  X = X + FLOAT(LNKFL0(L,I))/12.
      CONTINUE
      LNKFL0(L,13) = IFIX(X)
      WRITE (KOUT,290) L,(LNKFL0(L,I),I - 1,13)
290  FORMAT (2I5,13I8)
      IF (LOPT) 320,320,300
300  WRITE (KOUT,310) (XCLL(L,I),I - 1,12)
310  FORMAT (1X,4X,4HLOSS,12F9.0,/)
320  CONTINUE
      IF (IRTN.EQ.0) RETURN
      WRITE (KOUT,330)
330  FORMAT (///1X,23HRETURN FLOWS CALCULATED,/)
      IBEG = ((IY - 1) * 12) + 1
      IEND = IBEG + 11
      DO 370 I = 1,NEQU
340  WRITE (KOUT,340) I,JRTF7(I)
      1NO.1,13,/)
      WRITE (KOUT,350) (J,J - 1,12)
350  FORMAT (1X,6HSEASON,BX,12(12,7X),/)
360  WRITE (KOUT,360) (JRTF(I,J),J - 1,IBEG,IEND)
370  CONTINUE
      RETURN
      END
SUBROUTINE OUT3      73/73      OPT=2 TRACE      FTH 4.6+452      79/05/10. 13.11.59
1      SUBROUTINE OUT3
      INTEGER /CONTROL/
      COMMON /KAP4/
1      COMMON /IPRINT/
      COMMON /PARR/
1      COMMON /NL
2      COMMON /MS
3      COMMON /NR
      COMMON /LNKFL0/
      COMMON /LNKFL0(50,13)
1      DIMENSION
      DIMENSION
      DATA AUE/4HMERG,4HAGE /,XPRX/4HMAXI,4HPLR /
      DATA DWA/4HNODE,4HYEAR/
20     IPTOB = 0
      IPTOU = 0
      IPTOI = 0
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IPTOD - 0
IPTOS - 0
IPTOL - 0
IPTOG - 0
25
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C
STEP 01
PRINT OUT YEARLY DATA FOR ALL NODES
30
DO 100 KY = 1,MYEAR
WRITE (KOUT,130) TITLE,DNR(2),KY,DNR(1)
DO 100 J = 1,NJ
100 WRITE (KOUT,160) J,(TOTLS(J,KY,N),N = 1,2),TOTLS(J,KY,4),TOTLS(J,
1V,8),TOTLS(J,KY,6),(TOTLS(J,KY,N),N = 11,12)
35
C
C
C
C
STEP 02
PRINT OUT NODE DATA FOR ALL YEARS
40
DO 120 J = 1,NJ
WRITE (KOUT,130) TITLE,DNR(1),J,DNR(2)
DO 110 KY = 1,MYEAR
110 WRITE (KOUT,160) KY,(TOTLS(J,KY,N),N = 1,2),TOTLS(J,KY,4),TOTLS(J,KY,
1),TOTLS(J,KY,6),(TOTLS(J,KY,N),N = 11,12)
45
C
IPTOB = IPTOB + TOTLS(J,KY,1)
IPTOU = IPTOU + TOTLS(J,KY,2)
IPTOD = IPTOD + TOTLS(J,KY,4)
IPTOS = IPTOS + TOTLS(J,KY,8)
IPTOE = IPTOE + TOTLS(J,KY,6)
IPTOL = IPTOL + TOTLS(J,KY,11)
IPTOG = IPTOG + TOTLS(J,KY,12)
50
C
110 CONTINUE
WRITE (KOUT,180) IPTOU,IPTOB,IPTOS,IPTOE,IPTOL
55
C
C
C
C
STEP 03
FIND YEARLY AVERAGES
80 SUBROUTINE OUT3
IPTOU = IPTOU/MYEAR
IPTOB = IPTOB/MYEAR
IPTOS = IPTOS/MYEAR
IPTOE = IPTOE/MYEAR
IPTOL = IPTOL/MYEAR
65
C
WRITE (KOUT,190) IPTOU,IPTOB,IPTOS,IPTOE,IPTOL
70
C
IPTOB = 0
IPTOU = 0
IPTOD = 0
IPTOS = 0
IPTOE = 0
IPTOL = 0
IPTOG = 0
75
120 CONTINUE

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79/05/10 13.11.59

0229 OT3  
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130 C          END          73/73  OPT=2 TRACE          FTN 4.6+462          073 1300
SUBROUTINE RIGHT          73/65/16. 13.11.59          073 1310
1          SUBROUTINE RIGHT (I,INDEX)          RHT 0010
COMMON /CONTROL/          RHT 0020
1          KAPE4          RHT 0030
COMMON /DATA/          RHT 0040
1          NR          RHT 0050
2          NTIME          RHT 0060
COMMON ILO(500)          RHT 0070
1          IJU(84)          RHT 0080
COMMON KOS(1000)          RHT 0090
1          LABL(84)          RHT 0100
COMMON JNU(1000)          RHT 0110
1          MID = MIDL(I)          RHT 0120
IA = NODE(I)          RHT 0130
DO 100 II = IA,MID          RHT 0140
IF (RIR(II) - INDEX) 100,130,100          RHT 0150
100 CONTINUE          RHT 0160
110 KWAY = 1          RHT 0170
WRITE (KOUT,160) I,INDEX,KWAY          RHT 0180
IFROM = NODE(I)          RHT 0190
120 FORMAT (316/(2016))          RHT 0200
RETURN          RHT 0210
130 ITEMP = MIR(MID)          RHT 0220
MIR(MID) = INDEX          RHT 0230
MIR(II) = ITEMP          RHT 0240
MIDL(I) = MID - 1          RHT 0250
RETURN          RHT 0260
ENTRY LEFT          RHT 0270
MID = MIDL(I) + 1          RHT 0280
IB = NODE(I + 1) - 1          RHT 0290
DO 140 II = MID,IB          RHT 0300
IF (RIR(II) - INDEX) 140,150,140          RHT 0310
140 CONTINUE          RHT 0320
KWAY = 2          RHT 0330
GO TO 110          RHT 0340
150 ITEMP = MIR(MID)          RHT 0350
MIR(MID) = INDEX          RHT 0360
MIR(II) = ITEMP          RHT 0370
MIDL(I) = MID          RHT 0380
RETURN          RHT 0390
160 FORMAT (5H NODE,15,5H ARC,15,16H LOST ON SHIFT ,14,4H LOC,14)
ENTRY DUMPO          RHT 0400
ID = INDEX          RHT 0410
MLINES = I          RHT 0420
WRITE (KOUT,210) ID          RHT 0430
DO 190 R = 1,MLINES          RHT 0440
N = R + NR          RHT 0450
J = NA(N)          RHT 0460
L = ILO(R)          RHT 0470
K = JSAVE(R)          RHT 0480
KOST = ISAVE(R)          RHT 0490
KBAR = KOS(R)          RHT 0500
RHT 0510
RHT 0520

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55      IFLOW = K - NC(N)
        IF (IFLOW.LT.L.OR.IFLOW.GT.K) WRITE (KOUT,220)
        IF (KBAR) 170,190,180
        IF (IFLOW.LT.K) WRITE (KOUT,230)
        GO TO 190
170      IF (IFLOW.GT.L) WRITE (KOUT,230)
180      WRITE (KOUT,200) N,I,J,L,K,IFLOW,KOST,KINAR
200      FORMAT ('315,310,5X,210')
60      SUBROUTINE RIGHT
      73/73 OPT=2 TRACE          FTM 4.6+452
      79/05/10. 13.11.59

210      FORMAT ('71H1 ARC I J L K IFLOW
1      KOST
      KBAR,115/')
220      FORMAT ('30H THE FOLLOWING ARC IS PRIMAL INFEASIBLE)
230      FORMAT ('37H THE FOLLOWING ARC IS DUAL INFEASIBLE)
      RETURN
65      C
      SUBROUTINE RTFLOU 73/73 OPT=2 TRACE          FTM 4.6+452
      79/05/10. 13.11.59

1      SUBROUTINE RTFLOU (NDM,IV,JFLAG2,ICONV,JPROV,L7,L8)
      COMMON /CONTROL/ KIN , KOUT , KAPE1 ,
1      INTEGER /ADATA/ FLOW , COST
      COMMON /MARC/ MARC , NMAX , FESIBL
1      NTIME , NT(500) , NF(500) , MI(500) ,
2      LO(500) , FLOW(500) , COST(500)
      COMMON /RI/ NEQU , NLAGS , A(10,15)
1      NDMENU(10) , IRTF(10,15) , JRTFF(10) ,
2      IDIUL(10,15) , IRI(10) , IPASTD(40,240) ,
1      IDIF(10)
      DATA IPASTD/960000/
      DO 110 I = 1,10
      DO 100 II = 1,15
      IADD(I,II) = 0
100      CONTINUE
110      CONTINUE
      DO 120 L = L7,L8
      JN = NF(L)
      IPASTD(JN,JPROV) = FLOW(L)
120      CONTINUE
      C
25      IF (ICONV.EQ.1) GO TO 140
      DO 130 I = 1,NEQU
      IRI(I) = 0
130      CONTINUE
      ICOUNT = 0
140      ICOUNT = ICOUNT + 1
      IF (JPROV.LE.NLAGS) GO TO 260
      DO 170 I = 1,NEQU
      IDURS = NDMENU(I)
      DO 150 J = 1,IDIURS
      IXX = IRTFF(I,J)
      IADD(I,1) = IADD(I,1) + IPASTD(IXX,JPROV)
      DO 150 N = 1,NLAGS
      IADD(I,N + 1) = IADD(I,N + 1) + IPASTD(IXX,JPROV - N)
      RTF 0010
      RTF 0020
      RTF 0030
      RTF 0040
      RTF 0050
      RTF 0060
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      RTF 0080
      RTF 0090
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      RTF 0210
      RTF 0220
      RTF 0230
      RTF 0240
      RTF 0250
      RTF 0260
      RTF 0270
      RTF 0280
      RTF 0290
      RTF 0300
      RTF 0310
      RTF 0320
      RTF 0330
      RTF 0340
      RTF 0350
      RTF 0360
      RTF 0370

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150 CONTINUE
160 CONTINUE
170 CONTINUE
DO 190 I = 1, NEQU
  IRTF(I, JRMNY) = INT(A(I, 1) + A(I, 2) * FLOAT(IADD(I, 1)))
  DO 180 N = 1, NLAGS
    IRTF(I, JRMNY) = IRTF(I, JRMNY) + INT(A(I, N + 2) * FLOAT(IADD(I, 1)))
    I, N + 1))) + INT(A(I, NLAGS + N + 2) * FLOAT(IRT(I, JRMNY -
1  I, N + 1)))
2 IRTF(I, JRMNY)
180 CONTINUE
190 CONTINUE
199 IF (ICONV.EQ.1) GO TO 220
200 DO 210 I = 1, NEQU
  IRI(I) = IRTF(I, JRMNY)
210 CONTINUE
  JFLAG2 = 0
  ICONV = 1
  RETURN
220 JFLAG2 = 1
  DO 230 I = 1, NEQU
    IRI(I) = IABS(IRI(I) - IRTF(I, JRMNY))
    IF (IDIF(I).LE.1) GO TO 230
    JFLAG2 = 0
60 SUBROUTINE RTFLOW 73/73 OPT=2 TRACE FTM 4.6*452 78/85/10. 13.11.59

  IRI(I) = IRTF(I, JRMNY)
230 CONTINUE
  IF (ICOUNT.GT.10) GO TO 240
  RETURN
240 WRITE (KOUT, 250) MON, IY
250 FORMAT (1H-, 5X, 12, /)
  IRTFLOW WILL NOT CONVERGE MONTH
  JFLAG2 = 1
  RETURN
260 NBACK = NLAGS - JRMNY + 1
  NPAST = NLAGS - NBACK
  DO 300 I = 1, NEQU
    IDLMB = NNEG(I)
    DO 300 J = 1, IDLMB
      IXX = IRTF(I, J)
      IADD(I, J) = IADD(I, J) + IPASTD(IXX, JRMNY)
      IF (NPAST.EQ.0) GO TO 280
      DO 270 N = 1, NPAST
        IADD(I, N + 1) = IADD(I, N + 1) + IPASTD(IXX, JRMNY - N)
        IADD(I, NLAGS + N + 1) = IRTF(I, JRMNY - N)
      CONTINUE
      DO 290 N = 1, NBACK
        IADD(I, NPAST + N + 1) = IDIVL(I, N)
        IADD(I, NLAGS + NPAST + N + 1) = IRTL(I, N)
      CONTINUE
290 CONTINUE
300 IRTF(I, JRMNY) = INT(A(I, 1) + A(I, 2) * FLOAT(IADD(I, 1)))
  DO 310 N = 1, NLAGS
    IRTF(I, JRMNY) = IRTF(I, JRMNY) + INT(A(I, N + 2) * FLOAT(IADD(I, 1)))
    I, N + 1))) + INT(A(I, NLAGS + N + 2) * FLOAT(IADD(I, NLAGS +
1  I, N + 1)))
2  IRTF(I, JRMNY)

```



```

310 CONTINUE
320 CONTINUE
GO TO 200
END
95 SUBROUTINE SETNET 73/73 OPT-2 TRACE FTM 4.6+462
1 SUBROUTINE SETNET
COMMON /CONTROL/
KIN , KAPE1 ,
1 COMMON /PARL/
NJ ,
2 COMMON /NL/
NC , NRES ,
3 COMMON /MS/
NYEAR , NUNJC ,
COMMON /LINK/
NPAIRS , INN , TITLE(20) ,
COMMON /ADATA/
LNODE(50,2) , CMAX(50) ,
COMMON /TIME/
NARC , NMAX , CRIN(50) ,
1 NT(500) , NF(500) , FESIBL ,
2 LO(500) , FLOW(500) , HI(500) ,
C COST(500) ,
C
15 STEP 01
C SET UP ALL FROM AND TO NODES BY LINK NO.
C
20 DO 100 L = 1,NL
C NF(L) = LNODE(L,1)
C NT(L) = LNODE(L,2)
C 100 CONTINUE
C
25 NARC = NL
C N = NJ + 1
C DO 110 K = 1,NJ
C NARC = NARC + 1
C NF(NARC) = N
C NT(NARC) = K
C 110 CONTINUE
C
30 STEP 02
C SET UP ALL INITIAL ARCS
C
35 N = NJ + 2
C DO 120 K = 1,NJ
C NARC = NARC + 1
C NF(NARC) = K
C NT(NARC) = N
C 120 CONTINUE
C
40 STEP 03
C SET UP ALL DESIRED STORAGE ARCS
C
45 DO 130 K = 1,NJ
C NARC = NARC + 1
C NF(NARC) = K
C NT(NARC) = N
C 130 CONTINUE
C
50

```

```

RTF 0920
RTF 0930
RTF 0940
RTF 0950
79/05/10. 13.11.59
SET 0010
SET 0020
SET 0030
SET 0040
SET 0050
SET 0060
SET 0070
SET 0080
SET 0090
SET 0100
SET 0110
SET 0120
SET 0130
SET 0140
SET 0150
SET 0160
SET 0170
SET 0180
SET 0190
SET 0200
SET 0210
SET 0220
SET 0230
SET 0240
SET 0250
SET 0260
SET 0270
SET 0280
SET 0290
SET 0300
SET 0310
SET 0320
SET 0330
SET 0340
SET 0350
SET 0360
SET 0370
SET 0380
SET 0390
SET 0400
SET 0410
SET 0420
SET 0430
SET 0440
SET 0450
SET 0460
SET 0470
SET 0480
SET 0490
SET 0500

```

```

STEP 05
SET UP ALL DEMAND ARCS
C
C
C
55      H = NJ + 3
        DO 140 K = 1, NJ
          NARC = NARC + 1
          NT(NARC) = N
          NF(NARC) = K
        140 CONTINUE
60 SUBROUTINE SETNET 73/73 OPT=2 TRACE      FTN 4.6+452      79/05/10. 13.11.59
C
C
C      STEP 06
      SET UP ALL SPILL ARCS
65      N = NJ + 4
        DO 150 K = 1, NRES
          NARC = NARC + 1
          NT(NARC) = N
          NF(NARC) = K
        150 CONTINUE
70      C
        C
        C      STEP 07
        SET UP MASS BALANCE ARCS
75      NMAX = NJ + 5
          NF(NARC + 1) = NJ + 2
          NT(NARC + 1) = NMAX
          NF(NARC + 2) = NJ + 4
          NT(NARC + 2) = NMAX
          NF(NARC + 3) = NJ + 3
          NT(NARC + 3) = NMAX
          NF(NARC + 4) = NMAX
          NT(NARC + 4) = NJ + 1
80      C
85      NARC = NARC + 4
          RETURN
        C
        C      END
SUBROUTINE SUPERK 73/73 OPT=2 TRACE      FTN 4.6+452      79/05/10. 13.11.59
1      SUBROUTINE SUPERK
      COMMON /CONTROL/
      1 COMMON /ADATA/
      1 COMMON /NTIME/
      2 COMMON /ILO(S00)/
      1 COMMON /IWI(B4)/
      1 COMMON /KOB(1000)/
      LOGICAL /JAU(1000)
      LOGICAL /FESIBL/
      NAXA = 500
      FESIBL = .TRUE.
      IFLW = 0
      KLAB = 0
5      KIN
      NR
      NI(S00)
      NC(S00)
      LABL(B4)
      RIR(1000)
      NSAU(B4)
      KOUT
      NI(S00)
      ISAU(S00)
      NODE(B4)
      MIDL(B4)
      KAPE1
      FESIBL
      JSAU(S00)
10     SPK 0010
      SPK 0020
      SPK 0030
      SPK 0040
      SPK 0050
      SPK 0060
      SPK 0070
      SPK 0080
      SPK 0090
      SPK 0100
      SPK 0110
      SPK 0120
      SPK 0130
      SPK 0140
      SPK 0150
15

```



```

70      170 MIDL(K) = KL - 1
        DO 200 L = 1, NR
          LL = L + NR
          J = NA(LL)
          I = MA(LL)
          KOST = KOS(LL)
          K = MC(LL)
          LO = - MC(LL)
C
C      80      RIGHT=2 LEFT=1
C
C      85      MAIN = 2
          MIRROR = 2
          IF (KOST) 190, 190, 190
          IF (K) 210, 210, 200
          IF (LO) 240, 250, 200
          MAIN = 1
          IF (KOST) 220, 230, 230
          IF (K) 240, 250, 250
          IF (LO) 240, 250, 250
          MIRROR = 1
          IF (MAIN.EQ.2) GO TO 260
          II = JUV(I)
          MIR(II) = L
          GO TO 270
          JUV(I) = II + 1
          II = MIDL(I)
          MIR(II) = L
          MIDL(II) = II - 1
          IF (MIRROR.EQ.2) GO TO 280
          II = JUV(J)
          MIR(II) = LL
          JUV(J) = II + 1
          GO TO 280
          II = MIDL(J)
          MIR(II) = LL
          MIDL(J) = II - 1
          200 CONTINUE
C
C      110      *****
          GO - SUPERKILTER
          *****
C
C      115      ND = INFIN
          MAIN LOOP (1000)
C
C      120      NR2 = NR * 2
          DO 1130 MAIN = 1, NR
            73/73 OPT=2 TRACE
          SUBROUTINE SUPERK
            MAINP = MAIN + NR
            DO 1130 MODE = 1, 2
              IF (MODE.EQ.2) GO TO 300
            73/85/10. 13.11.59
          FTN 4.8+452
          SPK 1210
          SPK 1220
          SPK 1230
          SPK 0700
          SPK 0710
          SPK 0720
          SPK 0730
          SPK 0740
          SPK 0750
          SPK 0760
          SPK 0770
          SPK 0780
          SPK 0790
          SPK 0800
          SPK 0810
          SPK 0820
          SPK 0830
          SPK 0840
          SPK 0850
          SPK 0860
          SPK 0870
          SPK 0880
          SPK 0890
          SPK 0900
          SPK 0910
          SPK 0920
          SPK 0930
          SPK 0940
          SPK 0950
          SPK 0960
          SPK 0970
          SPK 0980
          SPK 0990
          SPK 1000
          SPK 1010
          SPK 1020
          SPK 1030
          SPK 1040
          SPK 1050
          SPK 1060
          SPK 1070
          SPK 1080
          SPK 1090
          SPK 1100
          SPK 1110
          SPK 1120
          SPK 1130
          SPK 1140
          SPK 1150
          SPK 1160
          SPK 1170
          SPK 1180
          SPK 1190
          SPK 1200
          73/85/10. 13.11.59
          SPK 1210
          SPK 1220
          SPK 1230
    
```

```

125      II = MAIN
      JZ = MAIN
      GO TO 310
130      II = MAIN
      JZ = MAIN
      IF (NC(II)) 350,320,330
      IF (NC(JZ)) 340,1120,1120
      IF (K05(II)) 340,320,320
      C
      C      15, IT = START, END NODE NOS, JS, JT = ARC, MIRROR ARC NOS
      C      FOR ARC NEEDING FLOW INCREASE
      C      WANT TO INCREASE FLOW, START LABELING AT JJ
      C
      C      15 = NA(JZ)
      C      JS = II
      C      JT = NA(II)
      C      JT = JZ
      C      GO TO 360
      C
      C      WANT TO DECREASE FLOW, START LABELING AT II
      C
      C      15 = NA(JZ)
      C      JS = NA(II)
      C      JS = JZ
      C      JY = II
150      LABELING PROCEDURE
      C
      C      IPL = 1
      C      IPLL = 1
      C      IPS = 0
      C      NUMS = 0
      C      LABL(IT) = JS
      C      IUU(IPL) = IT
      C      KLAB = KLAB + 1
      C      GO TO 390
      C      IF (IPS - IPL) 390, 640, 390
      C      IPS = IPS + 1
      C      IA = IUU(IPS)
      C      IB = NODE(IA)
      C      IC = MIDL(IA)
      C      IF (IB - IC) 400, 400, 390
      C      DO 420 JJ = IB, IC
      C      J = MIR(JJ)
      C      MNODE = NA(J)
      C      IF (LABL(MNODE)) 420, 410, 420
      C      LABL(MNODE) = J
      C      IPL = IPL + 1
      C      IUU(IPL) = MNODE
      C      IF (MNODE - IS) 420, 430, 420
      C      CONTINUE
      C      GO TO 390
      C
      C      BREAKTHROUGH BREAKTHROUGH BREAKTHROUGH
      C      KBRK = KBRK + 1
175
170
165
160
155
145
140
135
300
310
320
330
340
350
360
370
380
390
400
410
420
430

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SPK 1248
SPK 1250
SPK 1252
SPK 1270
SPK 1280
SPK 1290
SPK 1300
SPK 1310
SPK 1320
SPK 1330
SPK 1340
SPK 1350
SPK 1360
SPK 1370
SPK 1380
SPK 1390
SPK 1400
SPK 1410
SPK 1420
SPK 1430
SPK 1440
SPK 1450
SPK 1460
SPK 1470
SPK 1480
SPK 1490
SPK 1500
SPK 1510
SPK 1520
SPK 1530
SPK 1540
SPK 1550
SPK 1560
SPK 1570
SPK 1580
SPK 1590
SPK 1600
SPK 1610
SPK 1620
SPK 1630
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SPK 1650
SPK 1660
SPK 1670
SPK 1680
SPK 1690
SPK 1700
SPK 1710
SPK 1720
SPK 1730
SPK 1740
SPK 1750
SPK 1760
SPK 1770
SPK 1780
SPK 1790

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SPK 1800  
79/05/10. 13.11.59

FTM 4.6+452

180 SUBROUTINE SUPERK IALPHA = IMFIN OPT=2 TRACE

```

C C C FIRST RETRACE
C C C IJ = PREDECESSOR ARC INDEX
C C C JI = MIRROR ARC INDEX
C C C K = JAU POINTER
C C C NEXT = PREDECESSOR NODE
C C C
C C C K = 0
C C C NOU = IS
C C C IJ = LABL( NOU )
C C C JI = IJ - NR
C C C IF ( JI ) 450, 460, 468
C C C JI = JI + NR2
C C C NEXT = NA( JI )
C C C K = K + 1
C C C IF (KOS(IJ)) 480, 480, 470
C C C NET = - NC( JI )
C C C JAU( K ) = NET
C C C GO TO 490
C C C NET = NC( IJ )
C C C JAU( K ) = NET
C C C IALPHA = MIMO( IALPHA, NET )
C C C IF ( NEXT - IS ) 500, 510, 500
C C C NOU = NEXT
C C C GO TO 440
C C C SECOND RETRACE
C C C K = 0
C C C NOU = IS
C C C IJ = LABL( NOU )
C C C JI = IJ - NR
C C C IF ( JI ) 530, 530, 546
C C C JI = JI + NR2
C C C NEXT = NA( JI )
C C C K = K + 1
C C C NC( IJ ) = NC( IJ ) - IALPHA
C C C NET = NC( JI )
C C C NETNU = NET + IALPHA
C C C NC( JI ) = NETNU
C C C IF (KOS(JI)) 500, 550, 580
C C C IF ( NET ) 560, 560, 500
C C C IF ( NETNU ) 580, 580, 570
C C C CALL LEFT ( NOU, JI )
C C C IF ( JAU( K ) - IALPHA ) 600, 590, 600
C C C CALL RIGHT ( NEXT, IJ )
C C C IF ( NEXT - IS ) 610, 620, 610
C C C NOU = NEXT
C C C GO TO 520
C C C ERASE LABELS AND GO FOR O-K CHECK
C C C

```

185  
190  
195  
200  
205  
210  
215  
220  
225  
230

SPK 1810  
SPK 1820  
SPK 1830  
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SPK 1850  
SPK 1860  
SPK 1870  
SPK 1880  
SPK 1890  
SPK 1900  
SPK 1910  
SPK 1920  
SPK 1930  
SPK 1940  
SPK 1950  
SPK 1960  
SPK 1970  
SPK 1980  
SPK 1990  
SPK 2000  
SPK 2010  
SPK 2020  
SPK 2030  
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SPK 2110  
SPK 2120  
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SPK 2160  
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SPK 2180  
SPK 2190  
SPK 2200  
SPK 2210  
SPK 2220  
SPK 2230  
SPK 2240  
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SPK 2260  
SPK 2270  
SPK 2280  
SPK 2290  
SPK 2300  
SPK 2310  
SPK 2320  
SPK 2330

```

235      DO 630 I = 1, IPL
          J = IUV(I)
          LABL(J) = 0
          GO TO 310
          C
          C      POTENTIAL CHANGE
          C
240 SUBROUTINE SUPERK 73/73 OPT=2 TRACE          FTM 4.6+452          73/05/10. 13.11.59
          C
          C      KPOT = KPOT + 1
          C      KSET = NURS
          C      NEULAB = 0
          C      NURS = 0
          C      JINTHRU = 0
          C      MIN = IMFIN
          C      NEU = NONS
          C      NONS = MAXA + 1
          C      IF (KSET) 740, 740, 650
          C      IF (NEU - MAXA) 660, 660, 690
          C
          C      NON-5 (L, L-) SET RECYCLING FILTER
          C
          C      MAXNEU = MAXA + NEU
          C      DO 680 L = NEU, MAXA
          C      K = MAXNEU - L
          C      KK = JUU(K)
          C      KKK = MA(KK)
          C      IF (LABL(KKK)) 680, 670, 680
          C      NONS = NONS - 1
          C      JUU(NONS) = KK
          C      CONTINUE
          C
          C      S-SET RECYCLING FILTER
          C
          C      DO 730 K = 1, KSET
          C      KK = JUU(K)
          C      KKK = MA(KK)
          C      IF (LABL(KKK)) 730, 700, 730
          C      IF (KOS(KK)) 720, 720, 710
          C      NURS = NURS + 1
          C      JUU(NURS) = KK
          C      MIN = MIN(MIN, KOS(KK))
          C      GO TO 730
          C      NONS = NONS - 1
          C      JUU(NONS) = KK
          C      CONTINUE
          C      CONTINUE
          C      IF (IPLL - IPL) 760, 760, 830
          C
          C      FIND MIN(C-BAR) OVER SET S
          C
          C      DO 820 LL = IPLL, IPL
          C      L = IUV(LL)
          C      JMIN = NIDL(L) + 1
          C      JNT = NODE(L + 1) - 1
          C      IF (JMIN - JNT) 700, 700, 820

```

```

SPK 2310
SPK 2350
SPK 2360
SPK 2370
SPK 2380
SPK 2390
SPK 2400
73/05/10. 13.11.59
SPK 2410
SPK 2420
SPK 2430
SPK 2440
SPK 2450
SPK 2460
SPK 2470
SPK 2480
SPK 2490
SPK 2500
SPK 2510
SPK 2520
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SPK 2580
SPK 2590
SPK 2600
SPK 2610
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SPK 2690
SPK 2700
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SPK 2870

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SPK 3420  
 SPK 3430  
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 SPK 3480  
 SPK 3490  
 SPK 3500  
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 SPK 3520  
 SPK 3530  
 SPK 3540  
 SPK 3550  
 SPK 3560  
 SPK 3570  
 SPK 3580  
 SPK 3590  
 SPK 3600  
 78/05/10. 13.11.59

SPK 3610  
 SPK 3620  
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 SPK 3800  
 SPK 3810  
 SPK 3820  
 SPK 3830  
 SPK 3840  
 SPK 3850  
 SPK 3860

```

345      IF (NONS - MAXA) 970,970,1050
          DO 1040 I = NONS,MAXA
             JJ = JUU(I)
             JI = IJ - NR
             IF (JI) 980,980,990
             JI = IJ + NR
             KOSTA = KOS(IJ)
             KOSTB = KOSTA - MIN
             KOS(IJ) = KOSTB
             KOS(JI) = - KOSTB
          C
          C CHECK FOR MIRROR LEAVING NJ STATE
          C CHECK LATER FOR COMBINING IF-CHECKS HERE
          C
355      IF (KOSTA) 1040,1000,1000
          IF (KOSTB) 1010,1040,1040
          IF (NC(IJ)) 1040,1020,1020
          IF (NC(JZ)) 1040,1040,1030
          CALL RIGHT (NA(IJ),JI)
          73/73 OPT-2 TRACE
          SUBROUTINE SUPERK
          C
          C 1040 CONTINUE
          C
          C OUT-OF-FILTER CHECK
          C
365      IF (NC(II)) 1090,1050,1070
          IF (NC(JZ)) 1080,1100,1100
          IF (KOS(II)) 1090,1060,1050
          C
          C BREAKTHROUGH CHECK
          C
370      IF (IPTHRU) 1090,1090,430
          IF (IPS - IPL) 370,640,370
          DO 1110 I = 1,IPL
             J = IJU(I)
             LAB(IJ) = 0
          1120 CONTINUE
          1130 CONTINUE
          TOTAL = 0.
          DO 1140 I = 1,NR
             KOS(I) = KOS(I) - ISAME(I)
             NC(I) = JSAME(I) - NC(I)
             TOTAL = TOTAL + NC(I) + ISAME(I)
          1140 CONTINUE
          RETURN
          C
385      END
  
```

FTN 4.6+452

APPENDIX E

ACKNOWLEDGMENT OF RESEARCH BY WATER COMMISSIONER,  
DISTRICT NO. 3



## DIVISION OF WATER RESOURCES

DEPARTMENT OF NATURAL RESOURCES

James R. Clark P.E.

IRRIGATION DIVISION ENGINEER

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On behalf of the Division of Water Resources I wish to compliment John Shafer and others on his thesis for the improved management of the waters in the high mountain reservoirs for the benefit of fishing and recreation interests without causing injury to irrigators.

Much of the data was obtained from the records of the Division of Water Resources compiled by myself and previous water commissioners. It is encouraging to have interested parties affirm the management of the water in the Poudre River for multipurpose use.

A handwritten signature in cursive script that reads 'John W. Neutze'. The signature is written in dark ink and is positioned above the printed name.

John W. Neutze

Water Commissioner, District No. 3

COMPLETION REPORT SERIES

<u>No.</u>	<u>Title</u>	<u>Date</u>	<u>Price</u>
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10.	Economics and Administration of Water Resources	6/69	2.50
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18.	Experimental Investigation of Small Watershed Floods	6/70	5.00
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