

TRA 2.10/91-8
c.2

Report No. CDOT-DTD-91-8

USE OF FLY ASH IN STRUCTURAL CONCRETE

Dave Woodham
Colorado Department of Transportation
4201 East Arkansas Avenue
Denver, Colorado 80222

Final Report
July, 1991

Prepared in cooperation with the
U.S. Department of Transportation
Federal Highway Administration

COLORADO STATE PUBLICATIONS LIBRARY
TRA2.10/91-8 c.2 local
Woodham, David B./The use of fly ash in



3 1799 00016 6082

The contents of this report reflect the views of the author who is responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views of the Colorado Department of Highways or the Federal Highway Administration. This report does not constitute a standard, specification, or regulation.

1. Report No. CDOT-DTD-R-91-8	2. Government Accession No.	3. Recipient's Catalog No.	
4. Title and Subtitle Use of Fly Ash in Structural Concrete		5. Report Date July, 1991	6. Performing Organization Code
		8. Performing Organization Rpt.No. CDOT-DTD-R-91-8	
7. Author(s) Dave Woodham		10. Work Unit No.(TR AIS)	
9. Performing Organization Name and Address Colorado Department of Highways 4201 E. Arkansas Avenue Denver, Colorado 80222		11. Contract or Grant No. DTFH71-85-59-CO-13	
		13. Type of Rpt. and Period Covered Final Report	
12. Sponsoring Agency Name and Address Colorado Department of Highways 4201 E. Arkansas Avenue Denver, Colorado 80222		14. Sponsoring Agency Code	
		15. Supplementary Notes Prepared in Cooperation with the U.S. Department of Transportation, Federal Highway Administration	
16. Abstract Limited data has been gathered on the performance of two bridge structures built in 1986 using fly ash concrete. Fly ash was used as a replacement for 15% of the cement in the mix. The use of fly ash caused several problems including: inconsistent setting, a rough and open surface texture, variable air and slump measurements, and shrinkage cracking. Most of these problems have been resolved due to increased knowledge of how fly ash works in concrete mixes and additional experience with the product. Implementation No changes to the current CDOT specifications, which allows contractors to substitute up to 20% fly ash (by weight), are proposed as the result of this research.			
17. Key Words Fly ash, Concrete Bridge Decks		18. Distribution Statement No Restrictions: This report is available to the public through the National Information Service, Springfield, Virginia 22161	
19. Security Classif. (of this report) Unclassified	20. Security Classif.(of this page) Unclassified	21. No. of Pages 29	22. Price

Table of Contents

Introduction 1

Background 1

Monitoring 3

Conclusions 4

Implementation 5

Appendices

- Appendix A. Photographs of the Bridges.
- Appendix B. Concrete Mix Designs.

Introduction

The structures and mix designs are given below for clarification. In 1986, three bridges were constructed using concrete containing fly ash under Demonstration Project 59, The Use of Fly Ash in Structural Concrete. A fourth structure was constructed using CDOT's standard class of structural concrete as a control. This Demonstration Project was designed to give states the opportunity to use fly ash on a highway project with technical and financial help from the Federal Highway Administration. The benefits of using fly ash in concrete include: increased strength, reduced alkali-silica reactions, and reduced cost of the mix.

This report discusses the performance of the structures during the past five years. A previously published report [1] describes the construction of the four structures and comments on the problems and anomalies observed.

Background

The four structures covered under this study were all constructed on route C-470 southwest of Denver (please see Figure 1). There were two sets of twin structures constructed—two over Kipling St. and two over Ken Caryl Rd. All structures were built in 1985 and 1986. Photographs of the structures are shown in Appendix A.

The Kipling structures were opened to traffic in the summer of 1986 while the two bridges at Ken Caryl were opened to traffic in October of 1990.

Fly ash was required in all concrete used at the Kipling St. structures and was optional for the two bridges at Ken Caryl. However, the contractor chose to use fly ash on one of the Ken Caryl structures as well. The contractor used fly ash as a replacement for 15% of the cement in the concretes. Colorado Class D mix is typically used in bridge decks with Class B mix being used in piers and abutments. The girders used for the bridges were of precast, prestressed concrete. Complete mix designs are shown in Appendix B.

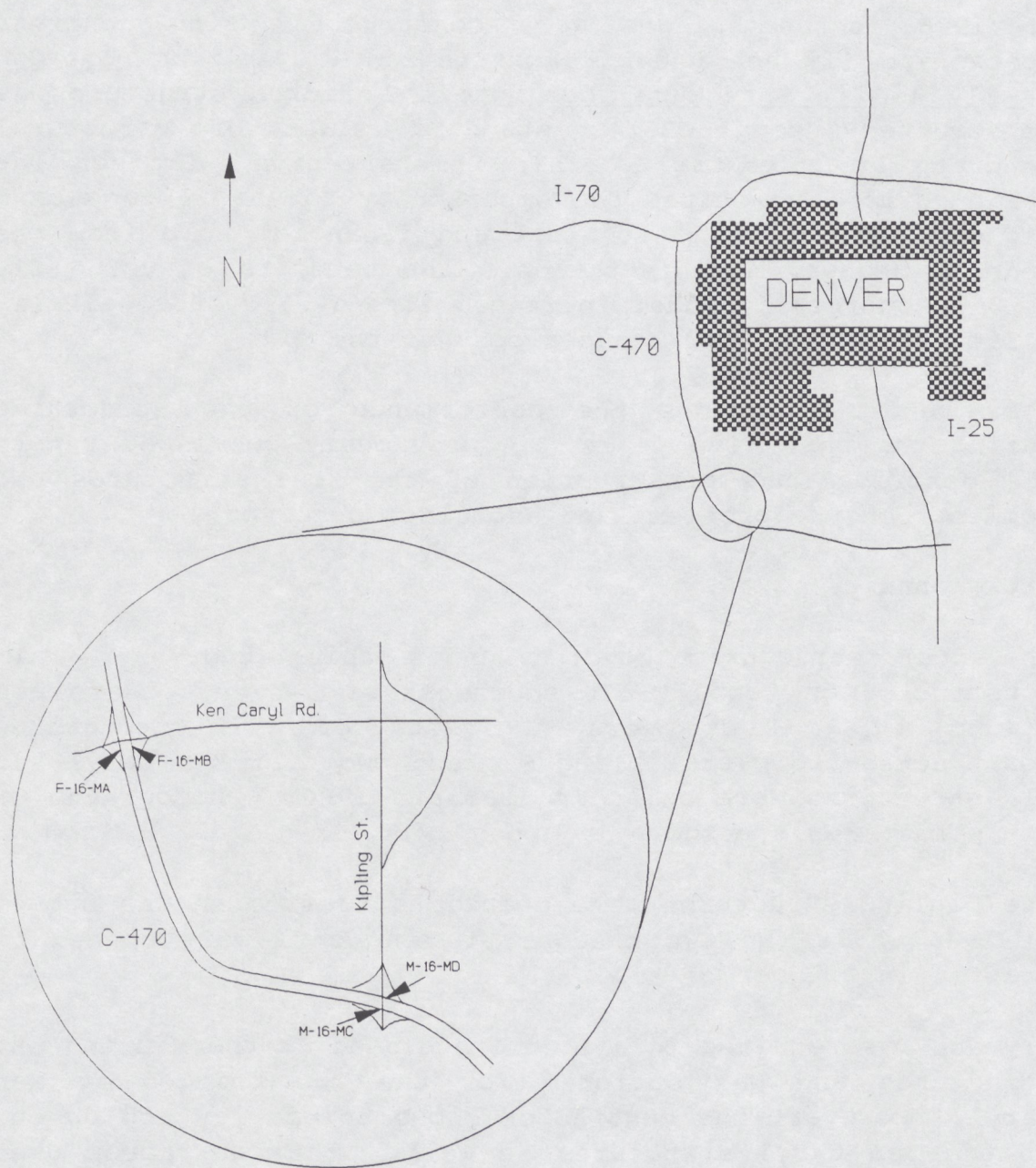


FIGURE 1. LOCATION OF STRUCTURES

The structures and mix designs are given below for clarification:

<u>Structure</u>	<u>Feature Intersected</u>	<u>Type of concrete</u>
F-16-MA	Ken Caryl Rd. (EB)	Class D & B w/ Fly Ash
F-16-MB	Ken Caryl Rd. (WB)	Class D & B no Fly Ash
F-16-MC	Kipling St. (EB)	Class D & B w/ Fly Ash
F-16-MD	Kipling St. (WB)	Class D & B w/ Fly Ash

A total of 54.2 tons of fly ash were used in place of cement on the Kipling St. structures. Given the cost difference between cement and fly ash (\$78.00 vs. \$30.90 per ton) in 1986, the use of fly ash saved some \$2,550 [1] in material costs on this project.

Energy savings of 394 million BTU [1] were also realized due to the use of fly ash on the two Kipling St. bridges. In other terms, this amount of energy is roughly equivalent to that contained in 3,200 gallons of gasoline.

Monitoring

Problems during placement of the fly ash mixture included: inconsistent setting, a rough and open surface texture, variable air and slump measurements, as well as shrinkage cracking.

Since the two structures at Kipling St. were covered with a membrane and asphalt overlay shortly after construction, monitoring of the structures consisted of looking for signs of cracking and efflorescence from the bottom side of the structure.

The parallel structures at Ken Caryl were finished in the spring of 1986 but were not opened to traffic until fall of 1990. The Ken Caryl bridges were located at the end of the Phase II construction and were not connected to the roadway until the final phase of C-470 was completed. Since these structures did not carry traffic until over four years later than the Kipling structures, comparisons between the two sets of structures are not meaningful at this time. Visual observations of the Kipling St. structures have not shown signs of deterioration.

Conclusions

The use of fly ash has the potential for cost savings in highway construction. Given the cost difference between cement and fly ash of approximately \$47 per ton in 1986, the savings amounts to \$2.35 per cubic yard for class D or \$2.00 per cubic yard for class B concretes. Both these figures are on the order of 1% of the in-place costs for these concretes [2].

Current prices in the metropolitan-Denver area are approximately \$63 per ton for cement and \$36.90 for fly ash. Given this cost difference of \$26.10 and a maximum replacement of 20% of the cement, the cost savings (per ton) are potentially \$1.70 for class D or \$1.50 for class B concretes.

The net savings in energy use as a result of using fly ash is dependent on the location of the fly ash source in relation to the project. If haul distances are too great both the energy and cost advantages of fly ash will be reduced.

One additional benefit of using fly ash (in any manner) is the reduction in volumes of ash that must be disposed of. This recycling aspect will most likely become more important as many landfills are reaching capacity and new landfills face public opposition and increased costs.

The use of fly ash created problems with workability and a quality finish on this project. However, many of the problems experienced during the construction of these bridges in 1986 have been resolved due to an increased knowledge of how fly ash works in concrete mixes and additional experience with the product.

Implementation

The use of fly ash up to 20% by weight of cement is currently at the contractor's option in CDOT work. Those contractors confident in their ability to produce a consistent fly ash concrete mix routinely use it as a replacement for up to 20% of the cement specified in the mix design. On the other hand, some contractors have decided that the cost savings as a result of using fly ash are not worth the possibility of rejected truckloads.

No changes to the current specifications are proposed as a result of this study.

References:

- [1] Swanson, Herbert, The Use of Fly Ash in Structural Concrete, Demonstration Project No. 59, Design and Construction Report, Colorado Report No. CDOH-DTP-R-86-12, July, 1986
- [2] 1985 Cost Data, Compiled by the Cost Estimates Squad of the Staff Design Branch, Colorado Department of Highways



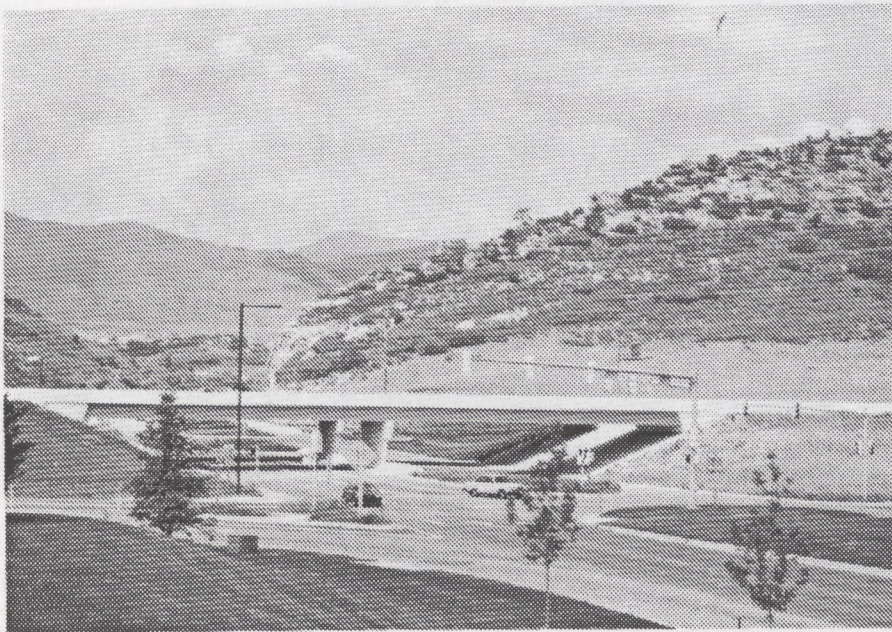
Photograph 1.
Overall view of
twin structures
at Ken Caryl Rd.

APPENDIX A

PHOTOGRAPHS OF THE BRIDGES

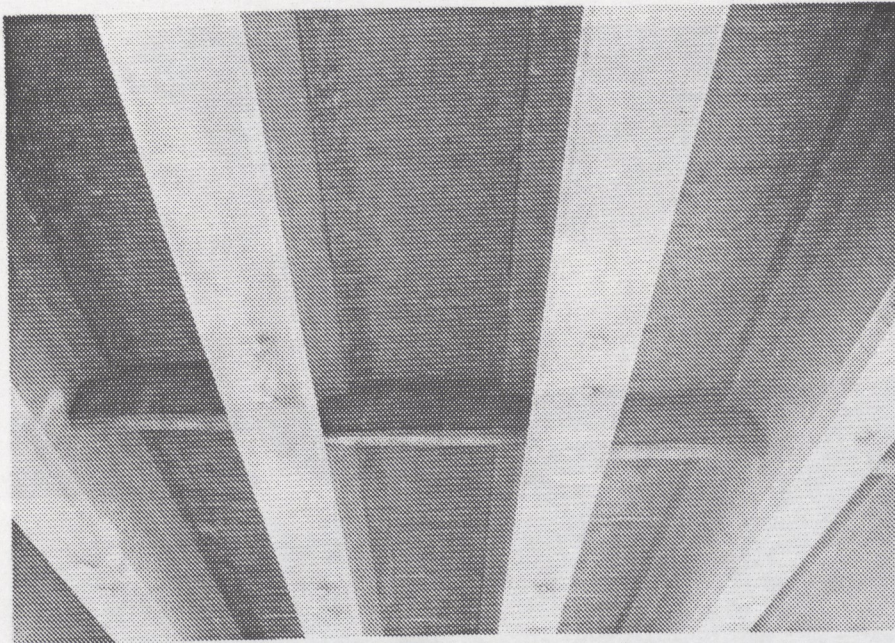


Photograph 2.
View of under-
side of deck.
Ken Caryl Rd.



Photograph 1.
Overall view of
twin structures
at Ken Caryl Rd.

of deck.
Ken Caryl Rd.

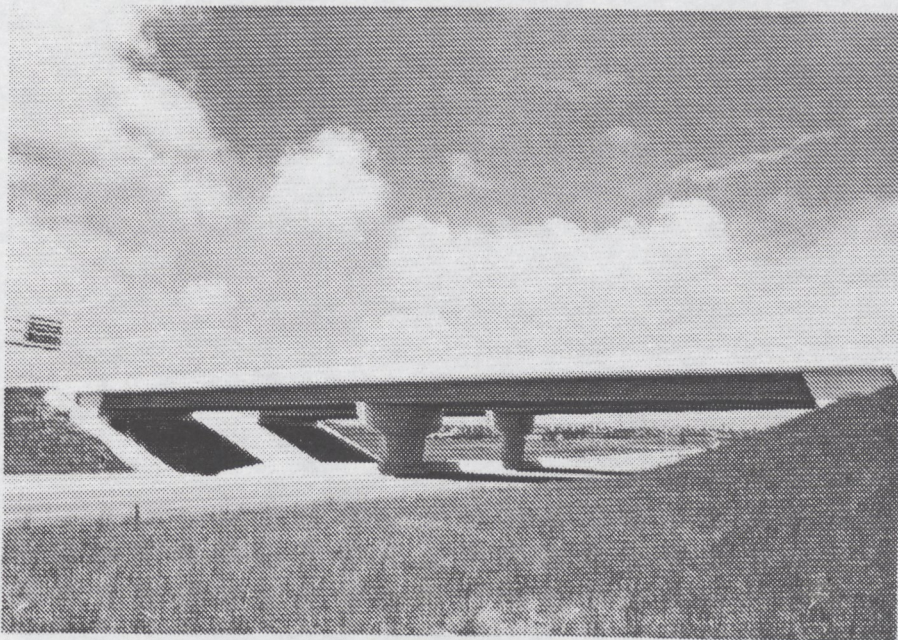


Photograph 2.
View of under-
side of deck.
Ken Caryl Rd.

of twin
structures at
Kipling St.



Photograph 3.
Slight efflores-
cence on
underside
of deck.
Ken Caryl Rd.

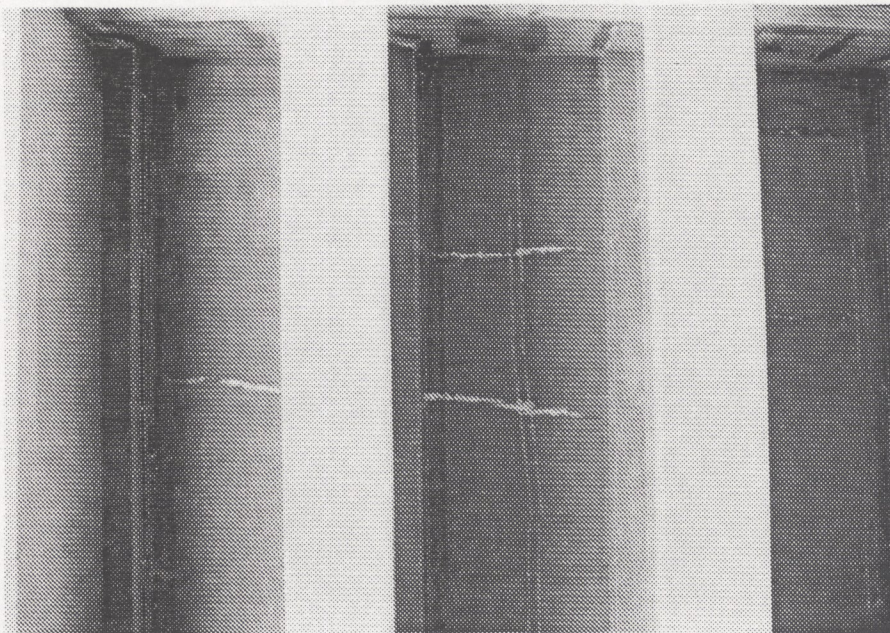


Photograph 4.
Overall view
of twin
structures at
Kipling St.



Photograph 5.
Mild efflorescence on underside of deck.
Kipling St.

CONCRETE MIX DESIGNS



Photograph 6.
Small cracks are visible in deck. Kipling St

TABLE 901-1

CONCRETE CLASSES with Field Compressive Strength and Brief Description	CONCRETE SPECIFICATIONS					Cracks Aggregate Section 702 Table 702 N. of Total Aggregate	Field Aggregate (Round) N. of Total Aggregate
	Cement Type (ASTM 101)	Maximum Water-Cement Ratio (per Article of Contract)	Air Content N. Range (%)	Maximum Slump (inches)	Maximum Free Water (inches)		
A 1 1/2" Aggregate 3000 Psi	565	6.09	4-8	4	4	467	45%
A1 Local Aggregate 4000 Psi	610		8-8	5		See Observation in subsection 601.03	
A2 1 1/2" Aggregate 4000 Psi	610		5-8	4		467	45%
B 1 1/2" Aggregate 3000 Psi	565		5-8	4		57	50%
B1 1 1/2" Aggregate 4000 Psi	610	6.40	5-8	4		67	50%
D Deck 1500 Psi	565	6.44	5-8	2.5 (Design) 2.25 (Field)		67	50%
D1 Deck Topping 4500 Psi	705	6.44	5-8	2.5		7	50%
D2 Local Aggregate Deck 4500 Psi	605	3.44	5-8	2.5 (Design) 2.25 (Field)		See Observation in subsection 601.03	
EA Elastic Aggregate 3800 Psi	565	6.55	5-8	3		6 of 67	40%
F Pavement 5000 Psi	565	6.35	4-8	3		467 or 607	45%
G Pre-stressed on job	565		specified on plans				

APPENDIX B

CONCRETE MIX DESIGNS

TABLE 601-1

CONCRETE CLASSES with Field Compressive Strength and Brief Description	CONCRETE SPECIFICATIONS					
	Cement (Lbs./cu. yd.)	Maximum Water/Cement Ratio (lbs. H ₂ O/lb of Cement)	Air Content % Range (Total)	Maximum Slump (inches)	Coarse Aggregate Section 703, Table 703- (Size No.)	Fine Aggregate (Maximum % of Total Aggregate)
A 1½" Aggregate 3000 Psi	565	0.50	4-8	4	467	45%
AX Local Aggregate 4000 Psi	610	0.45	5-8	3	See Gradation in subsection 601.03	
AZ 1½" Aggregate 4000 Psi	610	0.45	5-8	4	467	45%
B ¾" Aggregate 3000 Psi	565	0.53	5-8	4	67	50%
BZ ¾" Aggregate 4000 Psi	610	0.48	5-8	4	67	50%
D Deck 4500 Psi	660	0.44	5-8	2.5 (Design) 3.25 (Field)	67	50%
DT Deck Topping 4500 Psi	700	0.44	5-9	2.5	7	50%
DX Local Aggregate Deck 4500 Psi	660	0.44	5-8	2.5 (Design) 3.25 (Field)	See Gradation in subsection 601.03	
EA Exposed Aggregate 3000 Psi	565	0.53	5-8	4	6 or 67	40%
P Pavement 3000 Psi	565	0.50	4-8	3	467 or 357	45%
S Prestressed specified on plans	660	--	specified on plans	--	--	--

PAGE 2

Class of Concrete		<u>BFA</u>	<u>DFA</u>		
% Fine Agg. by Absolute Vol.		<u>41</u>	<u>44</u>		
Air Entraining Agent		<u>Protex A.E.S</u>	<u>Same</u>		
Quantity of Air Entraining Agent (ozs)		<u>5.0</u>	<u>4.5</u>		
Admixture		<u>Prokrete-N</u>	<u>Same</u>		
Quantity of Admixture (ozs)		<u>14.0</u>	<u>20.0</u>		
Cement: Source <u>So. Dakota</u> Type <u>I</u>					
Cement South Dakota	Lbs.	<u>480</u>	<u>560</u>		
Fly Ash Wheatland	Lbs. Cl. 'C'	<u>85</u>	<u>100</u>		
Fine Aggregate	Lbs.	<u>1250</u>	<u>1285</u>		
Intermediate Aggregate	Lbs.	<u>1800</u>	<u>1625</u>		
Coarse Aggregate	Lbs.	<u>0</u>	<u>0</u>		
Miscellaneous Aggregate	Lbs.	<u>0</u>	<u>0</u>		
Water	Lbs.	<u>260</u>	<u>270</u>		
Water	Gals.	<u>31.2</u>	<u>32.6</u>		
Slump	Inches	<u>1.75</u>	<u>-</u>		
Water Cement Ratio (% by Weight)		<u>.460</u>	<u>.411</u>		
Cement Factor (CWT per Yard)	(1)	<u>5.7</u>	(1) <u>6.6</u>		
Gals/CWT		<u>4.7</u>	<u>4.9</u>		

WEIGHT PER CU. FT. OF CONCRETE:

T. Theoretical (calculated-air free)			<u>150.0</u>		
C. Theoretical (calculated NS % air)			(2) <u>142.5</u>		
W. Determined (actual Wt./cu.ft.)		<u>144.0</u>	<u>142.1</u>		

Air Content Air Meter (Total Air) 5.5 5.4

Air Content -

Gravimetric Method % A = $\frac{T - W}{T} \times 100$

NS=Not Shown 5.3

- (1) Cementitious
- (2) 5% Air Design

7 days

Compressive Strength (P.S.I.)	Average	<u>4460</u>	<u>4580</u>		
		<u>4260</u>	<u>4540</u>		
		<u>4360</u>	<u>4560</u>		

28 days

Compressive Strength (P.S.I.)	Average	<u>5810</u>	<u>5830</u>		
		<u>5730</u>	<u>5750</u>		
		<u>5770</u>	<u>5790</u>		

NOTE: Quantities shown for admixtures are for information only.

REMARKS: Trial mixes run under project I 76-1(90)(100); the class SFA mix is proportioned identical to the required class DFA this project and meets CDOH design criteria. District 6 Materials has concurred on these changes. 3.25" maximum slump to be used on the class DFA

cc: District 6
 Brasher-Motchan
 Ihlanfeldt
 R.E. (2)

Stuart C. Fapp
 STAFF MATERIALS ENGINEER
 Staff Materials Engineer

jc: 10/18/85

PUBLICATION
Department of Highways-State of Colorado
Division of Transportation Planning

- 91-1 *Dynamic Measurements on Penetrometers for Determination of
Foundation Design Parameters
- 91-2 *Geotextiles in Bridge Abutments
- 91-3 *Industrial Snow Fence vs. Wooden Fences
- 91-4 *Rut Resistant Composite Pavement Design (Interim Report)
- 91-5 *Reflective Sheeting (Final)
- 91-6 Review of Field Tests and Development of Dynamic Analysis
Program for CDOH Flexpost Fence
- 91-7 *Geotextile Walls For Rockfall Control
- 91-8 Fly Ash in Structural Concrete
- 91-9 *Polyethylene Pipes for Use as Highway Culverts

*Reports soon to be published

PUBLICATION
Department of Highways-State of Colorado
Division of Transportation Planning

- 89-1 Truck Tire Pressures in Colorado
 - 89-2 Rockfall Modeling and Attenuator Testing
 - 89-3 Frost Heave Control With Buried Insulation
 - 89-4 Verglimit Evaluation (Boulder)
 - 89-5 Use of Road Oils by Maintenance
 - 89-6 Accelerated Rigid Paving Techniques
 - 89-7 IBC Median Barrier Demonstration
 - 89-8 Monitoring of Nondurable Shale Fill in Semi-Arid Climate
 - 89-9 Resilient Properties of Colorado Soils
 - 89-10 Consolidation Testing Using Triaxial Apparatus
 - 89-11 Reactive Aggregate in Structures
 - 89-12 Five Inch Asphalt Overlay
 - 89-13 Avalanche - Interim Report
 - 89-14 Sawed Joints in AC Pavements
 - 89-15 Mirimat Erosion Control Fabric
 - 89-16 Use of Spirolite Plastic Pipe
-
- 90-1 Pretreatment of Aggregates
 - 90-2 Experimental Gravel Shoulders
 - 90-3 Cold Recycling of Asphalt Pavement, US 24, Proj. CX-04-0024-25
 - 90-4 Pavement Marking Materials
 - 90-5 Geotextiles in Landfills
 - 90-6 Criblock Retaining Wall
 - 90-7 Project Level Pavement Management
 - 90-8 A Peak Runoff Prediction Method For Small Watersheds in Colorado
 - 90-9 Research Status Report
 - 90-10 Public Perception of Pavement Rideability
 - 90-11 Bridge Deck Repair Demonstration
 - 90-12 Highway Rockfall Research Project
 - 90-13 In-Service Evaluation of Highway Safety Devices, Exp. Proj. No. 7
 - 90-14 Study of Urban Interchange Performance

PUBLICATION
Department of Highways-State of Colorado
Division of Transportation Planning

- 87-01 Finite Element Analysis of Twin-T Test Walls in Glenwood Canyon, CO
- 87-02 Flow Conflict Study
- 87-03 Epoxy Thermoplastic Pavement Marking Demonstration Project 60
- 87-04 Elastometric Concrete End Dams Used in Conjunction With Bridge Deck Expansion Devices
- 87-05 Colorado Reactive Aggregate
- 87-06 Bridge Approach Settlement
- 87-07
- 87-08 Third Party Construction Engineering
- 87-09 Preloading of Sanitary Landfills
- 87-10 Frost Heave Control With Buried Insulation (Interim)
- 87-11 AC Gauge "Between Operator" Precision Experiment
- 87-12 Long-Term Creep of Geotextile in the Confinement of Soils Under Sustained Loading - Phase I
- 87-13 Dynaflect Benkelman Beam Correlation
- 87-14 Cathodic Protection
- 87-15 Rubber Modified Asphalt Concrete
- 87-16 Concrete Pavement Repair Bennett to Strasburg

- 88-1 Pavement Profile Measurement Seminar Proceedings, Vol. I, Seminar Overview
- 88-2 Pavement Profile Measurement Seminar Proceedings, Vol. II, Data Collection Equipment
- 88-3 Pavement Profile Measurement Seminar Proceedings, Vol. III, Workshop Summaries
- 88-4 Micro Computers in Project Field Offices
- 88-5 Development of a Risk Cost Methodology for Detour Culvert Design
- 88-6 Concrete Pavement Restoration Demonstration
- 88-7 Inservice Evaluation of Highway Safety Appurtenances, FHWA Experimental Project No. 7
- 88-8 Embankment Settlement in Glenwood Canyon
- 88-8 Rehabilitation of Concrete Pavements Follow-Up Study
- 88-10 Effectiveness of Geogrids and Geotextiles in Embankment Reinforcement
- 88-11 Spring Breakup Study
- 88-12 Plastic Pipe Use Under Highways
- 88-13 Geothermal Space Heating
- 88-14
- 88-15 Tapered Asphalt Shoulders
- 88-16 Development of a Retrievable Test Rig for Drilled Pier Bridge Foundations
- 88-17 Flexible Roadside Delineator Post Evaluation
- 88-18 Long Term Pavement Monitoring
- 88-19 Expandable Membrane Ground Anchors in Talus
- 88-20 Research Status Report

RECEIVED

MAR 25 1992

COLORADO STATE LIBRARY
State Publications Library