

SOUTH BOULDER CREEK INTERIM HYDROLOGY STUDY

JULY 2000



THE URBAN DRAINAGE AND FLOOD CONTROL DISTRICT
THE CITY OF BOULDER
BOULDER COUNTY
THE UNIVERSITY OF COLORADO



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July 2000

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RE: SOUTH BOULDER CREEK INTERIM HYDROLOGY STUDY,
PHASE III

Dear Mr. DeGroot:

This Phase III report presents hydrology for the entire South Boulder Creek Watershed, with emphasis on the reach from the foothills upstream of Highway 36 to the confluence with South Boulder Creek. This document was prepared in accordance with appropriate City, County, Urban Drainage and Flood Control District (UDFCD), Colorado Water Conservation Board (CWCB), and Federal Emergency Management Agency (FEMA) requirements. We believe this report and the hydrology model meet all requirements of the contract and regulatory requirements. It should serve to reasonably portray the flood hydrology and related general hazard in the watershed.

Our Phase I effort, completed in 1996, identified that the Flood Hazard Area Delineation Report (FHAD, July 1986) underestimated the flow leaving South Boulder Creek at Highway 36 and did not portray spillage paths to the west side of the valley, particularly along Foothills Parkway. The Phase II report, submitted in 1997, provided an initial reconnaissance of the overflow routes and approximate flows of the West Valley Overflow north of Highway 36 to the area of the Wellman Ditch.

We obtained and reviewed additional hydrology information from the U.S. Army Corps of Engineers (Corps). In Phase I we modified the Corps' Storm Water Management Model (SWMM) model to better reflect the Viele watershed and its outfall channel to South Boulder Creek. In Phase II we refined the SWMM model detail downstream of Highway 36 in order to identify significant flow paths and approximate discharges in that area.

After Phase II, the University of Colorado joined the effort as a sponsor. The sponsors directed both a Hydrology Study (Phase III) and a Master Planning (Phase IV) effort.

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We observed several discrepancies in the Corps' SWMM model during the Phase I and II studies. The two most important deficiencies include: 1) the drainage area in the Corp model is significantly less than the actual watershed area, and 2) the peak one-hour rainfall is less than that prescribed by local, regional, and National Oceanic and Atmospheric Administration (NOAA) procedures. In this Phase III study we determined that modifications were required for the Gross Reservoir storage and spillway characteristics, the stream hydraulics, and the land runoff characteristics. Changes were required to address each of these discrepancies.

During Phase III, we have constructed an essentially new hydrology model using the UDFCD UDSWMM computer program, but using portions of the Corps' model as a starting point. The following have been incorporated.

1. Revised rainfall using National Oceanic Atmospheric Agency (NOAA), City, County, UDFCD, and U.S. Bureau of Reclamation (USBR) procedures.
2. Electronic base mapping using City, County, and U.S. Geologic Survey (USGS) sources. Basins, streams, and other model features are delineated on this base.
3. Basin-wide review of National Resource Conservation Service (NRCS or formerly SCS) and U.S. Forest Service (USFS) soils and ground surface mapping to identify infiltration and other rainfall loss characteristics.
4. Updated Phase II model data downstream of Highway 36.
5. Detailed new modeling for the area from Eldorado Springs to Highway 36.
6. Correction of all Corps' modeling upstream of Gross Reservoir and redelineation of all basins downstream of Gross Reservoir.
7. Reasonableness comparisons with Eldorado Gage Data, Colorado Unit Hydrograph Procedure (CUHP) modeling of representative secondary watersheds, unit discharge (cubic feet per second (cfs) per acre), and regional discharge relationships.

The modeling was performed in accordance with regulatory requirements which do not permit incorporation of storage that exists in Gross Reservoir below the spillway and upstream of the rail line at many south tributary locations from the foothills to upstream of Gross Reservoir. The large floodplains below Eldorado Springs provide dynamic storage which is not well simulated by UDSWMM. Under actual conditions, this storage would attenuate the 100-year flood peaks below the figures in this report for South Boulder Creek downstream of Gross Reservoir. For this reason and others elaborated herein, we believe this hydrology

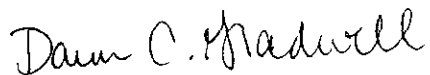
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should be considered interim until subsequent master planning is completed, efforts to formalize and sustain upstream storage are undertaken, and other refinements pursued.

We appreciate the cooperation we have received from the project sponsors, citizens, and the many agencies.

Sincerely,

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For any of those participants we missed we offer our apologies.

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LIST OF ACRONYMS

AcFt	Acre Foot
ARF	Area Reduction Factor
CADD	Computer Aided Design and Drafting
CDWR	Colorado Division of Water Resources
CFS	Cubic Feet per Second
CORPS	U.S. Army Corps of Engineers
CSU	Colorado State University
CU	Colorado University
CUHP	Colorado Unit Hydrograph Procedure
CWCB	Colorado Water Conservation Board
FEMA	Federal Emergency Management Agency
FHAD	Flood Hazard Area Delineation
FIRM	Flood Insurance Rate Map
FIS	Flood Insurance Study
G&O	Greenhorne & O'Mara, Inc.
HEC-1	Hydrologic Engineering Center - 1 Flood Hydrograph Package (Hydrology Program)
HEC-2	Hydrologic Engineering Center - 2 Water Surface Profile (Hydraulic Program)
M.S.L	Mean Sea Level
NOAA	National Oceanic and Atmospheric Administration
NRCS	National Resource Conservation Service
NWS	National Weather Service
RCN	Runoff Curve Numbers
SBC	South Boulder Creek
SCS	Soil Conservation Service now National Resource Conservation Service
Sq. Mi.	Square Mile
SWMM	Storm Water Management Model
SWMM EXTRAN	Storm Water Management Model Extended Transport Model
TEA	Taggart Engineering Associates, Inc.
TIN	Triangulated Irregular Network
TP	Technical Procedure
UDFCD	Urban Drainage and Flood Control District
UDSWMM	Urban Drainage and Flood Control District–Storm Water Management Model
UNET	One-Dimensional Unsteady Flow Through a Full Network of Open Channels
USBR	U.S. Bureau of Reclamation
USFS	U.S. Forest Service
USGS	U.S. Geologic Survey
WVO	West Valley Overflow

SECTION I

SUMMARY

WATERSHED

The South Boulder Creek Watershed encompasses 135.7 square miles (sq. mi.) of area starting from 13,294 feet elevation at the Continental Divide to its confluence with Boulder Creek at 5,160 feet elevation. As depicted by Drawings 1, 2, and 3 at the end of this report, the watershed is 27.2 miles long on a generally east west axis, and up to 6.3 miles wide. There are about 93.2 sq. mi. above Gross Reservoir and 42.5 sq. mi. below. The watershed is heavily forested between elevations 6,400 feet and 11,000 feet, particularly on the north facing slopes.

There are significant areas of rock outcroppings and steeply sloped, narrow streams and incised stream banks which can encourage *flashy runoff response*. The foothills are steep, have far less ground cover and higher peak rainfall than the mountain watershed, which leads to high runoff response. The lower valley and floodplain generally have higher soil infiltration characteristics, but have substantial rainfall runoff response because of the development of impervious areas and street drainage conveyances.

Gross Reservoir, completed in 1954 as a water reservoir for the Denver System, inadvertently provides a substantial flood control function for the Boulder community. Its purpose is to store up to 43,060 AcFt of water for domestic water supply. It is also authorized to generate power. Under current regulations, and due to the lack of any formal agreement to provide flood storage, this study can only assume storage above the crest of the spillway. The modeling herein estimates that during a 100-year flood, assuming the reservoir was full to the spillway crest, 1,780 acre feet of dynamic storage would occur, which attenuates the peak flow and delays the peak about 3 to 4 hours. The total 100-year rainfall volume tributary to the reservoir would be approximately 20,400 AcFt, while the total Basin Rainfall Volume would be 29,000 AcFt. Runoff would be roughly 5600 AcFt to the reservoir and 8000 AcFt for the total watershed. Therefore, Gross Reservoir, even if full to the spillway crest, has a significant effect on hydrology.

In the May 1969 Flood event, all runoff (5485 AcFt) from the mountains above Gross was captured with no discharge over the spillway. Reservoir statistics indicate that the average storage available for the months of May through August is 20% of the reservoir volume (8362 acre feet) with an average of 7.7% of the reservoir volume (3219 acre feet) available in June when the maximum volume of water is stored. However, modification of the reservoir operating practices could change these statistics.

Another historic facility that has substantial effects on actual hydrology is the rail line to Moffatt Tunnel. When the rail grade was constructed, the material excavated from ridges and tunnels was placed in valleys.

As the culverts placed are generally small, substantial storage exists. At one location, South Draw, the crossing provides on the order of 80 to 100 acre feet of storage, and practically reduces the 100-year peak to less than half. The next tributary to the west has a much smaller storage with no apparent culvert, and the runoff seeps through the embankment. We have not visited the other railroad storage sites. We believe there are 20 to 30 such storages, and total storage could amount to 500 to 1000 acre feet. There are roughly 5.1 square miles of tributary area to the rail line below Gross (or about 12 percent of the watershed below Gross) and 1.2 square miles of tributary area to the rail line above Gross.

The hydrology herein does not and cannot assume these rail line storages to be in place under current regulations until adequate institutional arrangements and appropriate improvements are made. It is also important to recognize these railroad storage areas pose a potential washout hazard, which could result in higher floods than predicted by the model herein.

The main waterway of South Boulder Creek has substantial effects on the hydrology because of its flood routing characteristics. In the mountains the sections vary widely. The steeper, narrower tributaries and higher elevation main streams can accelerate flows from upstream and cascade, or in lay terms, cause a flashy stream. Some segments with a shallow main stream overflow to moderately wide meadows. These segments would attenuate flows. In addition, there are other main stream segments which have deeper and steeper channels which would increase peaks.

As the flows leave the mountains, the waterways change dramatically to a wide alluvial valley. When depths exceed 2.5 to 4 feet, the water overflows into wide floodplains. Just above Highway 93, South Boulder Creek overflows to the West Valley Overflow. As shown on Drawings 4 through 11, South Boulder Creek and the West Valley Overflow repeatedly diverge and converge. The West Valley route often has a lower elevation than the corresponding elevation of South Boulder Creek across the floodplain. Dry Creek Ditch No. 2 diverts irrigation water in the midst of the upper split (see Drawing 4, element 1423). Generally Dry Creek Ditch No. 2 follows a shallow ridge between the two flow paths. However, at several locations the Dry Creek Ditch No. 2 is crossed by or carries flood waters.

The Flatirons Gravel Pit and Levee pushed the West Overflow toward South Boulder Creek (see Drawings 5 and 6). Without the levee, most of the West Valley Overflow would flow directly to the west of the Foothills and Highway 36 Interchange. Regardless of the levee, significant portions of flows in South Boulder

Creek just upstream of Highway 36 overflow to the West Valley, and potentially flood the urbanized area downstream.

South Boulder Creek downstream of Highway 36 to Arapahoe Road is largely natural with adjacent housing downstream of Baseline (Drawings 6, 7, and 8). The floodplain downstream of the Wellman Ditch is developed and is the location of another split across the golf course to the West Valley (Drawing 7). While the stream is natural here, it shows signs of aggregation from sedimentation, overgrowth, and resultant loss of capacity. Downstream of Arapahoe, South Boulder Creek is largely channelized.

The West Valley Overflow route downstream of Highway 36 is urbanized. The area is largely residential, with some commercial and office space near Foothills and Baseline and along and downstream of Arapahoe. Flood waters take many routes as illustrated on the drawings. The main overflow path starts downstream of Highway 36 on the west side of Foothills and travels northerly to the intersection of Baseline and Foothills.

At the intersection of Baseline and Foothills the flows split in seven directions. Three paths follow Foothills to the Wellman Canal. Some of this flood water enters the Wellman, but significant portions of the two roadway flows will largely leave the basin and enter Bear Canyon Creek. At the same time, Wellman Ditch flows from the west will enter as a transbasin flow, but the model, per contract and standard UDFCD practice, assumes none. There are probably some offsetting effects. That is, the Wellman brings flow in from Bear Creek while the flows on Foothills go to Bear Canyon.

Two of the flows from the Foothills and Baseline intersection follow Baseline. The last two are conveyed over and under Baseline, and join the Baseline flows after going through a minor storage, except for a small portion that crosses under Baseline to the drainage ditch on the north side, referred herein as the Crossover Ditch.

Spills from Baseline travel northerly through the Country Club Park, Centennial Trails, Arapahoe Ridge, and commercial areas to the north. The Wellman then receives most of these flows. While it has a significant cross section, its slope is flat, resulting in limited capacity which cannot convey significant flood waters. Spills would begin on the east side of the golf course, but as the flood discharge increases, sizable spills would occur to the west of 55th. Much of the flow on the west side of 55th will spill northerly to Boulder Creek through the commercial area.

The overflows on the golf course drain to Dry Creek Ditch No. 2, which is a large channel to the north of Arapahoe, then join South Boulder Creek flows and discharge to Boulder Creek.

PRIOR HYDROLOGY STUDIES

In 1977 the U.S. Army Corps of Engineers (Corps) conducted a hydrology study that included the South Boulder Creek Basin. That study provided the hydrology for the 1986 Urban Drainage and Flood Control District (UDFCD) Flood Hazard Area Delineation (FHAD) by Greenhorne and O'Mara (South Boulder Creek Flood Hazard Area Delineation), and the Federal Emergency Management Agency (FEMA) Flood Insurance Study (FIS) and Flood Insurance Rate Maps (FIRMs) for South Boulder Creek.

Although Gross Reservoir is not a flood control facility, it does affect flood runoff in two ways. First, if the reservoir level is lower than the spillway, it can trap some or all of the flood runoff. Second, even if the reservoir is full, dynamic flood storage can occur above the spillway level, lowering the flood peak discharged from Gross and delaying the flood discharge from the reservoir.

The 1973 R.W. Beck study determined that a release of 300 cfs would occur during the 100-year flood based upon examination of Denver Water Board records and policy. The G&O FHAD was based on Corps of Engineers modeling which assumed that the reservoir was full and that the flood from the 100-year rainfall above the reservoir would be attenuated by the storage volume above the spillway. The peak flow from the reservoir was modeled as 3900 cfs, and was several hours behind the downstream subbasin time of peak flow. The 1973 study is probably more realistic. The 1986 study is conservative, because it follows conventional UDFCD, CWCB, and FEMA practice to assume no storage below the spillway crest where there is no institutional agreement in place to provide and operate a flood storage function.

In 1996, Love and Associates (Flood Plain Analyses of South Boulder Creek at the Flatiron Property) identified that South Boulder Creek could spill greater flows than identified in the FHAD and that these spills could travel to the west side of the valley and overtop Highway 36, largely west of Foothills, and thus posed a hazard to the neighborhood north of Highway 36.

The TEA Phase I effort reviewed the FHAD and Love's investigation, and identified 100-year spills on the order of 2700 cfs from South Boulder Creek above Highway 36. The spill was shown to commingle with local drainage from the Dry Creek Ditch No. 2 and the Viele watershed. The Phase I effort obtained a copy of the Corps' hydrology model to identify the timing of the Viele inflows and allow simplified simulation of its drainage network. Some general problems were noted in the Corps' model, but the effort focused on the determination of how much of the South Boulder Creek spill would return via Viele and how much would continue to the West Valley Overflow route. Phase I analyses indicated that about 1800 cfs would continue to the West Valley Overflow north of Highway 36.

UDFCD authorized the Phase II Initial Reconnaissance Study to estimate the distribution of flooding in West Valley downstream of Highway 36 to the area of the Wellman Ditch. For the purposes of the Phase II study, the Corps' hydrology was not changed upstream of Highway 36 other than modifications to better reflect floodplain routing downstream of the mountains. All new basins and routing elements were inserted into the hydrology model for the Viele Basin and the area downstream of Highway 36.

Also, since questions regarding hydrology had been raised by the sponsors and by our work, requests to the Corps were made to obtain background data, basin mapping, and verification studies. A watershed basin map for the area near and above Gross Reservoir and a memorandum discussing model parameter sensitivity testing and rainfall were received.

OBJECTIVES OF THIS STUDY

The primary objective of this study is to prepare a new hydrologic analysis of the South Boulder Creek Watershed.

The initial use will be for the evaluation of flood damage mitigation alternatives for the reach of South Boulder Creek from Highway 93 to Boulder Creek.

Ultimate uses of the study will be for base hydrology for UDFCD flood hazard delineation studies (FHAD), FEMA Flood Insurance Rate Maps (FIRM), and planning of road and bridge improvements, channel modifications, and flood control structures. The hydrology should meet the requirements of the "Rules and Regulations for the Designation of Floodplains and of Storm or Flood Water Runoff Channels in Colorado" by CWCB and FEMA's "Guidelines and Specifications for Study Contractors."

SIMPLIFIED SCOPE

This effort is focused on:

1. Determining the design rainfall from NOAA references that is most appropriate for the South Boulder Creek watershed, particularly on the South Boulder watercourse from Highway 93 downstream to Boulder Creek.
2. Checking the Corps' SWMM runoff model upstream of Gross Reservoir, especially with respect to runoff area and infiltration characteristics.
3. Reconstructing the model, especially from just upstream of Highway 93 to Highway 36, using the City and County database (detailed topographic

mapping) and the previous hydraulic analysis of flow splits and floodplains by TEA and others.

4. Simulating the dual stream character of the floodplain downstream of Highway 93.
5. Calibrating the model to the 1969 flood or at least comparing for reasonableness, and spot checking major basin runoff using the UDFCD Colorado Unit Hydrograph Procedure (CUHP) for reasonableness. Review of the Eldorado stream gage data is also included, but efforts to review the Eldorado gage data and calibrate to the 1969 flood are limited.
6. Preparing basin and model maps, and model documentation such as representative hydrographs and discharge profiles.
7. Agency contact (Corps, USGS, CWCB, Natural Resource Conservation Service (NRCS), City of Boulder, Boulder County, Denver Water, and U.S. Forest Service (USFS)).
8. General characterization of flow timing, magnitude, and distribution in the South Boulder Creek floodplain below Highway 93.
9. Specific review and effort to comply with CWCB and FEMA requirements.
10. Summary report and technical appendices.

What is not required: snowmelt hydrology, infiltration testing, reservoir operations or storage statistical analysis, long term rainfall runoff modeling or statistical analysis using NWS or other long term rainfall records, extensive field surveys, floodplain storage routing, rain gage statistical analysis, hydraulics and split flow analysis beyond specific limits, floodplain hydraulic modeling or mapping.

MODIFICATION OR DEPARTURES FROM SCOPE

As with any study, the investigation raises facts and issues which inevitably lead to modification or departure from the scope. Some of these are as follows:

1. Rainfall. Contacts with NOAA were generally helpful. We attempted to get better guidance on arranging the temporal (time) pattern of the critical rainfall, however two of the references indicated didn't lead to fruitful results. UDFCD provided consultation with John Henz, meteorologist, which provided helpful guidance. We attempted to use a storm pattern he suggested, but were unable to satisfy NOAA statistics. Henz suggested providing a custom rainfall analysis of the UDFCD network and providing

design storms that were locally based, but this would require substantial funding and likely depart from NOAA based documentation, so the sponsors decided to not proceed beyond the TEA analysis herein.

2. Eldorado Stream Gage Data. The research revealed that the Eldorado Stream Gage had a substantial record of daily flows and was primarily used for management of water distribution to irrigation ditches. While peaks had been recorded, the gage had never been calibrated for flows greater than 600 cfs and had a rock control sill which had moved during floods.

The use of the gage data for flood statistics should probably be considered more qualitative and a reasonableness check. The sponsors decided that we *shouldn't proceed further with gage investigation.*

Review of the hydrology modeling herein, the Denver Water records, and inadvertent storage upstream of the rail line revealed that the gage record reflected substantial inadvertent storage, and thus cannot be used, per regulations.

3. Flood of May 1969. The 1969 event was investigated. The Denver data for Gross indicated that the upstream flood was entirely trapped in the reservoir. The USBR provided their files for rainfall data and analysis of the 1969 event. CU provided 15 minute rainfall data for the Boulder Creek watershed. While there were daily rain gage readings within the basin, there were no 5 or 15 minute rain data. Review of 1969 isopluvial maps from the USBR indicated that there could be a wide range of interpretation, with a resultant wide range of estimated model flows. Henz indicated that he might be able to review other data and construct detailed rainfall patterns at various locations in the watershed. The sponsors decided not to pursue this calibration concept further due to the expense and likely questionable results.
4. Upper Basin Modeling. Upon review of the Corps' model data for the mountains, TEA decided it was better to completely review all data for consistency to UDFCD/Boulder standards and correctness. Only the outline of the basins and element numbers were kept.

CONSULTATIONS

Numerous consultations with government and private agencies have taken place, highlighted as follows:

- City of Boulder and Boulder County
 - CADD base topographic maps
 - Rainfall criteria for frequent events

- Colorado Division of Water Resources (CDWR) -Stream gage data
- Colorado State Parks -Eldorado State Park topography and surveys
- Colorado State Engineer's Office -Gross and Marshall Lake Reservoir and Spillway characteristics
- Colorado State University (CSU) -Fort Collins rainfall
-Precipitation studies
- Colorado University (CU) -1969 rainfall
-Meteorological consultation
- Colorado Water Conservation Board (CWCB) -Study requirements
-Use of rainfall by NOAA
-Regional analysis
- Denver Water -Gross Reservoir operational data and guidelines
-Dam and spillway information and dam safety reports
- Federal Emergency Management Agency (FEMA) -Study requirements
-Use of Eldorado gage data
-Regional analysis
- Fort Collins -Precipitation studies
- Henz Meteorological -Storm precipitation review and suggestions
-1969 flood event approach
- National Oceanic Atmospheric Administration (NOAA) -Rainfall atlas data
-Area reduction and storm pattern
- National Resource Conservation Service (NRCS) -Soils
-Storm pattern
- United States Bureau of Reclamation (USBR) -1969 rainfall data
-Storm pattern
-Hydrology procedures

At the lower end of the watershed the model shows flow discharging at four locations. The main flow in South Boulder Creek joins with Boulder Creek at the historic confluence. At Foothills and the Wellman Ditch, spills to Bear Canyon Creek occur. On the west side of 55th downstream of Arapahoe some overflow from the Wellman traverses through an industrial/commercial area directly to Boulder Creek. Also, flow leaves South Boulder Creek just downstream of Arapahoe through overflows to Valmont.

The model does not depict flow leaving the watershed by following numerous other irrigation ditches and spills to Baseline reservoir, which can occur. The Wellman diversion is treated differently, per sponsors' direction, because its embankment physically crosses the main floodplain, and backs up and redistributes flood waters. The diversion to Valmont would immediately overflow to Boulder Creek and reflects overflow of the headworks.

TABLE I-1

SUMMARY 100-YEAR PEAK FLOOD FLOW HYDROLOGY COMPARISONS
 SOUTH BOULDER CREEK (SBC) AND WEST VALLEY OVERFLOW (WVO)
 (flow in cubic feet per second (cfs))

LOCATION	VALUES USED IN HEC-2 FLOODPLAIN	SWMM MODEL BY USACE 1977	TEA PHASE III HYDROLOGY sbc_1td.out MODEL		
			ELEMENT	ELEMENT FLOW (PEAK TIME)	*SIMULTANEOUS SBC & WVO @ PEAK DISCHARGE (PEAK TIME)
SBC into Gross	N/A	7696	#8	9148	N/A
SBC out of Gross	N/A	3862	#397	4029	N/A
Eldorado Gage	N/A	4462	#50	7883	N/A
SBC upstream of split above Highway 93	5740	5743	#1421	9200	N/A
HIGHWAY 93					
SBC @ Highway 93	2100	5743	#1509	2121 (9:50)	9552 (10:00)
WVO @ Highway 93	3850		#1533	7442(10:00)	
UPSTREAM HIGHWAY 36 BEFORE SPLIT					
SBC upstream of Highway 36 before split	4160	6163	#44	8238(10:30)	9362 (10:30)
WVO upstream of Highway 36 before split joins	2000		#1442	1127(10:35)	
HIGHWAY 36					
SBC downstream of Highway 36	4500	6163	#1427	3979(10:30)	9334** (10:35)
WVO spill from SBC @ Highway 36	1660		#262	5374(10:40)	
WVO from Upper Viele	N/D	N/D	#1920	922 (8:15)	9427*** (10:35)
WVO for Flatirons Pit	N/D	N/D	#304	78 (8:25)	

N/A = Not Applicable

N/D = Not Determined in Previous Study

*This column, where applicable, is the largest total of the flows in SBC and the WVO at the same time. Peak flows of each stream may occur at different times due to different travel times and local inflows. Thus the peaks in the column to the left may not sum to the value of this column.

** Compares flows similar to previous model flow data.

***Total flow at location including previously unmodeled flows.

TABLE I-1 (Continued)

SUMMARY 100-YEAR PEAK FLOOD FLOW HYDROLOGY COMPARISONS
SOUTH BOULDER CREEK (SBC) AND WEST VALLEY OVERFLOW (WVO)
(flow in cubic feet per second (cfs))

LOCATION	VALUES USED IN HEC-2 FLOODPLAIN	SWMM MODEL BY USACE 1977	TEA PHASE III HYDROLOGY sbc_1td.out MODEL		
			ELEMENT	ELEMENT FLOW (PEAK TIME)	*SIMULTANEOUS SBC & WVO @ PEAK DISCHARGE (PEAK TIME)
SOUTH BOULDER ROAD					
SBC upstream of Viele	4500		#243	3929(10:40)	
WVO return from Viele	1660	6163	#289	1113(11:20)	
WVO return from Anderson Ditch	N/D	N/D	#377	109 (11:30)	
WVO @ Highway 36 overflow west of Foothills	N/D	N/D	#1812	3872(11:15)	8757** (11:15)
Other small flows crossing into subdivisions-Dry Creek Ditch No. 2	N/D N/D N/D	N/D N/D N/D	#1366 #1367 #1374	128 (11:15) 14 (8:20) 36 (10:45)	8921*** (11:15)
BASELINE					
SBC @ Baseline	6400	6526	#241	4835(11:20)	
WVO @ Foothills and Baseline (Other small flows crossing Baseline)	N/D	N/D	#359	3868(11:25)	
E. side Foothills			#363	15 (8:10)	8872 (11:25)
Manhattan Dr. crossing			#366	170 (8:15)	
Dry Creek No. 2			#371	254 (8:20)	
Meadow Glen Dr. crossing			#338	103 (8:20)	
ARAPAHOE					
SBC @ Arapahoe	2600	6630	#232	2406(12:05)	
WVO @ Dry Creek Ditch No. 2	4030	N/D	#1909	3924(12:05)	
WVO just west of 55 th	N/D	N/D	#1365	974 (12:00)	6696 (12:05)
WVO at Range Street	N/D	N/D	#1371	4 (11:55)	

N/A = Not Applicable

N/D = Not Determined in Previous Study

*This column, where applicable, is the largest total of the flows in SBC and the WVO at the same time. Peak flows of each stream may occur at different times due to different travel times and local inflows. Thus the peaks in the column to the left may not sum to the value of this column.

**Compares flows similar to previous model flow data.

***Total flow at location including previously unmodeled flows.

TABLE I-1 (Continued)

SUMMARY 100-YEAR PEAK FLOOD FLOW HYDROLOGY COMPARISONS
 SOUTH BOULDER CREEK (SBC) AND WEST VALLEY OVERFLOW (WVO)
 (flow in cubic feet per second (cfs))

LOCATION	VALUES USED IN HEC-2 FLOODPLAIN	SWMM MODEL BY USACE 1977	TEA PHASE III HYDROLOGY sbc_1td.out MODEL		
			ELEMENT	ELEMENT FLOW (PEAK TIME)	*SIMULTANEOUS SBC & WVO @ PEAK DISCHARGE (PEAK TIME)
BOULDER CREEK AND ENDING SPILLS					
SBC @ Boulder Creek Confluence	6630	6634	#270	6320(12:55)	7516 (12:30)
WVO spill west of 55 th @ Range St. to Boulder Creek	N/D	N/D	#1372	620 (12:05)	
Spill to Valmont	N/D	N/D	#1403	103 (12:00)	
WVO lost to Bear Canyon Creek	N/D	N/D	#1305	1247(11:40)	

N/A = Not Applicable

N/D = Not Determined in Previous Study

*This column, where applicable, is the largest total of the flows in SBC and the WVO at the same time. Peak flows of each stream may occur at different times due to different travel times and local inflows. Thus the peaks in the column to the left may not sum to the value of this column.

**Compares flows similar to previous model flow data.

***Total flow at location including previously unmodeled flows.

DISCHARGE PROFILES

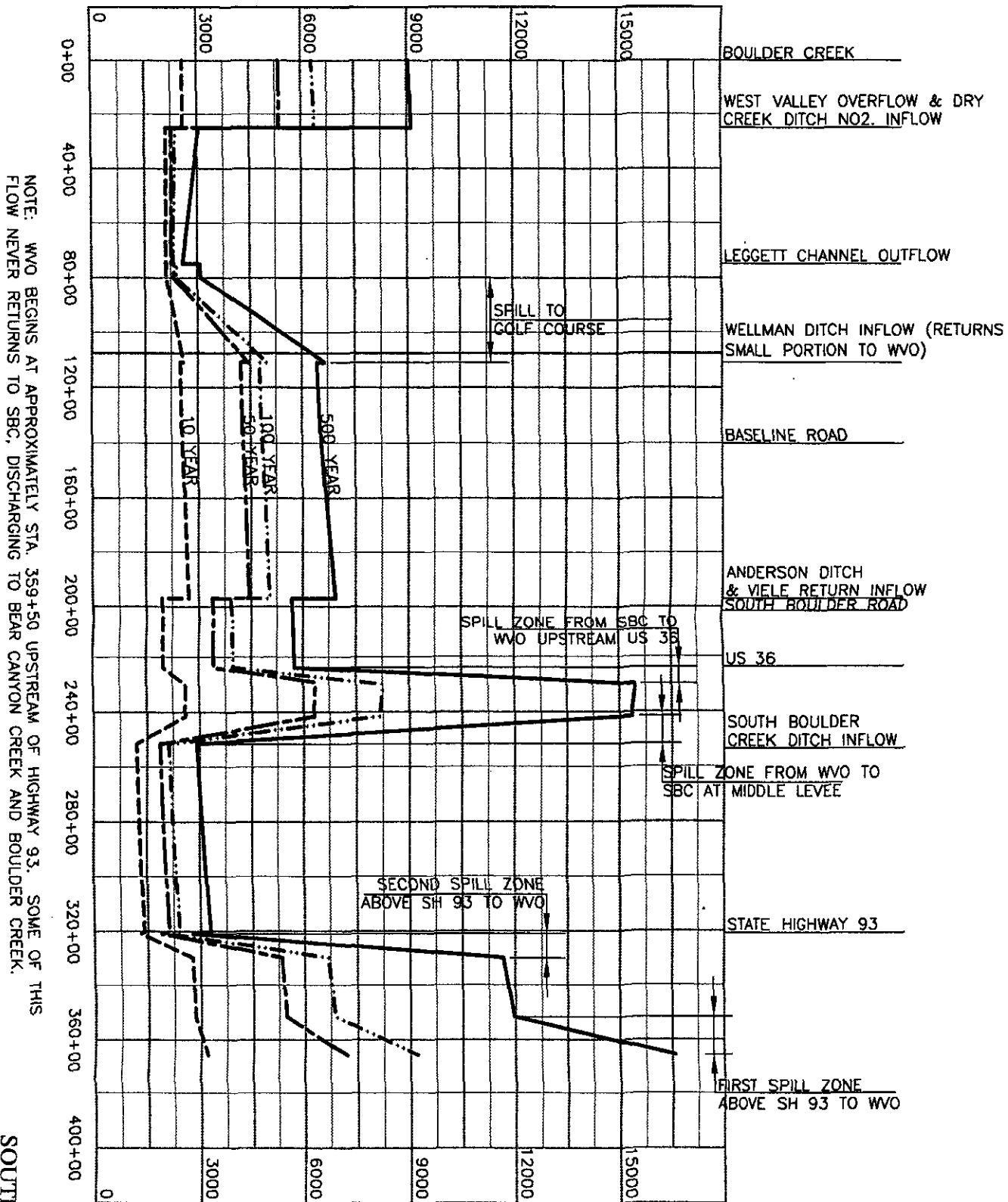
The discharge profiles for South Boulder Creek and the West Valley Overflow are presented in Figures I-1 and I-2, respectively. Stationing along South Boulder Creek begins at the confluence with Boulder Creek and increases going upstream. The significant spill from South Boulder Creek to the West Valley Overflow begins approximately at Station 359 + 50 on South Boulder Creek.

The Figure I-1 South Boulder Creek discharge profile shows four major spills to the West Valley Overflow: two upstream of Highway 93, one upstream of Highway 36, and one downstream of the Wellman to the golf course. Two major inflows occur: one from the West Valley Overflow in the area of the middle levee on CU's property, about 1500 to 2000 feet upstream of Highway 36, and the Viele/Anderson Ditch inflow which carries some of the West Valley Overflow discharge back to South Boulder Creek. There are also several tributary basin inflows, such as David's Draw and the areas along South Boulder Creek.

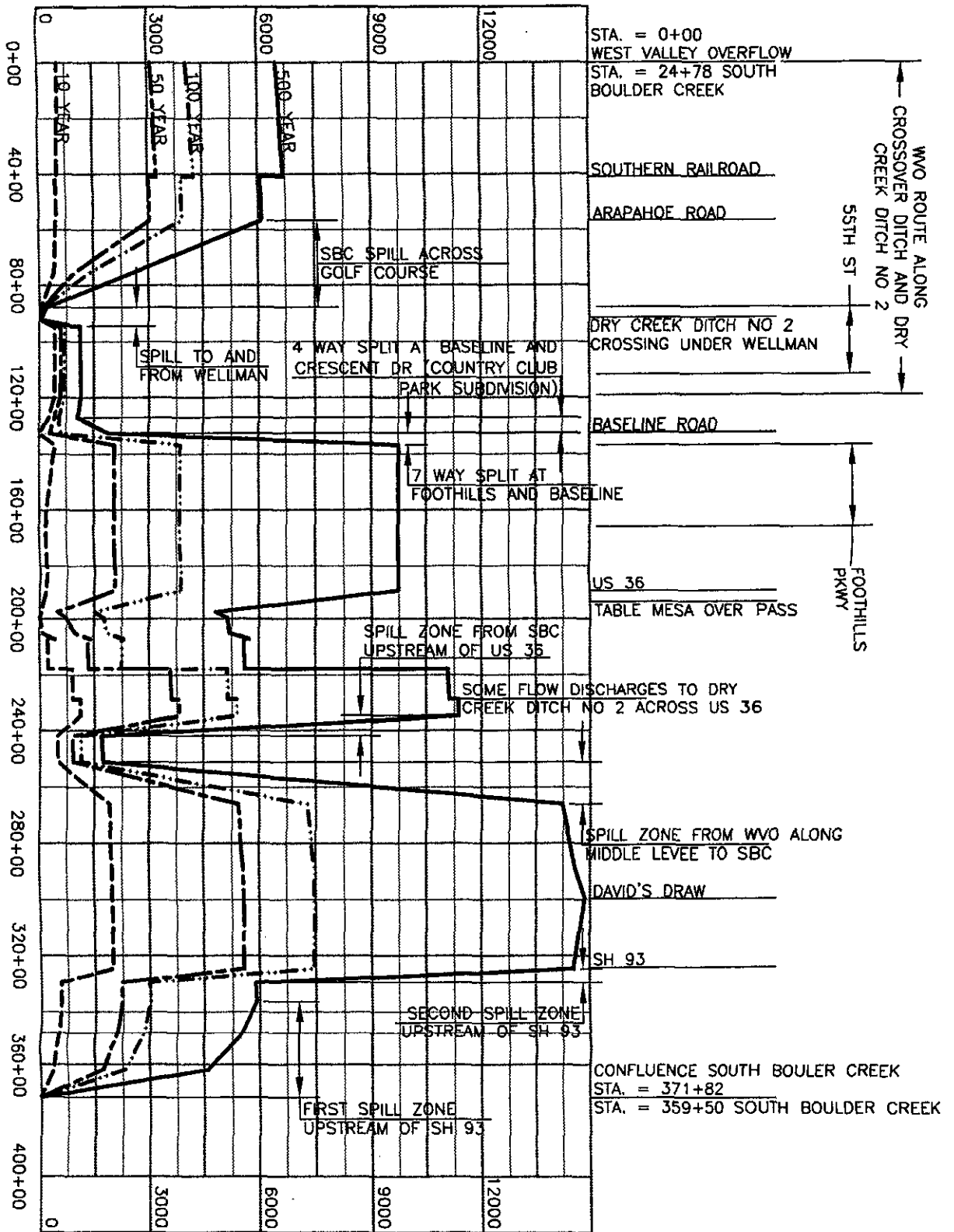
The Figure I-2 discharge profiles show the spills from South Boulder Creek above Highway 93 and Highway 36, and the flows returning to South Boulder Creek near the CU middle levee and the Viele channel and Anderson Ditch. At Baseline the West Valley Overflow spills seven different ways, three of which can send portions of their discharges to Bear Canyon Creek. Some of this flow, and flood discharges following other routes, discharge to the Wellman Ditch, with a portion of the total flow going north to Boulder Creek through neighborhoods midway between 55th and Foothills. From Foothills and Baseline, the West Valley Overflow discharge only reflects the estimated portion of the West Valley Overflow following the Crossover Ditch and Dry Creek Ditch No. 2. The discharge drops to nil (30 cfs) for the flow crossing under the Wellman. Thus, of all the flow arriving in the West Valley Overflow to Foothills and Baseline, most spills to Bear Canyon Creek or the Wellman Ditch, with portions of the Wellman overflow going north to Boulder Creek. Downstream of the Wellman the route along Dry Creek Ditch No. 2 increases as the Wellman spills just upstream and downstream of 55th, and increases again midway across the golf course due to the South Boulder Creek spill.

MODEL REASONABLENESS AND REFINEMENT

Detailed model verification and reasonableness evaluations are presented in Section V for individual basins, comparative Colorado Unit Hydrograph Procedure (CUHP) modeling for representative tributaries, for regional relations developed by CWCB, and other unit discharge (cfs/acre) comparison. It appears the results are reasonable for the tributary watersheds.



SOUTH BOULDER CREEK
DISCHARGE PROFILE
TEA
FIGURE I-1



WEST VALLEY OVERFLOW
DISCHARGE PROFILE
TEA
FIGURE 1-2

Mountain Modeling

Comparison of statistical analysis of the Eldorado Gage stream flow data with the UDSWMM deterministic model reveals an apparent disparity as the statistical methods give lower discharges than UDSWMM. We believe this is explained by the flood storage which is taking place in Gross Reservoir and the numerous storages upstream of the Moffatt rail line. To a lesser degree, refining the South Boulder Creek channel routing parameters based on representative field survey sections might reduce (or increase) the UDSWMM model result.

Storage exists upstream of the rail line on South Draw, the major tributary above the Eldorado gage. Other storages upstream of the rail line can be observed on the topographic maps, but we have not documented their characteristics or effects. Further, the Denver Water operational data for Gross Reservoir illustrate significant storage of flood type events, such as the flood of May 1969.

The regulations only allow recognition of storage above fixed spillways of water supply storage operated by governmental entities. Specifically prohibited is recognition of storages such as those formed by rail lines unless there are institutional agreements and the facilities are documented as adequate. Therefore, there are only two basic choices regarding selection of analytical model techniques:

- 1.a) Make institutional arrangements to either preserve the operational practices of Denver Water which result in flood storage, or explore other institutional *arrangements and improvements which would enhance storage at Gross.*
- b) Investigate characteristics, needed physical improvement, and make institutional arrangement with the Railway to preserve or enhance this storage.
- c) Refine the UDSWMM modeling accordingly to reflect the physical condition and changed facilities, comparing again with statistical methods if the physical and operational conditions are the same.

Or

2. Don't rely on the statistical data at the Eldorado gage, since it represents the result of inadvertent storage.

The sponsors have decided to proceed with the latter choice and issue this report on an Interim Basis, since making arrangements with Denver Water and the Railway could take too long. The sponsors are pursuing possible cooperative arrangements with Denver Water. They may pursue storage with the Railway, both to evaluate washout hazards and for flood control, but at a later date after the Master Planning effort has made significant progress toward an agreed solution.

Floodplain Hydrology Modeling below the Canyon through the Urban Area

While the model here gives reasonable results for the tributaries of the foothills and floodplain areas, the actual main stream routing is deficient because of the inherent limitations of UDSWMM, which doesn't simulate dynamic storage routing.

Review of the total discharges proceeding from Highway 93 downstream reveals that there is essentially no reduction of peak flow until past Baseline. Also, comparison of the hydrograph shapes at various points down the main stream and the West Valley Overflow reveals that the spiky peaks are not being attenuated. Floodplain dynamic storage routing is a well documented phenomena. We believe different modeling techniques should be used such as either HEC-1 stream routing based on HEC-2 model storage routing data, or a more advanced version of SWMM with routing capability EXTRAN, or UNET. Most importantly, the peaks of the main stream hydrographs are being spilled to the West Valley urban area. Any attenuation of the peaks in the main stream results in direct reductions of spills to the West Valley. Section V presents comparative hydrographs to illustrate these points.

The 500-year flood event appears to be reasonably simulated, but probably could be refined. For this and the other events, the model is subject to survey and hydraulic analysis refinements of the numerous splits and subsequent floodplain hydraulic modeling.

Reasons for Change from Previous Model

Basically the total flows are higher than the 1977 Corps' model because of increased and longer duration rainfall, increased area, and to a lesser degree, because of more appropriate land surface and stream routing characteristics. The flows would have been even higher, but Gross Reservoir was found to have larger storage than that previously used by the Corps based on information from both the Colorado State Engineer's Office and Denver Water.

GENERAL CONCLUSIONS

While we are satisfied with the results of the modeling effort and feel that the report will meet regulatory requirements, allow reliable and safe delineation of floodplains, hydraulic structure sizing, and form a base for initiating the master planning effort; there are several conditions to be aware of:

1. Gross Reservoir in reality provides significant flood storage below the crest of its spillway, which is to the benefit of the downstream residents so long as its operation is sustained. The model does not depict this storage below the spillway crest, as directed by the sponsors and following CWCB and FEMA

regulations. If a formal agreement was made with Denver Water to sustain their historic operating practices, or other arrangements made for providing flood storage, then the hydrology downstream would be lower, mainly from a total flood volume and duration perspective. Peak flows in the urban areas are dominated by storms occurring in Eldorado Canyon and the downstream watershed.

2. The rail line to the Moffatt Tunnel provides, we believe, significant flood storage on the south tributaries from the foothills to above Gross Reservoir. We are familiar in detail with one site on South Draw where about 80 to 100 acre feet of storage occurs and reduces the 100-year flood peak by more than half.

There may be as many as 20 to 30 storages that exist, that vary from the very small to a size such as that found in South Draw. Since agreements are not in place to sustain these storages, they have not been included. These storages exist, benefitting the downstream conditions for most events, but also may present a hazard, as the storages are not engineered for flood control and may be susceptible to breaching during large floods.

3. When flood control facilities, floodplain mapping, or refined surveys are available, the hydrology model can be further refined to better depict flow splits and hydraulic controls. Thus, we can envision further revisions to the hydrology model in the future.
4. The UDSWMM program has very limited stream flow routing algorithms. We feel it is inadequate to simulate the dynamic floodplain storage routing of the South Boulder Creek below Eldorado Springs and the West Valley Overflow. Thus the peak flows in these areas, determined in this study, are probably high. Effectively, the peaks of the hydrographs are "trimmed" and sent to the West Valley Overflow without the natural attenuation that exists.
5. Our limited sensitivity tests indicate that the model is highly responsive to the geometry given for the South Boulder Creek main stream. While our work for the Colorado State Parks has afforded the opportunity to incorporate field survey of representative sections at Eldorado State Park, it may be worthwhile to conduct field surveys of representative sections at other locations in order to better represent the mountain streams.

RECOMMENDATIONS

1. The hydrology modeling herein appears reasonable and should be adopted on an interim basis.

2. The hydrology can be used in the alternative evaluation process. Alternatives developed might consider options to "firm up" existing flood storage in the mountains, which may in turn lower flows to the significant, potentially impacted floodplain in the West Valley.
3. Stream flow routing model improvements should be pursued in the main stream below Gross and especially in the floodplains downstream of Eldorado Canyon, particularly if new floodplain mapping is to be pursued.
4. This new hydrology model should be considered as an interim result and subject to further change. Subsequent surveys, analysis, floodplain mapping, and design of improvements may reveal the need for refinements to reflect important splits, floodplain characteristics and dynamic storage, and other factors.

SECTION II

SOUTH BOULDER CREEK WATERSHED

GENERAL FEATURES

There are numerous features which influence South Boulder Creek flows arriving at the Highway 36 Bridge.

There are approximately 93.2 square miles of mountainous watershed above Gross Reservoir, ranging in elevation from about 7300 feet to the Continental Divide (11,900 to 13,294 feet M.S.L.). Flooding at these altitudes is often dominated by snowmelt runoff. Rainfall data is sparse and the NOAA Atlas statistics are less reliable at these elevations.

Gross Reservoir captures much of the basin runoff and stores it with diversions from the west slope. The west slope diversions are reduced when the reservoir is nearly filled. Practically, most flood runoff events would probably be trapped for later release. Even with a conservative assumption that the reservoir was full at the beginning of the flood, as made by the Corps and herein, the spillway and reservoir characteristics would greatly attenuate inflows and delay the upstream peak flows from joining downstream peak flows.

Downstream of Gross Reservoir to Eldorado Springs there are approximately 19.4 square miles of steeply sloping mountainous watershed ranging in elevation from 5720 to 8900 feet M.S.L. The Eldorado Stream Gage is about one mile upstream of Eldorado Springs. There, the tributary area below Gross is 18.2 square miles. This area can experience significant extreme rainfall with resultant large peak flows.

South Boulder Creek emerges from the mountains at Eldorado Springs and flows to Highway 93, gaining another 7.9 square miles of tributary area (27.3 square miles below Gross) of steep watershed ranging from 5400 to 8760 feet.

South Boulder Creek begins to have alluvial fan characteristics above Highway 93. Modest flood flows can spill from the main channel, which is generally on the east side of the valley, and travel along a west overflow path with two irrigation ditches (hereafter referred to as the West Valley Overflow). One of the ditches is the Dry Creek Ditch No. 2, which travels a separate 6 mile route before rejoining South Boulder Creek. Ground elevations in the valley are often lower west of Dry Creek Ditch No. 2, therefore, flood flows can be carried west of this Ditch.

From Highway 93 to Highway 36 another nine square miles are potentially tributary to South Boulder Creek at Highway 36 (36.3 square miles below Gross), ranging in elevation from 5350 M.S.L. to 8461 M.S.L. at Bear Peak. The character of the

of the watershed varies significantly. Bear Peak and steep mountain slopes aligned with the Flatirons are on the west. David's Draw, which is also on the west side, has some dense development. There are moderately steep to mildly sloping agricultural areas, open space, riparian cottonwood groves, and the gravel pit area in and along the valley bottom. There is a large foothills tributary on the east which includes the Marshall Reservoir and a downstream basin which has steeply sloped valley sides with a mixture of brush, grass, and trees. On the east side of the watershed there are moderately sloping agricultural areas which naturally drain to South Boulder Creek, but whose drainage is interrupted by several irrigation ditches.

The wide floodplains and multiple flow paths of South Boulder Creek provide an important balancing effect by storing, routing, and slowing the flashy peak runoff rates from the steep slopes and tributary streams. From Highway 93 to Highway 36 the main channel conveys day to day flows, and whatever flood flows do not spill upstream. The majority of the 100-year flood will be carried in the West Valley Overflow route. However, the West Valley Overflow is forced to carry much of the water back to South Boulder Creek by the Upper and Middle Flatirons Quarry Pit (CU) levees just upstream of Highway 36. Some minor amount of the overflow will not return to South Boulder Creek and will be conveyed by either Dry Creek Ditch No. 2 and or limited overbank conveyance to join the South Boulder Creek spill just downstream at Highway 36.

Downstream of Highway 36 and the main channel of South Boulder Creek there are another 6.2 square miles of potential tributary area (42.5 square miles below Gross Reservoir, 135.7 square miles total basin). This basin ranges in elevation from 5170 feet M.S.L. at the confluence with Boulder Creek to 6050 feet M.S.L. at the top of the Viele watershed. The watershed is largely urbanized with notable exceptions being the riparian corridor directly along the main channel of South Boulder Creek, the highest portion of the Viele watershed, the golf course, and some of the hills on the east side of the watershed. The valley bottom is a mile wide and is an alluvial fan, with varying cross slope direction and some moderate down valley slope.

The Viele watershed is on the southwest side of the basin, and begins on a ridge just south of the confluence of Bear Canyon Creek and Fern Canyon. It has four significant storage facilities and an outfall channel on the south side of the valley that crosses Highway 36 at the Foothills Interchange and then joins South Boulder Creek just north of South Boulder Road.

IRRIGATION DITCH DIVERSIONS

There are numerous water supply and irrigation diversions and ditches in Eldorado Canyon and the downstream watershed. Normally, the diversion effect of flood

waters by irrigation systems, such as transbasin diversions and storm drainage conveyance by ditches, is not considered in the sense of having a positive mitigating or other effect on flood control or conveyance because the local governments normally have no control of the ditch companies and because the ditch companies are not usually responsible for, nor are they required to convey runoff water which enters the ditches.

The irrigation diversions and ditches do have physical effects, both positive and negative, on the drainage and flood control for this watershed in the following ways:

1. Aggradation of stream beds can occur at diversion structures which can cause changes in flood flow distributions and levels. Examples include the South Boulder Ditch, Dry Creek Ditch No. 2, the Marshallville Ditch, the Shearer Ditch, the Leggett Canal, the McGinn Ditch, the New Anderson Ditch, the New Dry Creek Ditch, the Enterprise Ditch.
2. Redistribution and collection of flood waters, particularly in the South Boulder Creek overflow, occurs because of the ditches and related conveyance structures. Examples include South Boulder Ditch, Dry Creek No. 2 Ditch, Marshallville Ditch, the Anderson Ditch, the Wellman Ditch.

The East Boulder Ditch appears to have little potential effect.

Bear Canyon Creek can spill to the Anderson Basin (and Ditch) at Table Mesa and Broadway (Highway 93). However, no spillage or transbasin diversion is assumed herein according to the contract and accepted practice.

Downstream of Highway 36 on the west side of the basin there are three subbasins which are drained by storm sewers to Bear Canyon Creek, but which may contribute to the South Boulder Creek basin because of street drainage patterns and the Wellman Ditch. The Wellman Ditch can also bring in significant runoff from other watersheds, particularly Bear Canyon Creek. No transbasin flow is assumed.

There are three irrigation ditches which have been incorporated into the SWMM model, on a limited basis, because their bank topography and overflow carrying capacity significantly influence the redistribution of South Boulder Creek flood waters. These include:

1. The Wellman Ditch from upstream of Foothills to South Boulder Creek
2. The Anderson Ditch from Highway 36 to Viele and South Boulder Creek

3. The Leggett Canal to Valmont, which can receive headgate overflows and convey flood waters to Boulder Creek

KEY FLOOD CONTROL FEATURES

There are numerous features which presently control and/or potentially can change and affect the distribution of South Boulder Creek floodplain flows. For purposes of simplification and organization these can be grouped as follows.

The Upper or Highway 93 Split (See elements 1423 and 1413 and Drawings 4, 5, and 9.)

Two splits redistribute a major portion of the South Boulder Creek flow to the west side of the valley at Highway 93. There is a complex of several facilities and topographic characteristics, including the South Boulder Ditch and Dry Creek Ditch No. 2 diversions, low main channel capacity and flow characteristics, Highway 93 bridge capacity and the downstream Marshallville Ditch diversion, and the profile of the local access road which controls much of the overflow hydraulics and interaction with the spills just above Highway 93.

It is important, for the purposes of floodplain management, to realize that changes of any one component are unlikely to effectively reduce the spill. For example, if one enlarged the Highway 93 bridge over the main channel in order to decrease the spill, the upper portion of the net spill at the ditches would probably increase to somewhat negate the improvement.

The capacity of the double box culvert on the west side of the valley will be significantly exceeded during the 100-year event. The 93 roadway will be overtopped to the east of the box culvert because of the narrowing valley section. This, coupled with the cross slope of the super elevated road, should direct most of, if not all, of the flood waters to the west valley floodplain below, and not to the north along Highway 93, except for the local irrigation lateral and drainage ditch culvert on the west side of Highway 93.

Floodplain Characteristics between Highway 93 and the Flatirons Levee (Drawing 5)

For the most part, significant South Boulder Creek flood events are carried in two paths, one on the east side of the valley in the main channel, and the second, carrying the majority of extreme floods, in the left or West Valley Overflow route along the South Boulder and Dry Creek No. 2 ditches. Generally the west side of the valley is lower, except where the flow approaches the Flatirons Levee and is diverted east to the main channel. Because of the elevation differential, and locations where pits have been created in the floodplain, there is some risk that

additional flow could be directed to the west side of the valley from the main channel below Marshall Road.

Upper and Middle Flatirons Levee Area (Drawing 5)

The distinguishing features here include the upper portion of the levee which forces water back to South Boulder Creek, the middle levee section which sustains this deflection of flow, the adjacent Dry Creek Ditch No. 2 which conveys the ditch flow and keeps some of the west bank floodplain flow from going back to South Boulder Creek.

If the upper portion of the levee were to be breached or overtopped, most West Valley flow would continue on the west side to the approximate location of the Viele Channel west of the Foothills Parkway and Highway 36 Interchange. If the middle portion of the levee were to be breached, we would expect a smaller increase in spillage to the interchange than if the upper levee breached.

The Middle or Highway 36/South Boulder Main Channel Splits (Drawings 5 and 6)

Most of the flood flow in the West Valley Overflow drops back into South Boulder Creek by the Middle Flatirons Levee (see element 1513), due to lack of West Valley Overflow carrying capacity and the lower elevation of South Boulder Creek. For the 100-year event, the model shows the majority of the flow in South Boulder Creek (approximately 1800 feet upstream of Highway 36).

Analysis has shown significant 100-year spillage from South Boulder Creek back to the West Valley Overflow to begin about 500 feet upstream of Highway 36. (See element 261.) This spill is controlled by several components including: 1) the Highway 36 main stream bridge and the adjacent downstream McGinn Ditch Diversion, 2) the topography in the actual split area which is approximately 180 to 430 feet west of the creek centerline, and 3) the West Valley Overflow floodplain hydraulics and water surface profile which is controlled by the topography and roughness characteristics from the split area west for about 1200 feet.

Aggradation of the main channel area could lead to degradation of the open space area and increased flows to the West Valley. This aggradation could potentially be caused by upstream sediment movement and limited transport capability of the bridge area channel hydraulics and the McGinn Ditch, or by erosion of the overbank spill zone. Permanent transfer of the main channel to the West Valley is possible, but not likely. However, some increase in spillage appears likely with time given present conditions.

Flow arriving at the area of Highway 36 Bridge over the main channel of South Boulder Creek can potentially spill to the northwest. There are three major and several minor routes which the flow can take:

1. Main Channel. The main channel route conveys flow in a largely riparian cottonwood grove floodplain which has a mixture of open space, agriculture, residential, and commercial uses. As the main channel passes by the Wellman Ditch additional spills to the West Valley occur through a residential area and the golf course (element 237, Drawing 7). Below Arapahoe, the Leggett Canal to the Valmont reservoirs (Hillcrest, Valmont, Leggett) can also carry flood flows (236, Drawing 8). Also, there is another potential spill to the west to Dry Creek Ditch No. 2 near the railroad tracks, which has not been evaluated herein due to complex backwater analysis and perceived likely low magnitude.
2. Direct return to South Boulder Creek: Dry Creek No. 2, Viele, and the Anderson Ditch. The South Boulder Creek spillage upstream of Highway 36 that flows to the northwest would be joined by flows from Dry Creek Ditch No. 2.

There are three modest conveyance systems which will carry an initial portion of the flow across Highway 36 and, for the most part, back to South Boulder Creek just below South Boulder Road. The first 220 cfs would be conveyed in the Dry Creek Ditch No. 2 box culvert under Highway 36 (263 and 376, Drawing 10), and via an irrigation ditch to a spill structure (375) near South Boulder Road which would shed most of the flow to the New Anderson Ditch, which subsequently could spill to Viele (378). Greater spillage flow from South Boulder Creek, on the order of 500 to 800 cfs, will be intercepted by the Viele drainage system (265 and 1267) adjacent to the Foothills Parkway Interchange and conveyed under Highway 36, and then combine with the spillage from the lower Anderson Ditch and the Dry Creek Ditch No. 2, and flow under South Boulder Road to South Boulder Creek.

Greater South Boulder Creek spillage would overtop the Viele system and flow onto the freeway (292). Some portion of this spillage and local drainage flows can be conveyed by the Anderson Ditch to the east to South Boulder Creek, subject to some spillage to the north at several points, the first and most significant of which would occur near the Anderson culvert under the Highway 36 eastbound on ramp (383).

3. West Valley Overflow. Greater South Boulder Creek spillage (from 700 to 1000 cfs) would flow onto Highway 36 (360) and pass by the Anderson Ditch, and then largely overflow the Highway 36 barrier (352 and 1812) and

discharge to the north of the freeway on the west side of Foothills Parkway and travel north, along the west side of Foothills Parkway.

At the intersections of Foothills and Baseline (Drawings 7 and 9) flow is first retarded by two small storage ponds (356 and 398, Drawing 9). Flows such as the 100-year flood can follow any one of seven routes. Three potentially leave the watershed along Foothills Parkway to the northwest, two flow east on the lanes of Baseline and split again to the north through the Country Club Park neighborhood, and the last two either by the culverts under Foothills or over the roadway to the east storage.

The east storage first discharges by a box culvert (308) which has been partially obstructed by an earth dike to form a "poor man's" hydraulic control. This culvert under Baseline directs flow to the Crossover Ditch, on the north side of Baseline, which then carries flow easterly to Dry Creek Ditch No. 2 near 55th. However the east storage spills (396) at moderate flows to Baseline, which then can contribute to and join spillage from the Crossover Ditch, and add to the spillage through the Country Club Park subdivision. Reference documents refer to drainage problems in these areas. These spillages eventually go to the Wellman Ditch adding to runoff already being carried from Bear Creek and probably from the three South Boulder Creek spillages following Foothills.

Much of the Crossover Ditch is a levee situation of questionable stability. We have assumed the Crossover Ditch could carry flow to culvert full-flow capacity based on approximate hydraulics. If the Crossover Ditch breached, most of the flow could go north increasing the flow through the subdivision, and then to the Wellman. Regardless of Crossover Ditch breaching, the flow in the Wellman would be about the same.

The Crossover Ditch joins with Dry Creek Ditch No. 2 flow crossing Baseline, then the combined ditch flows northeast and then north along the west side of 55th as Dry Creek Ditch No. 2 in a boulder, wall-lined channel.

At 55th and the Wellman Ditch (Drawing 11), Dry Creek Ditch No. 2 and the Crossover Ditch flows join the Wellman Ditch except for minor flows conveyed in the Dry Creek Ditch No. 2 undercrossing pipe (1401).

The Wellman Ditch crosses Bear Canyon Creek in a combined diversion and spill structure that can potentially bring transbasin flood waters into the South Boulder Creek watershed. However, we have assumed this is not the case, per sponsors' direction, standard practice, and the knowledge that significant flood waters would be entering the Wellman from South Boulder Creek overflows to the West Valley. Drawing 11 reflects some of the key

details of these inflows. The westerly overflow at Baseline and Foothills, element 335, can convey significant flows to the Wellman upstream of Foothills. This flow can go down the Wellman (limited by the Foothills culvert and downstream Wellman capacity), but can also overflow to Bear Canyon Creek. Elements 333 and 334 (the Baseline and Foothills overflow to Foothills) convey flows up to the capacity of the inlets and a 36 inch storm sewer to the Wellman. For flows greater than storm sewer capacity, flood waters drain mostly to Bear Canyon Creek.

The Wellman Ditch acts as a major collector channel for other West Valley Overflow flow paths. The collected overflow flood waters in the Wellman simultaneously discharge with a small flow to South Boulder Creek (200 to 500 cfs), then to spills, in rough order:

- a) north to the golf course on the east side of 55th (element 390)
- b) north to the subdivision immediately west of 55th (element 324) which subsequently (element 323, Drawing 11 and element 1337, Drawing 7) splits twice again to the golf course and to the north (most of which finds its way to Dry Creek Ditch No. 2 but could overflow some to Boulder Creek)
- c) north to the subdivision along Merritt Drive, which then drains to both Dry Creek Ditch No. 2 (West Valley Overflow) and Boulder Creek

A major portion of West Valley Overflow (element 320, Drawing 7) joins the South Boulder Creek spill through the golf course (element 1906). The combined spillage (element 1909) would move through the industrial and commercial area toward the outfall Dry Creek Ditch No. 2, which at this location is a major flood conveyance.

SUMMARY CONTROL FEATURES

The direct flow control features starting at the Highway 36 main channel spill are tabulated in Table II-1, with annotation as to the relative effect on the overflow and local drainage distribution. High [H] denotes a control that is a major influence on overflow magnitude and drainage problems. Moderate [M] denotes control that moderately affects the intensity of the overall problem and local flooding characteristics. Lesser [L] denotes that the particular component or subsystem is important to understanding characteristics of the system, but whose accurate simulation may have only small effects on the overall performance and flood hazard recognition.

Table II-1

FEATURES DIRECTLY AFFECTING WEST VALLEY OVERFLOW SPILLAGE
AND LOCAL DRAINAGE

SOUTH BOULDER CREEK

- Rail line storages [H]
- Gross Reservoir [H]
- Two spills above Highway 93 [H]
- Spill above Highway 36 [H]
- Spill above Arapahoe Road to and including Wellman Ditch [H]
- Channel, diversion, and backwater characteristics downstream of Highway 36 [M]

DRY CREEK NO. 2 DITCH

- Culvert under Highway 36 including adjacent ditch and local drainage culverts under Highway 36 [H]
- Spill structure and crossing of South Boulder Road [H]
- Ditch, culvert, pipe and related storm sewers, minor spills, South Boulder Road to downstream of Baseline [L]
- 55th Ditch from Baseline to Euclid [M]
- 55th Ditch from Euclid to downstream of the Wellman [H]
- Downstream of 55th [M]

VIELE DRAINAGE SYSTEM

- Upper Basin conveyance network [M]
- Upper Viele storages [M]
- Viele storages and culverts at Interchange [H]
- Lower Viele outfall channel [M]

ANDERSON DITCH SYSTEM

- Diversion and spillage from Bear Creek [M]
- Anderson conveyance system from Broadway to Interchange [L]
- Anderson Ditch culvert entrance and multiple pipe conveyance under Interchange, and blockage issues [H]
- Anderson Ditch system east of Foothills through off ramp area to next culvert downstream, through likely spill zone [M]
- Anderson Ditch system east to spill zone [L]
- Anderson Ditch spill to Viele [M]
- Anderson Ditch to South Boulder Creek [L]

WEST VALLEY OVERFLOW

- Highway 36 from Viele culvert west to Basin Divide [M]
- Lower drainage network through Highway 36 and downstream along Foothills to near Baseline [M]
- Foothills and Baseline Intersection including two storages with controls, storm sewers, roadway grades [H]
- Westerly subbasin drainage characteristics influencing discharge characteristics to South Boulder and Bear Creek watersheds [M]
- Crossover Ditch from Foothills to Dry Creek No. 2 along Baseline [H]
- Lower Flatirons levee and culvert under the on ramp to Viele [M]
- Street drainage and subdivision characteristics north of Baseline [M]
- Street drainage and subdivision characteristics north of Wellman [M]
- Golf course and industrial/commercial area north of Wellman [M]

WELLMAN DITCH

- Bear Creek diversion and canal crossing to and including Wellman box culvert under Foothills [H]
- Combined hydrologic inflows and flow spill hydraulics along the Wellman [H]
- Canal flow and levee characteristics from Foothills to 55th [H]
- Canal flow and levee characteristics from 55th to South Boulder Creek [H]
- Foothills storm sewer and street flood water conveyance characteristics and flow/spillage to Wellman [M]

HISTORICAL FLOODS AND HYDROLOGY COMPARISON

The G&O study presented gage data for South Boulder Creek at Eldorado Springs for peak flows greater than 1,000 cfs. These data appear to be taken from the 1969 Corps of Engineers Floodplain Information Report, except that the May 7, 1969 is updated from "preliminary estimates." We have checked flow data through 1999 and there have been no additional flood peaks reported greater than 1000 cfs.

TABLE II-2

Historical Peak Discharges on South Boulder Creek at Gaging Station Near Eldorado Springs¹

Drainage Area: 109 Square Miles
Location: 6.7 miles downstream from Gross Reservoir
and 1 mile west of Eldorado Springs

Peak Discharges ^{2,3}	
Date of Occurrence	CFS
3 Jun 1895	1130
9 May 1990	1100
20 Jun 1909	1340
24 May 1914	1240
6 Jun 1921	1440
2 Sep 1938	7390
21 Jun 1947	1290
6 Jun 1949	1430
18 Jun 1951	2370
4 Jun 1952	1080
7 May 1969	1690

¹ Records taken from United States Department of Interior Geological Survey, "Water-Supply Papers 1310 and 1680" and the yearly "Water Surface Records for Colorado."

² Only peak discharges which exceeded 1,000 cubic feet per second (cfs) are listed.

³ There have been no events reported greater than 1,000 cfs through 1999.

The 1969 Corps study "Flood Plain Information, Boulder and South Boulder Creek" used these data (through 1969) as its basis for hydrology using a Log-Pearson Type III statistical methodology. A 100-year flood of 5000 cfs was recommended for South Boulder Creek.

The 1973 R.W. Beck study "Major Drainageway Planning, South Boulder Creek" used the 1969 flood event data, including rainfall and the Eldorado gage data to determine unit hydrograph coefficients. Then they used NOAA rainfall statistics, assumed a design rainfall event below Gross Reservoir, and routed subbasin hydrographs down the stream. This technique allowed prediction of discharges along the stream as various streams joined in. Their 100-year flood estimates for South Boulder Creek varied from 4300 cfs at Eldorado Springs, 5300 cfs at Highway 36, and 5000 cfs above the confluence with Boulder Creek. Based on assumed 1990 development conditions the flows increased to 5600 cfs at Highway 36 and 5400 cfs above the confluence, with peak discharges from Marshall Gulch of 2300 cfs and Viele Gulch of 900 cfs.

Thus, the studies support a 100-year discharge at Eldorado Springs in the 4300 to 5000 cfs range. However the Beck study assumed a constant discharge from Gross Reservoir of 300 cfs, rather than analyzing a rainfall runoff flood above Gross.

The latter Corps hydrology, which was used in the 1986 G&O study, was based on the SWMM computer program. In that model, they assumed rainfall flooding in the entire watershed and routed the flow through Gross Reservoir, assuming the reservoir was full to the spillway. G&O reports a 100-year flood at Eldorado Springs of 4800 cfs, which is similar to the 5000 cfs 1969 Corps statistical determination.

EXAMPLE FLOOD EVENTS

Two events are of particular interest, August 31 to September 4, 1938, because it is the largest historical event on South Boulder Creek and gives graphic evidence of the stream's capability to erode, scour, and move sediment and debris; and May 4 to 8, 1969, because it is a recent event, is of frequent recurrence interval, and actually flooded Highway 36.

31 August - 4 September 1938

The following excerpts from the Corps' 1969 report described the event:

"This storm produced general rains over all of eastern Colorado. The largest amounts of precipitation occurred in the mountains where over 6 inches was reported west of Eldorado Springs. Boulder reported 3.62

inches of precipitation from 31 August to 4 September with 2.32 inches falling during 2 September. Eldorado Springs had 4.42 inches of rainfall. Approximately 80 percent of the total precipitation falling in the South Boulder Creek basin fell in the late afternoon and evening of 2 September. The resulting flood, with a peak discharge of 7,390 c.f.s. arrived at Eldorado Springs at 10:00 p.m. on 2 September. The peak gradually subsided as the flood moved downstream. A maximum discharge of 4,410 c.f.s. occurred near the mouth of Boulder Creek at noon on 3 September. Several buildings in Eldorado Springs were destroyed as a result of the flood eroding away their foundations. Numerous bridges were destroyed and the valley from Eldorado Springs to Boulder Creek and down Boulder Creek to the St. Vrain Creek were in shambles. This flood is the highest recorded flood on South Boulder Creek."

Phyllis Smith reports in "History of Floods and Flood Control in Boulder, Colorado" on this event, with extensive photographs (by the Boulder Historical Society) of the damage in Eldorado Springs. They depict destruction of buildings and movement of rock in the 6 inch to 2 feet range. Ms. Smith notes that South Boulder Creek flooded again the following year, but apparently there is no reported gage data.

We believe that there is sufficient watershed below Gross Reservoir to allow such events, including large scale sediment and debris movement.

4-8 May 1969

The Corps also reported on this event in their 1969 study.

"This was also a flood of long duration general storm. Precipitation was heaviest in the mountains; part of it being snow. In the Boulder and South Boulder Creek basins the rainfall continued at a moderate rate for nearly four days. Total precipitation for the storm amounted to 7.60 inches at Boulder and 9.34 inches at the Boulder Hydroelectric Plant located about 3 miles up the canyon from Boulder. Precipitation amounts totaled 8.11 inches at Eldorado Springs and 10.05 inches at Gross Reservoir on South Boulder Creek. Peak flooding occurred on the 7th of May at Boulder and Eldorado Springs. Preliminary estimates based on the gaging records, indicate a peak discharge of 1,150 c.f.s. occurred on Boulder Creek. Flooding extended over large portions of the flood plain starting at the junction of the two streams near Valmont Road and extending downstream through the remainder of the Boulder Creek study reach. Evidence of two bridge failures is illustrated.

The gaging records show that floods the size of the May 1969 flood occur on an average of about once every five years on Boulder Creek and about once every seven years on South Boulder Creek."

The 1986 G&O study reports the 1969 event flow as 1690 cfs, and states that the recurrence interval is approximately once every seven years. We obtained calibration records for the Eldorado Gage. There were notes indicating that the boulders used as a control sill in the bed of the river moved.

Ms. Smith reports extensively regarding this event. Numerous streams, including Bear Canyon Creek, flooded. A photograph of South Boulder Creek by the Boulder Daily Camera shows the wide floodplain of South Boulder Creek. Regardless of location, flooding of this width would correlate to spills at Highway 93 and 36, based upon hydraulic analysis by others and TEA.

In the Wright McLaughlin report Urban Storm Drainage; Major Drainageway Planning, South Boulder, September 1970, it was reported that Highway 36 was overtopped and traffic halted for more than a day " . . . in the Lower Viele Basin." The study denotes the need for improved drainage facilities to take care of flow from Viele and Anderson Ditch, and future areas of urbanization.

In our further research, we identified the CDOT project manager, Ken Morrow, who observed the construction of the barrier. He was an eyewitness at the site during the flood. He indicated that the barrier was overtopped by flood waters, without damage, in the same area identified by Love and this study. Overtopping occurred for a brief period, followed by gradual draining through the openings in the barrier and the drainage network. Mr. Morrow reported that he was criticized by highway safety critics for allowing the openings.

We believe it is highly likely that a combination of local drainage from the Anderson Ditch tributary area, Viele, other local tributary areas, and spillage from South Boulder Creek led to this overtopping. We doubt that local flooding alone could lead to a shutdown in excess of a day.

GEOMORPHOLOGY

Figure II-1 is a compilation of 1950 and 1942 USGS topographic maps of South Boulder Creek for the reach of immediate interest. The topography of the valley bottom illustrates alluvial fan tendencies as evidenced by the fan shaped contours and numerous shallow stream patterns across the valley. We have delineated a zone where it is physically possible for flood waters in the valley bottom mainstream just above Highway 93 to disperse laterally across the valley bottom. Note that the South Boulder Creek main channel is on the right or east side of the

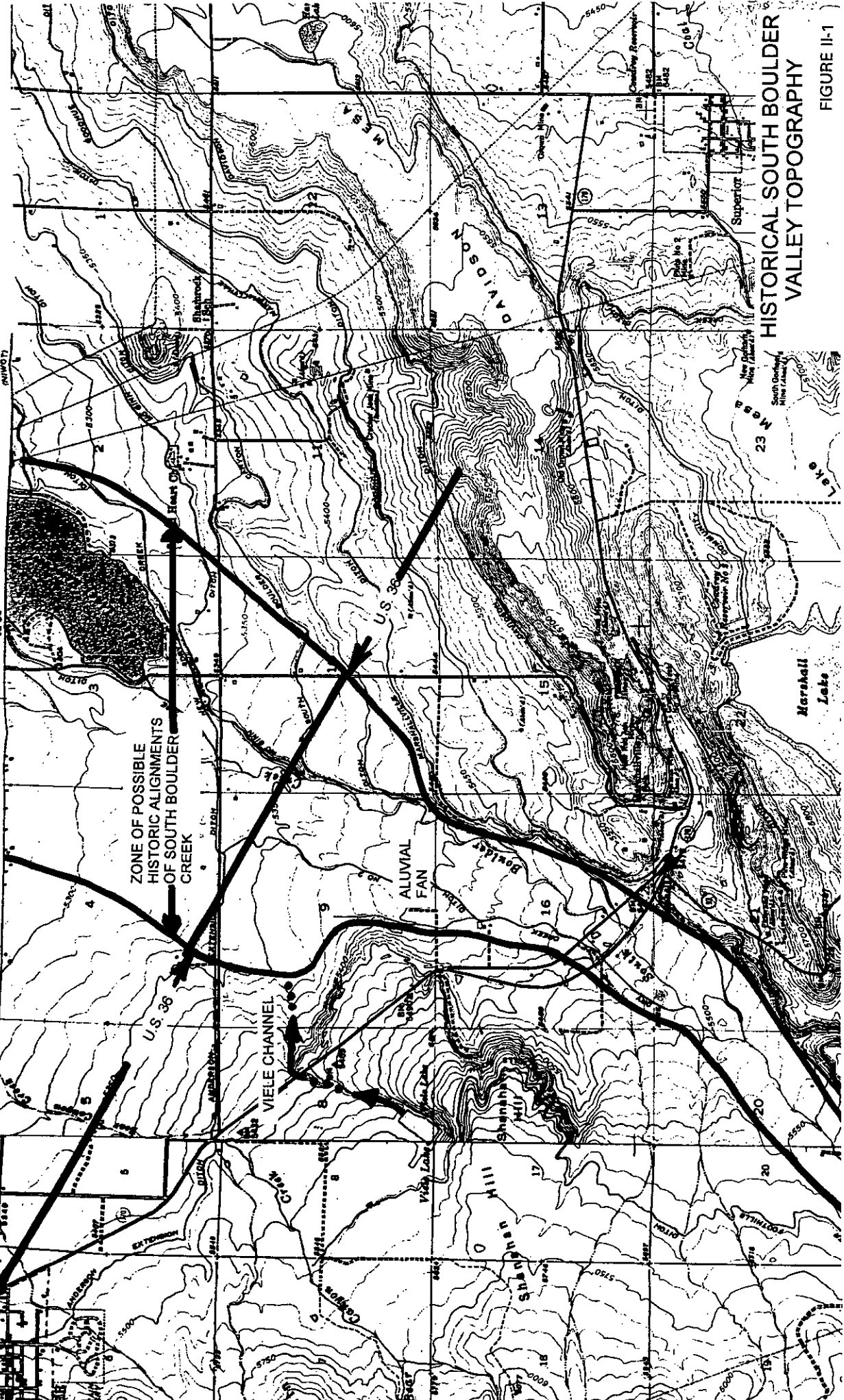
7 1/2-MINUTE SERIES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

FILE COPY
Investigation and Mapping

STATE HIGHWAY DEPARTMENT
CIT
DENVER BOARD OF WATER

1942 106'18"

12'30"



HISTORICAL SOUTH BOULDER
VALLEY TOPOGRAPHY

FIGURE II-1

valley, and that Dry Creek Ditch No. 2 at first follows the left or west side of the valley until it crosses the present location of Highway 36, where it goes down the middle of the valley. To the left or west side of the ditch, the contours are lower than the ditch location. Thus flood flows could make it to the west side of the valley once they were higher than Dry Creek Ditch No. 2, which is a likely occurrence in times of flood.

There are two geologic zones of alluvium, based upon USGS geology maps and report. The large center zone, denoted as Piney Creek Alluvium, is primarily associated with alluvium coming from the mountain area drained by South Boulder Creek and is related directly to "modern stream floodplains." The adjacent Broadway and deeper Louvers Alluvium have surface grades that are generally higher than the modern floodplains, but can have beds below the modern floodplain. They illustrate a broad potential floodplain. The Piney Creek Alluvium coupled with the historical topography illustrates a much wider potential floodplain than the FHAD or FIRM maps and the tendency for the streams and floodplains to migrate.

There is a significant tendency for the main channel to spill to the West Valley above Highway 93 and Highway 36. If a major event were to transport sediment from the mountains, we believe this tendency would increase. The east to west valley tendency occurs downstream of Marshall Road and in most of the lower South Boulder Creek floodplain.

Sediment transport potential for long term movement of sediment and bed change is slowed by Gross Reservoir, which traps sediment from a majority of the watershed. However, peak flood flow rates at the mouth of the canyon are unlikely to be significantly reduced by Gross Reservoir because of the steep, narrow, and large area below the reservoir. Therefore the stream at flood stage has nearly the same capacity to transport large sizes of material as in pre-Gross conditions, but the total volume of sediment would be reduced.

Further, there are numerous local effects which could lead to deposition and could lead to migration, such as at bridges, diversions, and low capacity channel sections. Also there are reaches where migration is potentially more likely, such as in the washing pits and at the bank upstream of Highway 36 where the spill presently occurs. These tendencies can affect the flow splits assumed herein, and thus affect the hydrology of South Boulder Creek and West Valley Overflow flows and duration of flooding.

The hazards associated with breaching or overtopping of the upper or middle segment of the Flatirons Levee need to be carefully analyzed for the aspect of major stream migration to the West Valley and for related worsening of the flood hazard for extreme events.

We expect that the aspect of sediment transport and potential adverse stream migration can be addressed with reasonable management efforts and modest refinements of design components and mitigation measures, such as land grading forms, levee protection, critical conveyance improvements and overflow erosion control, rather than with massive channels, groins, or other extreme measures.

SECTION III
PRECIPITATION

OVERVIEW

The South Boulder Creek hydrology study is concerned with flooding in Boulder from the perspective of peak flows and volume. Peak flows are dominated by rainfall in the area below Gross Reservoir, located approximately 18 miles upstream of South Boulder Creek's confluence with Boulder Creek. Since some of the solutions to potential flooding in Boulder might involve storage, the study is also concerned with runoff volume from the entire watershed. Therefore, models for the design storms use rainfall appropriate to locations above and below Gross Reservoir.

The watershed was divided by elevation ranges into rainfall zones. Data for each zone's rainfall were derived from NOAA statistics as described below. The four zones of the study were up to 6000 feet, (Zone 1); 6000 to 8000 feet (Zone 2); 8000 feet to 10000 feet (Zone 3); and 10000 to 12000 feet (Zone 4). Zone 2 was further divided into two sub-zones: below Gross Reservoir and above. The approximate percentages of the total watershed area taken by each zone are presented in the following table.

Table III-1
Watershed by Elevation Zone

Zone	Elevation Range	Percentage of Watershed
Zone 1	Up to 6000 feet	12.68
Zone 2 Below Gross	6000 to 8000 feet	18.64
Zone 2 Above Gross	6000 to 8000 feet	5.42
Zone 3	8000 to 10000 feet	43.78
Zone 4	Above 10000 feet	19.48

For 10-, 50-, 100-, and 500-year design storms for South Boulder Creek, the study used point rainfall statistics published by the National Oceanic and Atmospheric Administration (NOAA) in the *NOAA Atlas 2: Precipitation-Frequency Atlas of the Western United States, Volume III - Colorado*. The rainfall was then adjusted for Area Reduction Factors from the National Weather Service (NWS) Technical

Procedure No. 29 (TP 29), *Rainfall Intensity-Frequency Regime, Part 1 - The Ohio Valley*.

This study of area reduction factors was based on many large watershed rain gage networks in the Midwest, East Coast, and one network in California. While the relationships are reasonable and the best available as will be elaborated later, there are no proven relations in this region and the original study shows wide scatter. Also, while the large network was used for the 6 hour and 24 hour relations, the 1 hour relation is based on one network.

Design rainfall above Gross Reservoir is adjusted by Area Reduction Factors (ARF) based on the entire watershed area (135.7 square miles). Design rainfall below Gross Reservoir is adjusted based on the area downstream of the reservoir (42.5 square miles). The rainfall over the entire watershed using the ARF for the entire area was also calculated and subsequently used to further reduce the highest zone of rainfall. This procedure then resulted in having both the critical rainfall for peak flows below Gross in the lower watershed, and the correct total volume.

The resulting rainfall duration curve was rearranged by the commonly accepted practice of placing the peak value at one-third of the total rainfall duration or, for the twenty-four hour rainfall, at time eight hours. Less critical rainfall was rearranged in decreasing magnitude values around the peak time.

The end result is a rainfall pattern that is likely to be critical for the entire watershed and downstream of Gross. Realistically, this procedure may result in a 100-year flood that is slightly conservative, as in the real world each critical duration is not likely to have the same chance of occurrence. However, a study referred to us by NOAA does indicate that this region experiences a high likelihood of simultaneous critical durations (NOAA Technical Report NWS 27, *Interduration Precipitation Relations for Storms - Western United States*). Thus our opinion is that the rainfall events herein are realistic and reliable for purposes of flood hydrology, floodplain mapping, flood warning and proofing, and design flood control/facilities and waterway structures.

RAINFALL SPECIFICS

The following describes the specifics for determining the point rainfall, area reduction factors, adjusting the rainfall for the area reduction factors, and designating the rainfall event pattern.

Point Rainfall for the 10- to 100-Year Event

Point rainfall values for 360 minute and 1440 minute durations were determined from NOAA *Atlas 2* isopluvial maps at the centroid of each of the four elevation

zones. Sixty minute duration rainfall values for Zones 1 - 3 were taken from the *Boulder County Criteria Manual*, and are NOAA based. Values for 120 minute, 180 minute, and 720 minute durations were calculated from depth-duration diagrams in *NOAA Atlas 2*. For lesser duration values (5 minute, 15 minute, and 30 minute), adjustment factors found in *NOAA Atlas 2* for obtaining n-minute estimates from one-hour values were used.

Point Rainfall for the 500-Year Event

In order to determine a value for the 500-year rainfall, TEA extrapolated from NOAA's statistical rainfall data. The 15 minute, 30 minute, 60 minute, 120 minute, 360 minute, 720 minute, and 1440 minute data values were obtained. Four sets of data (using one of the time intervals, for example, the 30 minute interval, at 2, 10, 50, and 100 years) were each projected to the 500 year value, for each zone, by four methods:

- a) Taking logs of the four sets of x and y values, and using a regression analysis model to arrive at the 500 year value; the equation for the regression was in the form of $Y = \text{constant} + \text{constant} * \log X$
- b) Graphing the four sets of data on probability paper
- c) Graphing the four sets of data on Gumbel Distribution paper
- d) Graphing the four sets of data on Log Pearson III paper

Projected values for the 500 year rainfall determined by each method differed slightly. At the October 14, 1999 meeting, the sponsors concurred with the choice of the Log Pearson III values for the projections as it was noted that Log Pearson III is perhaps the most widely accepted procedure of the four methods used.

Application of Area Reduction Factors

Area reduction factors are a function of both duration and location. Data points for areas below and above Gross Reservoir were obtained directly from the depth/area curve of the *NOAA Atlas 2*. Point values for the 120 minute and 720 minute values were interpolated from the curve. The following table presents the key area reduction factors values used.

Table III-2
Area Reduction Factors vs. Duration

	30 minutes	60 minutes	120 minutes	360 minutes	1440 minutes
Below Gross Reservoir	0.73	0.83	0.873	0.937	0.950
Above Gross Reservoir	0.58	0.69	0.758	0.873	0.927

We attempted to apply equal ARF increments for given duration ranges to rainfall data points. This produced questionable results with a flat, blocky pattern. Reasoning that both rainfall data and area reduction factors are points on smooth curves, we found mathematical functions which fit the rainfall data and area reduction factors. Since the area reduction factors never go to zero, we estimated the curve intercepts for zero or infinitesimally small areas to determine the best curve fit. The function for the area reduction factor above Gross Reservoir is:

$$ARF_a = 0.38 + 0.5630 * T / (52.65 + T), \quad \text{III-1}$$

where T is the time in minutes;

the function for the area reduction factor below Gross Reservoir is:

$$ARF_b = 0.35 + 0.6104 * T / (17.67 + T) \quad \text{III-2}$$

For curve fitting the rainfall data P, precipitation in inches, the resulting mathematical equations are in the form of an equation for a hyperbola. Equations found for rainfall in each of the zones are:

$$\text{Zone 1: } P = 3.249 * T / (17.06 + T) + 3.568 * T / (1424 + T) \quad \text{III-3}$$

$$\text{Zone 2: } P = 2.834 * T / (15.27 + T) + 7.053 * T / (4171 + T) \quad \text{III-4}$$

$$\text{Zone 3: } P = 2.395 * T / (14.65 + T) + 4.504 * T / (1725 + T) \quad \text{III-5}$$

$$\text{Zone 4: } R = 2.161 * T / (16.30 + T) + 3.227 * T / (1716 + T) \quad \text{III-6}$$

Graphs illustrating example area reduction factor and rainfall curve fits are found in Figure III-1 and Figure III-2. The graphs illustrate curves in Zone 1. A greater difference between NOAA original rainfall points and the TEA design storm values was observed for higher elevation zones, which have larger area reduction factors.

Temporal Arrangement (Event Rainfall Patterns)

TEA maintained the statistical integrity of NOAA rainfall data in simulations of the various storms by embedding the values for all rainfall events (e.g., 15 minute, 30 minute, etc.) in the 24-hour storm. TEA chose the six-hour rainfall as the critical event in the watershed's 24-hour storm, and placed its peak at eight hours. Typically, hydrology texts (e.g., Viessman, Knapp, Lewis, and Harbaugh, *Introduction to Hydrology*, and Bedient and Huber, *Hydrology and Floodplain Analysis*) specify putting the storm's peak at a point between $\frac{1}{3}$ to $\frac{1}{2}$ of the storm's duration.

TEA created a spreadsheet which, once mathematical functions for rainfall and Area Reduction Factors were found, produced corrected rainfall values for each of 288 five-minute increments in the 24 hour period for each rainfall Zone, for each of the 10-, 50-, 100-, and 500-year storms. The spreadsheet was designed to include algorithms which would:

- create Area Reduction Factors and rainfall values, once the curve functions were entered into the spreadsheet, for each five-minute increment
- multiply Area Reduction Factors and rainfall values to produce TEA corrected rainfall for each five-minute increment
- subtract earlier from adjacent later values to determine the incremental increase of rainfall per five-minute interval
- rearrange each of the 288 incremental rainfall values in ascending order with peak at eight hours
- check to verify that NOAA statistics were maintained at all time periods in the storm, from 15 minutes to 24 hours (e.g., 2 hours, 3 hours, etc.)

The resultant design rainfalls are tabulated in the model input. The 100-year rainfall for Zone 1 is shown in Figure III-3. Note that the curve represents a series of five minute incremental values with each increment beginning at the end of the preceding five minute value.

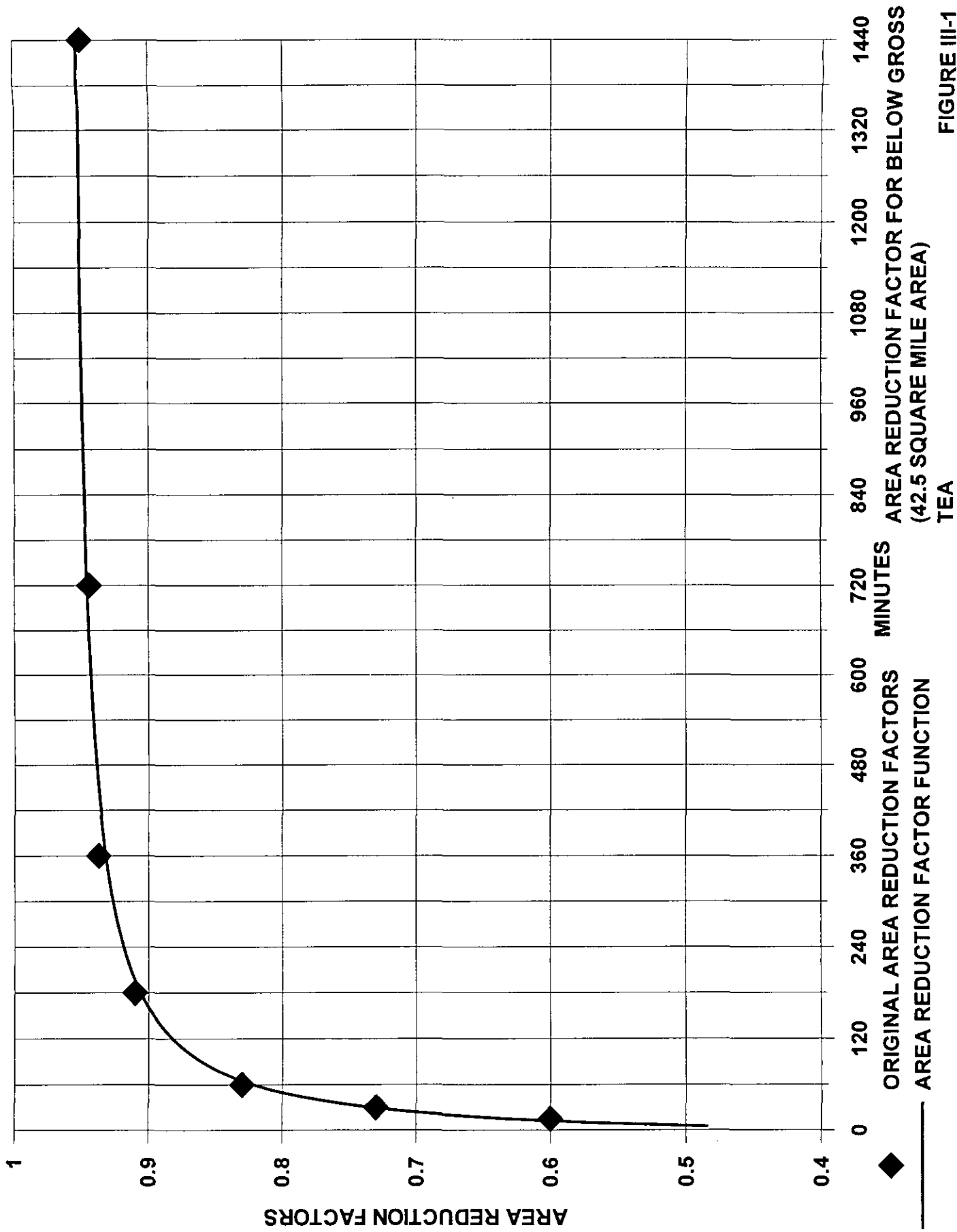
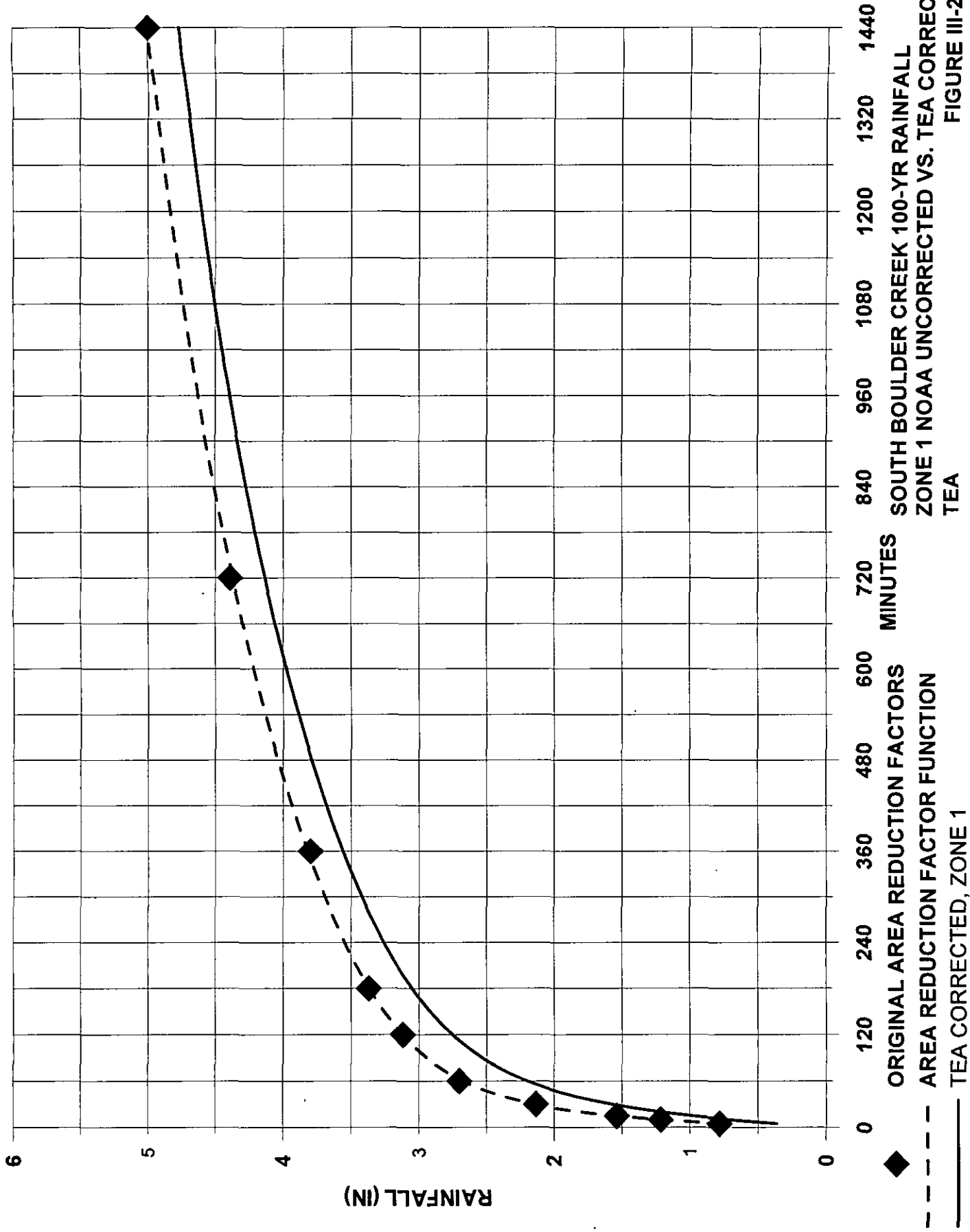


FIGURE III-1



SOUTH BOULDER CREEK 100-YR RAINFALL
 ZONE 1 NOAA UNCORRECTED VS. TEA CORRECTED
 TEA

FIGURE III-2

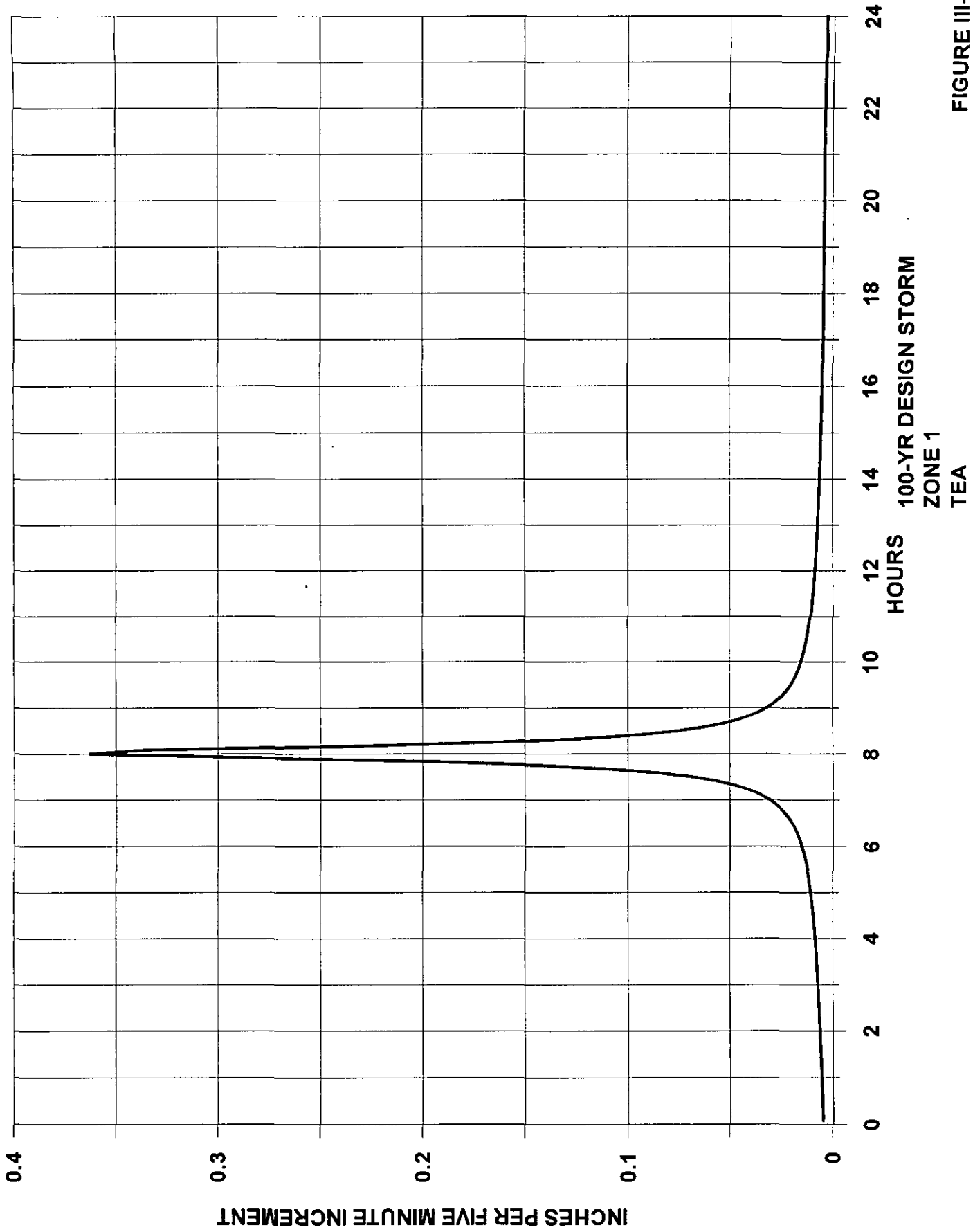


FIGURE III-3

Comparison

In a comparison of UDFCD, Corps, and TEA design storms for South Boulder Creek, TEA found that Corps rainfall was significantly lower. The Urban Drainage storm had the highest peak rainfall, possibly since the 15 minute Area Reduction Factor for that storm was devised in a more approximate manner. For Zone 1, TEA's design rainfalls compared to those of the Corps are as follows: thirty minute (1.56 vs. 1.38 inches), one hour (2.24 vs. 1.73 inches), two hour (2.72 vs. 2.38 inches), and three hour durations (3.56 vs. 3.47 inches). Other than the peak values, the TEA values compare well with UDFCD/Boulder criteria.

AGENCY REVIEW

Please refer to Section VII for copies of the correspondence.

Henz Meteorological Services

On July 22 1999, TEA outlined its anticipated procedures for simulating rainfall volumes in a letter to Bill DeGroot of UDFCD. Bill DeGroot then forwarded the letter to John Henz of Henz Meteorological Services for his comments. The approach and details of determining design event precipitation were reviewed by Henz Meteorological Services. John Henz responded that the "basic premise" of the TEA approach "appears valid." He also recommended consideration of recent specific storms from July 8, 1998 and August 4, 1999 for possible modeling, discussed aerial and temporal distributions typically found in the watershed, and mentioned the importance of considering antecedent moisture conditions

Some sponsors felt that, considering John Henz's experience in observing area storm patterns, there would be valuable information added to the study by having him construct a design storm. All sponsors did not, however, commit to this additional expenditure. The sponsors concurred with the concept of using classical, well-established hydrology procedures, which have widespread acceptance and are defensible.

National Weather Service

Early in August 1999, TEA wrote to the National Weather Service (NWS) requesting advice about area reduction factors, NOAA rainfall data, storm peak placement and rainfall distribution, embedded NOAA events nested within the critical event, etc. When information was not forthcoming, TEA wrote again on September 9. The NWS response, emailed on September 29, included the following:

- NWS thought the approach of using one Area Reduction Factor for all values in each storm area "reasonable...based on local knowledge and professional judgment."
- NWS agreed that the TEA approach of using a 24-hour design event to assure that the entire watershed was responding was "reasonable."
- NWS suggested NOAA Technical Memorandum NWS Hydro 40, *Depth-Area Ratios in the Semi-Arid Southwest United States* (Zehr and Myers, 1984) in response to questions about the appropriateness of using TP 29 Area Reduction Factor curves in Colorado.
- NWS suggested NOAA Technical Report NWS 27, *Interduration Precipitation Relations for Storms - Western United States* (Frederick, Miller, Richards, and Schwerdt, 1981) for TEA concerns regarding temporal distribution.
- NWS suggested *Flood Hydrology Manual*, U.S. Department of the Interior, Bureau of Reclamation (1992) for questions concerning the aerial distribution of rainfall across subbasins in the larger basin.

Depth-Area Ratios in the Semi-Arid Southwest United States, NWS Hydro 40, used data from a network of concentrated gages in Walnut Gulch, Arizona to extrapolate Area Reduction Factors for areas throughout Arizona and in New Mexico. The authors commented that, as distance from the concentrated gages increased, they felt less confident of the values presented.

TEA contacted Raymond Zehr, one of the authors of NWS Hydro 40. Mr. Zehr, who has worked in Fort Collins for approximately 15 years, said that he would not recommend the use of the NWS Hydro 40 Area Reduction Factor procedures for a study of South Boulder Creek hydrology. He noted that his study area (Walnut Gulch, in southeast Arizona) and the South Boulder Creek watershed were both "dry," but similarity between the two areas was not apparent beyond that.

TEA noted a problem in NWS Hydro 40, in that the 100-year Area Reduction Factors did not change with the storm duration, that is, Area Reduction Factors clustered at the approximately 0.58 - 0.60 point for all 100-year values, regardless of rainfall duration. The Bureau of Reclamation, Mr. Zehr thought, was working with Area Reduction Factors for the Colorado Front Range and recommended an individual at the Bureau of Reclamation to contact for information. However the sponsors directed that we not pursue this further as the Bureau's work was more likely related to extreme events and under study.

The TP 27 report deals principally with accumulated probability (joint probability) for various duration rainfall events within or around critical duration storms. An earlier study, NOAA Technical Report NWS 21, *Interduration Precipitation Relations for Storms - Southeast States* (Frederick, 1979), more clearly explains the procedure for using the probability charts in both studies. TEA created tables of values produced by this method, and found some values unrealistically large. TEA also found that NOAA Atlas statistical values were not maintained. TEA noted a flaw in the study's definition of a storm's starting point: as TP 27 defines the storm's beginning point, important, adjacent storms separated by a few hours can be overlooked. Henz specifically suggested that this type of pattern (two rainfall peaks separated by a no rain period) is critical to this region. The NWS analysis would have missed this type of event.

Table III-3, from the TP 27 report, illustrates the probability that critical hour events will occur together. This table is read as follows, assuming that the six hour duration (the independent, ID, factor for the storm) is the most critical for the area below Gross. Thus for this critical independent duration (ID = six hour), the percent of simultaneous occurrence of the 100-year, one hour, two hour, three hour, twelve hour, and 24 hour duration rainfalls would be, respectively, 57.6, 70.9, 78.3, 80.7, and 64.3 percent. We believe the percent of simultaneous occurrences would be even higher if the analysis technique had included two part storms as suggested by Henz. The percentages of simultaneous occurrences are high enough to well justify the approach herein.

TABLE III-3

PERCENT OF CONCURRENT STORMS AND RAINFALLS OF QUARTILE I
FOR THE FRONT FACE ROCKIES (SOUTH)
(NWS 27)

DD Dependent Duration (Hr)	ID INDEPENDENT DURATION (HR)					
	1	2	3	6	12	24
1		74.4	67.8	57.6	47.6	39.4
2	75.4		87.2	70.9	57.8	47.0
3	68.9	88.0		78.3	64.1	53.1
6	58.5	72.8	80.2		79.3	62.8
12	49.3	59.6	65.7	80.7		74.6
24	40.9	49.1	54.4	64.3	76.3	

TEA contacted Frank Richards, one of the authors of TP 27, on October 12. Mr. Richards stated that the studies had been done for the Soil Conservation Service (SCS), which hoped to find improved methods for constructing design storms. Authors of the reports conducted an additional study for SCS; this study described a problem in the dependence on choices presented to users of the procedure. With each decision/choice came the opportunity to take many divergent paths, and taking even a slightly different path could produce widely varying results. Mr. Richards regards the study as an "academic exercise"; SCS never adopted the procedure.

At the October 14, 1999 meeting, the sponsors directed the following:

- The NWS 40 and TP 27 procedures were not to be used.
- The Bureau of Reclamation would not be consulted further about the Area Reduction Factors which it may use in dam investigation.
- SCS (now NRCS, the National Resource Conservation Service) would not be consulted about its design storm patterns.
- The Bureau of Reclamation's *Flood Hydrology Manual* procedures would be followed, serving to reduce (i.e., make more realistic) the volume of rainfall produced by the upper basin (Zone 4) so that the total rainfall volume over the entire watershed was correct.

With respect to the last item above, the rainfall produced in TEA's spreadsheets for each design storm in Zone 4 was reduced further by approximately 0.93 percent to make sure the entire basin rainfall volume was correct.

May 1969 STORM

In an attempt to calibrate the rainfall/runoff model, the South Boulder Creek hydrology study included investigation of available rainfall data for the May 4 - May 8, 1969 storm. Unfortunately, 5 to 15 minute rainfall gage data were not recorded in the watershed. Hourly data were available from the Gross Reservoir recording station. Daily rainfall records were reported by a network of citizens in the basin for the May 1969 storm.

Hourly and more frequent rainfall values for the storm were available from a series of gages located at varying distances north and south of the South Boulder Creek basin boundary. TEA graphed data from the northern gages (Boulder 2, A1, B1, C1, and D4) to determine whether a pattern of the May 1969 storm peak's movement existed. Through an overlay of the graphs of the northern rainfall gage

data, the pattern of a moving storm became apparent. However, the southern gage data did not provide a similar pattern.

The Bureau of Reclamation provided TEA a copy of its isopluvial map for the May 1969 storm; TEA questioned the triangulated irregular network (TIN) mapping of the rainfall data, and realized that other isopluvial patterns could be constructed from the limited data available. Other TIN interpretations of the same data could produce different isopluvial patterns; thus a wide range of modeling results could occur. Therefore, it appeared unreasonable to simply transfer gage data from outside the watershed directly into a runoff model of South Boulder Creek.

At an October 6, 1999 meeting held to discuss, among other things, difficulties in obtaining 1969 storm data, John Henz (Henz Meteorological Services) indicated they could probably construct input data for the 1969 storm. Project sponsors agreed at an October 14, 1999 meeting that, because of problems with obtaining data for the May 4 - May 8, 1969 storm (e.g., lack of rain gages in the basin, additional effort involved in an attempt to fit data outside the basin to theoretical values for the storm in the South Boulder Creek watershed), TEA should not spend additional hours assembling data in an attempt to simulate the 1969 storm. The sponsors concurred with the plan to verify responses of selected individual subbasins in the UDSWMM model by the comparison to UDFCD's CUHP model for those subbasins.

SECTION IV

SURFACE RUNOFF

INTRODUCTION

This section summarizes:

- Pervious Surface Infiltration
- Pervious and Impervious Surface Depression (or Detention Losses)
- Land runoff, overland flow length, slope, and hydraulic flow resistance

INFILTRATION

The only comprehensive source of land surface condition and infiltration characteristics is soils mapping inventories by the National Resource Conservation Service (NRCS or SCS herein) and the United States Forest Service (USFS), which uses NRCS methodologies. For this study, maps for the watershed were obtained from both of these agencies.

For each of the subbasins the various soil types were identified by name on the maps, and then the soil infiltration classification(s) were assigned (A - low runoff potential—through D - high runoff potential). Other land surface conditions were observed on the aerial mapping and from field work in the lower watershed below Eldorado Springs. These conditions include vegetative cover and type, how much of the area was disturbed by development, and other factors that might discourage or encourage infiltration. This analysis is presented in the separate technical appendix in more detail for the subbasins. Based on the interpretive guidelines of NRCS, Runoff Curve Numbers (RCN) were selected for each basin.

In order to limit the number of infiltration combinations, it was determined that six to eight representative RCN categories would be allowed and the final RCN for each basin selected from these available choices. Subsequently, an analysis of comparable Horton's infiltration parameters was conducted to assure that infiltration amounts at the peak of the event and for the twenty-four hour rainfall were approximately equivalent to NRCS methodology.

Curve Numbers

Some subbasins contained two or more soil groups and, in those cases, if one soil category clearly dominated in the subbasin (for example, if the predominant soil group was estimated to cover 75% of the area), the dominant soil category was

used as the average soil type. If the areas covered by soil types in the subbasin were roughly equal, the soil category for the subbasin was designated as, e.g., "½ C, ½ D." In all cases where the subbasin soil group area was insignificant, that group was not included in the Curve Number tabulation.

Specific Curve Numbers for the subbasins were determined without considering the percent impervious areas. UDSWMM uses separate parameters for the basin's percentages of pervious and impervious land use coverages. The value range for good and poor ground cover, used in determining the Curve Number for each subbasin, was taken from the NRCS reference.

Ground cover or land use treatment was estimated in some subbasins by noting the percentage of the basin which had either southern, or northern, exposure. It was assumed that northern exposures generally indicate good ground cover (heavy forest and understory), and consequently those subbasins have a lower Curve Number, or less runoff from precipitation. Correspondingly, a southern exposure indicates a more moderate ground cover (grasses, lighter density trees, and brush), and a subbasin with southern exposure can be assumed to have more runoff than would the same soil type in a location with northern exposure.

For example, in the South Draw area, which has northern exposure, knowledge of the area confirmed this pattern. Groundwater monitoring wells indicate that the area is highly infiltrative. Curve Numbers in that area are in the low 60's, reflecting the infiltrative soils/geology of the area.

Also, there are areas with infiltration patterns of special interest. Some subbasins have a large extent of exposed rock and poor ground cover. For those areas, Curve Numbers appropriate for poor ground cover conditions were used. The ground cover along the South Boulder Creek floodplain (predominantly cottonwood trees) is conducive to infiltration. Elevations in certain areas in the watershed reach above the tree line, and in those areas where it was assumed that a subbasin's elevations would noticeably affect the percentage of tree cover, a slightly higher Curve Number was used.

Table IV-1 indicates typical ground cover that might be expected for the six Curve Number groups used in the model.

Table IV-1

Representative SCS Curve Number, Soil Types and Land Condition

Curve Number	Typical Soil Type, Land Use, and Ground Cover
45	A type soil, pasture or range land, good condition A type soil, open spaces (lawns, parks, golf courses) A or B type soil, with heavily forested areas
55	A, B, or A/B type soil in urban settings with good cover A or B type soil, with exceptionally good vegetative cover B type soil in forests, with good cover and northern exposure
60	A or B type soil, with moderately good vegetation - if in mountains or foothills northern exposure B type soil in meadow with good cover
65	B type soil in pasture or range land, with good cover B/C type soil with moderately good cover B type soil in open space with good cover B type soil with moderately good vegetative land cover - possibly urban setting with good lawn cover
70	C type soil, in mountains with general northern exposure and good cover C type soil, urban space with fair to good vegetation C type soil, urban setting with dirt roads
78	D type soil, or C and D type soil mix, with southern exposure - also poor ground cover C or D soil in urban setting open space (lawns, parks) with good or fair cover

Determination of Horton's Parameters

Horton's equation is not similar to the NRCS runoff equation, a standard for determining rainfall runoff. Horton's equation uses a soil's initial and final infiltration rates and a constant for the rate of decrease from the initial capacity. The Horton equation is a function of elapsed time from the start of the event. Because the time to the peak of the rainfall is much longer for the South Boulder Creek design storm than the normal UDFCD/Boulder criteria two or three hour event, the decay

rates have to be changed from the normal UDFCD/Boulder standards. The NRCS Curve Number estimates runoff by an algorithm that uses cumulative precipitation in the design event.

Horton's parameters that would reasonably simulate the eight hour and twenty-four hour infiltration were determined which would approximate results obtained with the NRCS Curve Number approach. In an iterative process, matching curves for the two approaches to infiltration were constructed, using the rainfall spreadsheets described in Section III. The Horton's parameters determined are presented in Table IV-2 for the South Boulder Creek UDSWMM model using a twenty-four hour design storm with the peak at eight hours. Figures IV-1 through IV-6 present the graphical comparison of the cumulative infiltration for Zone 1.

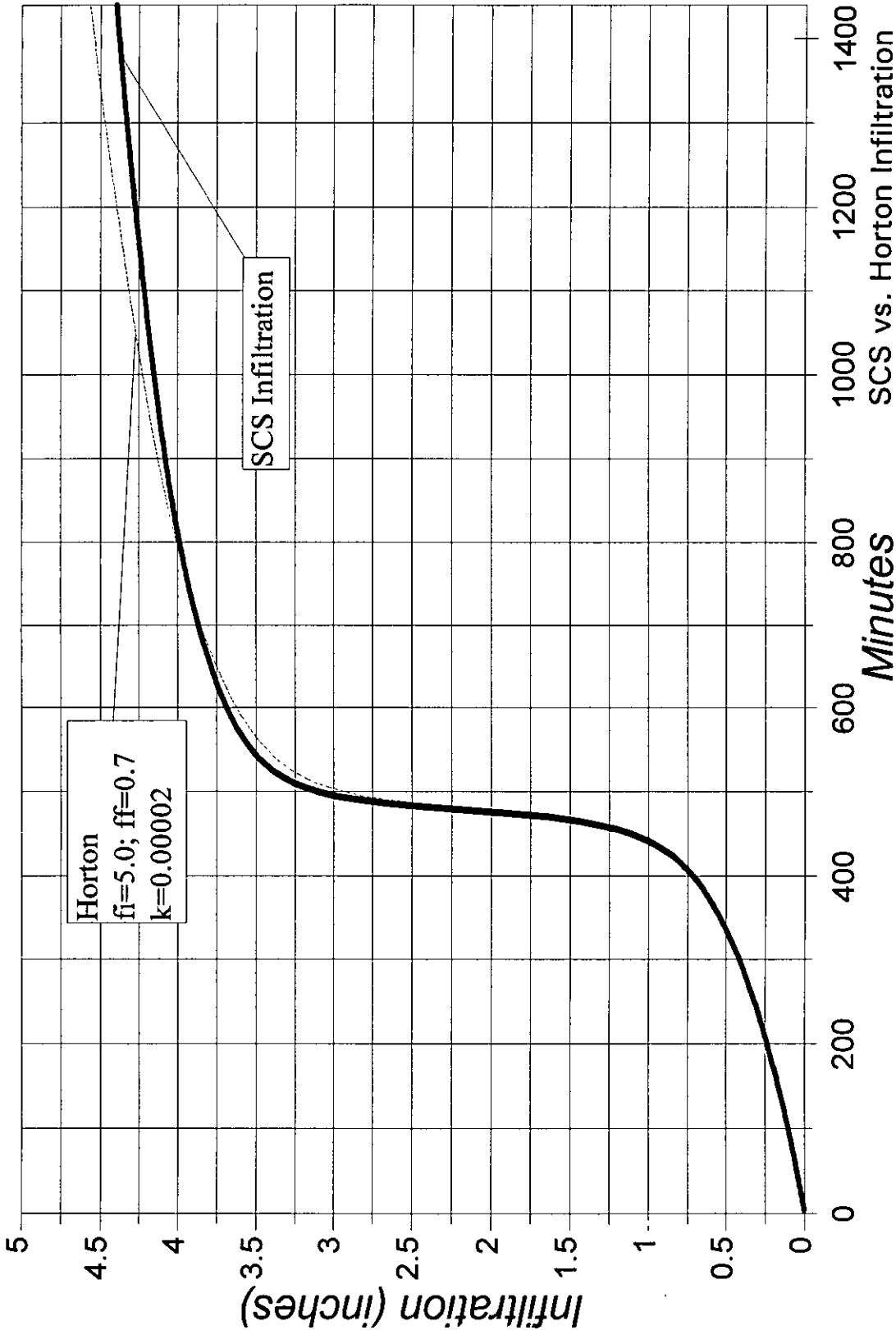
Table IV-2
SCS Curve Number and Comparable Horton's Infiltration Parameters
for South Boulder Creek 24 Hour Precipitation

SCS Curve Number	HORTON		
	Initial Infiltration Rate, f_i	Horton's Infiltration Rate, f_r	k , the Rate of Decrease
45	5.0	0.7	0.00002
55	5.0	0.6	0.000055
60	4.8	0.5	0.0001
65	4.5	0.6	0.0001
70	3.9	0.5	0.00024
78	3.5	0.2	0.001

IMPERVIOUS LAND SURFACES

Vast exposed rock areas or urbanized areas with streets, buildings, and parking lots are two examples of impervious surfaces.

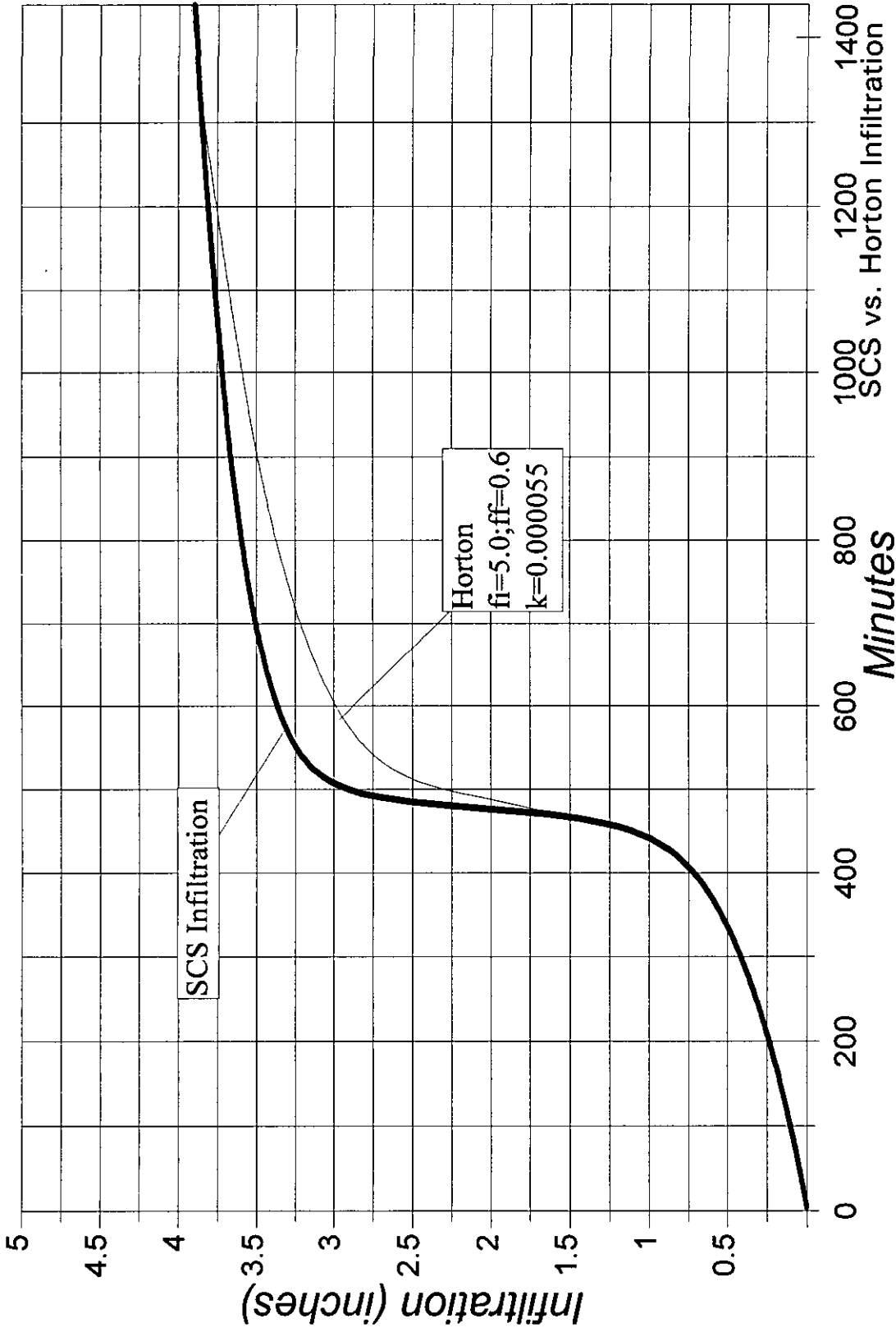
Percent imperviousness of the basin is another parameter in UDSWMM.



Horton
 $f_i=5.0$; $f_f=0.7$
 $k=0.00002$

SCS Infiltration

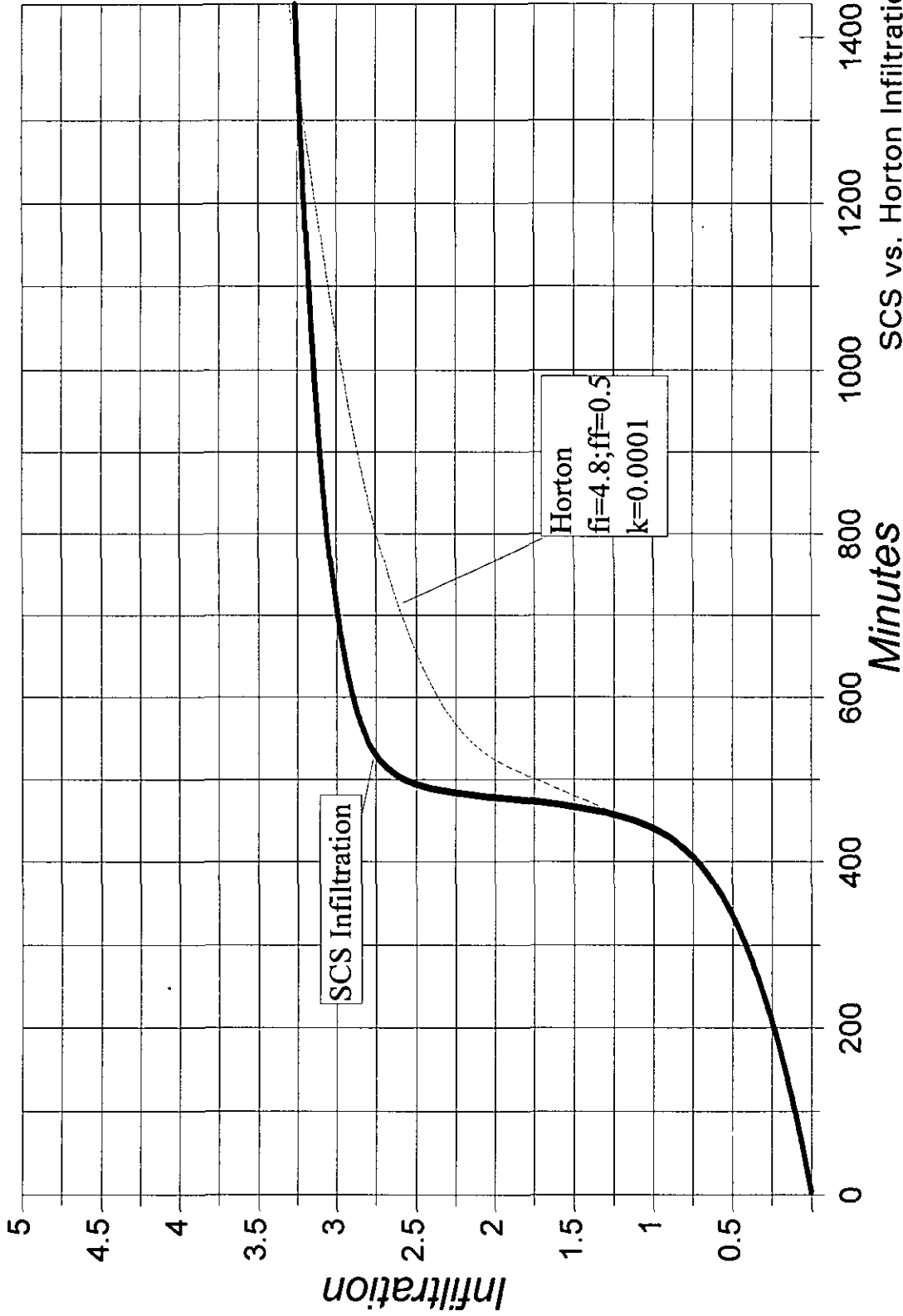
SCS vs. Horton Infiltration
 Zone 1, 100 Year,
 Cumulative, CN = 45
 TEA Figure IV-1



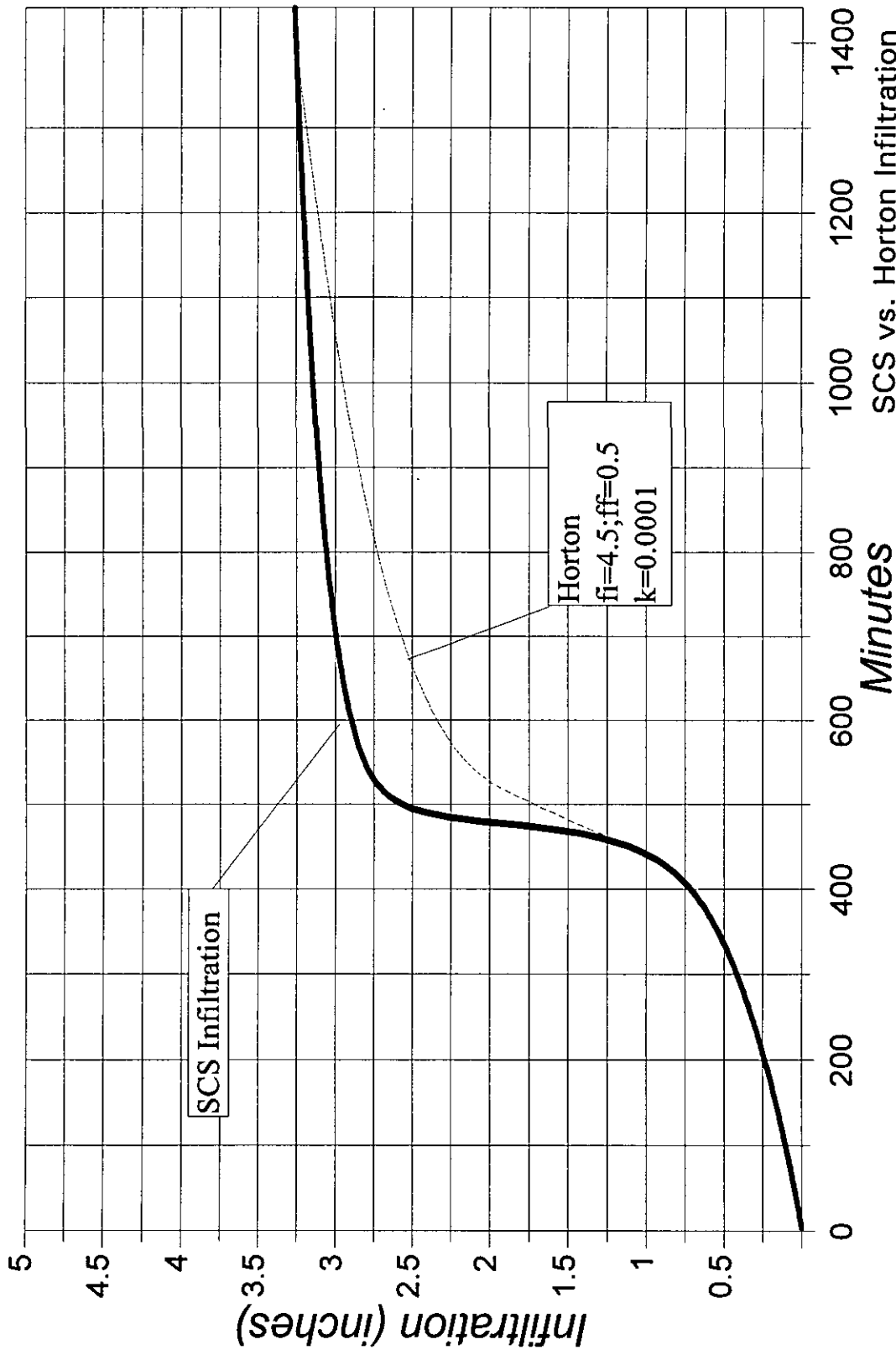
Horton
 $f_i=5.0; f_f=0.6$
 $k=0.000055$

SCS Infiltration

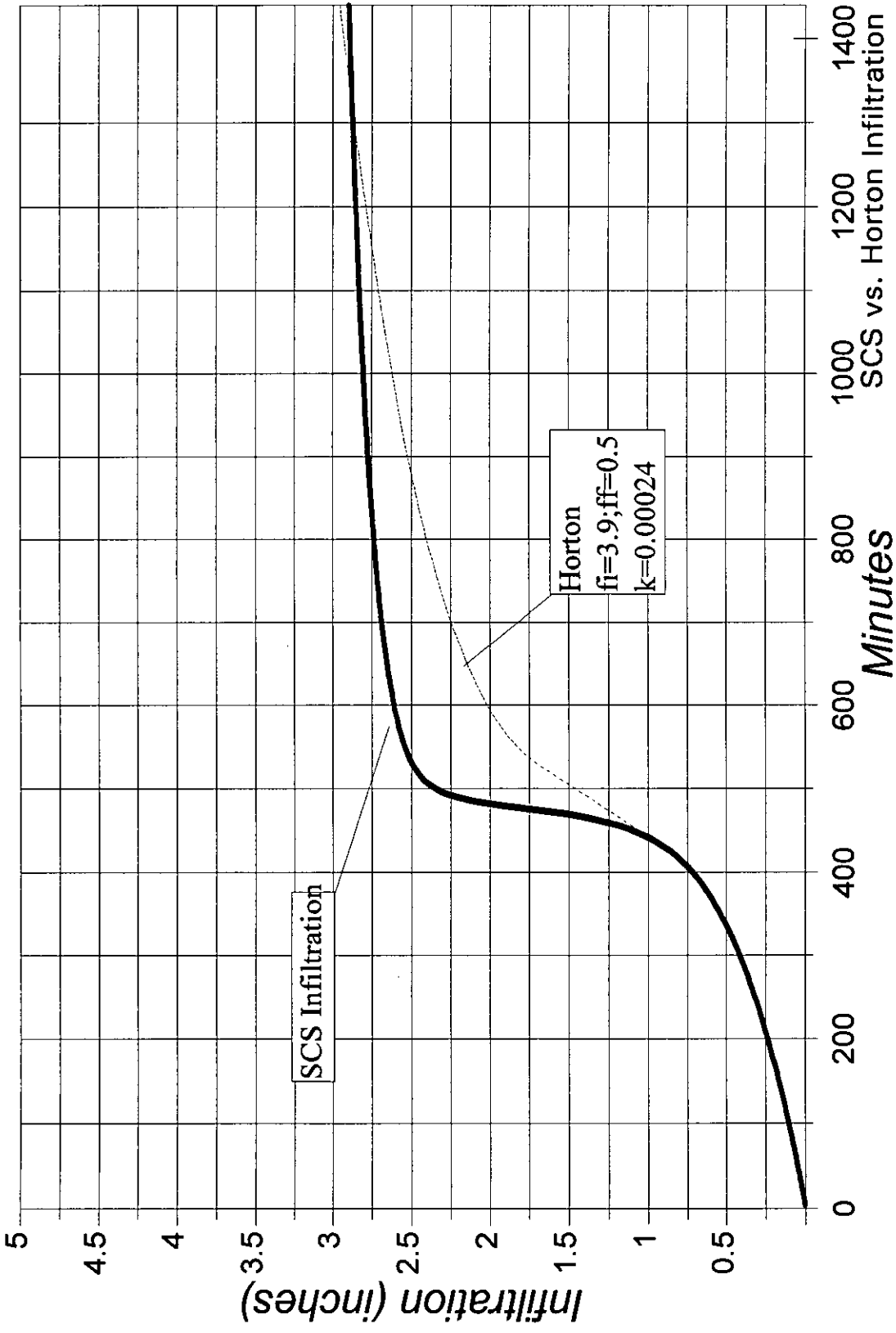
1000 1200 1400
 SCS vs. Horton Infiltration
 Zone = 1, 100 Year,
 Cumulative, CN = 55
 TEA Figure IV-2



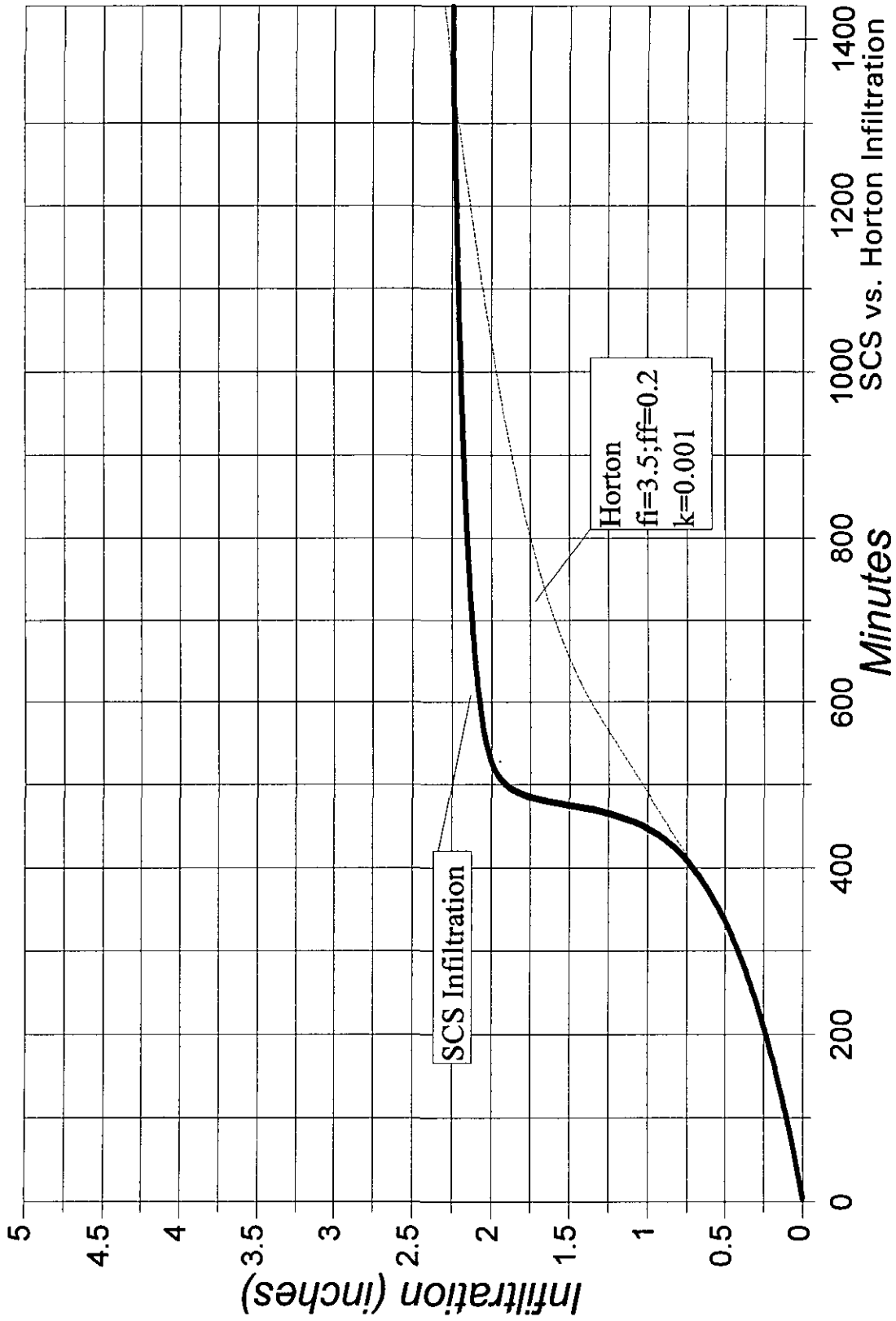
SCS vs. Horton Infiltration
 Zone 1, 100 Year,
 Cumulative, CN = 60
 TEA Figure IV-3



SCS vs. Horton Infiltration
 Zone 1, 100 Year,
 Cumulative, CN = 65
 TEA Figure IV-4



1000 1200 1400
 SCS vs. Horton Infiltration
 Zone 1, 100 Year,
 Cumulative, CN = 70
 TEA Figure IV-5



SCS vs. Horton Infiltration
 Zone = 1, 100 Year,
 Cumulative, CN = 78
 TEA Figure IV-6

In mountainous areas where large expanses of exposed rock can be seen in the SCS soils book aerial photographs, or when other sources indicate large rock outcroppings, the percent impervious factor used in the model ranged up to thirty percent. In mountainous areas without large expanses of exposed rock, the percent impervious area used in the model ranged from five to eight percent. If a mountain subbasin had been developed, its impervious factor ranged from ten or twelve to twenty-five percent

UDFCD/Boulder standard guidelines were used in urban areas. Direct experience with the lower watershed was used to identify the land uses and thus the impervious percentages per the guidelines.

DEPRESSION LOSSES

Depression losses are caused by rainfall lost to wetting impervious surfaces and holes or other features that trap runoff and prevent it from contributing to surface streams. The typical range of UDFCD/Boulder values are used in the model with two exceptions. In the mountains, particularly in Eldorado Canyon and at the Continental Divide, there are large expanses of exposed rock, or essentially impervious surfaces. The NRCS soils maps also identify these areas in Eldorado Canyon. Values of 0.3 inches depression loss were used to reflect that these surfaces are rough, irregular, and have adjacent talus slopes that hold runoff. Also in areas with mountain roadways, higher depression losses were used to reflect the rougher roads and impervious surfaces.

SURFACE RUNOFF HYDRAULIC PARAMETERS

Roughness parameters for the hydraulics of the shallow surface runoff over the various sources were determined using experience, UDFCD/Boulder guidelines, and review of references (HEC-1, Harley, Taggart).

The only exception to UDFCD guidelines is with respect to roughness of paved surfaces. A value in the UDFCD Criteria has been designated which is really for shallow stream flow, and is not appropriate for shallow overland flow. Values of 0.15 to 0.3 in the model have been used for shallow overland flow depending on whether the impervious surfaces are urban roads or rougher mountain roads.

OVERLAND FLOW LENGTHS AND SLOPES

Generally overland flow lengths of 100 to 500 feet have been used in urban areas, and 800 to 2000 feet in rural areas. The overland flow lengths were determined by reviewing the dominating or typical overland flow lengths in a given basin. Significantly longer lengths were generally not allowed, as it is difficult for runoff to travel further than this and not become stream flow.

In SWMM the "W" parameter was determined or checked by dividing the basin area by the overland flow length. This procedure has been verified in discussions with SWMM programmers and by experience with numerous other UDFCD and private drainage projects.

The slopes are determined based on the mapping, but adjusted downward to remove the various instantaneous drops that invariably occur.

OVERALL RESULTS

The UDSWMM model herein indicates that over the entire watershed for the 24 hour 100-year event there would be about 4 inches of precipitation and 1 inch of effective runoff.

SECTION V

HYDROLOGY MODEL

MODEL OVERVIEW

Drawings 1 through 11 (at the end of this report) illustrate both the watershed and the UDSWMM Hydrology Models. Key elements include:

- Basins, where the rainfall runoff process is simulated.
- Streams, which route the runoff down the tributary and main streams. In some cases simple trapezoids are used with appropriate geometry, slope, and roughness characteristics that will result in velocity and cross section areas that are perceived as representative. In larger channels, two stream elements are used where the low flows are carried in a smaller channel, and overflows in a wider and often rougher channel. The combination is intended to simulate the velocities and cross sections of the real channel.
- Nodes, which provide a variety of functions: receiving runoff, receiving stream elements, combining streams or other nodes and receiving flow splits.
- Flow splits, where flows are divided between two paths. Typically the discharge end goes to the downstream route which receives the initial or low flow. The split typically goes to the overflow route. Simple nodes are used on the upstream, downstream, and split side of the node to monitor accurate performance and avoid UDSWMM timing problems.
- Storages, which receive, store, and route hydrographs arriving at a given location.

Table I-1 presents a comparative summary of the model results with the previous Corps' model and the flows in the G & O Flood Hazard Area Delineation (FHAD). All input parameters and detail model peak flow results are presented in Appendix A.

LIMITATIONS

- The UDSWMM land runoff router flow algorithm uses "Linear Reservoir routing." It is not Kinematic Wave routing where lateral land surface runoff inflows continually to the stream. In UDSWMM the runoff flow for an entire subbasin either misses the stream routing or all of the runoff goes through the entire stream, instead of gradually entering along the stream. However, either Kinematic Wave or Linear Reservoir routing is well suited to simulation of mountain stream hydrology.

- This version of UDSWMM was apparently adopted to limit variances among modelers but there are problems:
 - No graphics output.
 - Numerically unstable at times and has difficulty linking numerous elements, particularly flow splits.
 - Very limited stream flow routing with only trapezoids, rectangular, triangular, and circular sections that don't depict natural sections and only lag hydrographs rather than actual dynamic routing. Floodplain sections are simulated poorly, where the combination channels can't possibly simulate the hydraulics that occur. Combination channels can cause flow acceleration, as documented in the work herein.
 - One dated infiltration method.
 - Comment cards cannot be added where needed in the input.

- The Colorado Unit Hydrograph Procedure (CUHP) has a statistical basis in its derivation of parameters and thus can be used as a limited reasonableness test for similar watersheds. However, many of the subbasins in Boulder Creek are out of the application range of CUHP.

STREAM FLOW MODELING

Two types of stream dominate the model. The first is a simple trapezoidal channel which is used to simulate the simpler and small discharge mountain tributaries. The second is a compound section which has a low flow channel and a separate overflow channel. This second type is used along the larger tributaries, tributaries where there is a low flow stream with a wider overbank, and along South Boulder Creek and the West Valley Overflow. In a few cases the low flow segment is simulated by a pipe.

In most cases, the section roughness is increased over "normal" stream roughness parameters to account for other energy losses that occur, such as contraction, expansion, and hydraulic jumps. Also the stream slopes selected are typically flatter than the average stream slope to simulate the dominant slope and thus velocity that the water will travel. In some cases HEC-2 models were available, which were used to adjust the parameters selected.

In the mountains, the information was largely taken from the USGS electronic maps, and very limited field work. In the foothills and lower South Boulder Creek areas, the much more detailed City and County topographic mapping was used as a base along with field observations and limited surveys, largely using a hand level.

In previous phases of the work, surveys have been recommended, typically to enhance flow split, control structure, and representative stream sections. However

these efforts have been deferred for consideration during scoping of possible subsequent studies, such as floodplain mapping.

REPRESENTATIVE 100-YEAR FLOOD HYDROGRAPHS

Gross Reservoir

Gross Reservoir, even assuming the beginning water surface is level to the crest of the dam, still significantly attenuates the flow as shown in Figure V-1. Approximately 1784 acre feet is stored.

Upstream Highway 93 to South Boulder Creek at Confluence with Boulder Creek

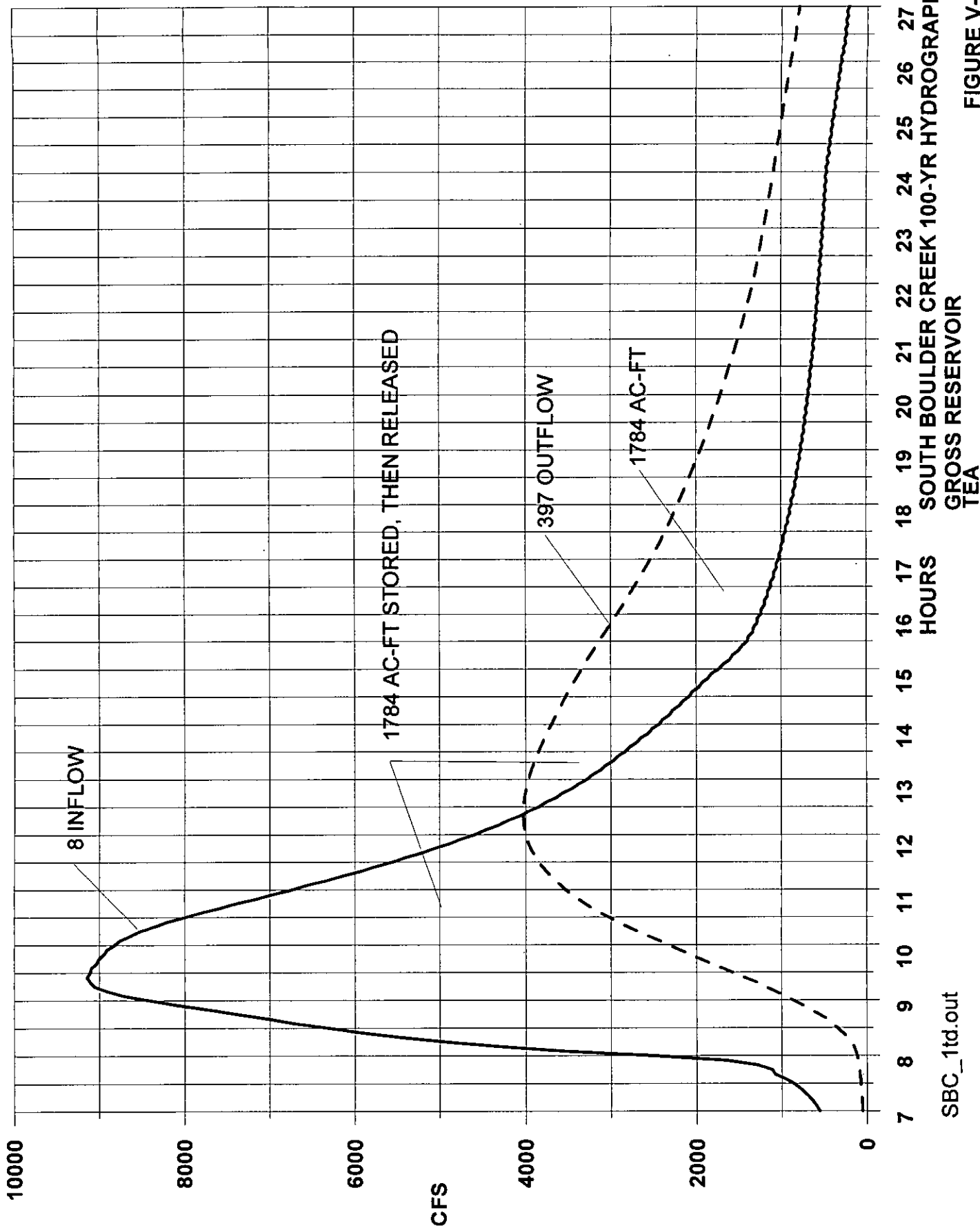
Figure V-2 compares South Boulder Creek flows at the Eldorado Gage, upstream of the split at Highway 93, and the direct discharge to Boulder Creek from the main South Boulder Channel. The upstream hydrographs show the spiky peak from Eldorado Canyon, and the delayed overflow of Gross. The discharge to Boulder Creek is missing a significant portion of West Valley spill to the west of 55th to Bear Canyon Creek and Boulder Creek and Valmont. Thus the total watershed discharge is really over 7500 cfs. The lower hydrograph shows the first peak from local drainage, the base of the upstream flood hydrograph carried from the main channel at Arapahoe (3000 cfs) and the overflow peak being routed through the West Valley Overflow through the golf course.

South Boulder Creek at Highway 93

As a result of two splits from South Boulder Creek upstream of Highway 93, only the hydrograph 1509 in Figure V-3 is left flowing under the bridge while the overflow spill hydrograph, plus additional local runoff (hydrograph 1533), goes to the West Valley Overflow.

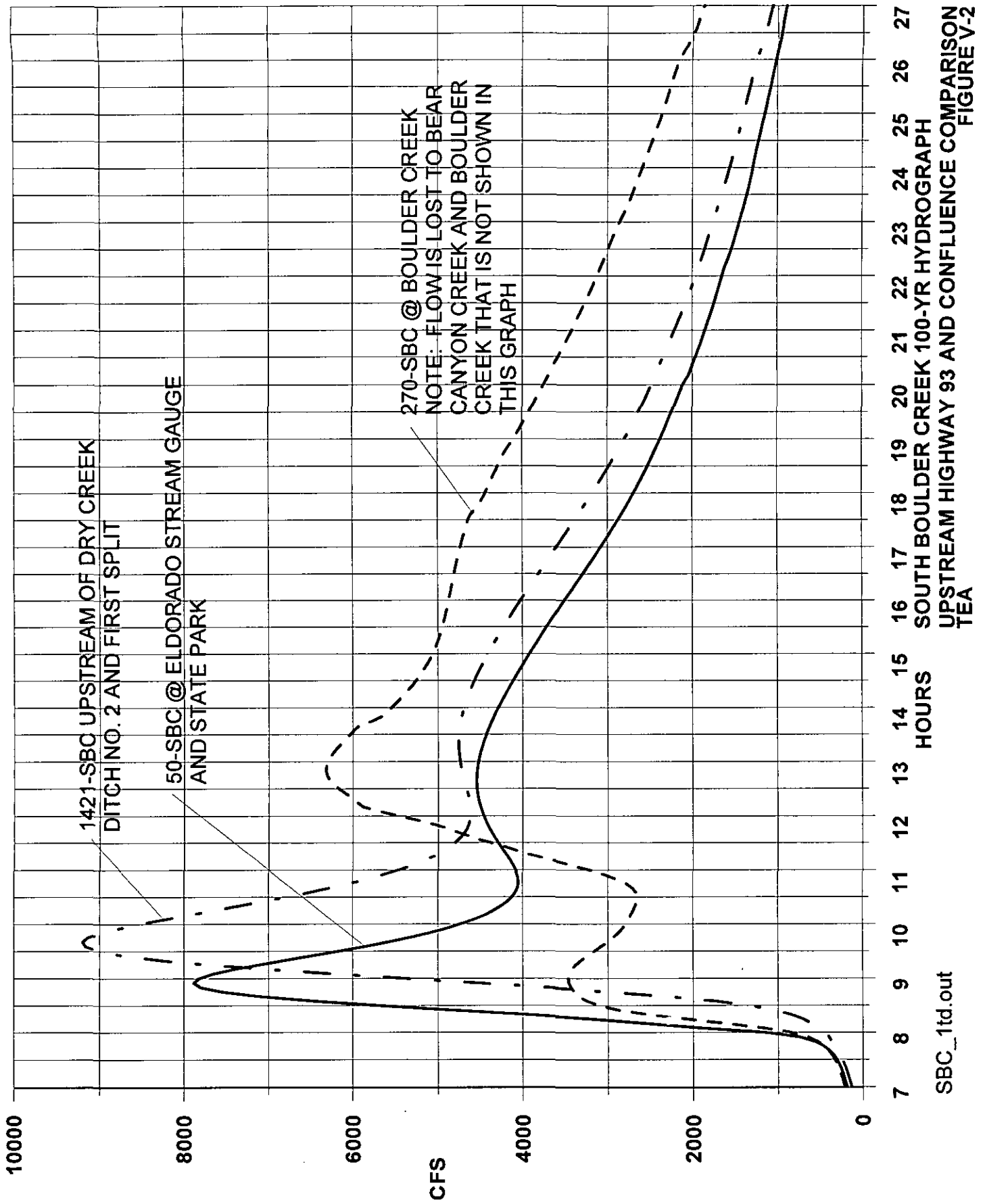
South Boulder Creek - Highway 93 to Highway 36

The lower hydrographs in Figure V-4 show the effect of the flow splits upstream, which have diverted the peaks, leaving a steady "base" flow in South Boulder Creek. Hydrograph 1800 shows the addition of flow from Marshall to the South Boulder Creek flow under Highway 93 (1509). Hydrograph 1506 shows some minor attenuation from the long route through the floodplain. 1512 shows the "peak" coming back in from the West Valley Overflow, which is hardly attenuated as shown in the following graphs.



SBC_1td.out

FIGURE V-1



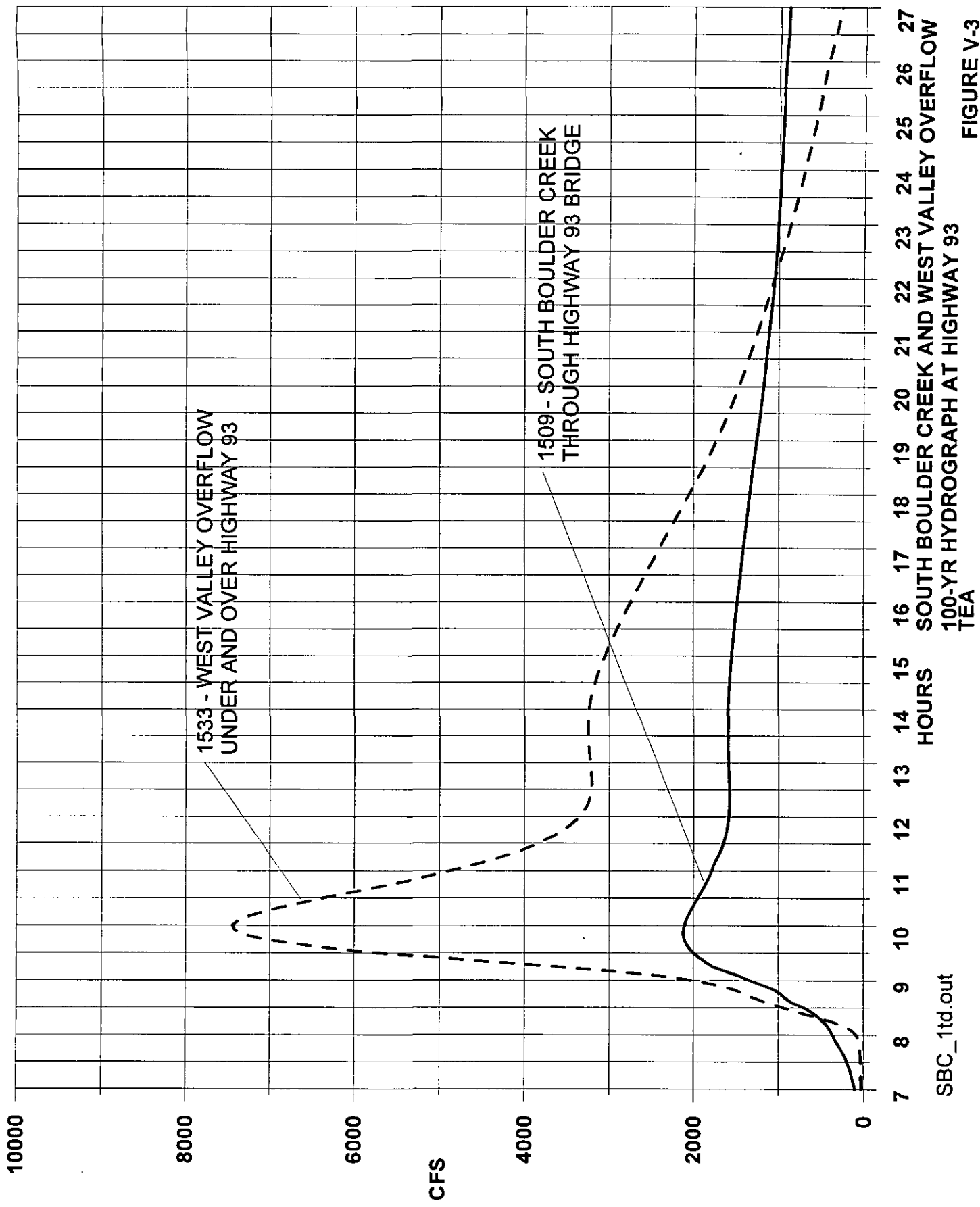
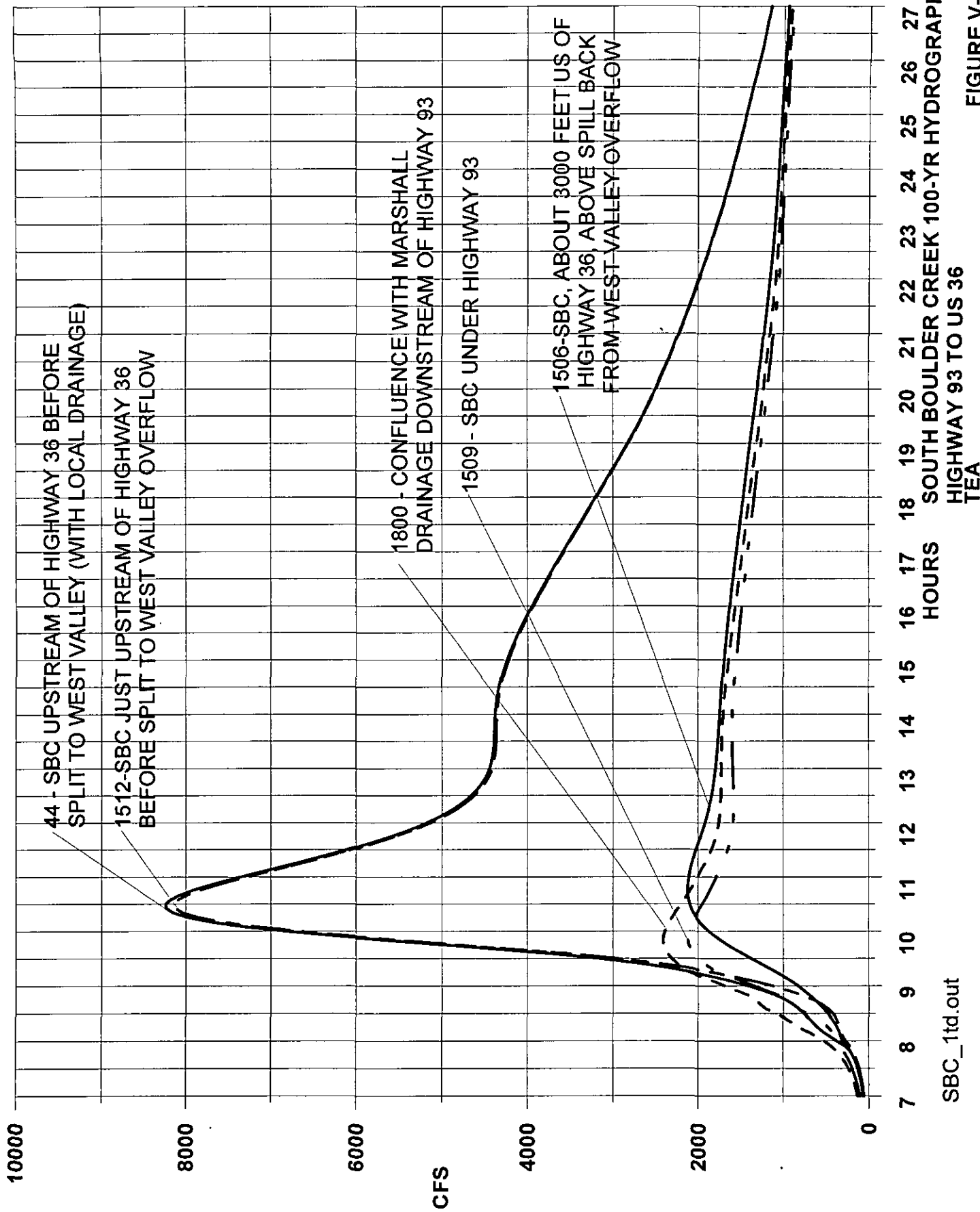


FIGURE V-3

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SOUTH BOULDER CREEK 100-YR HYDROGRAPH
HIGHWAY 93 TO US 36
TEA

FIGURE V-4

West Valley Overflows - Highway 93 to Flatirons Levee

Figure V-5 hydrographs illustrate the flashier peak overflowing from South Boulder Creek. Since the peaks are shaped nearly identically, only time lagging, not dynamic stream routing, has taken place.

Spill Above Highway 93 to West Valley

Figure V-6 depicts the hydrograph crossing Highway 93 at the West Valley Overflow. If a West Valley storage were to be constructed upstream of Highway 93, it would need to route this hydrograph, at minimum.

Total Flows Arriving at Highway 36 Area

As shown in Figure V-7, hydrographs 1442 (WVO) and 44 (SBC) represent the total stream flow arriving at Highway 36. The hydrographs have a very flashy peak from Eldorado Canyon and downstream areas, and a substantial middle section base from the Gross Reservoir overflow. Element 1442 illustrates the flow which will go directly to the West Valley in the channel that follows around the east side of the Flatirons Levee and roughly follows Dry Creek Ditch No. 2.

Spill Above Highway 36 to West Valley

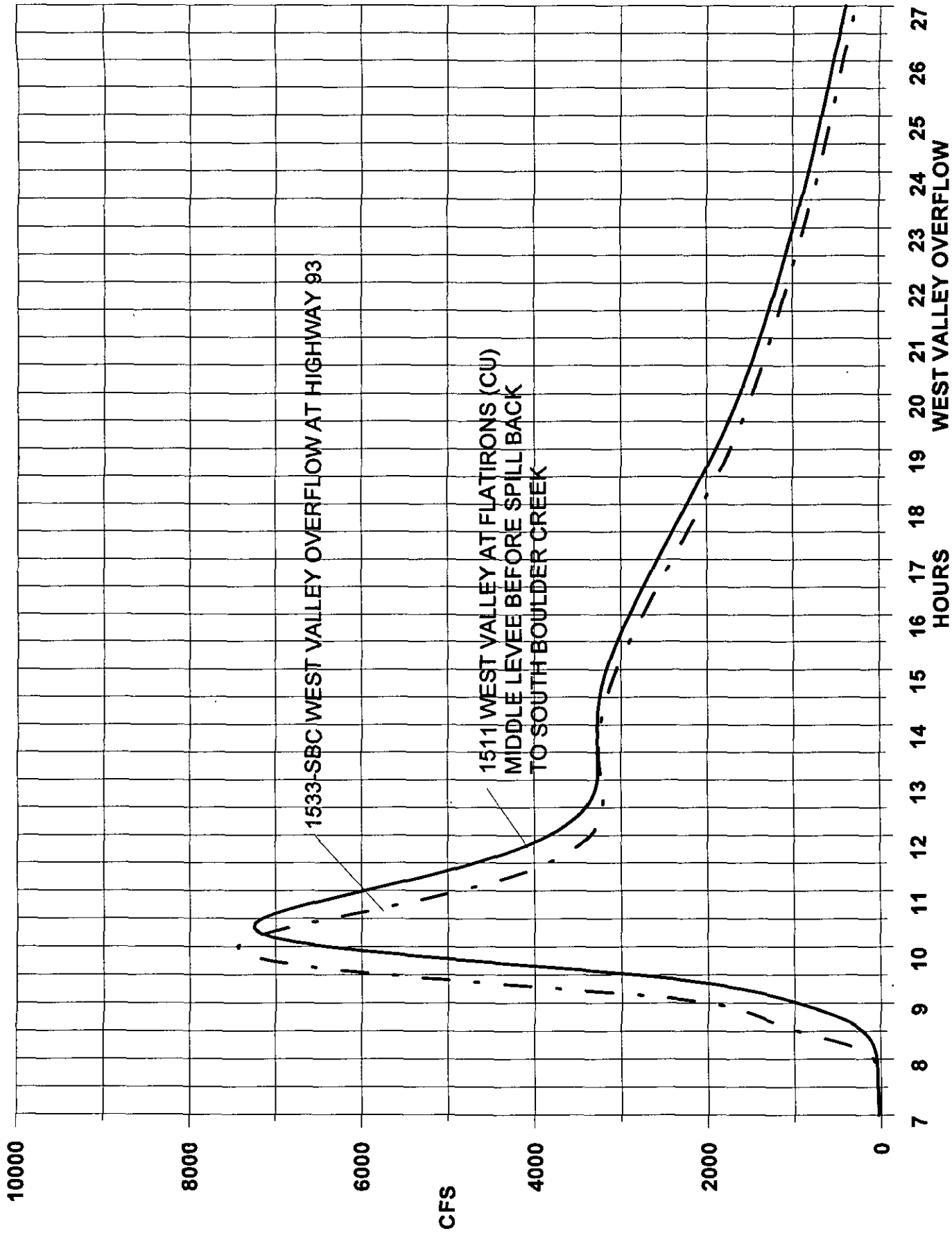
The Figure V-8 hydrograph represents the flow on the south side of the freeway directed toward the Highway 36 and Foothills interchange. Storage facilities at Highway 36 would probably need to manage this hydrograph.

South Boulder Creek from Highway 36 to the Wellman Ditch

The 242 hydrograph in Figure V-9 shows South Boulder Creek discharge downstream of the inflow of Viele. Comparison with the second (241 Baseline) and third (240 upstream of Wellman) shows hydrograph lagging, but not significant routing and attenuation. The spillway flow from Gross significantly extends the 4000 cfs duration.

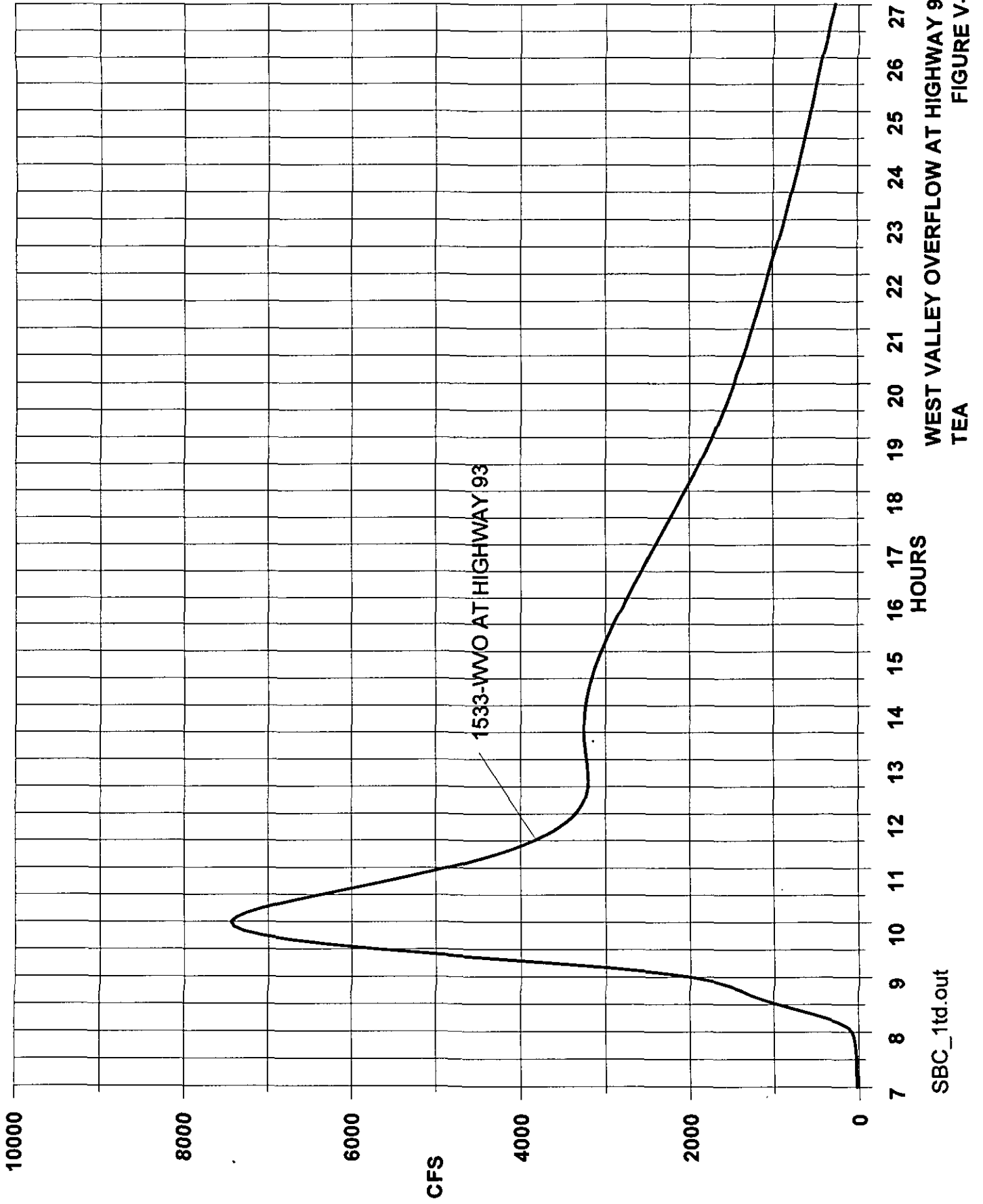
South Boulder Creek from the Wellman Ditch to Downstream

Figure V-10 hydrographs depict the flow in South Boulder Creek below the Wellman, the reduced hydrograph 233 after the spill to the golf course, and downstream hydrographs to above the confluence with Boulder Creek. By comparing 238 and 270, it is apparent that only a portion of the WVO is returning to South Boulder Creek as the spill to the golf course from South Boulder Creek (238 less 233) is a significant portion of the flow returning (270 less 231), while

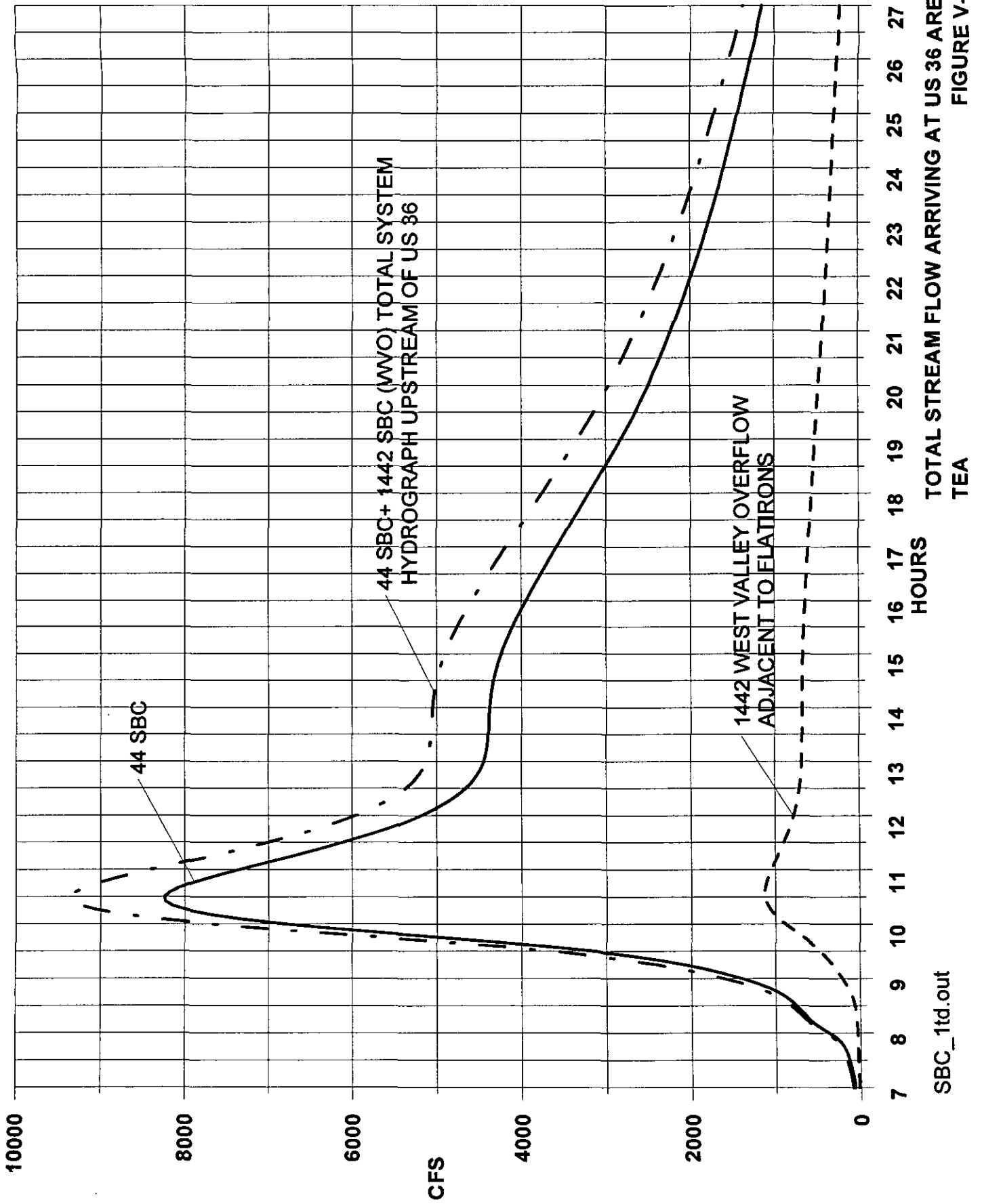


WEST VALLEY OVERFLOW
HIGHWAY 93 TO FLATIRONS (CU) LEVEE
TEA
FIGURE V-5

SBC_1td.out



WEST VALLEY OVERFLOW AT HIGHWAY 93
TEA
FIGURE V-6



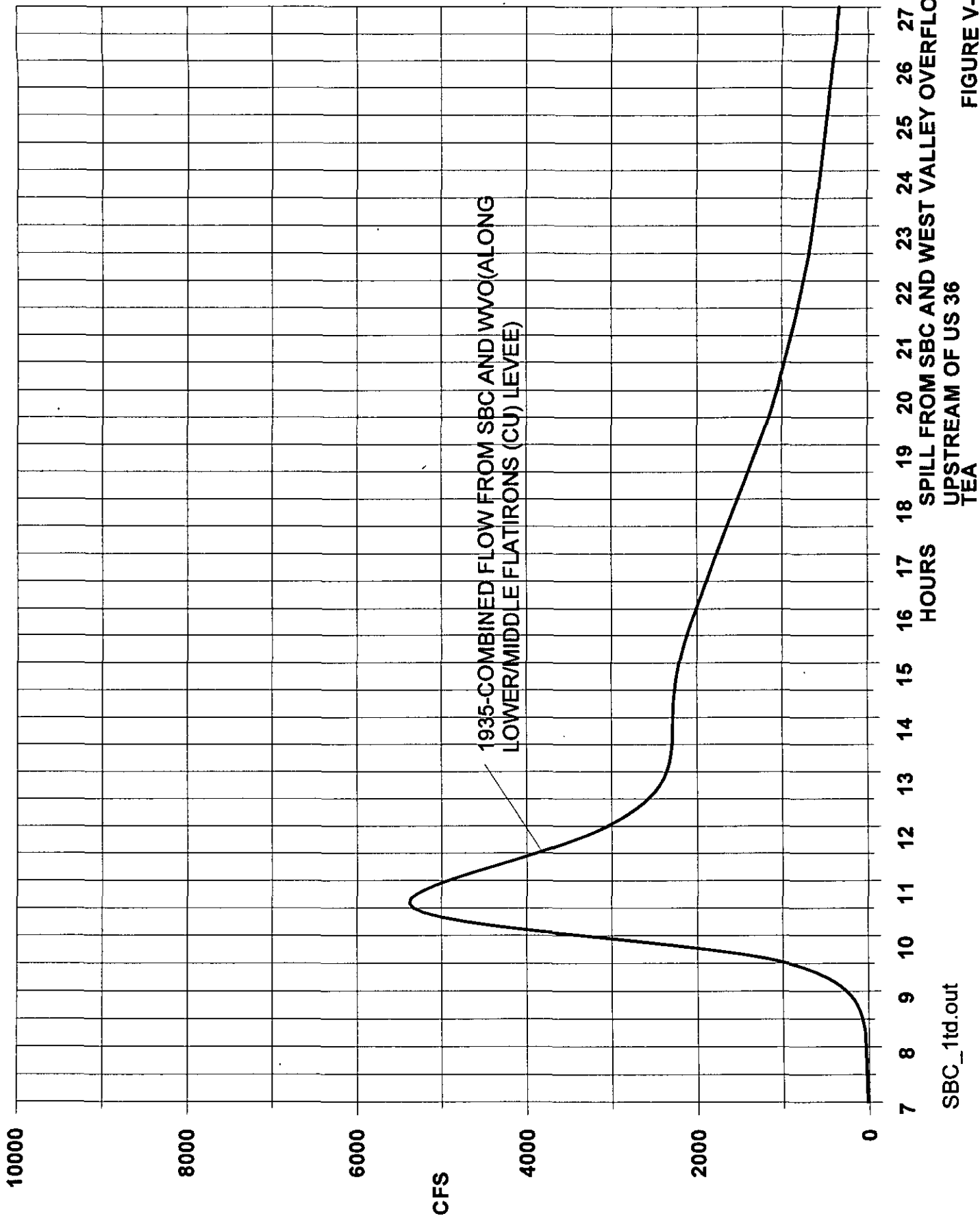
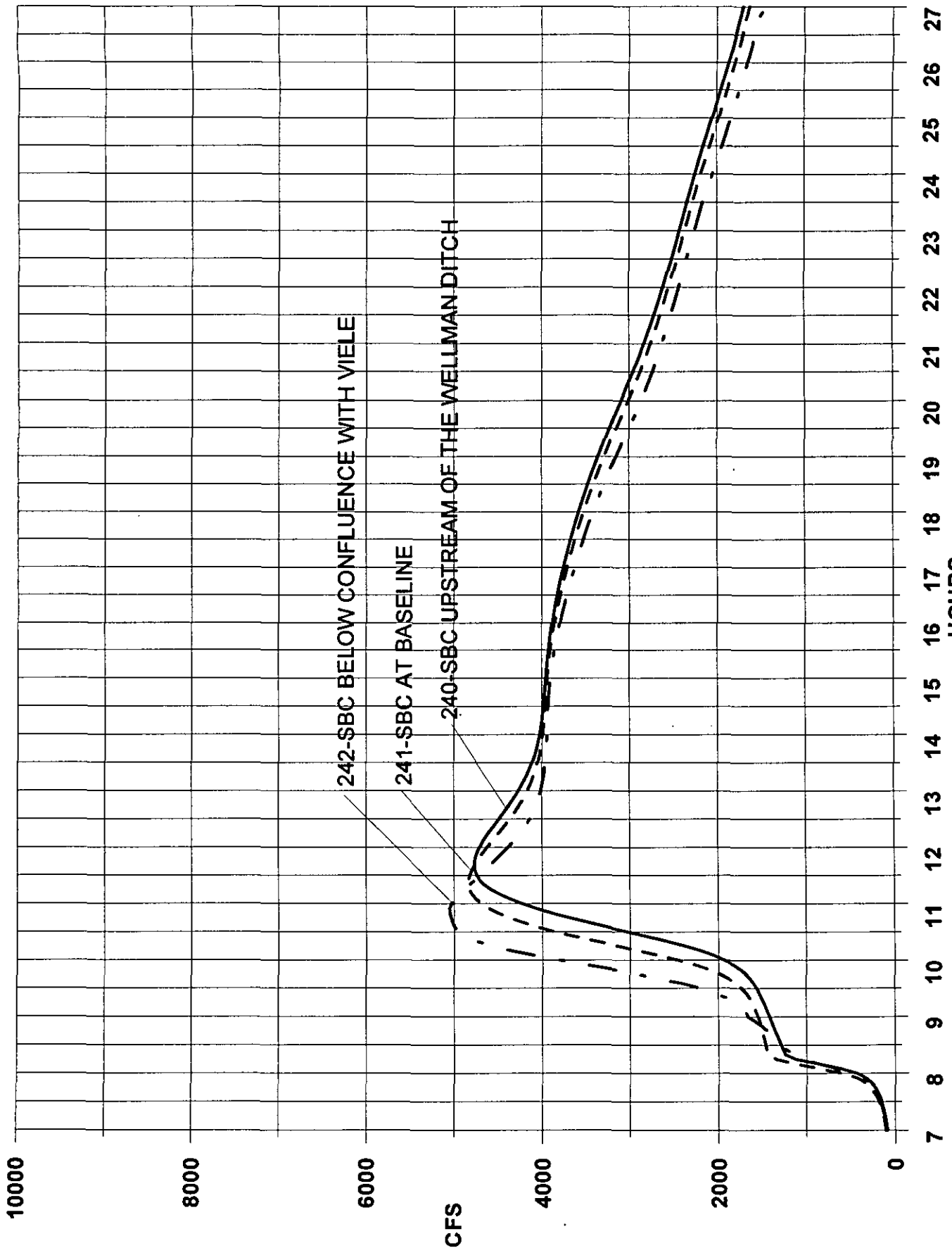


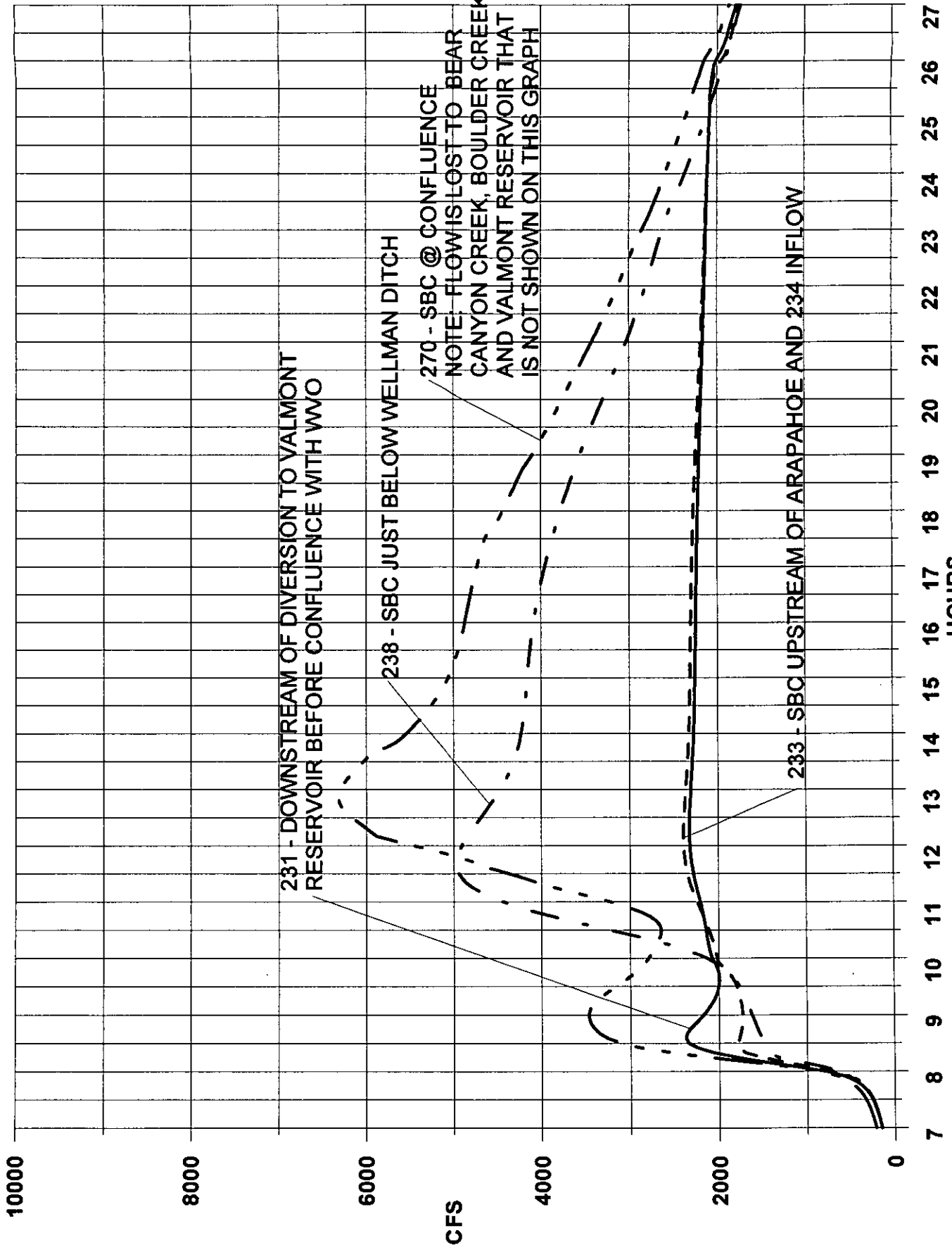
FIGURE V-8

SBC_1td.out



SBC FROM HIGHWAY 36 TO THE WELLMAN DITCH
TEA
FIGURE V-9

SBC_1td.out



SBC FROM THE WELLMAN DITCH DOWNSTREAM
TEA
FIGURE V-10

SBC_1td.out

the following hydrograph (Figure V-11) shows the magnitude of the West Valley Overflow.

West Valley Overflow~Highway 36 to Foothills and Baseline

Figure V-11 hydrographs depict the spiky spill hydrograph (352) that overflows Highway 36, then the addition of local inflow midway between Highway 36 and Foothills (1915) and further downstream at the intersection of Foothills and Baseline (359). Again, little routing effect is shown.

West Valley Overflow on Golf Course

The West Valley Overflows onto the golf course shown on Figure V-12 are from South Boulder Creek below the Wellman (1906), overflows from the West Valley via the Wellman east of 55th (1907), and Dry Creek Ditch No. 2 and portions of the West Valley Overflow from west of 55th (1908 and 1361). The last element (1909) is the combined West Valley discharge from the golf course to the Dry Creek Ditch No. 2 flood channel north of Arapahoe.

Hydrographs Spilling to Bear Canyon Creek and Boulder Creek (not included in South Boulder Creek Direct Discharge to Boulder Creek)

Figure V-13 presents estimated South Boulder Creek hydrographs discharging from the South Boulder Creek watershed to Bear Canyon Creek at Foothills, Boulder Creek between Bear Canyon Creek and 55th, and to Valmont Lakes. These hydrographs are not included in element 270, the direct South Boulder Creek discharge to Boulder Creek.

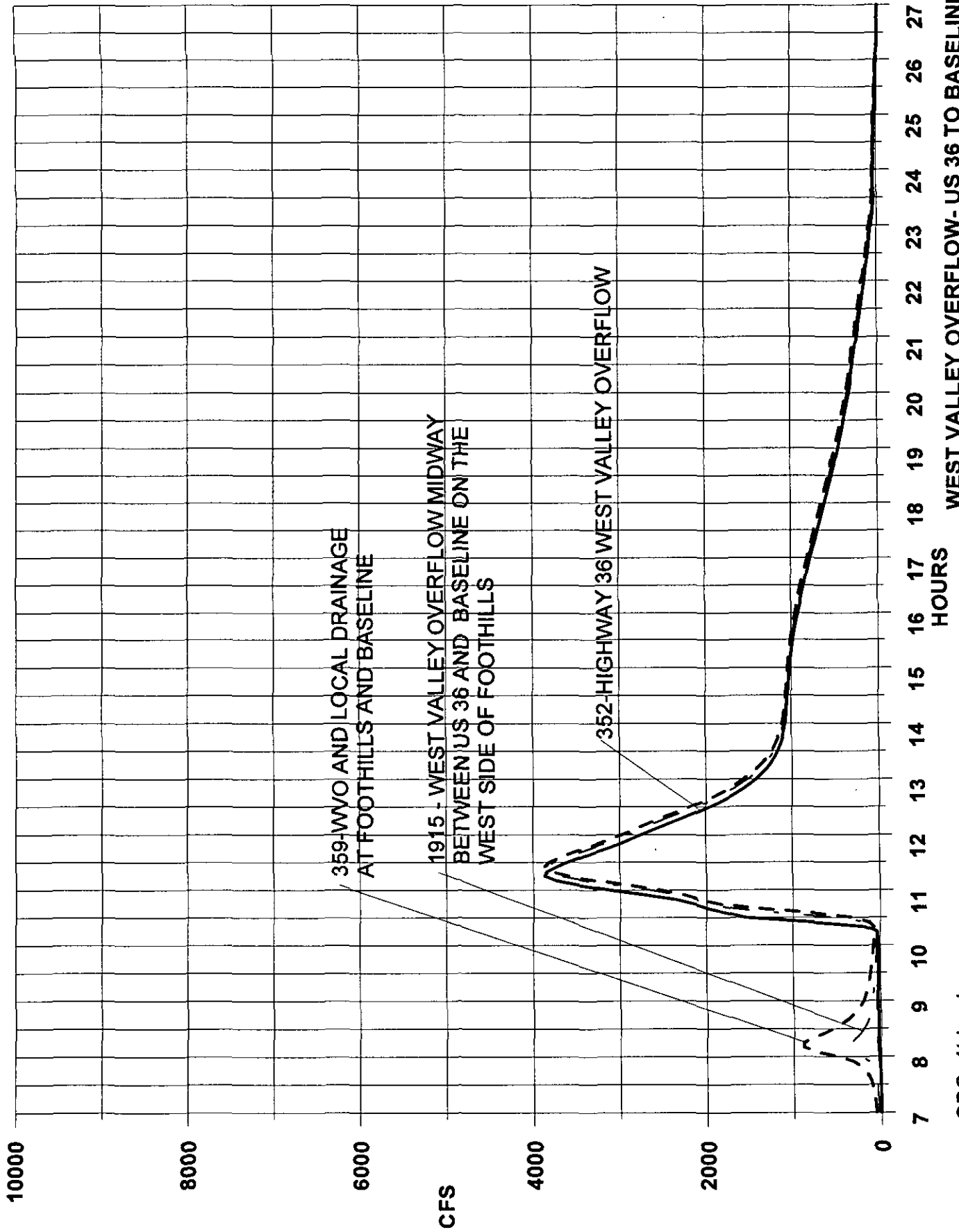
REASONABLENESS CHECKS

Several different types of reasonableness checks have been conducted, including statistical review of the Eldorado gage data and comparison with SWMM modeling results herein, comparisons with the Colorado Unit Hydrograph Procedure (CUHP) for representative basins, Unit Discharge reviews, and Regional Relations.

Comparison with Statistical Data at Eldorado Gage

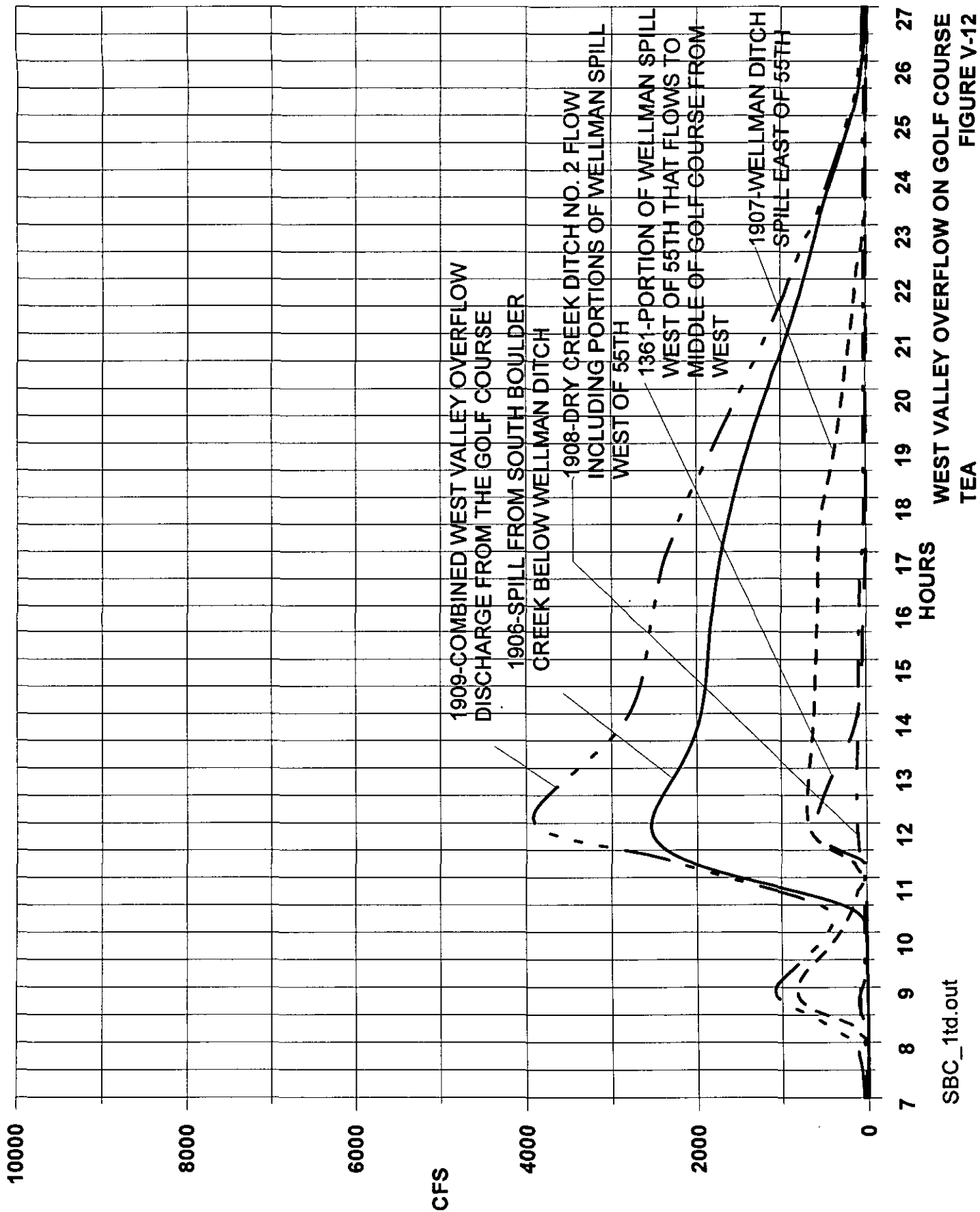
The Eldorado gage has records of peak discharge going back to 1888. There are four periods of interest:

1. 1888 to 1953 Before Gross
2. 1956 to 1965 Gross with no stoplogs on spillway
3. 1965 to 1972 Gross with 5 foot high stoplogs
4. 1973 to 1995 Gross with 2 foot high stoplogs (present)

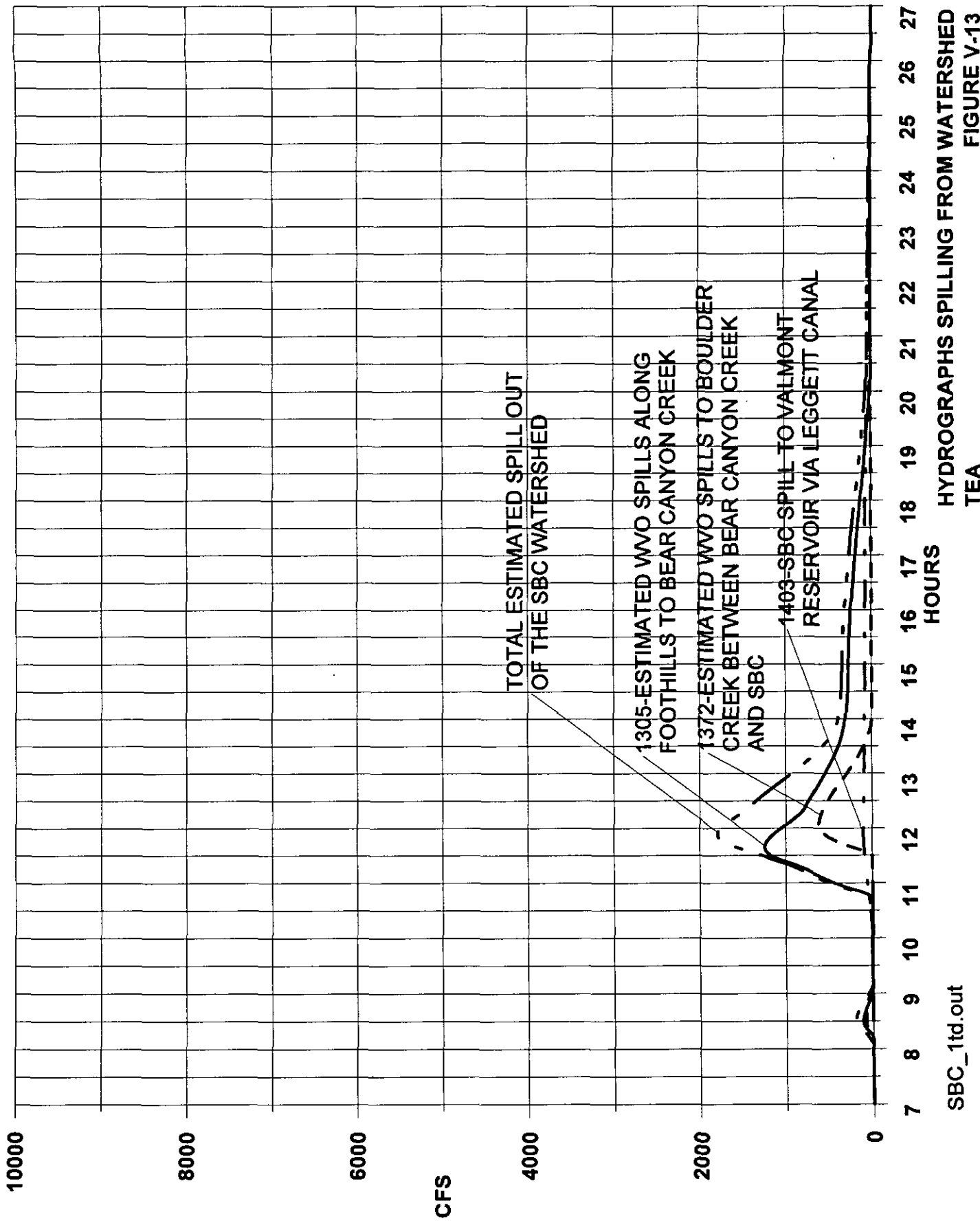


WEST VALLEY OVERFLOW-US 36 TO BASELINE
TEA
FIGURE V-11

SBC_1td.out



WEST VALLEY OVERFLOW ON GOLF COURSE TEA
 FIGURE V-12



HYDROGRAPHS SPILLING FROM WATERSHED
TEA
FIGURE V-13

SBC_1fd.out

These data are plotted on Figure V-14. The data for periods 1, 4, and 2 through 4 were fitted with a Log Pearson relationship following FEMA guidelines and "Guidelines for Determining Flood Flow Frequency."

The construction of the dam and the diversion facilities has had a substantial effect on both the average daily flows (per review of USGS Internet Data in Section VIII) and peak flows.

SWMM runs were completed for multiple frequencies and for three conditions:

1. With Gross removed to simulate historic conditions (Period 1),
2. With present dam conditions (Period 4),
3. With Gross configured to store all upstream flood waters.

The results were plotted on Figure V-14. The following observations are offered:

1. There is little difference between peak flow relationships for the SWMM runs with present conditions and with Gross storing all flood waters. Therefore, Gross already functions to control peaks at the gage site and downstream. The peaks at the gage site presently are dominated by the area below Gross.
2. The benefit of more storage at Gross would be to reduce volume at possible downstream storages, not necessarily to reduce peak flows.
3. Gross lowers the 100-year flood peaks at the Eldorado gage over conditions without Gross Reservoir. Gross has a substantial effect of lowering peaks for any given event (about 2000 cfs for the 100-year flood) over pre-dam conditions.
4. The plotting position of the 1938 event is nested within the predicted SWMM 50- to 100-year statistics. The review of the model results indicates that the peak flows at the gage are dominated by the area below Gross. The 1938 flood indicates that severe floods can still occur.
5. Flood frequency based on the statistical analysis of gage data shows significantly lower discharges than those based on the deterministic SWMM modeling, particularly for the frequent events. Therefore there are likely other significant factors occurring.
6. Likely explanations are that Gross is storing flood waters below the crest and that the rail line storages have affected the hydrology by reducing flood flows at the gage.

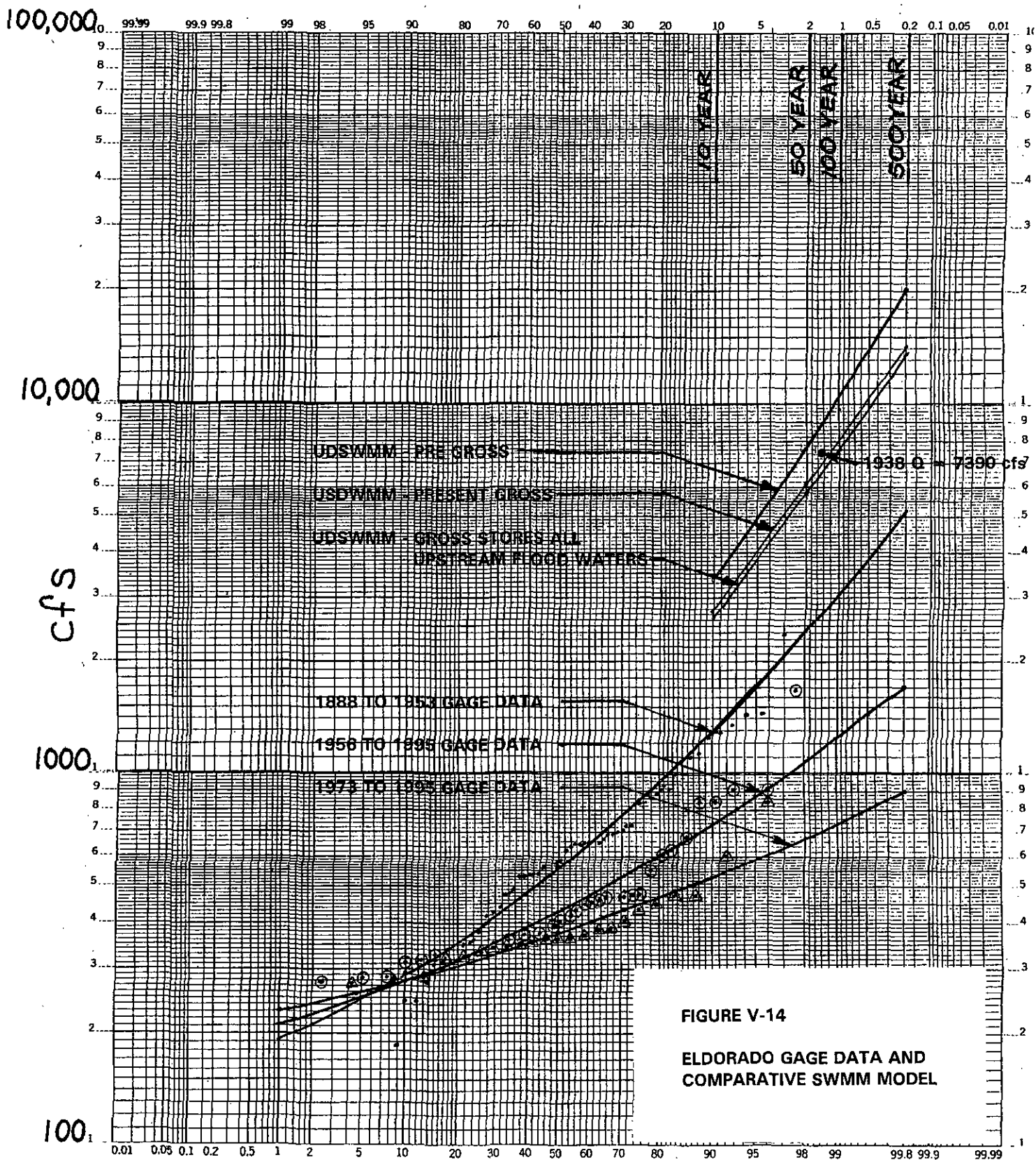


FIGURE V-14
 ELDORADO GAGE DATA AND
 COMPARATIVE SWMM MODEL

7. There are likely three phenomena that affect this range of flood events. The lower flood range is likely caused by reservoir releases, plus local thunderstorms. The higher flood range is likely associated with upslope storms and thunderstorms flowing to the west. The middle range is likely associated with moisture flow from the west, possibly associated with thunderstorms. Thus floods occurring from these three phenomenon may follow three different statistical distributions. Therefore, the statistical analysis of all of the events together may give misleading predictions, probably low, for floods in the 10- to 100-year range.

CUHP - SWMM Modeling Comparisons

The Colorado Unit Hydrograph Procedure (CUHP) is essentially based on statistical analysis of gaged watersheds in the region, and, as such, serves as a basis of modeling comparison for the UDFCD region. Selected urban, rural, mountain, foothills, and lower basins were used in the development of shaping coefficients. As CUHP can't accept the 24 hour event in 5 minute increments, the rainfall was truncated to a shorter period, and input to both the original SWMM model and to CUHP, whose hydrographs were routed by SWMM.

Table V-1 presents the results of these comparisons.

The following conclusions are offered:

1. The results compare favorably for the urbanized watersheds.
2. CUHP appears to give higher results in the steeper mountain and foothill basins where it doesn't have the data base to support its use.
3. All results are generally reasonable.

Note that an error in the draft model was found in Basin 1540 where the percent impervious in the original SWMM model was given as 50%, which was corrected in this model.

Unit Discharge Comparisons

Figures V-15 through V-18 present unit discharge (cfs/acre) for mountain areas above and below Gross, foothills, and urban areas. Compared to other studies, the results appear reasonable.

Regional Relationship

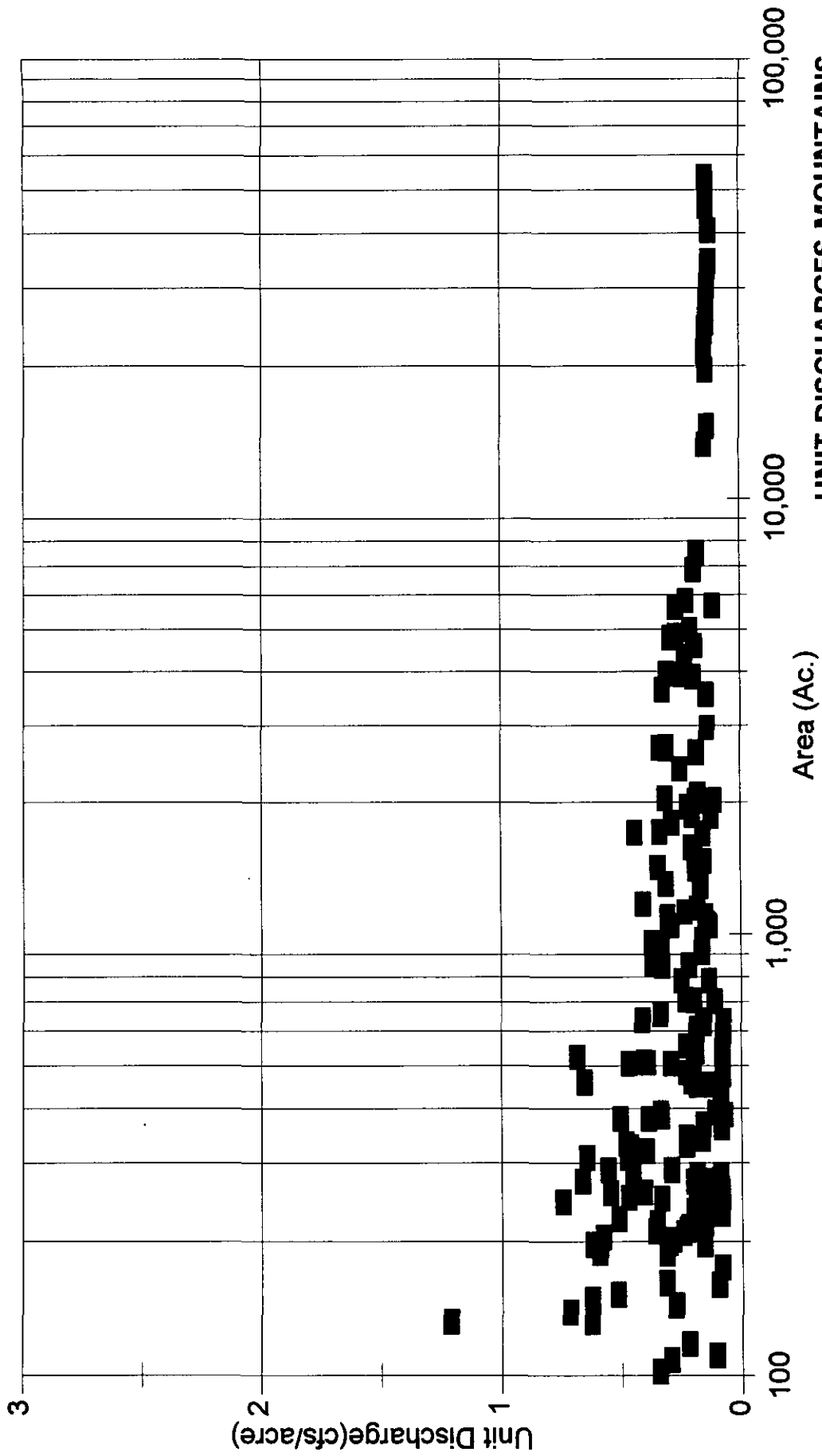
Figure V-19 is a map depicting regions in a CWCB regression analysis of past studies. Figure V-20 presents the CWCB regression compared to values from our study. We were informed to use the relationship for SPL-3, central foothills.

Table V-1

CUHP AND BASE SWMM MODEL COMPARISON

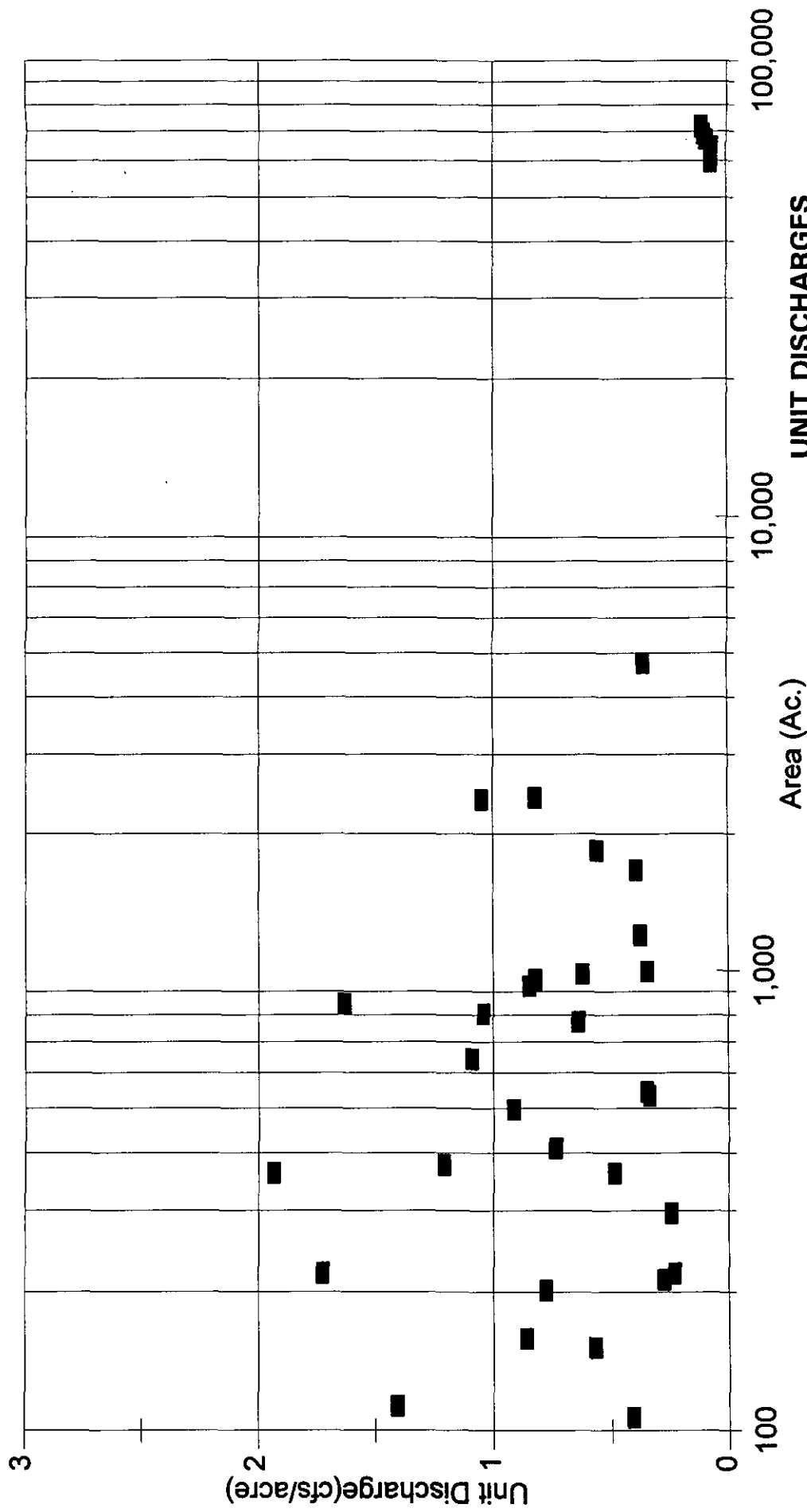
Feeder Basin	Node ID	Cumulative Drainage Area (acres)	CUHP/SWMM		SWMM		% SWMM varies
			Node type	Discharge (cfs)	Node Type	Discharge (cfs)	
South Draw - Mountain tributary with some development							
81	57	776	direct	630	channel	797	21.0
80	58	220	direct	46	channel	51	9.8
Flow	1001 N/A*	996	direct	669	direct	537	-24.6
North Mountain Tributary to South Boulder Creek at Eldorado Springs							
1665	1666	390	direct	885	channel	795	-11.3
1605	1606	471	direct	901	channel	723	-24.6
Foothills - mostly rural, some development							
1540	1542	345	direct	273	channel	204	-33.8
Viele Watershed - Foothills, urbanized							
301	301	177	direct	403	channel	435	7.4
	300	177	reservoir	11	reservoir	11	0
	1922	177	channel	11	channel	11	0
299	299	72	direct	174	channel	191	8.9
	303	249	direct	185	direct	201	18.0
	298	249	reservoir	121	reservoir	127	4.7
297	297	587	channel	921	channel	902	-2.1
Frasier Meadows - Floodplain - Urbanized							
346	346	71	direct	207	channel	210	1.4
345	345	149	channel	371	channel	377	1.6
Country Club Park - Floodplain - Urbanized							
336	1329	31	direct	119	channel	80	-48.7
East Valley Hillside South of Arapahoe - Urbanized							
235	235	187	direct	258	channel	245	-5.3

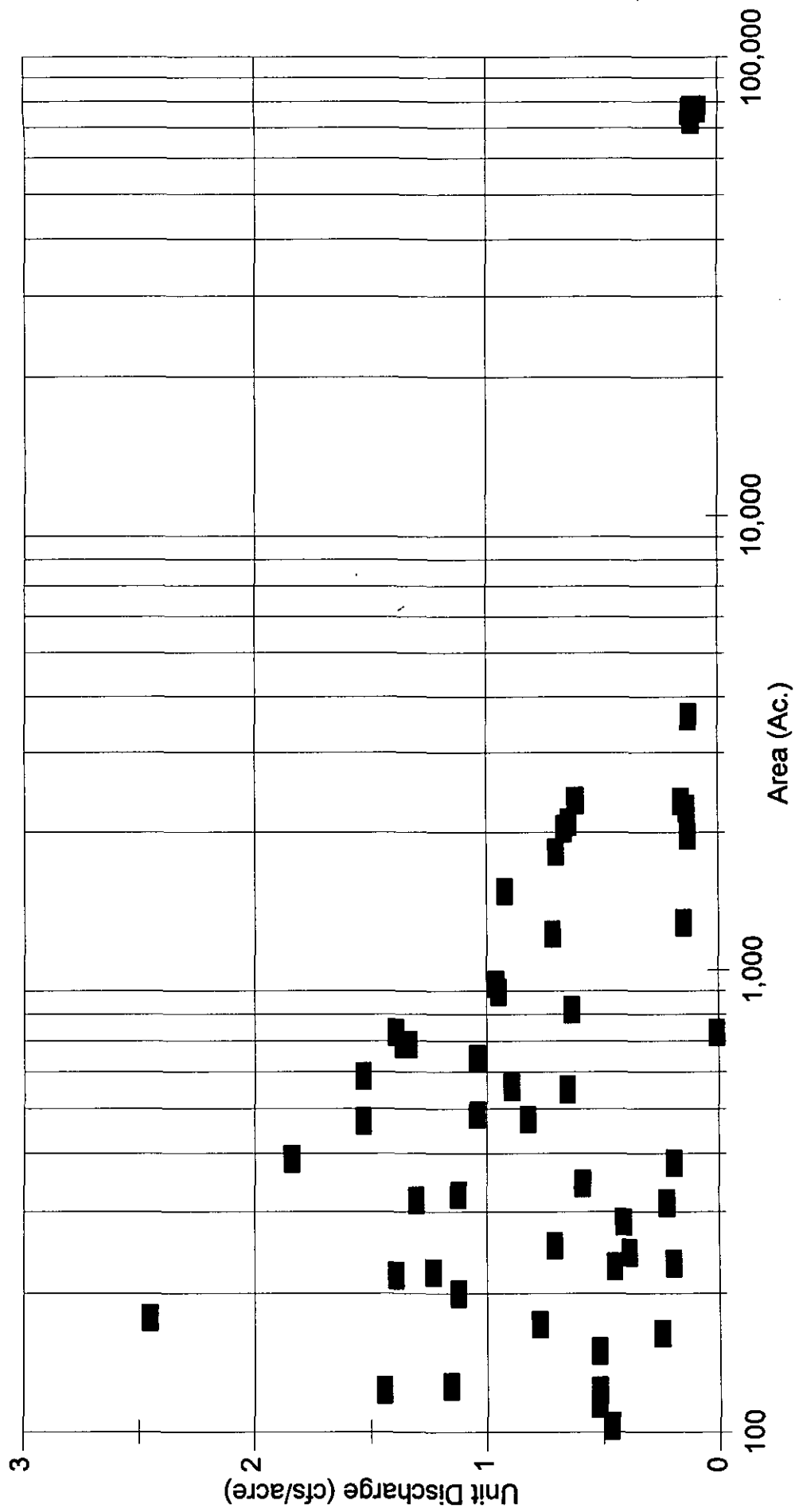
* CUHP/SWMM NODE | SWMM NODE

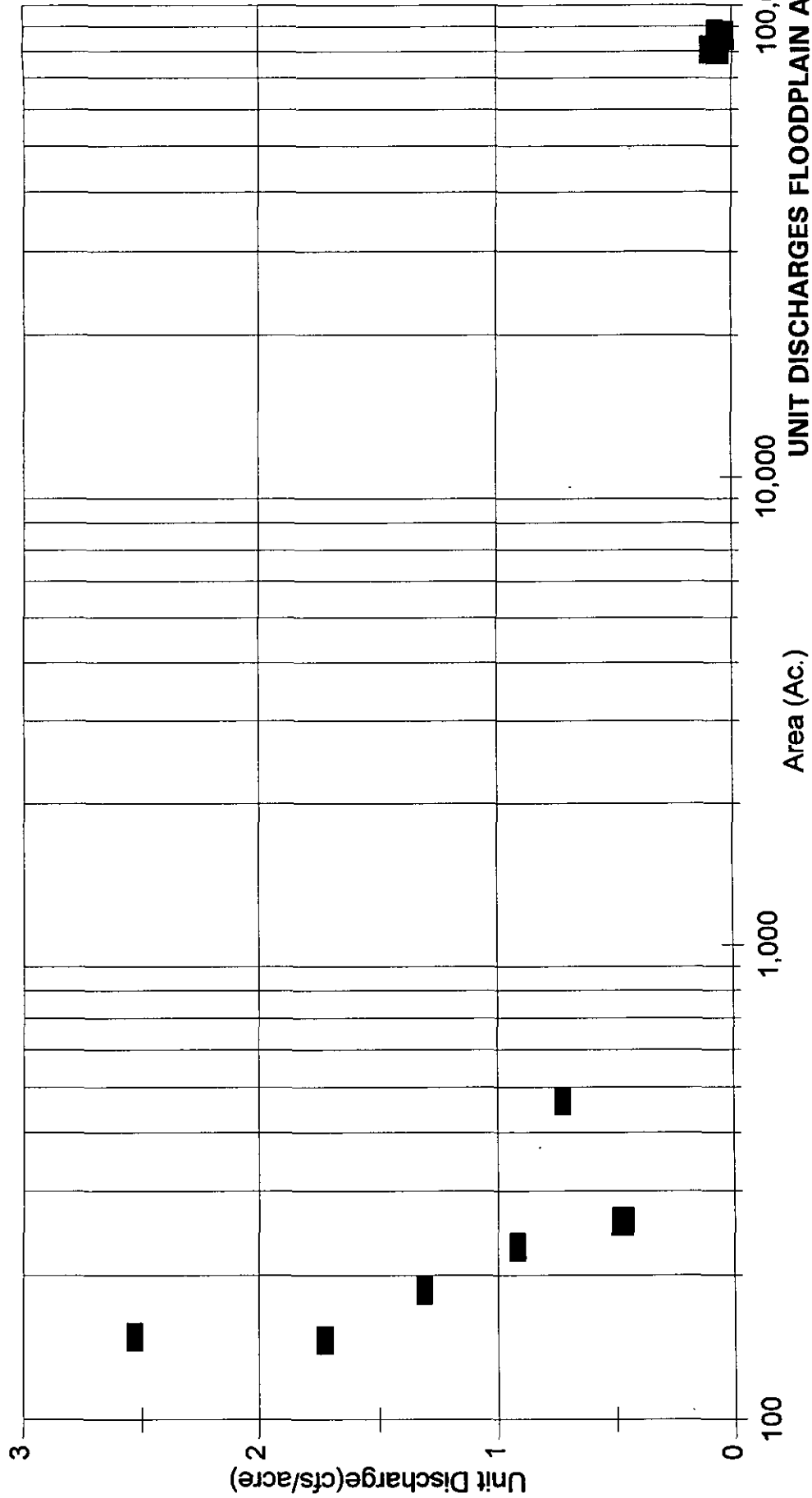


**UNIT DISCHARGES MOUNTAINS
ABOVE GROSS
TEA**

FIG V-15

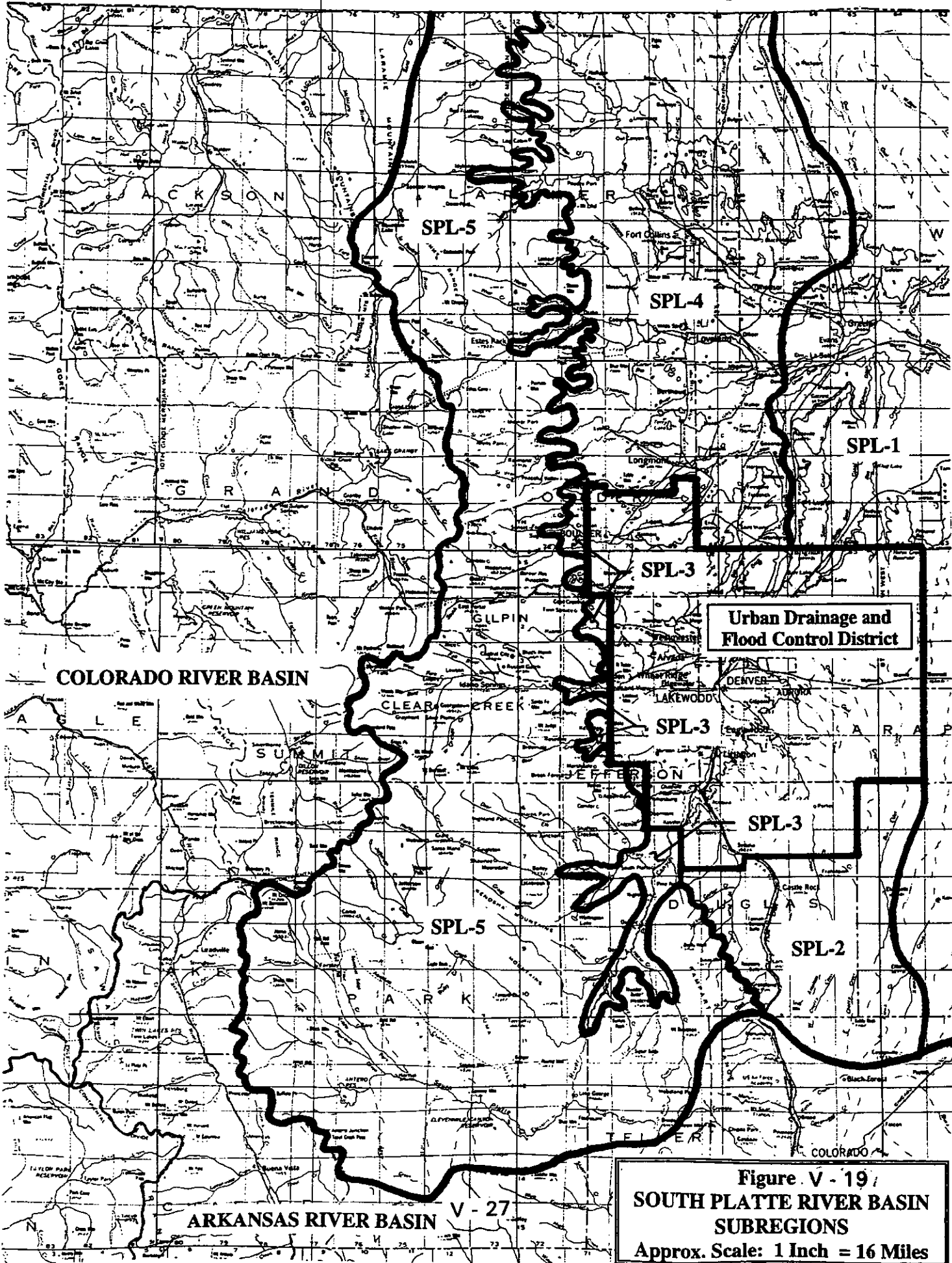






UNIT DISCHARGES FLOODPLAIN AREA
ELEMENT 44 TO BOULDER CREEK
TEA

FIG. V-18



Urban Drainage and Flood Control District

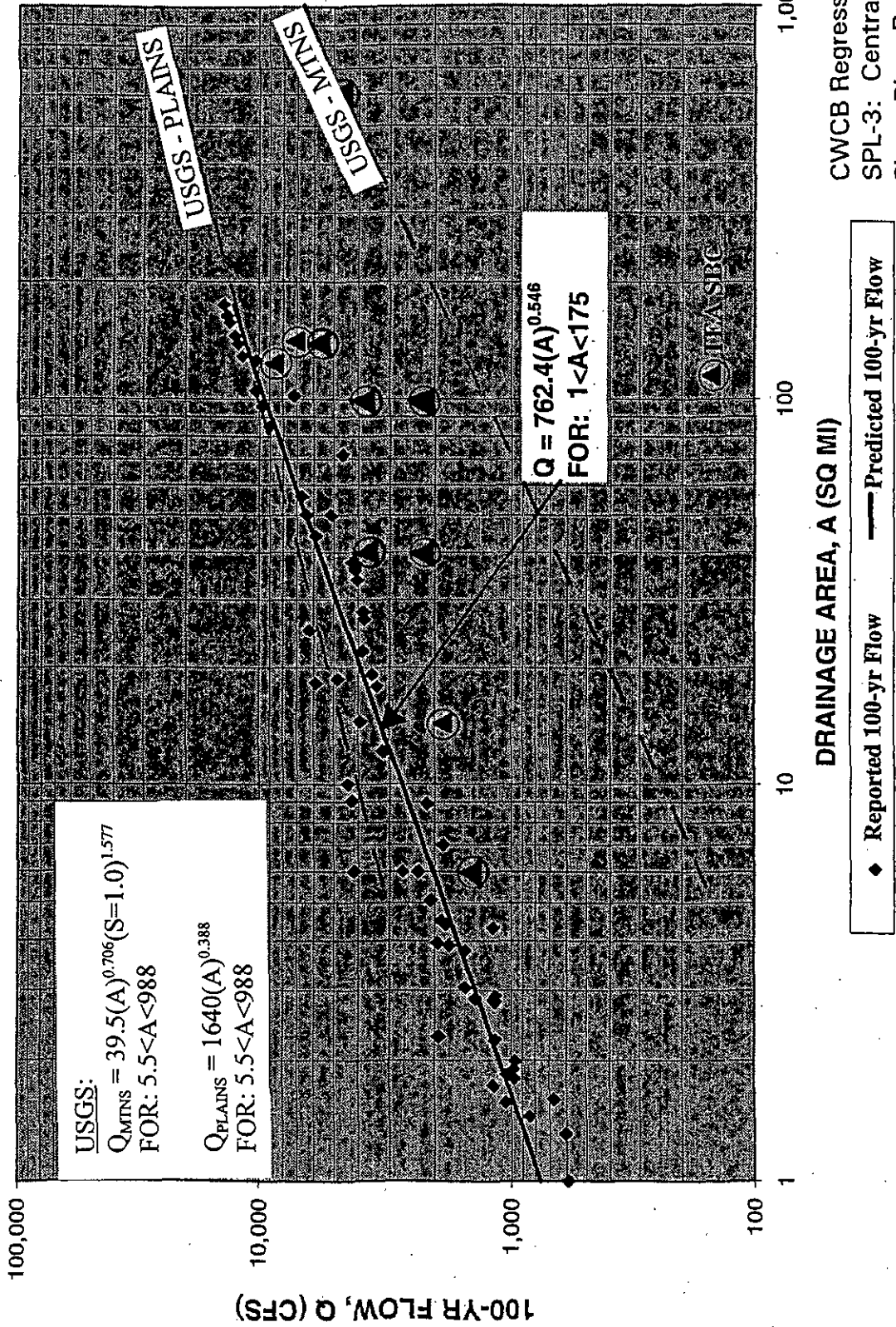
COLORADO RIVER BASIN

ARKANSAS RIVER BASIN

V - 27

Figure V - 19
SOUTH PLATTE RIVER BASIN
SUBREGIONS
Approx. Scale: 1 Inch = 16 Miles

SUBREGION SPL-3: CENTRAL FOOTHILLS South Platte River Basin



* BASE GRAPH OBTAINED FROM CWCB STUDIES AND ANALYSIS

The UDSWMM model values herein appear slightly lower than the foothills zones.

Since the foothill's adjacent mountain area up to South Draw dominates the peak South Boulder Creek discharges, we believe we have a reasonable comparison.

AGENCY AND CONSULTANT REVIEWS

The Agencies and consultants that have reviewed the draft of this report include:

Federal Emergency Management Agency - FEMA
Colorado Water Conservation Board - CWCB
Urban Drainage and Flood Control District - UDFCD

John Liou, Ph.D., P.E.
Tom W. Browning, P.E.
Bill DeGroot, P.E.

Consultants for the University of Colorado:

Love & Associates, Inc. Dave J. Love, P.E., Roger J. Peterson, Ph.D., P.E.

A review letter from Love and Associates is attached in Section VII.

All of the review comments were positive within the stated limitations herein.

John Liou of FEMA indicated that the study was adequate for the purposes of a master planning effort. However, FEMA would likely require dynamic stream flow modeling where significant floodplain storage exists, such as along South Boulder Creek and the West Valley Overflow from Highway 93 downstream. As indicated previously, this type of modeling would reduce peak flows downstream of Highway 93.

The Love & Associates letter generally concludes "We would not have a problem with utilizing the TEA hydrology as currently drafted so long as the Project Sponsors recognize it is conservative and that master planning efforts take this into account." Love concurs with the likely need to incorporate floodplain storage (dynamic stream flow routing) downstream of a point above Highway 93.

During review of the draft report, stream flow modeling parameters were discussed by Love, indicating the possibility that the selections made may result in overestimation of the flow. Table V-2 is a review of parameters and resultant velocity and Froude No.'s for representative streams selected by Bill Taggart as a reviewing principal responsible for the effort. Staff members had originally selected the values under TEA and UDFCD guidelines. Some values were changed in a test model based on the principal's review. This test illustrated that there exists no strong indication of high or low values.

ID	NAME & DESCRIPTION OF STREAM	MEASURED SLOPE %	TRIBUTARY AREA ACRES	US SWMM 100 YEAR MODEL RESULTS DISCHARGE CFS	US SWMM 100 YEAR MODEL RESULTS DEPTH FEET	UNIT GROSS/ACRE	LOWER CHANNEL PARAMETERS & PERFORMANCE	LOWER CHANNEL PARAMETERS & PERFORMANCE	OVERFLOW CHANNEL PARAMETERS & PERFORMANCE	OVERFLOW CHANNEL PARAMETERS & PERFORMANCE	REVIEW COMMENTS											
							DEPTH FEET	WIDTH FEET	SLOPE H/V RATIO	ROUGHNESS	SLOPE %	VELOCITY FEET/SEC	ROUTE NO.	DEPTH FEET	WIDTH FEET	SLOPE H/V RATIO	ROUGHNESS	SLOPE %	VELOCITY FEET/SEC	ROUTE NO.		
159	JENNY GULLCH, 1.1 MILE LONG & TRIBUTARY	8.8%	1865	231	1.2	0.12	1.22	20.0	5.0	0.050	8.18%	7.28	1.28	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	STREAM MIGHT BE HIGHER, EFFECTIVE SLOPE FLATTER AND/OR ROUGHNESS HIGHER. RESULTS COULD BE LOWER OR HIGHER, REASONABLE CHOICE.
167	SPR ABOUT 1 MILE UPSTREAM OF JENNY GULLCH AND BELOW MOFFATT TUNNEL	1.88%	14688	1804	3.8	0.14	3.00	32.0	4.0	0.040	1.00%	8.52	0.75	4.35	250.0	10.0	0.050	1.00%	3.20	0.54	1.00	STREAM MIGHT BE HIGHER, EFFECTIVE SLOPE FLATTER AND/OR ROUGHNESS HIGHER. RESULTS COULD BE LOWER OR HIGHER, REASONABLE CHOICE.
62	BOLLING GULLCH, 0.78 MILE LONG SOUTH TRIBUTARY	8.25%	2038	642	2.1	0.31	2.09	12.0	5.0	0.070	28.29%	13.70	2.02	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	STREAM MIGHT BE ROUGHER AND/OR EFFECTIVE SLOPE FLATTER, IN TEST MODEL, LOWERED STREAM SLOPE TO 7%, THIS REDUCED LOCAL STREAM FLOW LESS THAN 1%, BUT INCREASED SEC FLOWS DUE TO TRUNK. RESULTS OK.
80	SOUTH BOLDER CREEK FROM GULLCHES	13.00%	228	118	1.0	0.52	0.88	12.0	5.0	0.080	12.82%	7.20	1.47	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	STREAM MIGHT BE HIGHER, EFFECTIVE SLOPE FLATTER AND/OR ROUGHNESS HIGHER. RESULTS COULD BE LOWER OR HIGHER, REASONABLE CHOICE.
88	SOUTH BOLDER CREEK FROM PARK ABOVE ELWOOD STATE PARK	8.78%	1842	133	2.7	0.07	2.74	25.0	4.0	0.070	8.30%	10.51	1.28	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	THIS WAS WORKED ON WANTED ABOVE. THIS STREAM ALSO HAS RESULTS WITH MORE OF A VEE SECTION WHERE ONE BUT PROBABLY ESTABLISHED EST IS ON FOR NOW, BUT REASSES WITH ANY FUTURE STORAGE STUDY.
1608	NORTH SIDE TRIBUTARY AT ELWOOD CANYON	8.02%	471	723	2.7	1.54	2.00	5.0	4.0	0.046	8.12%	1.77	1.88	3.87	25.0	3.0	0.080	8.12%	8.88	1.31	4.51	THIS IS A STEEP STREAM WITH LESS VEGETATION AND A DEFINITE OVERFLOW SECTION. APPEARS SWMM MAY HAVE DIFFICULTY WITH THIS OVERFLOW SECTION. LOW MAY BE SOMEWHAT ON THE HIGH SIDE, BUT NOT UNREASONABLE.
1	SOUTH BOLDER CREEK ABOVE MARTIN GULLCH	2.57%	64741	4277	6.4	0.07	4.00	30.0	2.0	0.055	2.40%	9.04	0.28	8.40	50.0	2.0	0.065	2.40%	9.12	0.78	2.40	WITH ADJUSTED ROUGHNESS TO DUP SWMM.
50	SOUTH BOLDER CREEK IN ELWOOD STATE PARK	2.50%	71468	7883	6.2	0.11	4.00	40.0	5.0	0.060	2.88%	8.79	0.89	8.20	150.0	7.0	0.080	2.85%	4.82	0.83	1.22	THIS IS A RIGGED, STEEP STREAM, BY STRAIGHT LINES EQUATION THE OVERFLOW SHOULD BE FLAT, BUT STAGE ON SWMM OUTPUT INDICATES POSSIBLE HIGHER VELOCITIES MAY BE OCCURRING, ACCELERATING THE OVERFLOW FROM GROSS. POSSIBLE PROGRAM PROBLEM, HIGHER ROUGHNESS MIGHT MITIGATE IN OTHER REVISIONS.
48	SOUTH BOLDER CREEK IN ELWOOD SPRINGS	7.30%	72077	7815	9.0	0.11	5.00	30.0	2.0	0.070	1.33%	5.88	0.53	8.59	200.0	2.0	0.085	1.30%	8.89	0.48	0.48	AS A RESULT TO THE ABOVE, TEST WAS CONDUCTED AT A FLOOD PLAIN ANALYSIS FOR STATEWIDE. THE REASON FOR THIS WAS ABOUT 10 FEET, THE VALUE HERE ARE REASONABLE, BUT THE SLOPE SHOULD HAVE BEEN FLATTER 1. SWMM MAY HAVE SOME COMPUTATIONAL PROBLEMS WITH OVERFLOW SECTION.
297	VEE TRIBUTARY ABOVE TABLE mesa AND SOUTH LOOP ROAD	2.70%	657	902	4.8	1.84	4.51	8.0	3.0	0.045	2.60%	9.87	1.88	NOT USED	NOT USED	NOT USED	NOT USED	NOT USED	NOT USED	NOT USED	NOT USED	THIS IS A RIGGED, STEEP STREAM THROUGH ELWOOD SPRINGS. THE EFFECTIVE OVERFLOW SHOULD BE FLAT, BUT STAGE ON SWMM OUTPUT INDICATES POSSIBLE HIGHER VELOCITIES MAY BE OCCURRING, ACCELERATING THE OVERFLOW FROM GROSS. POSSIBLE PROGRAM PROBLEM, HIGHER ROUGHNESS MIGHT MITIGATE IN OTHER REVISIONS.
182	WEST TRIBUTARY ABOVE TABLE mesa AND SOUTH LOOP ROAD	1.15%	2178	737	4.8	1.84	4.51	8.0	3.0	0.045	2.60%	9.87	1.88	NOT USED	NOT USED	NOT USED	NOT USED	NOT USED	NOT USED	NOT USED	NOT USED	THIS IS A RIGGED, STEEP STREAM THROUGH ELWOOD SPRINGS. THE EFFECTIVE OVERFLOW SHOULD BE FLAT, BUT STAGE ON SWMM OUTPUT INDICATES POSSIBLE HIGHER VELOCITIES MAY BE OCCURRING, ACCELERATING THE OVERFLOW FROM GROSS. POSSIBLE PROGRAM PROBLEM, HIGHER ROUGHNESS MIGHT MITIGATE IN OTHER REVISIONS.
1808	SOUTH BOLDER CREEK FROM MARSHALL ROAD TO LEVEL AREA	1.08%	78714	2123	1.2	NOT APPLICABLE	2.50	33.0	4.0	0.080	0.64%	2.88	0.36	3.89	800.0	10.0	0.065	0.64%	1.87	0.30	0.30	THE EFFECTIVE STREAM SLOPE IS PROBABLY FLATTER AS THERE ARE A SERIES OF DIPS AND GULLCHES. THIS IS THE MODEL IS RIGGED FOR LOCAL DRAINAGE. IN TEST MODEL, FLATTENED TO 1.5%, DISCHARGES INCREASED 5.9%, BUT NO CHANGES DOWNSTREAM OF HWY 38. IMMEDIATELY DOWNSTREAM, THERE IS AN OFFLINE STORAGE WHICH IS FUNCTIONING AND TRIMS THE PEAK. THIS THERE IS NO SIGNIFICANT EFFECT ON SEC FLOWS.
241	SOUTH BOLDER CREEK FROM VEE CONFLUENCE TO BASELINE	1.07%	64351	4835	3.8	NOT APPLICABLE	3.00	65.0	2.0	0.045	1.00%	6.73	0.71	3.87	1200.0	200.0	0.055	1.00%	4.07	0.48	0.47	WITH ADJUSTED ROUGHNESS TO DUP SWMM.

The study could be improved first by dynamic storage routing in the lower valley, second by surveys and refined flow split analysis, and third (and to a lesser degree) by field section surveys to more accurately depict the major tributaries and South Boulder Creek above the Highway 93 splits.

CONCLUSIONS

1. The UDSWMM hydrology model results are reasonable and compare well with other studies and methodologies in the region.
2. Any apparent disparities between statistics of Eldorado Stream gage data and UDSWMM modeling results are likely associated with storage taking place below the level of the Gross Spillway crest and multiple storages along the rail line to the Moffatt Tunnel. Since these storages cannot be presently used in any modeling, the use of the statistical database for determining flood frequency is not appropriate.
3. Improved stream flow modeling can make the results along South Boulder Creek more reliable and realistic.
4. The above review indicates that the model results are reasonable and valid.
5. The major factors in improving the reliability and realism of the model would be to:
 - a) Explore the possibility of firming up institutionally the flood storage function that has occurred at Gross Reservoir.
 - b) Explore the storages along the rail line and meet with the Railway to pursue efforts to make these storages permanent and in compliance with standard storage/dam criteria.
 - c) Refine the South Boulder Creek stream routing elements and modeling by:
 - Refining hydraulic split modeling along Highway 36 and other locations.
 - Conducting limited cross section surveys of the streams and controls for critical splits, and using a dynamic storage routing algorithm to model the South Boulder Creek and the West Valley Overflow.
 - Conducting limited cross section surveys below Gross to the mouth of the canyon.

SECTION VI

REFERENCES

Addendum No. 1 to Seventh Periodic Safety Inspection Report for Gross Dam, FERC Project No. 2035, Boulder County, Colorado, June 1993.

Boulder's Flood Protection Decision - A Choice to Live With, U.S. Army Corps of Engineers, Pre-1977.

Boulder County Storm Drainage Criteria Manual, WRC Engineering, Inc., October 1986.

City of Boulder Big Dry Creek Ditch II Preliminary Design Report, McLaughlin Water Engineers, February 1996.

City of Boulder, Colorado Design and Construction Standards, July 2, 1998.

City of Boulder Storm Water Collection System Master Plan, WRC, December 1984.

Depth-Area Ratios in the Semi-Arid Southwest United States, NOAA Technical Memorandum NWS HYDRO-40, U.S. Department of Commerce, National Oceanic and Atmospheric Administration, National Weather Service, August 1984

A Disaggregation Model for Time Series Analysis and Synthesis, Daño Valencia R. and John C. Schaake, Jr., Ralph M. Parsons Laboratory for Water Resources and Hydrodynamics, Department of Civil Engineering, Massachusetts Institute of Technology, Report No. 149, June 1972.

55th Street Improvements Baseline Road to Arapahoe Avenue Plans, Carter Burgess, June 1996.

Final Report: Colorado Extreme Storm Precipitation Data Study: Summary of Accomplishments and Work Performed February 15, 1995 through October 31, 1996, Thomas B. McKee, Nolan J. Doesken, Colorado Climate Center, Department of Atmospheric Science, May 1997.

Flood Flow Frequency Analysis: Users Manual, U.S. Army Corps of Engineers, February 1982.

Flood Hydrology Manual: A Water Resources Technical Publication, U.S. Department of the Interior, Bureau of Reclamation, Arthur G. Cudworth, Jr., 1989.

Flood Plain Analyses of South Boulder Creek at the Flatiron Property, Love, July 1996.

Flood Plain Information - Boulder Creek and South Boulder Creek - Volume 11, Boulder Metropolitan Region, Colorado, U.S. Army Engineer District, Omaha Corps of Engineers - Omaha, Nebraska, August, 1969.

Gross Dam and Reservoir 1982 Dam Safety Inspection Report, DMJM Phillips-Riester-Haly, 1982.

Guidelines for Determining Flood Flow Frequency (Revised), Interagency Advisory Committee on Water Data, Reston, VA, March 1982.

Guidelines for Determining 100-Year Flood Flows for Approximate Floodplains in Colorado, Draft Version 2.0, Department of Natural Resources, Colorado Water Conservation Board, October 1996.

Handbook of Hydrology, David R. Maidment Editor, McGraw-Hill, Inc., 1993.

HEC-1 Flood Hydrology Package: Users Manual, U.S. Army Corps of Engineers, September 1990.

History of Floods and Flood Control in Boulder, Colorado, Phyllis Smith, September 1987.

Hydrology and Floodplain Analysis, 2nd Ed., Philip B. Bedient, Waayne C. Huber, Addison-Wesley Publishing Co., 1992.

Interduration Precipitation Relations for Storms - Southeast States, Ralph H. Frederick, NOAA, National Weather Service, March 1979.

Interduration Precipitation Relations for Storms - Western United States, R.H. Frederick, et.al., NOAA, National Weather Service, September 1981.

Introduction and Application of Kinematic Wave Routing Techniques Using HEC-1, Training Document No. 10, U.S. Army Corps of Engineers, May 1979.

Introduction to Hydrology, 3rd Ed., Warren Viessman, Jr., Gary L. Lewis, John W. Knapp, Harper & Row, Publishers, 1989.

Major Drainageway Planning - Boulder Creek - South Boulder Creek Confluence Area - Development of Preliminary Plan - Phase B, Simons, Li & Associates, Inc., March 1984.

Major Drainageway Planning Study - Phase A Development of Alternatives - Boulder Creek - South Boulder Creek Confluence Area, Simons, Li & Associates, Inc., August 1983.

Major Drainageway Planning for South Boulder Creek, R.W. Beck, December 1973.

A Modular Distributed Model of Catchment Dynamics, Brendan M. Harley, Frank E. Perkins, and Peter S. Eagleson, Ralph M. Parsons Laboratory for Water Resources and Hydrodynamics, Department of Civil Engineering, Massachusetts Institute of Technology, Report No. 133, December 1970.

Precipitation-Frequency Atlas of the Western United States, NOAA Atlas 2, Volume III-Colorado, U.S. Department of Commerce, National Oceanic and Atmospheric Administration, National Weather Service, 1973.

Probability, Statistics, and Decision for Civil Engineers, Jack R. Benjamin and C. Allin Cornell, McGraw-Hill Book Company, 1970.

Rainfall Intensity-Frequency Regime: Part 1-The Ohio Valley, Technical Paper No. 29, U.S. Department of Commerce, Weather Bureau, 1957.

Safety Inspection Report of Gross Dam and Reservoir 1972, Orly Phillips, 1972.

Safety Inspection Report of Gross Dam and Reservoir 1977, DMJM Phillips Riester, 1977.

Safety Inspection Report for Gross Dam, Reservoir, and Appurtenant Structures, Goodson & Associates with Engineering Consultants, October 1987.

Seventh Part 12DS Inspection Report, Gross Dam, FERC Project No. 2035, Boulder County, prepared for Denver Water by GEI Consultants, Inc. in association with Foothill Engineering Consultants, June 17, 1998.

Soil Survey of Boulder County Area, Colorado, United States Department of Agriculture, Soil Conservation Service in cooperation with Colorado Agriculture Experiment Station, January 1975.

Soil Survey of Golden Area, Colorado: Parts of Denver, Douglas, Jefferson and Park Counties, United States Department of Agriculture, Soil Conservation Service in cooperation with Jefferson County and the Colorado Agriculture Experiment Station, @ 1980.

South Boulder Creek Flood Hazard Area Delineation, Greenhorne and O'Mara, Inc., July 1986.

Supplemental Report to Periodic Safety Inspector Report for Gross Dam, Boulder County, Colorado, prepared for Denver Water by Woodward Clyde, May 1996.

Technical Report - a Compilation of Technical Information Prepared Throughout the Execution of a Drainage and Flood Control Planning Study for a Project Area along South Boulder Creek in Boulder County, Colorado, Oblinger-Smith Corporation, @ 1975.

Urban Storm Drainage Criteria Manual, Volume 1, Urban Drainage and Flood Control District, Wright McLaughlin Engineers, March 1969.

Urban Storm Drainage Major Drainageway Planning, South Boulder, Wright McLaughlin Engineers, September 1970.

Urban Storm Drainage Management, John R. Sheaffer, Kenneth R. Wright, William C. Taggart, Ruth M. Wright, Marcel Dekker, Inc., 1982.

Water and Related Land Resources Management Study, Vol. V, Appendix B - Flood Hazard Identification, U.S. Army Corps of Engineers, September, 1977.

SECTION VII

RAINFALL MEMORANDA AND RESPONSES, DRAFT REPORT REVIEW

- CITIZEN LETTER
- TEA APPROACH MEMO
- TWO LETTERS TO NOAA
- RETURN LETTER FROM NOAA
- RETURN FAX FROM NOAA
- JOHN HENZ LETTER
- LOVE & ASSOCIATES, INC. REVIEW

RECEIVED JUN 29 1999

June 25, 1999

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Taggart Engineering Associates, Inc.
2480 West 26th Ave., Suite 340-B
Denver, CO 80211

RE: South Boulder Creek Hydrologic Analysis

Dear Mr. Taggart,

It was good to meet you at the recent meeting of parties working on the South Boulder Creek hydrologic analysis. As I mentioned to you, I am a homeowner in the effected area and also a meteorologist with expertise in the hydrological cycle. Enclosed is a copy of a brief assessment by the National Research Council of the National Academy of Sciences regarding the issue of probable maximum precipitation estimates that you will use in your calculations. The assessment concludes that, despite some weaknesses, these maps of probable maximum precipitation (PMP) by the NOAA Office of Hydrology are still the best source for such estimates. Indeed, the report concludes that the use of PMP is a very conservative standard and recent paleohydrologic analysis of the Rockies indicate this procedure is consistent with flood events in this region back to the last 10,000 years.

The PMP maps for the western U.S. are available at the DOC/NOAA library in Boulder and are also now available digitized on the web at the western regional climate center at site www.wrcc.dri.edu/pcpnfreq.html. These maps are from 1973 and so I checked with the NOAA Office of Hydrology to see if an update was imminent. Although the Office of Hydrology would like to update the maps, an update is not likely for another 3-5 years. There are 20 years of automated raingauge data for the area, but I do not know if these data are digitized nor if doing a PMP for these data is in your scope of work. I doubt it would be very helpful to analyze these data, since there have been no great flood events in the last 20 years on South Boulder Creek. I understand these data are held by the Denver Urban Storm and Drainage District. If you are going to do a local PMP for these data, I would be interested in participating.

Daily rainfall data for Boulder are available on our web site at www.cdc.noaa.gov/Boulder.data.daily.html. These data are from a site in downtown Boulder. For the 5-8 May 1969 flood, they show that event was a multi-day event with daily rainfall totals of 1.25, 1.75, 3.37, and 1.00 inches of rain on each day. Weather watcher reports from south Boulder (unofficial) show 3-day totals of just greater than 9.00 inches of rain total for 5-7 May of 1969, slightly greater than in downtown Boulder, but not

extraordinarily different. The state climatologist has compiled a report on storms that exceed the 100-year event and reports a maximum of 15 inches over 4 days (Colorado Extreme Storm Precipitation Data Study, Climatology report #97-1). The most extreme rainfall event recently along the front range was the Fort Collins flood of a 28 July 1997. A detailed summary of this event was recently published in the Bulletin of the American Meteorology Society and I can provide you a copy of this. This event is considered to have a return frequency of between 500-1000 years. I have copies of both of these reports.

If I can be of any additional assistance, please do not hesitate to contact me. I have also included a copy of my business card, although I am writing to you here as a Boulder resident.

Sincerely,



John J. Bates, Ph.D. Meteorology
862 Cypress Dr.
Boulder, CO 80303

Attachments included

Xc: Mr. Alan Taylor, City of Boulder
Mr. Rich Lopez, Deputy Mayor



MEMORANDUM

TO: Bill DeGroot, P.E.
Urban Drainage and Flood Control District

FROM: Bill Taggart, P.E. *WET*
Walt Hime, *W.H.*

DATE: July 22, 1999

RE: South Boulder Creek - Proposed Draft Approach to Rainfall Volume
and Comparison with Previous U. S. Army Corps of Engineers
Assumptions

This memorandum provides proposed rainfall volume data to be used in the Hydrologic Analysis of South Boulder Creek. The existing U. S. Army Corps of Engineers (USACE) hydrology used only the 6 hour duration NOAA rainfall, which was distributed by their own methodology rather than preserving the other NOAA statistics for peak 5 minute to 3 hour values. Thus their methodology does not agree with the District or Boulder Criteria. Our previous investigation indicated that rainfall was underestimated. Thus, rainfall data used in the existing USACE hydrology is presented for comparison. The following numbers should be taken as a draft as we haven't worked on correcting the basin areas, double checked all the numbers, and are reviewing the literature regarding the proper use of area reduction factors and storm rainfall distributions.

PROPOSED RAINFALL

The South Boulder Creek hydrologic analysis will be based on existing NOAA rainfall information. For areas within the Urban Drainage and Flood Control District, the analysis will be based on the Urban Storm Drainage Criterial Manual and Boulder Manual rainfall information with adjustments for the larger watershed. Basically a 24 hour duration storm with the 2 hour Boulder storm imbedded in the event and other NOAA statistics for intermediate durations will be preserved (e.g. 6hr, 3hr). Rainfall will be bracketed by rough elevation ranges following the four Boulder zones to reflect the large altitude range of the watershed. Custom data for the highest zone IV will be used rather than using zone III data for zone IV per the Boulder Manual.

Rainfall above Gross Reservoir will be adjusted by NOAA reduction factors based on the entire watershed area. Rainfall below Gross will be adjusted based on the area downstream of the reservoir

We are still considering the use of a total 6 hour event versus a total 24 hour event. Based on previous USACE modeling, the time from the beginning of peak rainfall to peak runoff at Boulder Creek is 2.5 hours, though we suspect a longer lag of 3 to 3.5 hours with better stream routing. The flow from above Gross is delayed about 4 hours. The peak flow into Gross lags peak rainfall about 3 hours, with about 5.25 hours of lag immediately below Gross. Thus, a 6 hour duration event may not truly reflect runoff response at the mouth from the most distant parts of the basin. A 6 hour duration event would presumably use a larger area reduction factor, and thus reduce the model rainfall. A larger 24 hour duration event would have both greater total rainfall and a smaller area reduction factor. It would have more volume, but we doubt any significant difference in peak flows in the study area.

USACE RAINFALL

The rainfall values used in the USACE study were obtained from the NOAA Precipitation-Frequency Atlas of the Western United States, Atlas 2, Volume III, Colorado. Adjustments for depth-area were based on NOAA depth-area relationships. Adjustments for the length of record were made using Beard's table of expected probability adjustments for various lengths. Spatial variation was accounted for by the use of several hyetographs. USACE reported that the time variation of the 6 hour rainfall for each hyetograph was based on a study of hourly precipitation data recorded for the South Platte River basin. They presented a ratio table but no documentation. One-half hour intervals were used to distribute the rainfall.

TEA COMPARISON TABLE

The following table presents our first draft of rough rainfall volume in terms of inches and Acre-Feet for the suggested methodology and the previous USACE work. We suggest you and the sponsor carefully review and concur or direct adjustments. At the following meeting we hope to present detailed rainfall distributions. Our basic intent is to place the peak rainfall 2 hour duration storm in the manual at time 6 hours (25% of the total duration) with alternating lesser values about this peak, until hour 12, which will be followed by remaining descending values to the end of the 24 hours. This somewhat departs from suggestions in the Manual to place the peak 2 hour values first. We feel it is more realistic to have more rain in front of the peak to reflect wet ground conditions often experienced in floods.

SOUTH BOULL CREEK POINT RAINFALL

100 YR EVENTS

	ZONE 1 <8000 FT		ZONE 2 8000-8000		ZONE 3 8000-10,000 FT		ZONE 4 >10,000 FT		TOTAL BASIN	
	TEA	BEL GROS AB GROSS	TEA	TEA	TEA	TEA	TEA	TEA	TEA	TEA
ACRES	11458.00	15552.00	3392.00	43328.00	13248.00	86976.00	135.90			
SQ MI	17.90	24.30	5.30	67.70	20.70					
5 MIN DUR RAIN (IN)	0.763	0.708	0.708	0.821	0.534	0.648				
30 MIN DUR RAIN	2.133	1.928	1.928	1.891	1.454	1.784				
1 HR DUR RAIN	2.700	2.440	2.440	2.140	1.840	2.233				
2 HR DUR RAIN	3.120	2.820	2.820	2.470	2.127	2.580				
6 HR DUR RAIN	3.800	3.200	3.200	2.800	2.068	3.088				
24 HR DUR RAIN	5.000	4.500	4.500	4.400	3.900	4.401				
5 MIN DUR VOL (ACFT)	748	917	200	2241	589	4694				0.648
30 MIN DUR VOL	2036	2498	545	6104	1605	12768				1.784
1 HR DUR VOL	2578	3162	690	7727	2031	16188				2.233
2 HR DUR VOL	2979	3655	797	8918	2348	18697				2.580
6 HR DUR VOL	3628	4147	905	10832	2870	22382				3.088
24 HR DUR VOL	4773	5862	1300	15867	3974	31897				4.401

AVG RAINFALL	
TEA	0.648
	1.784
	2.233
	2.580
	3.088
	4.401

SOUTH BOULDER CREEK ADJUSTED RAINFALL

100 YR EVENTS

	ZONE 1 <8000 FT		ZONE 2 8000-8000		ZONE 3 8000-10,000 FT		ZONE 4 >10,000 FT		TOTAL BASIN	
	TEA	BEL GROS AB GROSS	TEA	TEA	TEA	TEA	TEA	TEA	TEA	TEA
ACRES	11458.00	15552.00	3392.00	43328.00	13248.00	86976.00	135.90			
SQ MI	17.90	24.30	5.30	67.70	20.70					
% AREA TEA	13.17%	17.89%	3.90%	11.18%	15.23%	17.93%				
% AREA CORP	9.90%	8.43%	15.69%	49.82%	48.16%					
5 MIN DUR RAIN (IN)	0.744	0.672	0.656	0.775	0.575	0.606				
30 MIN DUR RAIN	2.076	1.831	1.787	1.315	1.214	1.347	1.010	1.650	1.147	
1 HR DUR RAIN	2.585	2.318	2.282	1.845	1.518	1.994	1.395	1.706	2.089	1.433
2 HR DUR RAIN	2.984	2.879	2.814	2.270	2.000	2.390	1.925	1.972	1.735	1.977
6 HR DUR RAIN	3.610	3.040	2.988	3.285	2.900	2.781	2.785	2.410	2.285	2.823
24 HR DUR RAIN	4.750	4.370	4.284	4.078	4.078	3.337	4.114			
5 MIN DUR VOL (ACFT)	710	871	185	784	2077	548	4390			
30 MIN DUR VOL	1934	2373	505	794	2072	1488	11959			
1 HR DUR VOL	2449	3004	639	981	2591	1863	15139			
2 HR DUR VOL	2830	3472	739	1353	3574	2177	17485			
6 HR DUR VOL	3446	3940	839	1858	5718	2961	20827			
24 HR DUR VOL	4535	5984	1205	3219	14727	3684	28815			
% VOL TEA	15.21%	19.00%	4.04%	9.80%	16.12%	12.36%	14.52%			
% VOL CORP										

AREA REDUCTION FACTOR ABOVE GROSS = 0.927

0.96

AREA REDUCTION FACTOR BELOW GROSS = 0.96

AREA REDUCTION FACTORS AND MISC DATA STILL TO BE CHECKED
EXACT CORP ELEVATION BOUNDARIES UNKNOWN



DRAFT
SUBJECT TO CHANGE UPON CHECKING AND REVISIONS
TEA AND CORP ELEV BREAKDOWN ROUGH

07/22/99

EMAIL →

LESLIE, JULIAN @ NOAA, GO



TAGGART

ENGINEERING ASSOCIATES, INC.

2480 West 28th Avenue, Suite 340-B

Denver, Colorado 80211

(303)455-3800 FAX 455-9929

Mr. Gird,

Below is our initial rainfall approach for a hydrologic study for the South Boulder Creek watershed. The previous hydrology was accomplished by the U. S. Army Corps of Engineers. Within the following memo, please find our rationale, questions, and concerns. Highlighted sections are used to note that we are specifically looking for feedback.

This memorandum provides proposed rainfall volume data to be used in the Hydrologic Analysis of South Boulder Creek. The existing U. S. Army Corps of Engineers (USACE) hydrology (1986) used only the 6 hour duration NOAA rainfall, which was distributed by their own methodology rather than preserving the other NOAA statistics for peak 5 minute to 3 hour values. Thus their methodology does not agree with the District or Boulder Criteria, or NOAA as we understand it. Our previous investigation indicated that rainfall was underestimated. Thus, rainfall data used in the existing USACE hydrology is presented for comparison. The following numbers should be taken as a draft as we haven't worked on correcting the basin areas, double checked all the numbers, and are reviewing the literature regarding the proper use of area reduction factors and storm rainfall distributions.

PROPOSED RAINFALL

The South Boulder Creek hydrologic analysis will be based on existing NOAA rainfall information. For areas within the Urban Drainage and Flood Control District, the analysis will be based on the Urban Storm Drainage Criterial Manual and Boulder Manual rainfall information with adjustments for the larger watershed. Basically a 24 hour duration storm with the 2 hour Boulder storm imbedded in the event and other NOAA statistics for intermediate durations will be preserved (e.g. 6hr, 3hr). Rainfall will be bracketed by rough elevation ranges following the four Boulder County elevation zones to reflect the large altitude range of the watershed. Point rainfall will be taken from the NOAA atlas at the centroid of each of the four zones. Custom data for the highest zone IV will be used rather than using zone III data for zone IV per the Boulder Manual. (See attached DXF file for basin map).

We are still considering the use of a total 6 hour event versus a total 24 hour event. Based on previous USACE modeling, the time from the beginning of peak rainfall to peak runoff at Boulder Creek is 2.5 hours, though we suspect a longer lag of 3 to 3.5 hours with better stream routing. The flow from above Gross is delayed about 4 hours. The peak flow into Gross lags peak rainfall about 3 hours, with about 5.25 hours of lag immediately below Gross. Thus, a 6 hour duration event may not truly reflect runoff response at the mouth from the most distant parts of the basin. A 6 hour duration event would presumably use a larger area reduction factor, and thus reduce the model rainfall. A larger 24 hour duration event would have both greater total rainfall and a smaller area reduction factor (ARF). It would have more volume, but we doubt any significant difference in peak flows in the lower study area.

We are concerned with flooding in Boulder from the perspective of peak flows and volume. Peak flows are dominated by the area (40 square miles) and rainfall below Gross reservoir, which is located approximately 18 miles upstream of the mouth of South Boulder Creek in Boulder. Since some of the solutions to potential flooding in Boulder might involve storage, we are also concerned with runoff volume from the entire watershed. Therefore, our approach to "design rainfall" includes using appropriate rainfalls by elevation zones and location above or below Gross.

Rainfall above Gross Reservoir will be adjusted by NOAA area reduction factors (ARF) based on the entire watershed area. Rainfall below Gross will be adjusted based on the area downstream of the reservoir.

Conventional approach would apply the 24 hr duration area reduction factors to all increments within the design event. We are researching TP 29 to confirm this approach, but wonder if we should be using different area reduction factors for the various durations within the storm, (e.g. use the 1 hr duration area reduction factor curve for the peak rainfall between 1 hr and 2 hr durations, or using another approach.) Table 1 compares two options we see for use of the ARF's with the factors and rainfall used by the Corps.

USACE RAINFALL

The rainfall values used in the USACE study were obtained from the NOAA Precipitation-Frequency Atlas of the Western United States, Atlas 2, Volume III, Colorado. Adjustments for depth-area were based on NOAA depth-area relationships. Adjustments for the length of record were made using Beard's table of expected probability adjustments for various lengths. Spatial variation was accounted for by the use of several hyetographs. USACE reported that the time variation of the 6 hour rainfall for each hyetograph was based on a study of hourly precipitation data recorded for the South Platte River basin. They presented a ratio

table but no documentation. One-half hour intervals were used to distribute the rainfall.

TABLE 1

	USACE	TEA ALT 1 (IF ADJUST ALL DURATION BY CONTRAST ARF)	TEA ALT 2 (IF ADJUST GIVEN DURATION BY ARF FOR THAT DURATION)
ZONE 1 100 YR RAINFALL PER NOAA AND BOULDER CRITERIA (IN)	2.70 1HR 3.80 6HR	2.70 1HR 3.80 6HR	2.70 1HR 3.80 6HR
ADJUSTMENT FACTOR FOR THE 1 HR RAINFALL	.64 (ADJUSTMENT FACTOR FOR THE PEAK 1 HR DURATION BASED ON DEPTH-AREA REDUCTION AND EXPECTED PROBABILITY ADJUSTMENT)	.95 (ADJUSTMENT FACTOR BASED ON 24 HR DEPTH-AREA CURVE)	.82 (ADJUSTMENT FACTOR BASED ON 1 HR DEPTH- AREA CURVE)
ADJUSTMENT FACTOR FOR THE 6 HR RAINFALL	.913 (ADJUSTMENT FACTOR FOR THE PEAK 6 HR DURATION BASED ON DEPTH-AREA REDUCTION AND EXPECTED PROBABILITY ADJUSTMENT)	.95 (ADJUSTMENT FACTOR BASED ON 24 HR DEPTH-AREA CURVE)	.935 (ADJUSTMENT FACTOR BASED ON 6 HR DEPTH- AREA CURVE)
ZONE 1 CORRECTED RAINFALL (IN)	1.73 1HR 3.47 6HR	2.57 1HR 3.61 6HR	2.21 1HR 3.55 6HR

The USACE rainfall values would be closer to rainfall values obtained by applying varying area reduction factors for critical duration to incremental rainfall (TEA ALT2), e.g. using the 1 hr duration area reduction factor curve for the peak rainfall between 1 hr and 2 hr durations. Again we are researching the proper way to apply the Area Reduction Factor, and are interested in your advise.

TEA COMPARISON TABLE

The following table presents our first draft of rough rainfall volume in terms of inches and Acre-Feet for the suggested methodology and the previous USACE work. (See attached spreadsheet)

RAINFALL DISTRIBUTION

Our basic intent is to place the peak rainfall 2 hour duration storm in the Manual at time 6 hours (25% of the total duration) with alternating lesser values about this peak, until hour 12, which will be followed by remaining descending values to the end of the 24 hours. This somewhat departs from suggestions in the Manual to place the peak 2 hour values at the start of the design storm with the peak increment at 30 minutes. We understand the Manual distribution was determined from an analysis of the Stapleton Gage. We feel it is more realistic in terms of the size (140 square miles) and setting (mountains, foothills to plains transition) to have more rain in front of the peak to reflect wet ground conditions often experienced in floods.

QUESTIONS CONCERNING THE "DESIGN STORM"

For the following questions, please feel free to comment and make alternative suggestions as you see fit. Please recognize that we are under a constrained budget.

- 1) Do you agree with using 4 elevation zones as identified by Boulder County and picking point rainfall values from the centroid of each zone from the NOAA Atlas?
- 2) Do you agree with adjusting point rainfall for each zone by either the "above Gross area reduction factor" (represents entire watershed) or by the "below Gross area reduction factor" (represents basin area below Gross)?
- 3) Do you agree with the approach of using one 24 hr "design" event over the entire watershed, made up of rainfall for various elevation zones with all internal smaller durations, and area reduction factors as discussed?
- 4) Do you agree with using a 2 hour storm imbedded in a 24 hour storm to account for peak flow and flood volume? The NOAA rainfall values for various durations would be imbedded also .
- 5) Do you agree with placing the 2 hour storm peak at 6 hours (25% of the total duration) to allow for rainfall to wet the ground and decrease infiltration and allow more of the watershed to contribute to the peak, thus making a more conservative scenario?

6) Do you agree with applying the 24 hour area reduction factor curves for above and below gross to rainfall values for the various durations within the 24 hour event (TEA ALT1)? Or should we be adjusting various durations within the storm with different factors (TEA ALT2).

7) Do you agree with distributing alternating lesser values about the 2 hour storm peak, until hour 12, which will be followed by remaining descending values to the end of the 24 hours?

Thanks for your assistance,
V/R Walt Hime
Bill Taggart



September 9, 1999

Dr. Danny L. Fread
Director
Office of Hydrology
U.S. Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
1325 East-West Highway
Silver Spring, MD 20901-3283

RE: Your response of September 3, 1999 regarding South Boulder Creek Hydrology

Dear Dr. Fread:

We were disappointed in your letter, especially after we had e-mailed the request at the beginning of August, 1999 and had been told that the right person would be identified and would be able to respond. We are working for the Urban Drainage and Flood Control District in sponsorship with the City of Boulder, Boulder County and the University of Colorado.

Fundamentally, we were asking questions about NOAA documents and points at which the application of NOAA/NWS data is unclear. We would appreciate answers to our questions, including:

1. TP29, Part 1 puts forward two curves for area reduction factors for the 1 and 24 hour durations. Later Parts 2-4 indicated added curves for other durations, which are explained to be interpolated with no discussions as to how the interpolation was made. Questions:
 - a. How were the interpolations made for the other durations?
 - b. Is it still appropriate to use these curves, as indicated in your atlas for Colorado?
 - c. In some cases engineers in this region use one area reduction factor over all values in the design storm. Thus if they think a 6 hour duration event is critical to the watershed response, then they use the one area reduction factor for all internal rainfall (e.g., the NOAA 1 hour rainfall is corrected by the 6 hour area reduction factor). What is the correct procedure?
 - d. We intend to use a 24 hour duration design event so that we are

sure the entire watershed is responding. We also intend to make sure that the design event has internal "duration" (e.g. 30 min., 1 hr., 3 hr., 6 hr.) rainfall that corresponds to the NOAA Colorado Atlas. This would require application of varying area reduction factors that result in the correct amounts for each of the durations. Do you agree and/or do you have directions on the use of the NOAA atlases to deduce the design rainfall? Please be specific in your response.

2. What is the correct or best procedure to derive a "design" rainfall event (e.g. the temporal pattern) from the Colorado Atlas?
3. Do you believe the Colorado NOAA Atlas is the best source for rainfall design data? If not, what is?
4. What, if any, are NOAA's current actions and plans for revising or refining the Colorado Rainfall Atlas and preparation of design guidelines?
5. Since we don't have the raw data or the detailed analysis behind the preparation of the atlas, and NOAA does, and since much of the watershed is in the mountains, we are specifically asking you to indicate the reliability of the atlas in the mountains, and how we should apply the atlases. In our previous memo we discussed that much of the mountain area is tributary to Gross Reservoir, which even if full, has a substantial routing effect. Our thoughts were to use an area reduction factor below Gross that was based on that lower area (35 to 40 square miles), which would result in a small rainfall correction and thus larger peaks than if we used the area reduction factor for the entire watershed. For the area above Gross we were going to use the area reduction factor for the entire watershed (130-140 square miles). This seemed especially reasonable considering the altitude range. Again, we don't have NOAA's data or its analysis of the effects of altitude. Do you agree that our approach would result in a reasonable application of NOAA's Colorado Atlas? If not, what do you suggest?
6. The Corps of Engineers in 1977 used the NOAA atlas hour values, but state that they didn't use the 1 hour values based on their examination of Front Range events. This has created a significant issue that led to this restudy. Based on many rainfall events in the last years, and the level of work apparent in the NOAA atlas, it seems very likely that the Corps' "judgment" is incorrect and that NOAA's atlas values are more realistic. Perhaps NOAA's values are also low based on the Fort Collins 1997 event and recent Front Range rainfalls. We believe it is most reasonable to use the NOAA values, with due recognition that future restudies are likely to

Dr. Danny L. Fread
September 9, 1999
Page 3

increase rainfall. Do you agree or what would you suggest?

I would much appreciate your response, especially as these are questions regarding a key government document to which only NOAA has the data, analysis, and knowledge.

Sincerely,

TAGGART ENGINEERING ASSOCIATES, INC.



William C. Taggart, P.E.

RECEIVED SEP 16 1999



U.S. DEPARTMENT OF COMMERCE
National Oceanic and Atmospheric Administration
NATIONAL WEATHER SERVICE
1325 East-West Highway
Silver Spring, Maryland 20910-3283

SEP 03 1999

Mr. Bill Taggart
Taggart Engineering Associates, Inc.
2480 West 26th Avenue, Suite 340-B
Denver, Colorado 80211

Dear Mr. Taggart:

Thank you for the opportunity to review your memorandum and proposed rainfall analysis for the Hydrologic Analysis of South Boulder Creek. To answer the questions you have raised would require our doing work outside of the scope of what Congress has authorized for us. Our office acts as a neutral agency in establishing rainfall spatial and temporal distribution characteristics for design purposes. The application of this information is at the discretion of various other government and private organizations in hydrometeorological community.

Possible alternatives for review of your study might be meteorological consultants or the academic community. We regret that we are not in a position to assist you at this time.

Sincerely,

A handwritten signature in black ink, appearing to read "Danny L. Fread".

Danny L. Fread
Director
Office of Hydrology

cc:
Walt Hime
Ron Gird



Printed on Recycled Paper





U.S. DEPARTMENT OF COMMERCE
National Oceanic and Atmospheric Administration
NATIONAL WEATHER SERVICE
 1325 East-West Highway
 Silver Spring, Maryland 20910-3283

SEP 29 1999

Mr. Walt Hime
 Taggart Engineering Associates, Inc.
 2480 West 26th Avenue, Suite 340B
 Denver, Colorado 80211

Dear Mr. Hime:

The questions you asked are scientifically valuable and are subject to considerable professional judgment. The best available rainfall data and statistical analysis were used to generate the documents in question.

The National Weather Service (NWS), Office of Hydrology, Hydrometeorological Design Studies Center (HDSC), lead by Dr. Lesley Julian ((301) 713-1669 x109), has reviewed your most recent letter. The information enclosed addresses those questions falling within the responsibilities of the HDSC mission. I hope the information provided sufficiently addresses your concerns on these issues.

Sincerely,

Danny L. Fread
 Director
 Office of Hydrology

Enclosure



Response to Taggart Letter Dated September 9, 1999

1.
 - a. The interpolations for other durations (3 hours and 6 hours) were done using the 1- and 24-hour curves. The 30-minute curve is based on short-record data from Muskegum, Ohio [see TP 29, Part 1, Section II Applications, item 62, page 15].
 - b. As you can tell from TP 29, Part 1 [Figure 1-5, page 10], the dense gauge networks from which the curves were developed, are all in the Midwest or East. Subsequent evaluations found little or no regional variation. These curves are applicable in Colorado, using appropriate professional judgment. However, for short durations, usually convective storms, you may want to look at *NOAA Technical Memorandum NWS Hydro 40, Depth-Area Ratios in the Semi-Arid Southwest United States* (Zehr & Myers 1984).
 - c. This seems a reasonable approach, based on local knowledge and professional judgment.
 - d. Your approach seems reasonable.
2. For a "design" rainfall event, the temporal distribution is not addressed in NOAA Atlas 2; but is covered in *NOAA Technical Report NWS 27, Interduration Precipitation Relations for Storms - Western United States* (Frederick et al 1981). In addition, you can consider the rainfall timing effects on the basin for your area. You can test the effects of front, middle, and end loading for the response of the stream/basin, and decide which is most critical to your purpose.
3. NOAA Atlas 2 - Colorado is the best source at present. NWS is in the process of updating Technical Paper 40 (precipitation frequencies for the Midwest and Eastern U.S.) and NOAA Atlas 2 for the Western U.S. However, Colorado will not be completed for 2 to 3 years.
4. See 3.
5. For dividing up a basin into sub-basins, see the *Flood Hydrology Manual*, U.S. Department of the Interior, Bureau of Reclamation (1992) pages 59-61. It is important to remember that storm volume depends on the entire basin. The sum of the sub-basin volumes cannot exceed the total basin volume. At the risk of being obvious, the procedure is to compute the total (T) basin (South Boulder Creek Basin) volume ($\text{Volume}_T = \text{Area}_T \times \text{Depth}_T$); then compute the volume of the sub-basin (e.g., below Gross Reservoir) of interest in the same way. To find the volume of the other sub-basin (all but "below Gross Reservoir"), subtract the sub-basin volume of "below Gross Reservoir" from Total basin volume.
6. We agree that it is reasonable to use the NOAA Atlas 2 values at this time.

HENZ METEOROLOGICAL SERVICES
1401 West Dry Creek Road
Littleton, Colorado 80120
303.458.1464

Dear Mr. DeGroot:

Per your request I have reviewed and evaluated the attached letter sent by Walt Hime and Bill Taggart of Taggart Engineering Associates on their initial approaches to rainfall for a hydrologic study for South Boulder Creek. I discussed my findings with you at a meeting on August 26, 1999. This letter provides a summary of our discussion points and my evaluation.

Basic Premise of Taggart Approach appears valid

First, the "Taggart" approach is a reasonable attempt to improve on the previous approach utilized by the U. S. Army Corps of Engineers in their Hydrologic Analysis of South Boulder Creek (COE approach). The Taggart approach does not propose radical departures from the prior study. Rather, it proposes reasonable scientific adjustments that are sensitive to the unique meteorological and hydrological characteristics of South Boulder Creek. However, Henz Meteorological Services would like to make the following observations on the techniques proposed, provide several reasonable adjustments to the Taggart approach and address each of the questions posed at the end of their letter.

General observations relative to either the COE or Taggart approaches

NOAA Atlas II is old, needs revision and relies on a database that consists of station records that are less than 25 years in duration for over 68 percent of the records.

The primary observation is that the approach relies on the validity of the 100-year 1-hr, 3-hr, 6-hr, 12-hr and 24-hr rain events as described for Boulder County and the South Boulder Creek basin in NOAA Atlas II, Precipitation-Frequency Atlas of the Western United States. This atlas was published in 1973 and the Colorado analyses are based on the records of 346 rain gauges in the state. Of these gauges only 109 gauges or 31.5 percent had a period of record greater than 25 years. Another 25 years plus of rainfall events have occurred since the publication of NOAA Atlas II and it is in dire need of updating. Several Western states have already had their sections of the precipitation-frequency atlas updated with many surprising results. A weakness of any study accomplished on South Boulder Creek will be the short duration of the database it relies on and the asymmetric rainfall distributions, which have occurred since 1973.

The meteorology of the basin supports the inclusion of thunderstorms as the primary source of rainfalls of six-hour or less duration.

My experiences with rainfall events in the Boulder basin as the primary meteorological service for the Urban Drainage & Flood Control's Flash Flood Prediction Program spans 21 years from 1979 to present. I have been an operational meteorologist along the Front Range since 1968 and become a published expert on both Colorado precipitation and Front Range thunderstorm and precipitation events. I would like to emphasize that most intense 6-hour rainfall events are associated with multi-cell thunderstorm systems that become stationary or move very slowly either up or down the basin. A multi-cell thunderstorm will create two rainfall peaks during a 2-3 hour period.

Most heavy thunderstorm events occur on Day Two or Day Three of a four to six day period of monsoon generated storminess.

In my experience over 80 percent of the thunderstorm rainfall events occurring from June to August are preceded by 24 to 48 hours of either thunderstorms or general rainfall. These conditions frequently make for nearly saturated soil conditions in foothills basins prior to a major event. Two notable exceptions to this observation are the Big Thompson Flash Flood of 1976 and the Frijole Creek Flash Flood of 1981 which were singular precipitation events following a near-drought period.

Additionally, very efficient general upslope rainfall with no thunderstorms could produce a six-hour or less flooding event if the conditions were proper. Steady rain rates of 0.50" to 0.75" per hour could be sustained for periods of 6 hours or more. Fortunately, while the storm total rainfall would be similar to a thunderstorm event, the temporal distribution of the upslope rainfall would be more evenly distributed than that observed with a thunderstorm event.

Suggested improvements to the proposed Taggart approach

HMS suggests that three improvements be considered to the Taggart approach related to the temporal distribution, aerial distribution and antecedent moisture conditions of the rainfall event. The temporal and aerial distribution improvements are based on two recent near-100 year precipitation events observed in the South Boulder Creek basin during 1998 and 1999. The improvements are based on using the observed temporal, aerial and intensity distributions of these two rain events to provide guidance on the distributions.

The antecedent moisture improvement is related to a study accomplished by George Sabol and John Henz for the District that provided guidance to assist in the prediction of flash floods in the District foothills. One aspect of the study dealt with the effects of saturated soils on runoff in the basins.

Temporal distribution of 100-year rainfall event could be modeled on two recent storm events observed in South Boulder Creek's basin.

The Taggart approach has advocated using either a 2-hour event embedded in a 6-hour or 24-hour event or the standard NOAA 3-hour, 6-hour and 12-hour distributions in a 24-hour event. First, HMS advocates the use of a 24-hour rain event with a 100-year 6-hour event embedded in the second twelve hours of the 24-hour event. The 24-hour event that begins at 9PM on Day 1 and ends at 9PM on Day 2. The 24-hour period chosen allows two periods of convective rainfall over the basins in a manner similar to the recent Fort Collins Flash Flood of July 27, 1997.

A general overnight rain of 1.00"-1.50" is distributed over the entire basin from 9PM, Day 1 to 9AM, Day 2. No rain will fall from 9AM to 3PM on Day 2. A six-hour 100-year event will be distributed from 3PM-9PM on Day 2. These suggestions are very similar to the existing Taggart approach and could be easily accommodated. *really* Please note that the 100-year, 1-hour event is 2.70" while the 100-year, 6hour event is 3.80". The observed rainfall from the two storms cited in this section closely approximate these 100-year values.

The temporal distribution of the key 6-hour event could be modeled on the observed rainfall from two key events:

A westward-moving evening thunderstorm observed in South Boulder Creek's basin on July 8, 1998 provides the temporal distribution for the most intense portion of the embedded 6-hour thunderstorm event. This storm produced a District measured 2.76"/45 min rainfall and a radar estimated 4.5"-5.5"/3 hours. The peak rainfall was observed in the lower portions of South Boulder Creek below Goss reservoir. It covered an estimated 25 square miles of the lower basin with the heavy rain and moved over the upper basin before dissipating. **The observed 2.76"/45minutes exceeds the 100-year, 1-hour intensity and would provide a good temporal model for the most intense hour of rainfall.**

A general rain event with embedded thunderstorms was observed on August 4, 1999 in South Boulder Creek's basin which dropped a lower basin average of 3.07"/6 hours and an upper basin average of 2.36" of rain. This event could provide valuable information on the temporal distribution of rainfall in the lower versus the upper portions of the basin. If this distribution were used in concert with the most intense 1-hour values from the July 8, 1998 storm, a realistic temporal distribution could be obtained for use in the Taggart approach.

While the observed 6-hour rain totals of 3.07" are only about 80percent of the 3.80"/6-hour values recommended, they could provide the realistic temporal guidance and resolution for the temporal rain distribution.

Aerial distribution of 100-year rainfall event could also be modeled on two recent storm events observed in South Boulder Creek's basin.

The Taggart approach also expressed concern about the aerial distribution of event rainfall in lower basin versus the upper basin and for four elevation zones. The general rain event with embedded thunderstorms offers a good model for the aerial rainfall distribution.

An example of a recent rain event which approximates a 6-hour event which is 80 percent of a 100-year, 6-hour event can be found on August 4, 1999. Table 1 shows the observed rainfall in the South Boulder Creek Flood Detection Network. This event suggests that the rainfall in the lower portion of the basin below Gross Reservoir was 30 percent more than the observed rain fall in the upper basin above Gross reservoir.

Table 1 Rainfall observed in South Boulder Creek on August 4, 1999.

GAUGE NUMBER		RAINFALL 15L - 21L
# 1	4090	3.19"
# 2	4100	2.24"
	4110	2.01"
	4730	2.09"
	4360	2.28"
Average Rainfall =		2.36"
Average Rainfall =		
	4010	3.07"
	4020	2.68"
⇒	4030	3.15"
	4040	3.19"
	4050	2.95"
	4060	3.39"
Average Rainfall =		3.07"

HMS has predicted and then verified rainfall for its quantitative precipitation forecasts for over 10 years. The use of the August 4, 1999 storm to quantify both the aerial and temporal distribution of rainfall during a 100-year, 6-hour event is highly encouraged. It is suggested that the observed values be partitioned according to the four Taggart approach zones and used as identified above.

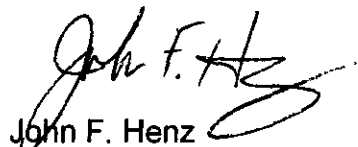
Antecedent moisture impacts on storm runoff due to saturated soil conditions could be based on the Sabol-Henz approach used to provide foothills flood guidance values to the District's Flash Flood Prediction Program.

HMS does not provide hydrologic consulting services, however, it wishes to remind the District of a foothills flood guidance tool prepared by Dr. George Sabol in cooperation with John Henz in 1992. This tool measures the escalating impact of the maximum average 1-hour, 10 square mile rainfall falling on four soil conditions ranging from very dry to saturated on the noted return frequency of the anticipated flooding. Figure 1 shows Figure III-1 of the Sabol and Henz report.

Please note that a 2.00" 1-hour rain on 10 square miles area would produce a 10-year flood if it fell on dry soil and a 100-year flood if it fell on saturated soil.

Finally, HMS recommends that the suggestions presented above be given serious consideration for inclusion into the Taggart approach for rainfall in South Boulder Creek basins study.

Sincerely yours,

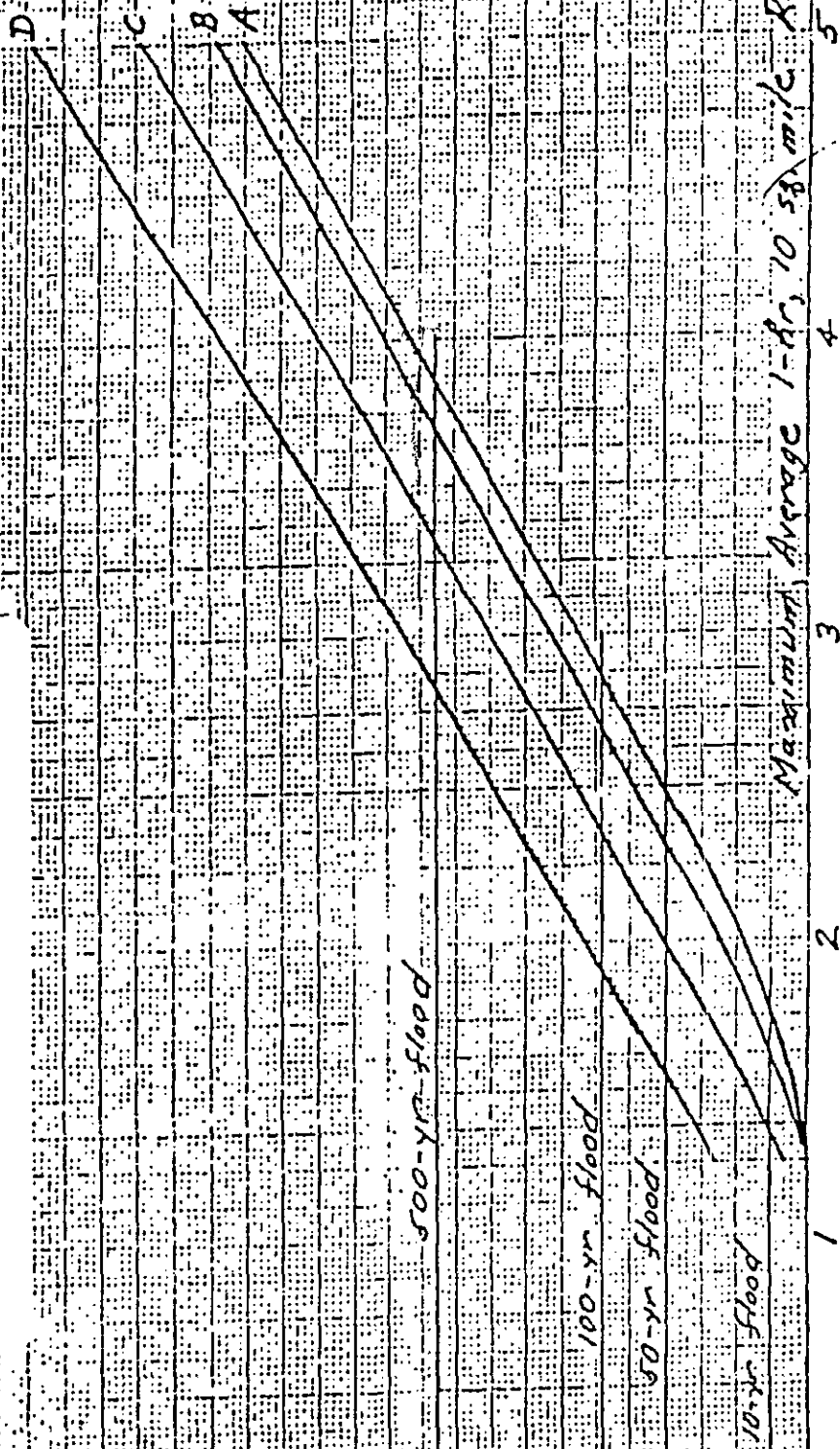


John F. Henz
Certified Consulting Meteorologist #270

FIGURE III-1

Mountain Canyon Flash Flood Guidance

- A - very dry, wilting point
- B - late summer and fall
- C - moist, field capacity
- D - early summer
- E - wet, greater than field capacity
- F - spring snowmelt
- G - saturated





July 12, 2000

841 Front Street
Louisville, Colorado 80027-1849
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E mail: loveassociates@tetter.com

Mr. Jeff Lipton
Director
Department of Facilities Management
University of Colorado at Boulder
Campus Box 53
Boulder, Colorado 80309-0053

REF: 2001B – South Boulder Creek Hydrology

Dear Jeff:

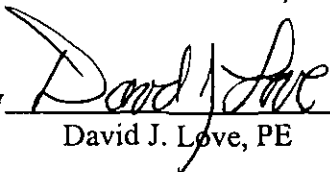
Bill Taggart has provided us additional explanations and documentation on stream flow modeling parameters utilized in his hydrology study of South Boulder Creek. We understand that he modified a few of these parameters in his current hydrologic model.

We concur with Taggart Engineering Associates (TEA) work and support their modeling efforts. We still believe that this hydrology shows 100-year discharges that are higher than what we would actually see in the creek during the 100-year event, since floodplain storage (dynamic stream flow routing) is not taken into account. This is beyond Taggart's current contract, however, a significant amount of storage occurs in the floodplain below the canyon mouth. Taking floodplain storage into account would decrease the size of the floodplain and the volume of storage required for the master plan alternates.

We would not have a problem with utilizing the TEA hydrology as currently drafted so long as the Project Sponsors recognize that it is conservative and that master planning efforts take this into account.

Sincerely,

LOVE & ASSOCIATES, INC.

By 
David J. Love, PE

SECTION VIII

ELDORADO GAGE AND GROSS RESERVOIR INFORMATION

MEMORANDUM

TO: Bill DeGroot, P.E.
Urban Drainage and Flood Control District

FROM: Bill Taggart, P.E.
Walt Hime, P.E.

DATE: August 12, 1999

RE: South Boulder Creek - Eldorado Springs Stream Gage and Gross Reservoir Initial Data

This memorandum provides information concerning two subjects (Eldorado Springs stream gage and Gross reservoir) that are significant regarding the Hydrologic Analysis of South Boulder Creek. The purpose for obtaining Eldorado Springs stream gage data is for simulating the 1969 flood for model calibration and possible statistical analysis. Review of the 1969 data indicates that the gage may not be reliable for high flow measurements. TEA is investigating how Colorado Division of Water Resources calculated flow rates during the May flood of 1969.

The current modeling approach is to assume Gross Reservoir full. However, review of Gross Reservoir data indicates that significant storage typically exists. During the month of June, when the reservoir is typically is at its fullest, an average of 7.7 % (3,219 Acre Feet) of the reservoir volume is still available for storage, not including surcharge. Thus, rainfall-runoff modeling above Gross may be overestimated if the reservoir is assumed full.

ELDORADO STREAM GAGE

The subject gage is a water-stage recorder in a metal box shelter and corrugated well. The gage is located 6.7 miles downstream of Gross Reservoir and 1.8 miles downstream of the South Boulder Canal Diversion which supplies water to Denver. The gage measures water that bypasses this diversion. Thus, the intent of the gage is to monitor water rights (per Mr. Bob Cooper at the Colorado Division of Water Resources). The control is a boulder sill downstream. The waterway is cobble and gravel lined upstream and downstream. High flows scour the channel, thus probably making accurate flood flow measurements unreliable. Review of gage height measurements and discharge recordings of South Boulder

Creek taken at the gage during the month of May 1969 raises many questions (see attachments). For example: the recorded daily average discharge for May 7 1969 was 1120 cfs with the max flow calculated to be 1690 cfs. However, the greatest flow recorded on the applicable rating curve (No. 19) is 542 cfs (see attached two example graphs). The first table is the Eldorado Springs gage height (and flow) daily summary for water year 68-69. Note the "S" for May 7, which indicates the flow is subdivided and which we believe is based on calculated flow not calibrated stream measurements. TEA plans to investigate how the May 7th flows were obtained and how the higher flows are determined. A new rating curve was used on May 8th indicating that the control changed. The 1969 calibration summary table specifically denoted the use of new rating table No. 19. Comparison of gage height and flows support the conclusion that the bed and control changed during the May 7, 1969 flood. Note that on September 9, 1969 there is a comment that the control changed 9-2-69. Similar notes are recorded on various dates. For example, the 1978 calibration summary table on 8-31-78 notes "Control washed down" and on 9-14-78 "Rocks missing in center of control."

We believe the highwater data for the Eldorado Gage and the basis of determining flood flows should be reviewed, however, the information used for general calibration / high mark comparison, but probably not as a rigid statistical basis test of the rainfall runoff modeling.

GROSS RESERVOIR

As previously discussed, Gross Reservoir is a water supply reservoir and not a flood control reservoir. Therefore, it is possible that the reservoir could be full at any time. Thus, the current modeling approach is to assume that the reservoir is full and that flood storage routing would be utilized above the spillway elevation. This is a conservative assumption for downstream flooding. The following sheets from Denver Water provide operating procedures for Gross and volume statistics for water years 1947-1991. The operating procedures came from the 1973 R.W. Beck study. Denver Water indicated that the same procedures are used today. The reservoir data indicates significant available volumes exist below the Gross spillway elevation. The statistics indicate that average storage available for months May thru August is 20% of the reservoir volume (8362 acre feet) with an average of 7.7% of the reservoir volume (3219 acre feet) available in June when the maximum volume of water is stored. The general operating plan is to store and regulate water imported through the Moffat Tunnel and native flows from South Boulder Creek. Prior to spring runoff, Denver Water historically draws down the reservoir level no lower than about 15,000 acre feet of storage. The reservoir is filled as fast as practicable in the spring. To avoid spilling at

volumes greater than 41,811 acre-feet, West Slope input is reduced as the reservoir is about to fill.

Review of stage records of Gross Reservoir during the flood of 1969 indicate that the reservoir did not spill. The storage went from 27,015 acre-feet to 32,500 acre-feet from May 5 to May 10.

We believe that Gross Reservoir significantly effects flood statistics downstream. The reported peak flows at the Eldorado Springs gage, which may be somewhat low, confirm this situation. It may be worthwhile to investigate reservoir level and available storage statistics and use joint probability risk assessment to show more available storage. For example, we could model the 100 yr rainfall (1% probability) with the 10 yr available volume (10% probability) which should be conservative and more realistic. A dichotomy which exists is the call for the use of Eldorado Springs Gage flood statistics but the direction for rainfall runoff modeling to use the assumption of Gross Reservoir being full.

REQUEST FOR DIRECTION

Do you wish us to:

- 1.) Continue researching the Eldorado Springs Gage high flow data and its basis of determination (backwater calculation, high water marks and calibrations at other locations; documentation on gage control sill damage, repairs, and bed movement)?
- 2.) Obtain the strip recorder data and conduct verification of peak flows and statistical analysis? Or do you want us to do step 1 and report back? (Note that we have a 60 hour budget for analysis of the Eldorado gage data of which 8 hours is used. Also we have a budget of 60 hours for 1969 flood calibration of which 10 hours is used.)
- 3.) Conduct statistical analysis of the Available Storage below the spillway at Gross Reservoir and refine an approach to the use of this data? (Note that we have no contract requirement or budget to conduct such work.)

Gross Reservoir



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Location:

On South Boulder Creek, 4 miles north of Wondervu, 35 road miles, (56 km) 26 airline miles northwest of Denver.

Route from Denver:

Colorado Highway 72, (Coal Creek Canyon) northwest to approximately 1 miles east of Wondervu, north on reservoir access roads.

Elevation:

Spillway crest - 7,285 feet, (2,220 m) above sea level.

Year completed:

1954

Type:

Gravity arch-concrete. Height - 340 feet, (103 m) above streambed.
Crest length - 1,050 feet, (320 m).

Facility value:

\$16,937,184

Function:

Stores and regulated western slope water coming from the Moffat Tunnel through South Boulder Creek before it goes on to the South Boulder Creek diversion to Ralston Reservoir and the Moffat Treatment Plant.

Capacity:

43,065 acre feet, (53,000,000 m³).

General:

The dam and reservoir are named for Dwight D. Gross, who served as a Chief Engineer of the Denver Water Department. Dedication was held August 2, 1955.
Some 627,559 cubic yards of concrete, representing 1,203 railroad carloads, were used in construction.

Recreation:

Shore fishing, picnic facilities available.

Hours:

4 A.M. to 9 P.M.

PLATTE RIVER BASIN

06729500 SOUTH BOULDER CREEK NEAR ELDORADO SPRINGS, CO

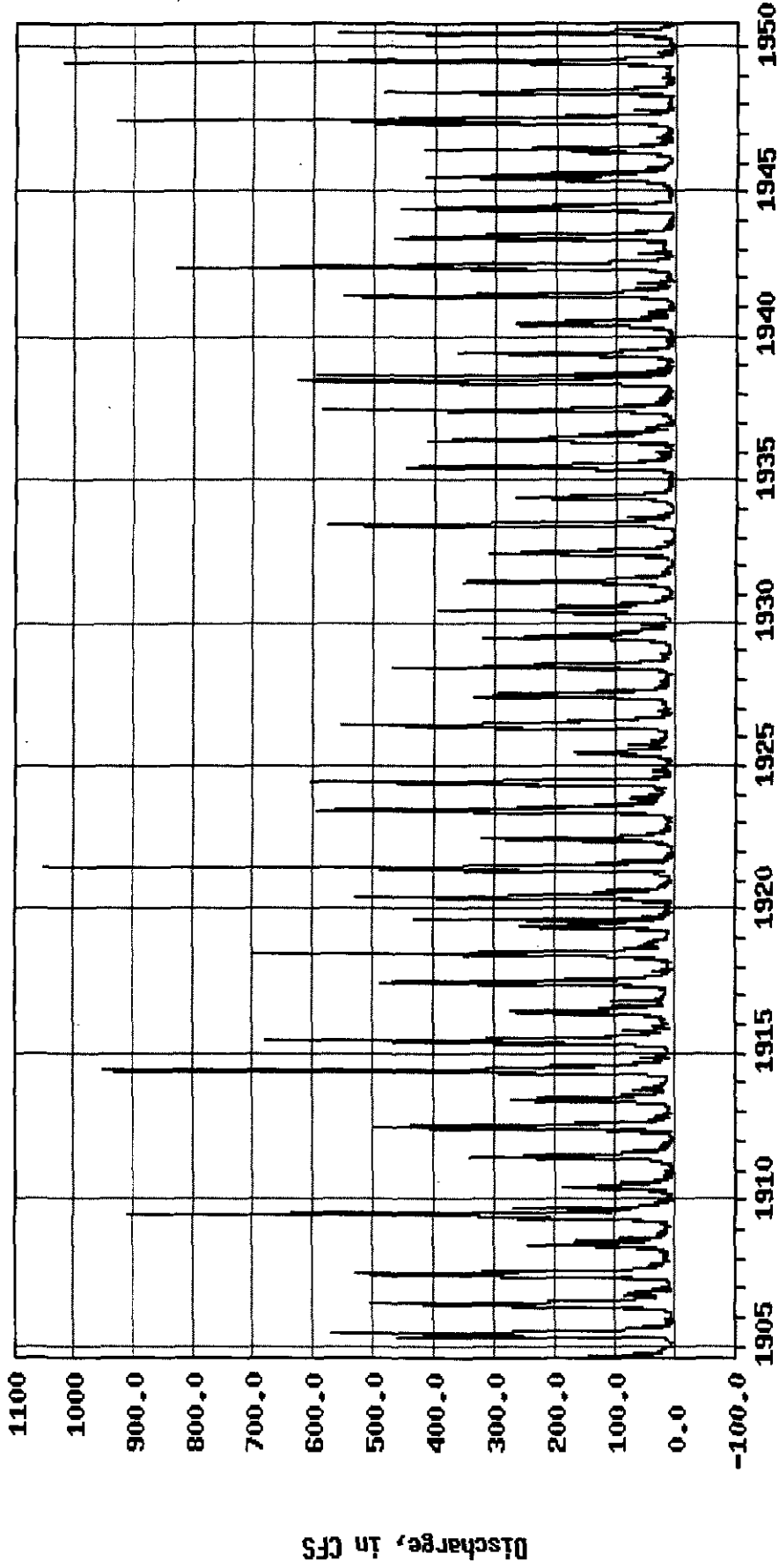
LOCATION.—Lat 39°55'52", long 105°17'43", in SE¼ sec. 26, T.1 S., R.71 W., Boulder County Hydrologic Unit 10190005, on left bank 0.2 mi downstream from South Draw, 1.0 mi west of Eldorado Springs, 1.8 mi downstream from South Boulder diversion canal, 5.0 mi south of Boulder, and 6.7 mi downstream from Gross Reservoir.

DRAINAGE AREA.—109 mi².

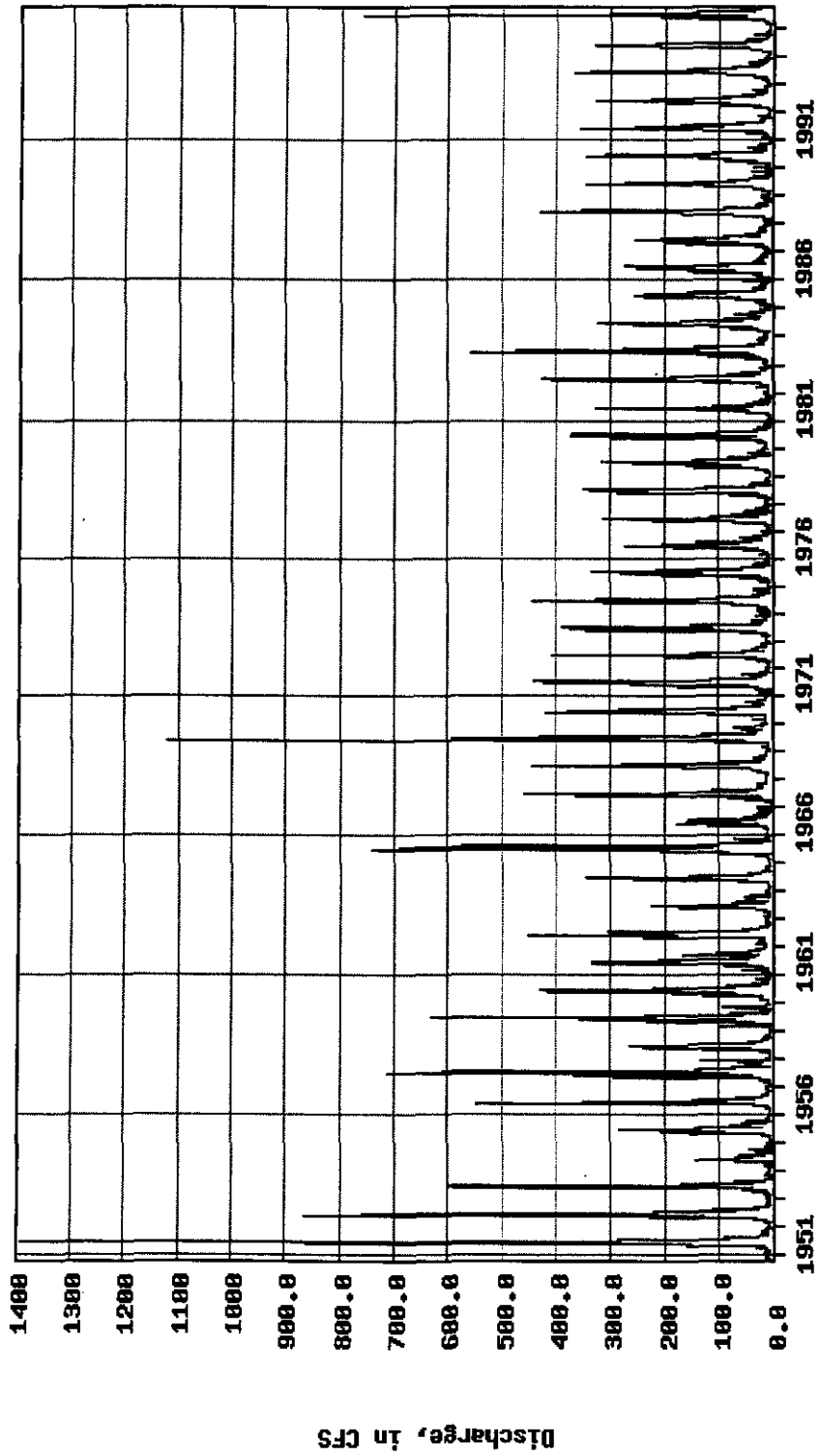
GAGE.—Water-state recorder with satellite telemetry and shaft encoder in metal box shelter with supplemental outside chain gage. DCP is the primary record with chart recorder as backup.

REMARKS.—Record is complete and reliable except for the following periods: Nov. 10-11; Dec. 18, 1998; Mar. 6-7, 13, 1999 when stage-discharge relationship ice affected; Dec. 19-28, 1998 when float frozen in well; Dec. 29, 1998-Mar. 4, 1999 when station closed for winter. Record good except for estimated days listed. Station maintained and record developed by G. T. Anderson.

South Boulder Creek Near Eldorado Springs, Co.
Station Number: 06729500



South Boulder Creek Near Eldorado Springs, Co.
Station Number: 06729588



Legend: — Discharge, in CFS
- - - Estimated Discharge, in CFS

MEAN DAILY DISCHARGE

SECTION IX

SUPPLEMENTAL DEFINITIONS

SOUTH BOULDER CREEK

HYDROLOGIC ANALYSIS and MAJOR DRAINAGEWAY PLANNING

BRIEF DEFINITIONS, BACKGROUND, AND STUDY SCOPE

August 26, 1999

I. DEFINITIONS

In the following, the bold word is defined followed by the tasks and topics often involved, and units. The tasks which are effectively under the contract scope to a significant degree are underlined.

- **METEOROLOGY - PREDICTION OF PRECIPITATION**

Tasks and Topics Involved:

Type, extent, intensity, duration, time [temporal], distribution [isohyets and isopluvial], and patterns [hyetograph], lifting effects [orographic and frontal], moisture sources and/or direction

Units:

- Inches, inches per hour, probability (1% chance or 100-year rainfall)

- **HYDROLOGY - PREDICTION OF RUNOFF FLOW AND VOLUME**

Tasks and Topics Involved:

Infiltration dependent on ground cover, soils, geology, and wet ground [antecedent moisture conditions] using simple [Horton] to complex [Green Ampt] methods; land surface runoff [effective rainfall]; stream routing [ranging from simple lagging or shifting based on general travel velocities to flow dependent travel rates during events without backwater or floodplain storage effects (kinematic wave) to simple floodplain/channel storage routers to full dynamic models]; reservoir routing; hydrographs; discharge profile for various probability floods; snowmelt runoff; statistical analysis of stream gage peak flow data; statistical analysis of reservoir storage; reservoir operations; long term rainfall runoff simulations and statistical analysis of simulations to arrive at flood statistics.

Units:

- Flow - cubic feet per second (cfs or second feet)
- Volume - acre feet (1 cfs per day = 2 AcFt), inches of runoff per acre.
- Probability - (1% chance or 100-year flood) [Note 100-year rainfall does

not necessarily equal the 100-year flood because other factors come into play but often this assumption is made, which is planned and has been used on South Boulder Creek.]

- **HYDRAULICS - PREDICTION OF WHERE THE FLOW WILL GO, AND ITS CHARACTER** (depth, water elevation, velocity, ponded, tranquil [subcritical], turbulent [supercritical] or unstable [critical])

Tasks and Topics Involved:

Land surface topographic mapping, field instrument survey, floodplain flow patterns, representative cross sections, hydraulic modeling [one dimensional, two dimensional, three dimensional], water surface profile analysis, flow splits, bridge, culvert, control structure and feature hydraulic analysis, floodplain delineation and mapping, floodway analysis and mapping, debris blockage analysis; junction, subcritical, critical, supercritical, and hydraulic jump analysis

Units:

- Velocity - feet per second (fps)
 - 0-2 slow, non erosive, sediment settles.
 - 2-8 moderate, minor erosion begins depending on soils, vegetation, and magnitude. Sediment from upstream passes through, more so with higher velocity.
 - 8-15 high, significant erosion, rock lining necessary. Occurs at culverts, bridges, and above or below drop structures/low dams. Deep flows in creeks can be in this range.
 - 15 ± extreme, flow over low dam, deep constrictions, pressurized conduits.
- Depth - feet (ft)
- Froude No. [no dimension, indicator of character of flow]
 - < 1 subcritical [reservoir to moderate moving water] sensitive to downstream effects
 - = 1 critical [transitioning flow, moderate to high velocity, unstable, wavy]
 - > 1 supercritical [spillway] steep stream, controlled by upstream effects and discharge, jumps up to subcritical state with large downstream backwater
- Energy - feet of water (Accountants bookkeep dollars, engineers bookkeep energy to do hydraulic analysis.)
- Momentum - force

- **GEOMORPHOLOGY - PREDICTION OF STREAM BED AND BANK MOVEMENT, AND SEDIMENT FLOW AND DEPOSITION** (and related hydraulic effect or outcome)

Tasks and Topics Involved:

Agradation, degradation, local scour (banks, bridges, dams), general scour, alluvial fans, bank erosion

Units:

Depth of scour (feet)

Tractive Force (lb/ft²)

Shear Stress (lb/ft²)

Bed movement (feet)

- **HAZARD, RISK AND DAMAGE ANALYSIS - HAZARDS ARE THE NEGATIVE OUTCOMES [e.g. STRUCTURE LOSS BY UNDERMINING FLOODING OR WASHING AWAY] OF A PHENOMENON (EROSION) OR FAILURE (DAM WASH OUT); RISK ANALYSIS IS ASSIGNING PROBABILITY TO VARIOUS EVENTS AND PHENOMENA; DAMAGE ANALYSIS IS THE COMBINATION ANALYSIS OF THE ABOVE TO CONCLUDE THE GENERAL MAGNITUDE OR SPECIFIC DETERMINATION IN DOLLARS, LOSS OF LIFE, OF THE LIKELY OUTCOMES OVER TIME**

Tasks and Topics Involved:

Hazards (loss of life, injury, flooding, sedimentation, debris impact), damage (qualitative [range of depths of flooding and approximate areas for various event magnitudes], quantitative [depth of inundation and estimated dollar amount of damage for various flood events, analysis of long term cumulative damages or average annual damage, utility and infrastructure, public inconvenience])

Units:

Probability, 5-, 10-, 100-year flood damage dollars, average annual damages, general depths of flooding (feet), velocity hazards (fps), depth velocity multipliers ft x fps anything above 5 to 6 trouble. (A car floats in 18 inches and totals car because the electrical system is flooded.)

- **FHAD - FLOOD HAZARD AREA DEFINITION: A FLOODPLAIN DELINEATION STUDY UNDER THE AUSPICES OF THE URBAN DRAINAGE AND FLOOD CONTROL DISTRICT (UDFCD) CONDUCTED IN AGREEMENT WITH LOCAL COMMUNITIES.** Usually involves topographic mapping of the water course, cursory meteorology from published data, hydrology, hydraulics, and floodplain profile and map drawing preparation.

- **FIRM AND FIS - FLOOD INSURANCE RATE MAP AND FLOOD INSURANCE STUDY. THE FEDERAL EMERGENCY MANAGEMENT AGENCY (FEMA) CONDUCTS FIS AND PREPARES FIRM'S IN COOPERATION WITH LOCAL COMMUNITIES.** For communities in compliance with FEMA requirements, Federally subsidized flood insurance is made available. Communities are responsible to provide floodplain mapping updates where developers or communities have modified the floodplains shown in the FIRM. This modification process is called a Letter of Map Revision (LOMR or CLOMR) and has been troublesome because of the sheer magnitude of changes that take place and extensive LOMR requirements. FEMA and UDFCD are working on a pilot program to help everyone with this process.
- **MASTER PLANNING (PHASE A): A STUDY WHICH FIRST FOCUSES ON CHARACTERIZING THE TYPE OF FLOODING, HAZARDS, AND CAUSATIVE FACTORS, IDENTIFIES COMPONENTS OR STRATEGIES WHICH COULD BE USED TO MITIGATE OR CORRECT PROBLEMS, THEN FORMULATES COMPREHENSIVE ALTERNATIVES AND SCREENS TO THE MOST VIABLE ALTERNATIVES IN CONSENSUS WITH THE LOCAL COMMUNITIES. THESE ALTERNATIVES ARE FURTHER REFINED, COST ESTIMATES, ADVANTAGES - DISADVANTAGES COMPARED, AND RECOMMENDATIONS MADE. THE PARTICIPATING COMMUNITIES AND UDFCD SELECT THE PLAN INCLUDING DIRECTING MODIFICATIONS WHICH MAY HAVE BEEN REALIZED DURING THE ANALYSIS AND REVIEW PROCESS.**
- **CONCEPTUAL AND/OR PRELIMINARY ENGINEERING PLAN (PHASE B): ONCE AN ALTERNATIVE IS SELECTED, THE INITIAL LAYOUT AND KEY DETAILS WHICH SUPPORT THE FEASIBILITY OF THE PLAN ARE REFINED AND ILLUSTRATED ON ENGINEERING DRAWINGS. SUPPORTIVE NARRATIVE OF THE PLANNING PROCESS, THE PLAN, AND OPINIONS OF PROBABLE COSTS ARE PREPARED.**



Explanation of Terms

For more information, please see Circular 1123: The Stream-Gaging Program of the U.S. Geological Survey.

Control

designates a feature downstream from the gage that determines the stage-discharge relation at the gage. This feature may be a natural constriction of the channel, an artificial structure, or a uniform cross section over a long reach of the channel.

Control structure

a structure on a stream or canal that is used to regulate the flow or stage of the stream or to prevent the intrusion of salt water.

Cubic foot per second

(ft³/s also CFS) is the rate of discharge representing a volume of 1 cubic foot passing a given point during 1 second and is equivalent to 7.48 gallons per second or 448.8 gallons per minute or 0.02832 cubic meter per second.

Discharge

is the volume of water (or more broadly, volume of fluid plus suspended sediment) that passes a given point within a given period of time.

Drainage area

of a stream at a specified location is that area, measured in a horizontal plane, enclosed by a topographic divide from which direct surface runoff from precipitation normally drains by gravity into the stream above the specified point.

Drainage basin

is a part of the surface of the earth that is occupied by a drainage system, which consists of a surface stream or a body of impounded surface water together with all tributary surface streams and bodies of impounded surface water.

Gage height

(G.H.) is the water-surface elevation referred to some arbitrary gage datum. Gage height is often used interchangeably with the more general term "stage," although gage height is more appropriate when used with a reading on a gage.

Gaging station

is a particular site on a stream, canal, lake, or reservoir where systematic observations of hydrologic data are obtained.

Hydrologic unit

is a geographic area representing part or all of a surface drainage basin or distinct hydrologic feature as delineated by the Office of Water Data Coordination on State Hydrologic Unit Maps; each hydrologic unit is identified by an eight-digit number.

Instantaneous discharge

is the discharge at a particular instant of time.

Mean discharge

(MEAN) is the arithmetic mean of individual daily mean discharges during a specific period.

National Geodetic Vertical Datum of 1929

(NGVD) is a geodetic datum derived from a general adjustment of the first order level nets of both the United States and Canada. It was formerly called "Sea Level Datum of 1929" or "mean sea level". Although the datum was derived from the average sea level over a period of many years at 26 tide stations along the Atlantic, Gulf of Mexico, and Pacific Coasts, it does not necessarily represent local mean sea level at any particular place.

Sea level

refers to the National Geodetic Vertical Datum of 1929 (NGVD of 1929)--a geodetic datum derived from a general adjustment of the first-order level nets of the United States and Canada, formerly called Sea Level Datum of 1929.

Stage

See Gage height

Stage-discharge relation

is the relation between gage height (stage) and the volume of water per unit of time (discharge) flowing in a channel.

Streamflow

is the discharge that occurs in a natural channel. Although the term "discharge" can be applied to the flow of a canal, the word "streamflow" uniquely describes the discharge in a surface stream course. The term "streamflow" is more general than "runoff" as streamflow may be applied to discharge whether or not it is affected by diversion or regulation.

Surface area

of a lake is that area, in acres, outlined on the latest USGS topographic map as the boundary of the lake and measured by a planimeter. In localities not covered by topographic maps, the areas are computed from the best maps available. All areas shown are those corresponding to the stage existing at the time when the planimetered map was made.

Water year

is the 12-month period, October 1 through September 30. The water year is designated by the calendar year in which it ends and which includes 9 of the 12 months. Thus, the year ending September 30, 1992, is called the "1992 water year."

We are aware of a problem with the clickable county imagemaps. When you click on a map you may not get stations for the county you expected, or the click may register as having missed the state. We are working on this problem.

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APPENDIX A

UDSWMM

n MODEL

10-YEAR

50-YEAR

100-YEAR

500-YEAR

UDSWMM

10-YEAR MODEL

10_ltd.wpd July 12, 2000 10-YR SWMM MODEL

URBAN DRAINAGE STORM WATER MANAGEMENT MODEL - 32 BIT VERSION 1998
 REVISED BY UNIVERSITY OF COLORADO AT DENVER

*** ENTRY MADE TO RUNOFF MODEL ***

model sbc_ltd.sw1
 10-year model

QNUMBER OF TIME STEPS 865
 QINTEGRATION TIME INTERVAL (MINUTES) 5.00

1.0 PERCENT OF IMPERVIOUS AREA HAS ZERO DETENTION DEPTH
 QFOR 288 RAINFALL STEPS, THE TIME INTERVAL IS 5.00 MINUTES
 QFOR RAINGAGE NUMBER 1 RAINFALL HISTORY IN INCHES PER HOUR

.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.07	.07	.07	.07	.07	.07	.07
.07	.08	.08	.08	.08	.08	.08	.08	.09	.09
.09	.09	.10	.10	.10	.10	.11	.11	.11	.12
.12	.12	.13	.13	.14	.15	.15	.16	.17	.18
.20	.21	.23	.25	.27	.30	.34	.39	.45	.54
.66	.83	1.09	1.50	2.16	2.77	2.57	1.80	1.27	.94
.73	.59	.49	.42	.36	.32	.29	.26	.24	.22
.20	.19	.18	.17	.16	.15	.14	.14	.13	.13
.12	.12	.11	.11	.11	.10	.10	.10	.10	.09
.09	.09	.09	.09	.08	.08	.08	.08	.08	.08
.07	.07	.07	.07	.07	.07	.07	.07	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.02	.02	.02	.02	.02	.02

QFOR RAINGAGE NUMBER 2 RAINFALL HISTORY IN INCHES PER HOUR

.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.08	.08	.08	.08	.08	.09
.09	.09	.10	.10	.10	.11	.11	.12	.13	.14
.15	.16	.17	.19	.21	.24	.27	.31	.37	.45
.56	.71	.95	1.33	1.95	2.54	2.34	1.61	1.12	.82
.63	.50	.41	.34	.29	.25	.22	.20	.18	.17
.15	.14	.13	.12	.12	.11	.11	.10	.10	.09
.09	.09	.09	.08	.08	.08	.08	.08	.07	.07
.07	.07	.07	.07	.07	.07	.07	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05

QFOR RAINGAGE NUMBER 3 RAINFALL HISTORY IN INCHES PER HOUR

.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.08	.08	.08
.08	.08	.08	.08	.09	.09	.09	.09	.10	.10
.10	.11	.11	.12	.12	.13	.13	.14	.15	.16
.17	.18	.20	.22	.24	.27	.30	.34	.39	.45
.53	.65	.81	1.05	1.45	2.25	1.77	1.22	.92	.72
.59	.49	.42	.36	.32	.28	.25	.23	.21	.19
.18	.17	.16	.15	.14	.13	.12	.12	.11	.11
.11	.10	.10	.10	.09	.09	.09	.09	.08	.08
.08	.08	.08	.08	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05

10_ltd.wpd July 12, 2000 10-YR SWMM MODEL

.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05

OFOR RAINGAGE NUMBER 4 RAINFALL HISTORY IN INCHES PER HOUR

.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.09	.10	.10	.10	.10	.11	.11	.11	.11	.12
.12	.12	.13	.13	.14	.14	.15	.16	.16	.17
.18	.19	.21	.22	.24	.26	.29	.32	.36	.41
.48	.57	.70	.90	1.23	1.94	1.51	1.04	.79	.63
.52	.44	.38	.34	.30	.27	.25	.23	.21	.20
.19	.18	.17	.16	.15	.15	.14	.14	.13	.13
.12	.12	.12	.11	.11	.11	.10	.10	.10	.10
.10	.09	.09	.09	.09	.09	.09	.08	.08	.08
.08	.08	.08	.08	.08	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03

OFOR RAINGAGE NUMBER 5 RAINFALL HISTORY IN INCHES PER HOUR

.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.07	.07	.07	.07	.07	.07	.07
.07	.08	.08	.08	.08	.08	.08	.09	.09	.09
.09	.10	.10	.10	.11	.11	.12	.12	.13	.13
.14	.15	.16	.17	.19	.20	.22	.25	.28	.32
.37	.45	.55	.72	1.01	1.69	1.26	.84	.63	.50
.41	.34	.30	.26	.23	.21	.19	.18	.17	.15
.15	.14	.13	.12	.12	.11	.11	.11	.10	.10
.10	.09	.09	.09	.09	.08	.08	.08	.08	.08
.08	.07	.07	.07	.07	.07	.07	.07	.07	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03

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model sbc_ltd.swi
10-year model

SUBAREA NUMBER	GUTTER OR MANHOLE	WIDTH (FT)	AREA (AC)	PERCENT IMPERV.	SLOPE (FT/FT)	RESISTANCE FACTOR		SURFACE STORAGE (IN)		INFILTRATION RATE (IN/HR)			GAGE NO
						IMPERV.	PERV.	IMPERV.	PERV.	MAXIMUM	MINIMUM	DECAY RATE	
227	226	7480.	286.0	30.0	.4076	.300	.500	.300	.470	3.90	.50	.00024	5
226	225	6240.	152.0	30.0	.5701	.300	.500	.300	.470	3.90	.50	.00024	5
225	224	8440.	488.0	20.0	.3704	.300	.500	.300	.470	4.50	.60	.00010	5
224	223	11920.	309.0	20.0	.2882	.300	.500	.300	.450	3.50	.20	.00100	5
222	221	13040.	250.0	20.0	.5139	.300	.500	.300	.450	3.90	.50	.00024	5
221	220	15160.	506.0	20.0	.4510	.300	.500	.300	.450	3.50	.20	.00100	5
219	218	3320.	44.0	6.0	.2945	.300	.500	.300	.470	3.90	.50	.00024	5
220	219	10200.	437.0	5.0	.3544	.300	.500	.300	.480	4.50	.60	.00010	5
223	222	2280.	182.0	6.0	.4444	.300	.500	.300	.470	4.80	.50	.00010	5
214	216	16320.	505.0	20.0	.4409	.300	.500	.300	.450	3.90	.50	.00024	5
212	214	13760.	482.0	15.0	.4325	.300	.500	.300	.450	3.90	.50	.00024	5
211	213	11800.	511.0	20.0	.3390	.300	.500	.300	.440	3.50	.20	.00100	5
210	212	12200.	588.0	5.0	.2915	.300	.500	.300	.420	4.80	.50	.00010	5
213	215	6480.	539.0	6.0	.3847	.300	.400	.150	.420	3.90	.50	.00024	5
215	217	9720.	245.0	5.0	.2985	.250	.450	.300	.500	3.90	.50	.00024	5
209	211	6800.	284.0	6.0	.4718	.300	.400	.150	.460	3.90	.50	.00024	5
185	186	8520.	461.0	15.0	.2842	.300	.500	.300	.450	4.80	.50	.00010	5
184	185	7440.	232.0	8.0	.3661	.300	.500	.300	.400	3.90	.50	.00024	5
182	183	16000.	599.0	6.0	.1690	.300	.500	.300	.450	4.50	.60	.00010	5
180	181	13280.	438.0	6.0	.2725	.300	.500	.300	.450	4.50	.60	.00010	5

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183	184	7080.	217.0	6.0	.2820	.300	.500	.300	.400	3.90	.50	.00024	5
181	182	9200.	507.0	7.0	.2836	.300	.500	.300	.450	4.50	.60	.00010	5
179	180	9040.	501.0	5.0	.2840	.250	.450	.300	.500	3.50	.20	.00100	4
204	204	13440.	854.0	30.0	.3985	.300	.500	.300	.470	3.90	.50	.00024	5
203	203	7000.	258.0	25.0	.4793	.300	.500	.300	.470	3.90	.50	.00024	5
199	201	15400.	843.0	5.0	.3343	.300	.500	.300	.470	4.50	.60	.00010	5
198	200	14440.	542.0	5.0	.2842	.300	.500	.300	.450	3.90	.50	.00024	5
200	202	7640.	250.0	5.0	.2900	.300	.500	.300	.500	4.80	.50	.00010	5
196	198	14440.	797.0	5.0	.4198	.250	.450	.300	.450	3.90	.50	.00024	5
195	196	14640.	387.0	5.0	.2370	.250	.450	.300	.500	4.50	.60	.00010	5
197	199	18040.	634.0	5.0	.2744	.250	.450	.300	.450	3.90	.50	.00024	5
190	195	9520.	251.0	5.0	.2833	.250	.450	.300	.470	3.90	.50	.00024	5
189	194	15120.	847.0	9.0	.3487	.150	.400	.300	.500	4.50	.50	.00010	4
208	208	8520.	275.0	5.0	.3120	.250	.450	.300	.450	3.90	.50	.00024	5
207	207	8560.	772.0	6.0	.4592	.150	.400	.300	.430	3.50	.20	.00100	5
206	206	7720.	250.0	5.0	.3693	.250	.450	.300	.470	3.90	.50	.00024	5
205	205	9800.	395.0	7.0	.4113	.150	.400	.300	.450	3.90	.50	.00024	4
187	192	1540.	115.0	6.0	.5495	.150	.400	.300	.430	3.50	.20	.00100	4
188	193	8960.	273.0	9.0	.3629	.150	.400	.300	.400	3.50	.20	.00100	4
186	187	19200.	1018.0	8.0	.3200	.150	.400	.300	.450	3.90	.50	.00024	4
177	178	13000.	392.0	7.0	.2685	.150	.400	.300	.450	3.90	.50	.00024	5
178	179	7720.	211.0	5.0	.3191	.250	.450	.300	.420	3.50	.20	.00100	5
175	176	15040.	716.0	5.0	.3492	.250	.450	.300	.400	3.50	.20	.00100	4
176	177	12040.	233.0	6.0	.2396	.250	.450	.300	.450	3.90	.50	.00024	4
174	175	3800.	78.0	5.0	.2684	.250	.450	.300	.450	3.90	.50	.00024	4
173	174	8120.	188.0	8.0	.3071	.150	.400	.300	.430	3.90	.50	.00024	4
172	173	11520.	230.0	5.0	.3401	.250	.450	.300	.400	3.50	.20	.00100	4
171	172	3720.	73.0	7.0	.2083	.150	.400	.300	.450	3.90	.50	.00024	4
167	168	7240.	259.0	5.0	.2386	.300	.500	.300	.500	3.90	.50	.00024	5
168	169	6280.	175.0	5.0	.2720	.300	.500	.300	.500	3.90	.50	.00024	5
164	165	13840.	350.0	6.0	.3519	.300	.500	.300	.470	3.90	.50	.00024	4
166	167	10720.	215.0	6.0	.3188	.300	.500	.300	.500	3.90	.50	.00024	4
165	166	1040.	99.0	5.0	.2782	.300	.500	.300	.500	3.90	.50	.00024	4
170	171	8840.	139.0	5.0	.2244	.250	.450	.300	.400	3.50	.20	.00100	4
169	170	9680.	332.0	5.0	.2538	.250	.450	.300	.400	3.50	.20	.00100	4
162	163	5280.	112.0	5.0	.2935	.250	.450	.300	.470	3.90	.50	.00100	4
163	164	8000.	76.0	5.0	.3938	.300	.500	.300	.450	3.90	.50	.00024	4
156	157	1660.	103.0	7.0	.3821	.250	.450	.300	.460	3.50	.20	.00100	4
160	161	8760.	341.0	5.0	.3148	.300	.500	.300	.470	3.90	.50	.00100	4
161	162	11600.	362.0	5.0	.3269	.300	.500	.300	.470	3.90	.50	.00100	5
158	159	12760.	476.0	5.0	.2852	.300	.500	.300	.470	3.90	.50	.00100	5
159	160	6720.	342.0	6.0	.3021	.300	.500	.300	.470	3.90	.50	.00100	4
155	156	9960.	523.0	6.0	.3280	.250	.450	.300	.400	3.90	.50	.00024	4
157	158	11400.	344.0	5.0	.2728	.250	.450	.300	.460	3.90	.50	.00024	4
152	153	8760.	249.0	5.0	.2831	.300	.500	.300	.500	3.90	.50	.00024	4
153	154	5760.	249.0	6.0	.3299	.250	.450	.300	.450	3.90	.50	.00024	4
154	155	2180.	161.0	5.0	.3792	.300	.500	.300	.400	3.50	.20	.00100	4
148	149	6440.	214.0	6.0	.3001	.250	.450	.300	.400	3.50	.20	.00100	4
149	150	5560.	58.0	6.0	.1610	.250	.450	.300	.400	3.50	.20	.00100	4
150	151	8240.	189.0	5.0	.2338	.250	.450	.300	.400	3.50	.20	.00100	4
151	152	13960.	501.0	8.0	.3572	.250	.450	.300	.450	3.90	.50	.00024	4
145	146	6930.	318.0	5.0	.2782	.300	.500	.300	.460	3.90	.50	.00024	4
146	147	11200.	283.0	5.0	.2727	.250	.450	.300	.500	3.90	.50	.00024	4
147	148	5440.	453.0	5.0	.3306	.250	.450	.300	.470	3.90	.50	.00024	4
141	142	4160.	103.0	6.0	.2843	.250	.450	.300	.450	3.90	.50	.00024	4
142	143	9680.	187.0	5.0	.3565	.250	.450	.300	.470	3.90	.50	.00024	4
143	144	4400.	274.0	5.0	.3218	.300	.500	.300	.460	3.90	.50	.00024	4
144	145	4320.	79.0	5.0	.2164	.300	.500	.300	.500	3.90	.50	.00024	4
139	140	8640.	184.0	6.0	.3125	.250	.450	.300	.460	3.90	.50	.00024	4
140	141	7600.	132.0	5.0	.2104	.250	.450	.300	.450	3.50	.20	.00100	4
136	137	6200.	142.0	15.0	.2104	.150	.400	.150	.470	3.50	.20	.00100	4
137	138	8780.	383.0	10.0	.0823	.150	.400	.150	.420	3.50	.20	.00100	4
138	139	3760.	70.0	15.0	.1898	.250	.450	.150	.450	3.90	.50	.00024	4
133	134	20040.	530.0	8.0	.3229	.250	.450	.300	.460	3.90	.50	.00024	4
134	135	8160.	160.0	5.0	.2440	.250	.450	.300	.450	3.90	.50	.00024	5
135	136	6000.	282.0	5.0	.2300	.250	.450	.300	.460	3.90	.50	.00024	5
130	131	9720.	290.0	12.0	.3042	.150	.400	.150	.500	3.90	.50	.00024	4
131	132	9120.	213.0	8.0	.1964	.250	.450	.300	.470	3.90	.50	.00024	4
132	133	15440.	496.0	7.0	.1806	.250	.450	.300	.470	3.90	.50	.00024	4
128	129	7040.	151.0	12.0	.5988	.300	.500	.200	.450	3.90	.50	.00024	4
129	130	6720.	110.0	15.0	.2077	.150	.400	.150	.450	3.90	.50	.00024	4
124	125	7600.	220.0	5.0	.1948	.300	.500	.300	.500	3.90	.50	.00024	4
125	126	6840.	88.0	5.0	.2679	.300	.500	.300	.500	3.90	.50	.00024	4
126	127	16000.	548.0	8.0	.2341	.250	.450	.300	.480	3.90	.50	.00024	4
120	124	15040.	397.0	13.0	.1127	.150	.400	.150	.500	3.90	.50	.00024	4
127	128	17320.	472.0	8.0	.2160	.250	.450	.300	.470	3.90	.50	.00024	4
118	122	18880.	481.0	8.0	.2138	.150	.400	.200	.450	3.90	.50	.00024	4
119	123	8320.	389.0	12.0	.1613	.150	.400	.200	.450	3.90	.50	.00024	4
113	116	19040.	702.0	5.0	.1137	.300	.500	.300	.500	3.90	.50	.00024	4
93	96	12640.	579.0	5.0	.2560	.250	.450	.300	.460	3.90	.50	.00024	4
230	95	8000.	200.0	5.0	.2312	.250	.450	.300	.450	3.90	.50	.00024	4
88	85	3840.	118.0	5.0	.2369	.250	.450	.300	.400	3.90	.50	.00024	4
89	86	11760.	331.0	5.0	.2521	.250	.450	.300	.400	3.90	.50	.00024	4
90	87	16080.	655.0	5.0	.1364	.250	.450	.300	.400	3.50	.20	.00100	4
84	81	12440.	303.0	5.0	.2148	.250	.450	.300	.400	3.50	.20	.00100	4
85	82	2220.	96.0	5.0	.1143	.250	.450	.300	.400	3.50	.20	.00100	4
86	83	4760.	197.0	5.0	.1438	.250	.450	.300	.400	3.90	.50	.00024	4
87	84	5440.	106.0	5.0	.1919	.250	.450	.300	.400	3.90	.50	.00024	4
83	80	31300.	862.0	9.0	.1050	.150	.400	.200	.400	3.50	.20	.00100	4
74	121	9400.	326.0	6.0	.1923	.150	.400	.200	.400	3.50	.20	.00024	4
70	79	16040.	633.0	7.0	.1589	.250	.450	.300	.400	3.50	.20	.00100	4
61	75	3200.	62.0	5.0	.3363	.250	.450	.300	.400	3.90	.50	.00024	4
63	76	12840.	379.0	8.0	.1972	.250	.450	.300	.400	3.50	.20	.00100	4
65	77	4040.	66.0	8.0	.2100	.250	.450	.300	.430	3.90	.50	.00024	4
66	78	7560.	256.0	5.0	.1250	.250	.450	.300	.450	3.90	.50	.00024	4
58	74	9400.	411.0	8.0	.3384	.250	.450	.300	.400	3.50	.20	.00100	4
228	89	8480.	319.0	8.0	.1659	.150	.400	.150	.450	3.50	.20	.00100	4
229	93	4880.	111.0	5.0	.2059	.250	.450	.300	.450	4.50	.60	.00010	4
91	88	16520.	352.0	6.0	.1576	.250	.450	.300	.450	3.90	.50	.00024	4
114	117	12000.	390.0	15.0	.1571	.150	.400	.150	.430	3.90	.50	.00024	4
115	118	16440.	453.0	6.0	.1736	.250	.450	.300	.460	3.90	.50	.00024	4

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116	119	2600.	34.0	15.0	.1472	.150	.400	.150	.500	3.90	.50	.00024	4
117	120	7960.	220.0	15.0	.1331	.150	.400	.150	.470	3.90	.50	.00024	4
101	104	6880.	205.0	15.0	.1564	.150	.400	.150	.450	3.50	.50	.00100	4
102	105	9120.	343.0	10.0	.1175	.150	.400	.150	.500	3.90	.50	.00024	4
103	106	12760.	273.0	8.0	.1121	.250	.450	.300	.500	3.90	.50	.00024	4
99	102	10440.	314.0	10.0	.1275	.150	.400	.150	.480	3.90	.50	.00024	4
100	103	8170.	150.0	8.0	.1343	.150	.400	.150	.450	3.90	.50	.00100	4
109	112	7280.	208.0	7.0	.4086	.250	.450	.300	.470	3.90	.50	.00024	4
110	113	10120.	209.0	7.0	.2899	.250	.450	.300	.500	3.90	.50	.00024	4
111	114	9000.	230.0	5.0	.2973	.300	.500	.300	.470	3.90	.50	.00024	5
112	115	6480.	102.0	6.0	.4123	.250	.450	.300	.460	3.90	.50	.00024	4
107	110	4140.	399.0	8.0	.3550	.250	.450	.300	.470	3.90	.50	.00024	4
105	108	12480.	202.0	5.0	.3863	.300	.500	.300	.470	3.90	.50	.00024	4
106	109	5520.	216.0	7.0	.1680	.250	.450	.300	.500	3.90	.50	.00024	4
108	111	11200.	199.0	5.0	.4732	.300	.500	.300	.460	3.90	.50	.00024	4
104	107	5440.	106.0	8.0	.2557	.250	.450	.300	.480	3.90	.50	.00024	4
97	100	19960.	458.0	7.0	.5159	.250	.450	.300	.480	3.50	.20	.00100	4
95	98	14000.	309.0	18.0	.1544	.250	.450	.200	.470	3.50	.20	.00100	4
96	99	2880.	55.0	10.0	.3003	.250	.450	.300	.480	3.50	.20	.00100	4
98	101	1380.	82.0	8.0	.1629	.250	.450	.200	.470	3.50	.20	.00100	4
94	97	11440.	472.0	8.0	.3012	.250	.450	.300	.470	3.90	.50	.00024	4
92	94	5120.	475.0	7.0	.1426	.250	.450	.300	.500	3.90	.50	.00024	4
56	72	8960.	197.0	7.0	.1792	.150	.400	.150	.420	3.50	.20	.00100	4
57	73	16000.	636.0	8.0	.1300	.150	.400	.150	.440	3.90	.50	.00024	4
55	71	9640.	261.0	7.0	.1967	.250	.450	.300	.470	3.50	.20	.00100	4
43	59	8040.	296.0	9.0	.1912	.150	.400	.150	.400	3.90	.50	.00024	4
47	63	7960.	234.0	6.0	.4083	.250	.450	.300	.470	3.90	.50	.00024	4
48	64	7480.	258.0	6.0	.3750	.250	.450	.300	.500	3.90	.50	.00024	4
45	61	15000.	552.0	8.0	.2077	.250	.450	.200	.470	3.50	.20	.00100	4
42	46	6440.	197.0	7.0	.3799	.250	.450	.200	.400	3.50	.20	.00100	4
44	60	8160.	225.0	7.0	.2515	.250	.450	.200	.470	3.50	.20	.00100	4
46	62	2800.	39.0	5.0	.3963	.250	.450	.300	.470	3.50	.20	.00100	4
50	66	6120.	108.0	6.0	.4444	.250	.450	.300	.500	3.90	.50	.00024	4
51	67	13240.	636.0	7.0	.3651	.250	.450	.300	.470	3.50	.20	.00100	4
53	69	7480.	197.0	12.0	.2552	.150	.400	.150	.470	3.50	.20	.00100	4
54	70	13920.	246.0	12.0	.2827	.150	.400	.150	.420	3.50	.20	.00100	4
49	65	7920.	212.0	5.0	.3375	.250	.450	.300	.480	3.90	.50	.00024	4
52	68	4240.	80.0	7.0	.3917	.250	.450	.300	.500	3.50	.20	.00100	4
41	42	15160.	593.0	8.0	.4922	.250	.450	.200	.450	3.90	.50	.00024	4
39	40	13160.	356.0	20.0	.4570	.250	.450	.100	.450	3.90	.50	.00024	3
40	41	6200.	205.0	9.0	.5172	.250	.450	.200	.500	3.50	.20	.00100	4
18	18	15200.	565.0	7.0	.3792	.250	.450	.200	.420	3.50	.20	.00100	3
19	20	10680.	606.0	9.0	.1670	.150	.400	.150	.470	3.90	.50	.00024	4
20	21	13920.	379.0	6.0	.3275	.250	.450	.300	.400	3.90	.50	.00024	3
14	14	6160.	132.0	25.0	.4006	.250	.450	.100	.500	3.50	.20	.00100	3
15	15	3000.	36.0	25.0	.3169	.250	.450	.100	.450	3.50	.20	.00100	3
16	16	3840.	117.0	25.0	.2094	.250	.450	.100	.400	3.50	.20	.00100	3
17	17	5640.	156.0	20.0	.3423	.250	.450	.100	.400	3.50	.20	.00100	3
8	8	14200.	1227.0	67.0	.2919	.250	.450	.050	.450	3.50	.20	.00100	3
37	38	5060.	368.0	7.0	.2400	.250	.450	.200	.420	3.90	.50	.00024	4
38	39	10280.	290.0	7.0	.3153	.250	.450	.300	.420	3.50	.20	.00100	4
36	37	16320.	466.0	5.0	.1439	.250	.450	.300	.480	3.90	.50	.00024	4
33	34	13680.	445.0	8.0	.1186	.150	.400	.200	.410	3.90	.50	.00024	4
34	35	6280.	148.0	7.0	.2940	.250	.450	.300	.420	3.50	.20	.00100	4
35	36	10680.	251.0	6.0	.1368	.250	.450	.300	.400	3.50	.20	.00100	4
31	32	6520.	144.0	6.0	.2938	.250	.450	.300	.420	3.90	.50	.00024	4
32	33	10360.	257.0	12.0	.1275	.150	.400	.150	.420	3.50	.20	.00100	4
30	31	5440.	107.0	7.0	.2363	.150	.400	.150	.450	4.50	.60	.00010	3
22	23	9840.	195.0	8.0	.1920	.250	.450	.200	.460	3.50	.20	.00100	3
29	30	11560.	546.0	12.0	.0980	.150	.400	.150	.450	3.50	.20	.00100	4
26	27	5080.	107.0	5.0	.2510	.250	.450	.300	.450	3.90	.50	.00024	3
27	28	5040.	300.0	9.0	.1461	.150	.400	.150	.430	3.90	.50	.00024	3
28	29	6120.	152.0	7.0	.2020	.150	.400	.150	.450	3.50	.20	.00100	4
24	25	5920.	363.0	9.3	.3292	.250	.450	.300	.450	3.50	.20	.00100	3
25	26	3720.	94.0	8.0	.1772	.150	.400	.150	.450	3.50	.20	.00100	3
23	24	1740.	104.0	7.0	.1530	.250	.450	.300	.450	3.50	.20	.00100	3
21	22	12000.	447.0	20.0	.2822	.150	.400	.200	.400	3.50	.20	.00100	3
9	9	20640.	411.0	8.0	.2894	.250	.450	.300	.470	3.90	.50	.00024	2
10	10	7520.	202.0	6.0	.3773	.250	.450	.300	.480	3.90	.50	.00024	2
7	7	9880.	373.0	7.0	.2911	.300	.500	.300	.500	3.90	.50	.00024	2
3	3	22000.	929.0	8.0	.3243	.250	.450	.200	.450	3.50	.20	.00100	2
4	4	25560.	960.0	8.0	.2675	.250	.450	.200	.500	3.50	.20	.00100	2
2	2	14480.	519.0	7.0	.4504	.300	.500	.300	.420	3.50	.20	.00100	2
6	6	16100.	296.0	10.0	.4790	.300	.500	.300	.450	3.50	.20	.00100	2
5	5	18300.	336.0	6.0	.2506	.300	.500	.300	.420	5.00	.60	.00006	2
1	1	30900.	567.0	7.0	.5000	.300	.500	.300	.420	3.50	.20	.00100	2
11	11	6000.	113.0	25.0	.3243	.250	.450	.200	.500	3.90	.50	.00024	2
12	12	8360.	159.0	6.0	.3715	.300	.500	.300	.500	3.90	.50	.00024	2
13	13	10480.	229.0	7.0	.3542	.300	.500	.300	.500	3.90	.50	.00024	2
256	247	39100.	808.0	7.0	.1652	.250	.450	.200	.450	3.50	.20	.00100	2
257	248	31200.	645.0	8.0	.2217	.250	.450	.200	.450	3.50	.20	.00100	2
258	249	18300.	377.0	7.0	.1984	.250	.450	.300	.420	3.50	.20	.00100	2
259	250	5300.	109.0	5.0	.1627	.250	.450	.300	.450	4.80	.50	.00010	2
253	244	36900.	848.0	50.0	.2354	.300	.500	.300	.350	3.90	.50	.00024	2
254	245	7300.	100.0	7.0	.2934	.250	.450	.200	.450	3.50	.20	.00100	2
255	246	21800.	450.0	8.0	.2396	.250	.450	.300	.450	3.50	.20	.00100	2
76	54	10300.	213.0	8.0	.3735	.300	.500	.300	.500	5.00	.60	.00006	2
77	55	25900.	297.0	7.0	.4316	.300	.500	.300	.500	5.00	.60	.00006	2
75	53	2400.	26.0	6.0	.4875	.300	.500	.300	.460	3.50	.20	.00024	2
73	52	38400.	441.0	18.0	.3662	.300	.500	.300	.400	3.50	.20	.00100	2
82	51	19700.	362.0	25.0	.3938	.250	.450	.300	.400	3.50	.20	.00100	2
71	50	11300.	207.0	25.0	.4627	.300	.500	.400	.450	3.50	.20	.00100	2
80	58	12000.	220.0	6.0	.3854	.300	.500	.300	.480	5.00	.60	.00006	2
81	57	42200.	776.0	8.0	.5226	.250	.450	.200	.470	4.50	.60	.00010	2
78	56	22000.	404.0	18.0	.4013	.250	.450	.300	.500	4.80	.50	.00010	2
79	56	21400.	442.0	15.0	.3303	.300	.500	.300	.450	4.50	.50	.00010	2
72	49	16000.	220.0	35.0	.5698	.300	.500	.300	.500	4.50	.50	.00010	2
69	48	9400.	391.0	35.0	.2301	.250	.450	.300	.400	3.90	.50	.00024	2
1635	1635	12865.	317.0	12.0	.3700	.300	.500	.300	.450	3.50	.20	.00100	2
1645	1645	5640.	126.0	5.0	.2900	.250	.450	.150	.450	3.50	.20	.00100	2
1640	1640	8667.	200.0	10.0	.2900	.300	.500	.320	.450	3.50	.20	.00100	2

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1630	1630	8660.	159.0	6.0	.1300	.400	.450	.150	.450	3.50	.20	.00100	2
1625	1625	10700.	197.0	9.0	.2100	.200	.400	.150	.450	3.50	.20	.00100	1
1610	1610	6780.	109.0	9.0	.0200	.200	.400	.150	.450	4.80	.50	.00010	1
1665	1665	14692.	390.0	35.0	.2870	.200	.400	.150	.450	3.50	.20	.00100	2
1605	1605	7689.	81.0	6.0	.1100	.200	.400	.150	.450	4.80	.50	.00010	1
1660	1660	23764.	552.0	7.0	.2000	.200	.450	.150	.460	3.90	.50	.00024	2
1650	1650	13676.	382.0	7.0	.2300	.200	.200	.150	.450	3.50	.20	.00100	2
1655	1655	22832.	558.0	6.0	.1600	.200	.450	.150	.460	3.50	.20	.00100	2
1620	1620	17977.	324.0	7.0	.0500	.200	.400	.150	.470	4.80	.50	.00010	2
1615	1615	11967.	228.0	7.0	.1200	.200	.400	.150	.470	4.50	.60	.00010	2
1710	1710	9974.	245.0	5.0	.0100	.200	.400	.150	.350	3.90	.50	.00024	1
1600	1600	3273.	25.0	7.0	.0500	.200	.450	.150	.600	5.00	.70	.00002	1
1705	1705	2245.	67.0	5.0	.0100	.200	.400	.150	.350	3.90	.50	.00024	2
1450	1450	4800.	198.0	5.0	.0200	.150	.450	.150	.600	3.90	.50	.00024	1
1445	1445	6714.	164.0	5.0	.0800	.200	.400	.150	.350	5.00	.60	.00006	1
1440	1440	12663.	66.0	7.0	.0100	.150	.450	.150	.600	3.90	.50	.00024	1
1480	1938	34034.	732.0	35.0	.0200	.200	.400	.150	.300	3.90	.50	.00024	1
1435	1435	6984.	232.0	5.0	.0800	.200	.400	.150	.460	5.00	.60	.00006	1
1430	1430	6338.	82.0	5.0	.0700	.200	.400	.150	.460	5.00	.60	.00006	1
1425	1425	4940.	68.0	6.0	.0400	.200	.400	.150	.600	5.00	.70	.00002	1
1420	1420	26178.	59.0	9.0	.0220	.200	.450	.150	.600	3.90	.50	.00024	1
1570	1570	3089.	171.0	6.0	.3540	.200	.450	.150	.450	3.50	.20	.00100	2
1555	1555	7055.	83.0	7.0	.1300	.200	.450	.150	.450	4.80	.50	.00010	1
1565	1565	4112.	95.0	9.0	.3200	.200	.450	.150	.470	3.50	.20	.00100	2
1560	1560	5353.	123.0	8.0	.4400	.200	.450	.150	.450	3.50	.20	.00100	2
1550	1550	20321.	424.0	7.0	.0700	.200	.400	.150	.450	3.50	.20	.00100	1
1415	1415	5148.	307.0	5.0	.0260	.200	.400	.150	.500	3.90	.50	.00024	1
1410	1410	5300.	195.0	5.0	.0100	.150	.450	.150	.500	3.90	.50	.00024	1
1455	1455	19899.	542.0	11.0	.0037	.200	.400	.150	.350	4.80	.50	.00010	1
1490	1490	8100.	698.0	10.0	.0620	.200	.400	.150	.350	4.50	.50	.00010	1
1465	1465	19569.	93.0	10.0	.0348	.150	.500	.150	.350	4.50	.60	.00010	1
1460	1460	12745.	286.0	9.0	.0603	.200	.400	.150	.350	5.00	.60	.00006	1
1575	1575	10554.	222.0	10.0	.4060	.200	.450	.150	.450	3.50	.20	.00100	2
1545	1545	15603.	253.0	7.0	.0890	.200	.400	.150	.450	4.80	.50	.00010	1
1530	1530	8269.	345.0	6.0	.1080	.200	.400	.150	.350	4.80	.50	.00010	1
1525	1525	14343.	53.0	10.0	.0200	.150	.400	.150	.350	3.90	.50	.00024	1
1505	1505	49306.	262.0	10.0	.0100	.150	.450	.150	.350	3.50	.20	.00100	1
1520	1520	21460.	99.0	10.0	.0100	.200	.450	.150	.350	3.50	.20	.00100	1
1715	1715	3131.	115.0	7.0	.1200	.150	.400	.150	.350	3.90	.50	.00024	1
1515	1515	3666.	8.0	60.0	.0200	.150	.400	.150	.350	3.50	.20	.00100	1
1540	1541	19881.	345.0	15.0	.0300	.200	.400	.150	.350	4.50	.60	.00010	1
1510	1510	16588.	76.0	3.0	.0100	.150	.400	.150	.350	3.90	.50	.00024	1
1500	1500	21483.	465.0	10.0	.0400	.200	.400	.150	.250	3.90	.50	.00024	1
299	299	20092.	72.0	40.0	.1300	.150	.500	.150	.350	4.80	.50	.00010	1
301	301	38137.	177.0	31.0	.1600	.150	.500	.150	.350	4.80	.50	.00010	1
297	297	84806.	338.0	40.0	.1200	.150	.500	.150	.350	4.80	.50	.00010	1
305	1917	1795.	103.0	10.0	.0240	.150	.350	.150	.250	3.90	.50	.00024	1
304	304	2970.	150.0	10.0	.0240	.150	.350	.150	.250	3.90	.50	.00024	1
262	262	3964.	39.0	5.0	.0200	.200	.400	.150	.250	3.90	.50	.00024	1
264	264	1734.	26.0	5.0	.0200	.200	.400	.150	.250	3.90	.50	.00024	1
243	243	46293.	82.0	7.0	.0200	.200	.350	.150	.350	3.90	.50	.00024	1
384	384	27915.	77.0	45.0	.0900	.150	.500	.150	.350	4.80	.50	.00010	1
290	290	4748.	29.0	5.0	.0250	.300	.400	.150	.400	3.90	.50	.00024	1
353	353	12867.	41.0	50.0	.0700	.150	.500	.150	.350	5.00	.60	.00006	1
350	350	13939.	51.0	70.0	.0550	.150	.400	.150	.350	4.80	.50	.00010	1
351	351	17043.	59.0	70.0	.0600	.150	.450	.150	.350	5.00	.60	.00006	1
376	376	1390.	3.0	10.0	.0100	.150	.450	.150	.350	4.80	.50	.00010	1
368	368	7225.	99.0	50.0	.0070	.150	.450	.150	.350	3.90	.50	.00024	1
361	361	6400.	30.0	60.0	.0060	.150	.450	.150	.350	3.90	.50	.00024	1
369	369	7449.	17.0	60.0	.0400	.150	.450	.150	.350	4.80	.50	.00010	1
354	1818	6316.	6.0	95.0	.0400	.150	.350	.150	.250	4.80	.50	.00010	1
355	355	9583.	7.0	65.0	.0400	.150	.350	.150	.250	4.80	.50	.00010	1
363	363	9593.	7.0	33.0	.0550	.150	.350	.150	.250	4.80	.50	.00010	1
366	366	26706.	81.0	45.0	.0550	.150	.500	.150	.350	4.80	.50	.00010	1
367	367	9047.	23.0	65.0	.0450	.150	.500	.150	.350	4.80	.50	.00010	1
373	373	4140.	38.0	6.0	.0200	.150	.400	.150	.350	4.80	.50	.00010	1
241	241	45665.	343.0	45.0	.0200	.150	.400	.150	.450	3.90	.50	.00024	1
346	346	21083.	71.0	40.0	.0600	.150	.450	.150	.350	3.90	.50	.00024	1
345	345	20528.	78.0	50.0	.0600	.150	.450	.150	.350	4.80	.50	.00010	1
349	349	1951.	13.0	15.0	.0200	.150	.450	.150	.350	4.80	.50	.00010	1
347	347	11476.	55.0	65.0	.0500	.150	.400	.150	.350	4.80	.50	.00010	1
371	371	12050.	83.0	50.0	.0500	.150	.450	.150	.250	4.80	.50	.00010	1
338	338	14259.	73.0	8.0	.0250	.150	.350	.150	.250	3.90	.50	.00024	1
333	333	6300.	5.0	60.0	.0400	.200	.450	.150	.550	3.50	.20	.00100	1
334	334	6300.	5.0	60.0	.0400	.150	.350	.150	.250	3.50	.20	.00100	1
240	240	2500.	46.0	25.0	.1100	.150	.450	.150	.600	3.90	.50	.00024	1
318	318	20255.	157.0	20.0	.0300	.150	.550	.150	.500	3.90	.50	.00024	1
335	335	8868.	36.0	45.0	.0500	.150	.450	.150	.450	3.90	.50	.00024	1
336	1329	10002.	31.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
337	337	14520.	50.0	50.0	.0350	.150	.450	.150	.450	3.90	.50	.00024	1
312	312	7094.	12.0	70.0	.0400	.150	.450	.150	.250	3.90	.50	.00024	1
315	315	8712.	28.0	45.0	.0400	.150	.450	.150	.450	3.90	.50	.00024	1
316	316	12777.	43.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
358	358	4084.	12.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
320	320	22099.	161.0	50.0	.0250	.250	.450	.250	.600	3.90	.50	.00024	1
1323	1323	2406.	9.0	50.0	.0080	.150	.450	.150	.450	3.90	.50	.00024	1
321	321	47509.	25.0	60.0	.0450	.150	.450	.150	.350	3.90	.50	.00024	1
319	319	43000.	164.0	70.0	.0250	.150	.400	.150	.250	3.90	.50	.00024	1
370	370	14400.	41.0	70.0	.0250	.150	.400	.150	.250	3.90	.50	.00024	1
233	233	42776.	281.0	25.0	.0500	.150	.500	.150	.500	3.90	.50	.00024	1
235	235	20400.	187.0	20.0	.1100	.150	.500	.150	.500	3.90	.50	.00024	1
231	231	58487.	390.0	55.0	.0200	.150	.400	.150	.250	3.90	.50	.00024	1

OTOTAL NUMBER OF SUBCATCHMENTS, 314
 OTOTAL TRIBUTARY AREA (ACRES), 86852.00
 1

model sbc_ltd.swi
 10-year model

10_ltd.wpd July 12, 2000 10-YR SWMM MODEL

*** CONTINUITY CHECK FOR SUBCATCHMENT ROUTING IN UDSWM386 MODEL ***

WATERSHED AREA (ACRES) 86852.000
 TOTAL RAINFALL (INCHES) 2.697
 TOTAL INFILTRATION (INCHES) 2.188
 TOTAL WATERSHED OUTFLOW (INCHES) .483
 TOTAL SURFACE STORAGE AT END OF STORM (INCHES) .027
 ERROR IN CONTINUITY, PERCENTAGE OF RAINFALL -.031

1
 model sbc_ltd.swi
 10-year model

GUTTER NUMBER	GUTTER CONNECTION	NDP	NP		WIDTH OR DIAM (FT)	LENGTH (FT)	INVERT SLOPE (FT/FT)	SIDE SLOPES		MANNING N	OVERBANK/SURCHARGE		JK
								HORIZ L	TO VERT R		DEPTH (FT)		
226	224	0	1	CHANNEL	20.0	3740.	.1337	4.0	4.0	.040	15.00	0	
225	224	0	1	CHANNEL	5.0	1862.	.0600	10.0	10.0	.045	15.00	0	
224	222	0	1	CHANNEL	4.0	4220.	.1300	3.0	3.0	.055	15.00	0	
223	222	0	1	CHANNEL	10.0	5960.	.1406	10.0	10.0	.040	15.00	0	
222	218	0	1	CHANNEL	5.0	2280.	.1000	4.0	4.0	.055	15.00	0	
221	218	0	1	CHANNEL	5.0	6520.	.1992	5.0	5.0	.055	15.00	0	
220	219	0	1	CHANNEL	8.0	7580.	.2107	7.0	7.0	.050	15.00	0	
218	219	0	1	CHANNEL	5.0	1660.	.0900	4.0	4.0	.055	15.00	0	
219	215	0	1	CHANNEL	10.0	2531.	.1000	7.0	7.0	.055	15.00	0	
216	215	0	1	CHANNEL	20.0	8160.	.1875	10.0	10.0	.055	15.00	0	
214	212	0	1	CHANNEL	10.0	6880.	.1727	10.0	10.0	.055	15.00	0	
213	212	0	1	CHANNEL	10.0	5900.	.1268	10.0	10.0	.055	15.00	0	
212	211	0	1	CHANNEL	15.0	6100.	.1511	7.0	7.0	.060	15.00	0	
215	211	0	4	CHANNEL	10.0	5210.	.0600	4.0	4.0	.050	2.00	0	
				OVERFLOW	50.0	5210.	.0600	6.0	6.0	.055	25.00	0	
217	215	0	1	CHANNEL	20.0	4860.	.3560	5.0	5.0	.040	15.00	0	
211	207	0	4	CHANNEL	8.0	2390.	.0500	3.0	3.0	.050	2.00	0	
				OVERFLOW	25.0	2390.	.0500	5.0	5.0	.055	25.00	0	
186	184	0	1	CHANNEL	10.0	4260.	.1002	9.0	9.0	.060	15.00	0	
185	184	0	1	CHANNEL	5.0	3720.	.0594	6.0	6.0	.060	15.00	0	
183	182	0	1	CHANNEL	10.0	8000.	.1050	6.0	6.0	.060	15.00	0	
181	180	0	1	CHANNEL	5.0	6640.	.1583	7.0	7.0	.060	15.00	0	
184	182	0	1	CHANNEL	15.0	3540.	.1158	8.0	8.0	.055	15.00	0	
182	180	0	4	CHANNEL	15.0	4600.	.0720	4.0	4.0	.050	2.50	0	
				OVERFLOW	100.0	4370.	.0758	15.0	15.0	.055	20.00	0	
180	176	0	4	CHANNEL	10.0	4520.	.0507	4.0	4.0	.045	3.00	0	
				OVERFLOW	35.0	4294.	.0534	3.0	3.0	.060	20.00	0	
204	201	0	1	CHANNEL	15.0	6720.	.0911	6.0	6.0	.050	15.00	0	
203	201	0	1	CHANNEL	5.0	3500.	.2286	5.0	5.0	.055	15.00	0	
201	198	0	4	CHANNEL	15.0	7700.	.0835	4.0	4.0	.050	3.00	0	
				OVERFLOW	50.0	7315.	.0879	7.0	7.0	.060	20.00	0	
200	198	0	1	CHANNEL	5.0	7220.	.1722	7.0	7.0	.055	15.00	0	
202	198	0	1	CHANNEL	5.0	3820.	.1971	5.0	5.0	.060	15.00	0	
198	194	0	4	CHANNEL	25.0	7220.	.0370	4.0	4.0	.050	3.00	0	
				OVERFLOW	200.0	6860.	.0389	7.0	7.0	.060	20.00	0	
199	194	0	1	CHANNEL	5.0	9020.	.1233	6.0	6.0	.060	15.00	0	
196	194	0	1	CHANNEL	5.0	7320.	.1243	5.0	5.0	.060	15.00	0	
195	194	0	1	CHANNEL	10.0	4760.	.1513	5.0	5.0	.060	15.00	0	
194	192	0	4	CHANNEL	20.0	7560.	.0921	4.0	4.0	.055	3.00	0	
				OVERFLOW	80.0	7182.	.0969	10.0	10.0	.060	20.00	0	
208	207	0	1	CHANNEL	10.0	4260.	.2230	8.0	8.0	.060	15.00	0	
207	205	0	4	CHANNEL	25.0	5000.	.0150	4.0	4.0	.040	2.00	0	
				OVERFLOW	200.0	5000.	.0150	10.0	10.0	.050	25.00	0	
206	205	0	1	CHANNEL	25.0	3860.	.2591	5.0	5.0	.040	15.00	0	
205	192	0	4	CHANNEL	20.0	4900.	.0349	4.0	4.0	.045	3.00	0	
				OVERFLOW	100.0	4900.	.0349	8.0	8.0	.055	25.00	0	
192	187	0	4	CHANNEL	32.0	1540.	.0120	4.0	4.0	.040	3.00	0	
				OVERFLOW	250.0	1540.	.0120	20.0	20.0	.050	25.00	0	
193	187	0	1	CHANNEL	25.0	4480.	.1897	4.0	4.0	.040	15.00	0	
187	172	0	4	CHANNEL	32.0	7388.	.0100	4.0	4.0	.040	3.00	0	
				OVERFLOW	250.0	7388.	.0100	20.0	20.0	.050	25.00	0	
178	177	0	1	CHANNEL	5.0	6500.	.1186	8.0	8.0	.060	15.00	0	
177	175	0	1	CHANNEL	8.0	6020.	.0862	7.0	7.0	.055	15.00	0	
179	176	0	1	CHANNEL	20.0	3860.	.2383	5.0	5.0	.045	15.00	0	
176	175	0	4	CHANNEL	20.0	7520.	.0386	4.0	4.0	.045	3.00	0	
				OVERFLOW	100.0	7144.	.0406	5.0	5.0	.060	20.00	0	
174	173	0	1	CHANNEL	5.0	4060.	.1421	6.0	6.0	.055	15.00	0	
175	173	0	4	CHANNEL	30.0	1900.	.0353	4.0	4.0	.035	3.00	0	
				OVERFLOW	150.0	1905.	.0372	15.0	15.0	.045	20.00	0	
173	172	0	4	CHANNEL	25.0	5760.	.0587	4.0	4.0	.035	3.00	0	
				OVERFLOW	200.0	5472.	.0618	15.0	15.0	.045	20.00	0	
172	157	0	4	CHANNEL	25.0	1860.	.0100	3.0	3.0	.045	3.00	0	
				OVERFLOW	75.0	1860.	.0100	5.0	5.0	.050	25.00	0	
168	165	0	1	CHANNEL	5.0	3620.	.1740	7.0	7.0	.060	15.00	0	
169	165	0	1	CHANNEL	5.0	3140.	.1720	7.0	7.0	.060	15.00	0	
165	166	0	1	CHANNEL	10.0	6920.	.1026	5.0	5.0	.060	15.00	0	
167	166	0	1	CHANNEL	5.0	5360.	.1940	6.0	6.0	.060	15.00	0	
166	163	0	1	CHANNEL	15.0	1040.	.0673	10.0	10.0	.055	15.00	0	
164	163	0	1	CHANNEL	10.0	4000.	.1263	8.0	8.0	.050	15.00	0	
163	157	0	1	CHANNEL	25.0	2640.	.0568	5.0	5.0	.050	15.00	0	
170	157	0	1	CHANNEL	5.0	4840.	.1543	5.0	5.0	.055	15.00	0	
171	157	0	1	CHANNEL	5.0	4420.	.1837	7.0	7.0	.055	15.00	0	
157	156	0	4	CHANNEL	25.0	1660.	.0220	3.0	3.0	.045	3.00	0	
				OVERFLOW	75.0	1660.	.0220	4.0	4.0	.050	25.00	0	
161	160	0	1	CHANNEL	5.0	4380.	.1667	5.0	5.0	.060	15.00	0	

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162	160	0	1	CHANNEL	5.0	5800.	.2121	5.0	5.0	.060	15.00	0
160	158	0	1	CHANNEL	10.0	3360.	.0908	10.0	10.0	.055	15.00	0
159	158	0	1	CHANNEL	10.0	6380.	.1293	6.0	6.0	.060	15.00	0
158	156	0	1	CHANNEL	20.0	5700.	.0619	5.0	5.0	.050	15.00	0
156	154	0	4	CHANNEL	35.0	4980.	.0190	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	4980.	.0190	3.0	3.0	.055	25.00	0
155	154	0	1	CHANNEL	12.0	2180.	.2683	4.0	4.0	.050	15.00	0
153	152	0	1	CHANNEL	12.0	4380.	.1530	4.0	4.0	.060	15.00	0
154	152	0	4	CHANNEL	35.0	2880.	.0200	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	2880.	.0200	3.0	3.0	.055	25.00	0
152	149	0	4	CHANNEL	30.0	6980.	.0150	4.0	4.0	.045	3.00	0
				OVERFLOW	200.0	6980.	.0150	5.0	5.0	.050	25.00	0
150	149	0	1	CHANNEL	5.0	2780.	.1691	4.0	4.0	.055	15.00	0
151	149	0	1	CHANNEL	6.0	4120.	.1286	4.0	4.0	.055	15.00	0
149	139	0	4	CHANNEL	35.0	3220.	.0140	4.0	4.0	.045	3.00	0
				OVERFLOW	300.0	3220.	.0140	5.0	5.0	.050	25.00	0
147	146	0	1	CHANNEL	8.0	5600.	.1625	6.0	6.0	.060	15.00	0
148	146	0	1	CHANNEL	8.0	2720.	.1048	8.0	8.0	.060	15.00	0
146	142	0	1	CHANNEL	10.0	5540.	.0727	8.0	8.0	.055	15.00	0
144	143	0	1	CHANNEL	5.0	2200.	.1568	8.0	8.0	.060	15.00	0
145	143	0	1	CHANNEL	3.0	2160.	.1574	5.0	5.0	.060	15.00	0
143	142	0	1	CHANNEL	8.0	4840.	.1184	5.0	5.0	.060	15.00	0
142	140	0	1	CHANNEL	10.0	2080.	.0514	8.0	5.0	.055	15.00	0
141	140	0	1	CHANNEL	5.0	3800.	.1237	5.0	5.0	.060	15.00	0
140	139	0	1	CHANNEL	15.0	4320.	.0505	8.0	7.0	.055	15.00	0
138	137	0	1	CHANNEL	10.0	5440.	.0432	10.0	10.0	.055	15.00	0
139	137	0	4	CHANNEL	30.0	1880.	.0160	4.0	4.0	.045	3.00	0
				OVERFLOW	200.0	1880.	.0160	5.0	5.0	.050	25.00	0
137	129	0	4	CHANNEL	30.0	2009.	.0130	4.0	4.0	.040	3.00	0
				OVERFLOW	200.0	2009.	.0130	5.0	5.0	.050	25.00	0
135	134	0	1	CHANNEL	5.0	4080.	.1716	5.0	5.0	.060	15.00	0
136	134	0	1	CHANNEL	5.0	3000.	.1433	6.0	6.0	.060	15.00	0
134	133	0	1	CHANNEL	10.0	10020.	.0868	5.0	5.0	.055	15.00	0
133	130	0	1	CHANNEL	15.0	7720.	.0505	5.0	5.0	.055	15.00	0
131	130	0	4	CHANNEL	15.0	4860.	.1008	3.0	3.0	.055	3.00	0
				OVERFLOW	100.0	4617.	.1061	10.0	10.0	.060	20.00	0
132	130	0	1	CHANNEL	8.0	4560.	.0789	6.0	6.0	.060	15.00	0
130	129	0	1	CHANNEL	25.0	3360.	.0363	7.0	7.0	.055	15.00	0
129	96	0	4	CHANNEL	30.0	3520.	.0160	3.5	3.5	.055	4.00	0
				OVERFLOW	100.0	3520.	.0160	4.0	4.0	.060	25.00	0
125	124	0	1	CHANNEL	5.0	3800.	.1842	8.0	8.0	.055	15.00	0
126	124	0	1	CHANNEL	5.0	3420.	.1871	6.0	6.0	.060	15.00	0
124	122	0	1	CHANNEL	10.0	7520.	.0535	8.0	8.0	.055	15.00	0
127	123	0	1	CHANNEL	10.0	8000.	.1056	10.0	10.0	.055	15.00	0
128	123	0	1	CHANNEL	10.0	8660.	.1236	15.0	15.0	.055	15.00	0
123	122	0	1	CHANNEL	15.0	4160.	.0317	15.0	15.0	.055	15.00	0
122	96	0	1	CHANNEL	20.0	9440.	.0607	5.0	5.0	.060	15.00	0
96	95	0	4	CHANNEL	25.0	6320.	.0170	2.0	2.0	.055	4.00	0
				OVERFLOW	50.0	6320.	.0170	2.0	2.0	.060	25.00	0
116	95	0	4	CHANNEL	5.0	9520.	.0772	3.0	3.0	.050	2.50	0
				OVERFLOW	70.0	9044.	.0813	8.0	8.0	.055	20.00	0
95	94	0	4	CHANNEL	30.0	4000.	.0120	3.0	3.0	.040	3.00	0
				OVERFLOW	150.0	4000.	.0120	5.0	5.0	.050	25.00	0
85	84	0	1	CHANNEL	5.0	2220.	.0396	4.0	4.0	.060	15.00	0
86	84	0	1	CHANNEL	8.0	5880.	.1259	4.0	4.0	.060	15.00	0
84	82	0	1	CHANNEL	10.0	2720.	.0890	10.0	10.0	.060	15.00	0
83	82	0	1	CHANNEL	10.0	2380.	.0450	12.0	12.0	.060	15.00	0
82	80	0	1	CHANNEL	20.0	2220.	.0396	12.0	12.0	.060	15.00	0
87	81	0	1	CHANNEL	10.0	8040.	.0796	5.0	5.0	.065	15.00	0
81	80	0	1	CHANNEL	15.0	6220.	.0691	7.0	7.0	.065	15.00	0
80	79	0	1	CHANNEL	20.0	6380.	.1993	10.0	10.0	.065	15.00	0
121	79	0	4	CHANNEL	8.0	4700.	.0660	4.0	4.0	.055	2.50	0
				OVERFLOW	60.0	4465.	.0695	12.0	12.0	.057	20.00	0
79	75	0	1	CHANNEL	25.0	8020.	.0212	10.0	10.0	.060	15.00	0
78	75	0	1	CHANNEL	8.0	3780.	.0688	20.0	20.0	.060	15.00	0
75	77	0	1	CHANNEL	25.0	1600.	.0188	3.0	5.0	.060	15.00	0
77	74	0	1	CHANNEL	40.0	2020.	.0198	3.0	3.0	.060	15.00	0
76	74	0	4	CHANNEL	10.0	6420.	.0779	4.0	4.0	.050	2.00	0
				OVERFLOW	60.0	6420.	.0779	8.0	8.0	.055	20.00	0
74	59	0	4	CHANNEL	30.0	4700.	.0130	4.0	4.0	.050	4.00	0
				OVERFLOW	75.0	4700.	.0130	4.0	3.0	.055	25.00	0
89	88	0	1	CHANNEL	8.0	4240.	.0217	10.0	10.0	.055	15.00	0
93	88	0	1	CHANNEL	5.0	2440.	.0984	10.0	10.0	.055	15.00	0
88	77	0	4	CHANNEL	11.0	7200.	.1380	10.0	10.0	.060	3.00	0
				OVERFLOW	100.0	7200.	.1380	50.0	50.0	.045	20.00	0
120	119	0	4	CHANNEL	5.0	3980.	.0879	3.0	3.0	.050	3.00	0
				OVERFLOW	200.0	3791.	.0925	10.0	10.0	.055	20.00	0
118	119	0	4	CHANNEL	5.0	8220.	.1095	3.0	3.0	.050	3.00	0
				OVERFLOW	150.0	7809.	.1153	10.0	10.0	.055	20.00	0
119	104	0	4	CHANNEL	5.0	1300.	.0400	3.0	3.0	.050	3.00	0
				OVERFLOW	150.0	1235.	.0421	10.0	10.0	.055	20.00	0
117	104	0	4	CHANNEL	5.0	6000.	.0587	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	5700.	.0618	10.0	10.0	.055	20.00	0
104	103	0	4	CHANNEL	10.0	3440.	.0343	3.0	3.0	.045	3.00	0
				OVERFLOW	150.0	3268.	.0361	10.0	10.0	.050	20.00	0
105	103	0	4	CHANNEL	5.0	4560.	.0811	3.0	3.0	.045	3.00	0
				OVERFLOW	100.0	4332.	.0854	10.0	10.0	.050	20.00	0
106	102	0	4	CHANNEL	5.0	6380.	.0690	3.0	3.0	.045	3.00	0
				OVERFLOW	70.0	6061.	.0726	10.0	10.0	.050	20.00	0
103	102	0	4	CHANNEL	8.0	1380.	.0362	4.0	40.0	.050	3.00	0
				OVERFLOW	68.0	1311.	.0381	25.0	25.0	.055	20.00	0
102	101	0	4	CHANNEL	11.0	5220.	.0383	8.0	8.0	.055	3.00	0
				OVERFLOW	100.0	4959.	.0403	5.0	5.0	.060	20.00	0
114	112	0	1	CHANNEL	5.0	4500.	.1467	5.0	5.0	.060	8.00	0
115	112	0	1	CHANNEL	5.0	3240.	.1759	5.0	5.0	.060	8.00	0
112	110	0	4	CHANNEL	5.0	3640.	.1745	3.0	3.0	.055	2.50	0
				OVERFLOW	40.0	3458.	.1837	10.0	8.0	.060	20.00	0
113	110	0	4	CHANNEL	5.0	5060.	.1690	3.0	3.0	.055	3.00	0
				OVERFLOW	40.0	4807.	.1779	10.0	10.0	.060	20.00	0
110	109	0	4	CHANNEL	11.0	4140.	.0531	4.0	4.0	.055	3.00	0
				OVERFLOW	60.0	3933.	.0559	50.0	50.0	.060	20.00	0

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111	109	0	4	CHANNEL	5.0	5600.	.2348	3.0	3.0	.050	2.00	0	
				OVERFLOW	20.0	5320.	.2472	6.0	6.0	.055	20.00	0	
108	107	0	4	CHANNEL	5.0	6240.	.1875	3.0	3.0	.050	2.00	0	
				OVERFLOW	20.0	5928.	.1974	6.0	6.0	.055	20.00	0	
109	107	0	4	CHANNEL	11.0	2760.	.0525	4.0	4.0	.050	3.00	0	
				OVERFLOW	60.0	2622.	.0553	6.0	6.0	.055	20.00	0	
107	101	0	4	CHANNEL	11.0	2720.	.0368	4.0	4.0	.050	3.00	0	
				OVERFLOW	45.0	2584.	.0387	6.0	6.0	.055	20.00	0	
101	99	0	4	CHANNEL	11.0	1380.	.0268	4.0	4.0	.050	3.00	0	
				OVERFLOW	50.0	1311.	.0282	5.0	5.0	.055	20.00	0	
100	99	0	4	CHANNEL	5.0	9980.	.1735	3.0	3.0	.050	2.00	0	
				OVERFLOW	25.0	9481.	.1826	5.0	5.0	.055	20.00	0	
99	97	0	4	CHANNEL	11.0	1440.	.0299	4.0	4.0	.050	3.00	0	
				OVERFLOW	50.0	1368.	.0315	5.0	5.0	.055	20.00	0	
98	97	0	4	CHANNEL	8.0	7000.	.1179	3.0	3.0	.050	2.00	0	
				OVERFLOW	35.0	6650.	.1241	6.0	6.0	.055	20.00	0	
97	94	0	4	CHANNEL	11.0	5720.	.0332	4.0	4.0	.050	2.50	0	
				OVERFLOW	50.0	5434.	.0349	4.0	4.0	.055	20.00	0	
94	74	0	4	CHANNEL	32.0	2560.	.0120	4.0	4.0	.040	3.50	0	
				OVERFLOW	150.0	2560.	.0120	8.0	8.0	.050	25.00	0	
72	71	0	1	CHANNEL	10.0	4480.	.0808	5.0	5.0	.055	15.00	0	
73	71	0	1	CHANNEL	10.0	8000.	.0303	8.0	8.0	.055	15.00	0	
71	59	0	1	CHANNEL	12.0	4820.	.0664	5.0	5.0	.060	15.00	0	
59	46	0	4	CHANNEL	30.0	4020.	.0140	4.0	4.0	.050	4.00	0	
				OVERFLOW	60.0	4020.	.0140	3.0	3.0	.055	25.00	0	
63	61	0	1	CHANNEL	9.0	6420.	.0779	5.0	5.0	.070	20.00	0	
64	61	0	1	CHANNEL	9.0	2020.	.0198	5.0	5.0	.070	20.00	0	
61	62	0	1	CHANNEL	12.0	7500.	.0633	5.0	5.0	.070	20.00	0	
60	46	0	1	CHANNEL	12.0	4080.	.1262	5.0	5.0	.060	20.00	0	
46	42	0	4	CHANNEL	25.0	3220.	.0300	3.0	3.0	.055	5.00	0	
				OVERFLOW	50.0	3220.	.0300	4.0	4.0	.060	25.00	0	
66	65	0	1	CHANNEL	9.0	3060.	.2026	4.0	4.0	.060	15.00	0	
67	65	0	4	CHANNEL	10.0	6620.	.0853	3.0	3.0	.050	4.00	0	
				OVERFLOW	45.0	6289.	.0898	3.0	3.0	.060	25.00	0	
65	62	0	4	CHANNEL	15.0	3960.	.0088	3.0	3.0	.050	4.00	0	
				OVERFLOW	50.0	3762.	.0093	3.0	3.0	.060	25.00	0	
62	42	0	1	CHANNEL	12.0	1400.	.2629	5.0	5.0	.070	20.00	0	
69	68	0	1	CHANNEL	10.0	3740.	.1056	6.0	6.0	.055	15.00	0	
70	68	0	1	CHANNEL	12.0	6960.	.0912	6.0	6.0	.055	15.00	0	
68	42	0	1	CHANNEL	12.0	2120.	.1203	5.0	5.0	.060	15.00	0	
41	40	0	1	CHANNEL	12.0	3100.	.2423	5.0	5.0	.060	20.00	0	
42	40	0	4	CHANNEL	20.0	7580.	.0500	3.0	3.0	.055	4.00	0	
				OVERFLOW	50.0	7580.	.0500	2.0	2.0	.060	25.00	0	
40	16	0	4	CHANNEL	20.0	3000.	.0330	3.0	3.0	.055	4.00	0	
				OVERFLOW	50.0	3000.	.0330	2.0	2.0	.060	25.00	0	
20	18	0	1	CHANNEL	10.0	5340.	.0534	8.0	8.0	.050	15.00	0	
18	17	0	4	CHANNEL	11.0	7600.	.0605	3.0	3.0	.050	3.00	0	
				OVERFLOW	40.0	7220.	.0637	5.0	5.0	.055	20.00	0	
21	17	0	1	CHANNEL	10.0	6960.	.1042	5.0	5.0	.060	15.00	0	
17	16	0	4	CHANNEL	11.0	1000.	.0493	10.0	10.0	.040	3.00	0	
				OVERFLOW	40.0	1000.	.0493	8.0	8.0	.055	20.00	0	
14	15	0	1	CHANNEL	15.0	3080.	.2662	3.0	3.0	.060	15.00	0	
15	8	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
16	15	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
8	397	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
397	6	0	2	PIPE	.1	1.	.0050	.0	.0	.013	.10	0	
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW													
		.0	.0	207.0	170.0	415.0	476.0	833.0	1330.0	1254.0	2417.0	1677.0	3678.0
		2104.0	5078.0	2535.0	6591.0	2968.0	8200.0	3405.0	9896.0	3847.0	12853.0	4292.0	16870.0
		6098.0	37861.0	7880.0	91713.0								
38	37	0	1	CHANNEL	12.0	5060.	.1146	15.0	15.0	.050	15.00	0	
39	37	0	1	CHANNEL	10.0	5140.	.0807	10.0	10.0	.050	20.00	0	
37	23	0	4	CHANNEL	11.0	8160.	.0386	4.0	4.0	.050	3.00	0	
				OVERFLOW	60.0	7752.	.0406	25.0	25.0	.055	20.00	0	
35	34	0	1	CHANNEL	10.0	3140.	.0930	10.0	10.0	.050	15.00	0	
36	34	0	1	CHANNEL	12.0	5340.	.0549	15.0	15.0	.050	15.00	0	
34	23	0	4	CHANNEL	11.0	6840.	.0450	4.0	4.0	.050	3.00	0	
				OVERFLOW	50.0	6498.	.0474	25.0	25.0	.055	20.00	0	
32	31	0	1	CHANNEL	8.0	3260.	.0883	8.0	8.0	.055	15.00	0	
33	31	0	1	CHANNEL	8.0	5180.	.0788	8.0	8.0	.055	15.00	0	
31	23	0	1	CHANNEL	12.0	2720.	.0393	10.0	10.0	.055	15.00	0	
23	22	0	4	CHANNEL	11.0	4920.	.0315	3.0	3.0	.050	3.00	0	
				OVERFLOW	50.0	4674.	.0332	10.0	10.0	.055	20.00	0	
29	28	0	1	CHANNEL	5.0	3060.	.1471	6.0	6.0	.055	15.00	0	
30	28	0	1	CHANNEL	12.0	5780.	.0484	15.0	15.0	.050	15.00	0	
27	26	0	1	CHANNEL	10.0	2540.	.1693	10.0	10.0	.040	15.00	0	
28	26	0	4	CHANNEL	11.0	2520.	.0595	10.0	10.0	.040	3.00	0	
				OVERFLOW	80.0	2394.	.0626	25.0	25.0	.045	15.00	0	
25	24	0	1	CHANNEL	6.0	5920.	.1309	8.0	8.0	.050	15.00	0	
26	24	0	4	CHANNEL	12.0	1860.	.0242	4.0	4.0	.050	3.00	0	
				OVERFLOW	80.0	1767.	.0255	10.0	10.0	.055	15.00	0	
24	22	0	4	CHANNEL	12.0	1740.	.0287	4.0	4.0	.050	3.00	0	
				OVERFLOW	100.0	1653.	.0302	10.0	10.0	.055	20.00	0	
22	8	0	4	CHANNEL	11.0	3600.	.0658	3.0	3.0	.050	3.00	0	
				OVERFLOW	40.0	3600.	.0658	6.0	6.0	.055	20.00	0	
9	7	0	4	CHANNEL	3.0	10320.	.1556	3.0	3.0	.060	2.00	0	
				OVERFLOW	20.0	9804.	.1638	2.0	2.0	.080	25.00	0	
10	7	0	1	CHANNEL	15.0	3760.	.1293	3.0	3.0	.040	15.00	0	
7	5	0	4	CHANNEL	5.0	4940.	.0656	2.0	2.0	.060	2.50	0	
				OVERFLOW	25.0	4693.	.0691	2.0	2.0	.080	20.00	0	
3	2	0	1	CHANNEL	25.0	11000.	.0682	4.0	4.0	.040	15.00	0	
4	2	0	1	CHANNEL	25.0	12780.	.1033	4.0	4.0	.040	15.00	0	
2	1	0	4	CHANNEL	8.0	7240.	.0631	2.0	2.0	.070	3.00	0	
				OVERFLOW	30.0	6878.	.0664	2.0	2.0	.080	20.00	0	
6	5	0	4	CHANNEL	35.0	4840.	.0340	2.0	2.0	.055	4.00	0	
				OVERFLOW	60.0	4840.	.0340	2.0	2.0	.065	25.00	0	
5	1	0	4	CHANNEL	30.0	4960.	.0240	2.0	2.0	.055	4.00	0	
				OVERFLOW	55.0	4960.	.0240	2.0	2.0	.065	25.00	0	
1	245	0	4	CHANNEL	30.0	10240.	.0240	2.0	2.0	.055	4.00	0	
				OVERFLOW	55.0	10240.	.0240	2.0	2.0	.065	25.00	0	
11	13	0	1	CHANNEL	12.0	3000.	.1200	3.0	3.0	.040	15.00	0	

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12	13	0	1	CHANNEL	12.0	4180.	.1340	3.0	3.0	.040	15.00	0	
13	5	0	4	CHANNEL	15.0	5240.	.1202	4.0	4.0	.040	5.00	0	
				OVERFLOW	100.0	4978.	.1265	40.0	40.0	.045	20.00	0	
248	250	0	4	CHANNEL	25.0	9340.	.0931	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	8873.	.0980	40.0	40.0	.080	20.00	0	
249	250	0	4	CHANNEL	20.0	3940.	.0964	4.0	4.0	.060	5.00	0	
				OVERFLOW	80.0	3743.	.1015	40.0	40.0	.080	20.00	0	
247	246	0	4	CHANNEL	25.0	8120.	.0924	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	7714.	.0973	40.0	40.0	.080	20.00	0	
250	246	0	4	CHANNEL	25.0	2060.	.0485	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	1957.	.0511	40.0	40.0	.080	20.00	0	
246	245	0	4	CHANNEL	25.0	4660.	.0676	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	4427.	.0712	40.0	40.0	.080	20.00	0	
244	52	0	4	CHANNEL	25.0	8700.	.0989	4.0	4.0	.070	5.00	0	
				OVERFLOW	100.0	8265.	.1041	40.0	40.0	.080	20.00	0	
245	52	0	4	CHANNEL	30.0	3060.	.0300	3.0	3.0	.070	4.00	0	
				OVERFLOW	60.0	3060.	.0300	2.0	2.0	.080	20.00	0	
54	53	0	1	CHANNEL	5.0	4000.	.1500	3.0	3.0	.060	15.00	0	
55	53	0	1	CHANNEL	5.0	5500.	.1382	3.0	3.0	.060	15.00	0	
53	52	0	1	CHANNEL	5.0	1200.	.1083	3.0	3.0	.060	15.00	0	
51	50	0	4	CHANNEL	5.0	5200.	.1327	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	4940.	.1397	40.0	40.0	.080	20.00	0	
52	50	0	4	CHANNEL	35.0	9160.	.0218	3.0	3.0	.055	4.00	0	
				OVERFLOW	65.0	9160.	.0218	2.0	2.0	.065	25.00	0	
50	48	0	4	CHANNEL	40.0	3400.	.0294	5.0	5.0	.060	4.00	0	
				OVERFLOW	150.0	3400.	.0294	75.0	75.0	.080	25.00	0	
57	56	0	4	CHANNEL	25.0	8400.	.1262	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	7980.	.1328	40.0	40.0	.080	20.00	0	
58	56	0	1	CHANNEL	5.0	2200.	.1636	3.0	3.0	.060	15.00	0	
56	50	0	4	CHANNEL	25.0	10000.	.0930	4.0	4.0	.070	5.00	0	
				OVERFLOW	100.0	9500.	.0979	40.0	40.0	.080	20.00	0	
49	48	0	1	CHANNEL	12.0	3200.	.2594	3.0	3.0	.060	8.00	0	
48	1626	0	4	CHANNEL	30.0	4700.	.0133	2.0	2.0	.070	5.00	0	
				OVERFLOW	200.0	4700.	.0133	2.0	2.0	.085	25.00	0	
1238	1927	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1927	238	0	4	CHANNEL	15.0	964.	.0012	3.5	3.5	.045	4.00	0	
				OVERFLOW	70.0	964.	.0012	7.5	5.0	.055	20.00	0	
1295	295	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
295	1296	10	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0	
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW													
		.0	.0	8.3	.5	17.8	1.0	28.1	10.5	39.4	18.2	52.5	23.5
		68.3	278.0	86.7	1321.5	107.1	5035.0	150.0	10000.0				
1296	296	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
296	1382	6	3		.0	1.	.0010	.0	.0	.001	10.00	1383	
DIVERSION TO GUTTER NUMBER1383 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	24.0	.1	278.0	250.0	1321.0	1290.0	5035.0	5000.0	10000.0	9964.0
1382	1381	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
384	1820	0	5	PIPE	3.0	4047.	.0176	.0	.0	.020	3.00	0	
				OVERFLOW	1.0	4047.	.0176	20.0	20.0	.020	50.00	0	
1820	383	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1383	1820	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
383	1405	8	3		.0	1.	.0010	.0	.0	.001	10.00	1360	
DIVERSION TO GUTTER NUMBER1360 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	150.0	1.0	223.0	23.0	285.0	75.0	426.0	201.0	1592.0	1342.0
		3953.0	3653.0	10000.0	9690.0								
1405	1381	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1381	382	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
382	381	0	5	PIPE	7.5	1142.	.0020	.0	.0	.015	7.50	0	
				OVERFLOW	7.5	1142.	.0020	20.0	20.0	.015	50.00	0	
381	1926	4	3		.0	1.	.0010	.0	.0	.001	10.00	1366	
DIVERSION TO GUTTER NUMBER1366 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	150.0	1.0	342.0	182.0	2438.0	2050.0				
369	1821	0	4	CHANNEL	.5	1030.	.0089	12.0	12.0	.016	.50	0	
				OVERFLOW	10.0	1030.	.0089	20.0	20.0	.020	10.00	0	
1926	1821	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1821	380	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
380	379	0	1	CHANNEL	8.0	754.	.0040	1.5	1.5	.050	10.00	0	
379	1406	4	3		.0	1.	.0010	.0	.0	.001	10.00	1367	
DIVERSION TO GUTTER NUMBER1367 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	180.0	.1	629.0	354.0	3656.0	3293.0				
1406	1378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1404	1378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1378	378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
378	1925	5	3		.0	1.	.0010	.0	.0	.001	10.00	1289	
DIVERSION TO GUTTER NUMBER1289 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	90.0	1.0	95.0	5.0	363.0	253.0	528.0	390.0		
1925	377	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
377	242	0	1	CHANNEL	8.0	2080.	.0040	1.5	1.5	.055	10.00	0	
1715	1716	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1716	1517	0	4	CHANNEL	10.0	3321.	.0032	8.0	8.0	.035	.50	0	
				OVERFLOW	30.0	3321.	.0032	80.0	80.0	.035	15.00	0	
1515	1517	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1517	1522	0	4	CHANNEL	4.0	851.	.0035	8.0	8.0	.035	.50	0	
				OVERFLOW	20.0	851.	.0035	60.0	60.0	.035	15.00	0	
1541	1542	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1542	1544	0	4	CHANNEL	5.0	10122.	.0260	4.0	4.0	.040	2.00	0	
				OVERFLOW	30.0	10122.	.0260	80.0	80.0	.045	15.00	0	
1520	1521	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1525	1526	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1528	1428	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1428	1429	0	4	CHANNEL	4.0	1682.	.0131	2.0	2.0	.025	2.00	0	
				OVERFLOW	400.0	1682.	.0131	40.0	40.0	.035	15.00	0	
1415	1416	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1550	1551	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1560	1561	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1561	1563	0	4	CHANNEL	3.0	2480.	.1940	4.0	4.0	.050	2.00	0	
				OVERFLOW	25.0	2480.	.1940	50.0	50.0	.055	15.00	0	
1565	1566	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1566	1563	0	4	CHANNEL	3.0	2240.	.2140	4.0	4.0	.050	2.00	0	
				OVERFLOW	25.0	2240.	.2140	6.0	6.0	.055	15.00	0	
1563	1551	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	

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1551	1553	0	4	CHANNEL	3.0	8900.	.0560	5.0	5.0	.040	2.00	0
				OVERFLOW	30.0	8900.	.0560	50.0	50.0	.045	10.00	0
1570	1571	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1571	1557	0	1	CHANNEL	5.0	1200.	.2670	40.0	40.0	.055	10.00	0
1556	1557	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1557	1553	0	4	CHANNEL	3.0	5620.	.0240	5.0	5.0	.040	2.00	0
				OVERFLOW	25.0	5620.	.0240	40.0	40.0	.045	15.00	0
1553	1416	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1416	1429	0	4	CHANNEL	5.0	4085.	.0225	4.0	4.0	.050	2.00	0
				OVERFLOW	25.0	4085.	.0225	40.0	40.0	.055	15.00	0
1429	1526	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1526	1532	0	4	CHANNEL	2.0	1410.	.0136	2.0	2.0	.055	2.00	0
				OVERFLOW	400.0	1410.	.0136	40.0	40.0	.065	15.00	0
1530	1531	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1545	1546	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1575	1576	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1576	1546	0	4	CHANNEL	2.0	3500.	.0229	5.0	5.0	.050	2.00	0
				OVERFLOW	30.0	3500.	.0229	50.0	50.0	.055	15.00	0
1546	1531	0	4	CHANNEL	5.0	7763.	.0840	4.0	4.0	.050	2.00	0
				OVERFLOW	30.0	7763.	.0840	75.0	75.0	.055	15.00	0
1531	1532	0	4	CHANNEL	5.0	5288.	.0872	4.0	4.0	.040	2.00	0
				OVERFLOW	30.0	5288.	.0872	80.0	80.0	.045	15.00	0
1532	1537	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1537	1533	0	4	CHANNEL	2.0	1127.	.0035	2.0	2.0	.035	2.00	0
				OVERFLOW	400.0	1127.	.0035	5.0	40.0	.035	15.00	0
1414	1534	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1534	1533	0	4	CHANNEL	10.0	1966.	.0080	5.0	5.0	.050	1.00	0
				OVERFLOW	400.0	1966.	.0080	50.0	3.0	.065	15.00	0
1533	1521	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1521	1544	0	4	CHANNEL	4.0	2633.	.0093	2.0	2.0	.050	2.00	0
				OVERFLOW	500.0	2633.	.0093	25.0	25.0	.065	10.00	0
1544	1548	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1548	1522	0	4	CHANNEL	4.0	1054.	.0038	8.0	8.0	.035	.50	0
				OVERFLOW	500.0	1054.	.0038	60.0	60.0	.035	15.00	0
1522	1511	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1510	1511	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1511	1513	0	4	CHANNEL	4.0	3213.	.0057	2.0	2.0	.050	2.00	0
				OVERFLOW	512.0	3213.	.0057	50.0	50.0	.060	10.00	0
1513	1514	8	3		.0	1.	.0010	.0	.0	.001	10.00	1508
DIVERSION TO GUTTER NUMBER 1508 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	50.0	.1	140.0	48.0	415.0	192.0	1791.0	1299.0	3930.0 3176.0
		7762.0	6551.0	15011.0	13210.0							
1514	1442	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1442	1935	0	4	CHANNEL	2.0	2252.	.0097	4.0	4.0	.040	1.00	0
				OVERFLOW	300.0	2252.	.0097	80.0	80.0	.060	15.00	0
1262	1916	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1916	1935	0	4	CHANNEL	2.0	1211.	.0046	5.0	3.0	.035	1.00	0
				OVERFLOW	400.0	1211.	.0046	100.0	3.0	.035	20.00	0
1935	262	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
262	263	0	4	CHANNEL	2.0	529.	.0058	5.0	3.0	.035	1.00	0
				OVERFLOW	500.0	529.	.0058	150.0	3.0	.035	20.00	0
263	1905	8	3		.0	1.	.0010	.0	.0	.001	10.00	266
DIVERSION TO GUTTER NUMBER 266 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	175.0	174.9	412.0	185.0	908.0	198.0	1902.0	212.0	3161.0 228.0
		6477.0	233.0	13854.0	256.0							
1905	264	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
264	265	0	4	CHANNEL	2.0	1138.	.0017	5.0	3.0	.035	.50	0
				OVERFLOW	600.0	1138.	.0017	150.0	3.0	.035	20.00	0
265	269	8	3		.0	1.	.0010	.0	.0	.001	10.00	1267
DIVERSION TO GUTTER NUMBER 1267 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	170.0	169.9	227.0	195.0	710.0	516.0	1689.0	1249.0	2933.0 1956.0
		6244.0	3358.0	13598.0	6585.0							
269	1294	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1294	294	0	4	CHANNEL	2.0	1043.	.0027	4.0	4.0	.025	1.00	0
				OVERFLOW	375.0	1043.	.0027	80.0	3.0	.035	15.00	0
304	294	0	1	CHANNEL	8.0	2370.	.0060	5.0	5.0	.035	10.00	0
299	303	0	4	CHANNEL	.5	3612.	.0400	12.0	12.0	.016	.50	0
				OVERFLOW	24.0	3612.	.0400	20.0	20.0	.020	10.00	0
301	300	0	4	CHANNEL	.5	3743.	.0800	12.0	12.0	.016	.50	0
				OVERFLOW	24.0	3743.	.0800	20.0	20.0	.020	10.00	0
300	1922	5	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	5.4	10.0	28.7	11.0	36.6	32.0	39.3	468.0	
1922	303	0	4	CHANNEL	.5	899.	.0667	12.0	12.0	.016	.50	0
				OVERFLOW	10.0	899.	.0667	20.0	20.0	.020	10.00	0
303	298	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
298	297	11	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	.1	15.0	.5	45.0	1.4	94.0	2.9	130.0	5.3 158.0
		9.3	182.0	12.2	192.0	15.9	225.0	20.4	286.0	25.0	827.0	
297	1921	0	4	CHANNEL	6.0	5106.	.0250	3.0	3.0	.045	6.00	0
				OVERFLOW	50.0	6800.	.0188	3.0	3.0	.035	10.00	0
1917	1921	0	4	CHANNEL	5.0	1894.	.0079	8.0	8.0	.035	1.00	0
				OVERFLOW	40.0	1894.	.0079	80.0	80.0	.035	15.00	0
1921	1920	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1920	294	0	4	CHANNEL	18.0	785.	.0013	6.0	6.0	.035	6.00	0
				OVERFLOW	100.0	785.	.0013	12.0	12.0	.035	15.00	0
294	280	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
280	1293	6	3		.0	1.	.0010	.0	.0	.001	10.00	1295
DIVERSION TO GUTTER NUMBER 1295 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	295.0	1.0	370.0	42.0	1046.0	661.0	2827.0	2327.0	8734.0 8169.0
1293	293	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
293	267	0	5	PIPE	8.5	757.	.0020	.0	.0	.015	8.50	0
				OVERFLOW	8.5	757.	.0020	.0	.0	.015	20.00	0
1267	267	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
267	268	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
268	1291	8	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	1.4	81.0	5.0	267.0	10.4	465.0	16.9	632.0	25.0 1145.0
		35.1	1888.0	140.0	10000.0							
1291	291	0	3		.0	1.	.0010	.0	.0	.001	10.00	0

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291		1290		6		3		.0		1.		.0010		.0		.0		.001		10.00		1923				
DIVERSION TO GUTTER NUMBER1923 - TOTAL Q VS DIVERTED Q IN CFS																										
		.0		.0		515.0		1.0		1249.0		471.0		1956.0		1098.0		6585.0		5685.0		10000.0		9000.0		
1290	290	0	3																							
290	1924	0	4	CHANNEL	30.0	1375.	.0017	4.0	4.0	.045																
				OVERFLOW	100.0	1375.	.0017	20.0	20.0	.050																
1289	1924	0	3																							
1924	289	0	3																							
289	242	0	4	CHANNEL	30.0	1962.	.0017	4.0	4.0	.045																
				OVERFLOW	100.0	1962.	.0017	20.0	20.0	.050																
1505	1506	0	3																							
1410	1411	0	3																							
1420	1421	0	3																							
1435	1436	0	3																							
1436	1438	0	4	CHANNEL	2.0	3730.	.0350	4.0	4.0	.050																
				OVERFLOW	30.0	3730.	.0350	16.0	16.0	.055																
1430	1431	0	3																							
1431	1438	0	4	CHANNEL	2.0	1670.	.0820	4.0	4.0	.040																
				OVERFLOW	12.0	1670.	.0820	15.0	15.0	.045																
1438	1426	0	3																							
1425	1426	0	3																							
1426	1421	0	4	CHANNEL	5.0	2319.	.0190	8.0	8.0	.040																
				OVERFLOW	40.0	2319.	.0190	75.0	75.0	.045																
1445	1446	0	3																							
1446	1453	0	4	CHANNEL	2.0	6667.	.0606	3.0	3.0	.040																
				OVERFLOW	25.0	6667.	.0606	6.0	6.0	.045																
1645	1646	0	3																							
1646	1643	0	4	CHANNEL	5.0	5300.	.1450	4.0	4.0	.060																
				OVERFLOW	25.0	5300.	.1450	15.0	15.0	.065																
1640	1641	0	3																							
1641	1643	0	4	CHANNEL	2.0	5800.	.0160	3.0	3.0	.060																
				OVERFLOW	25.0	5800.	.0160	8.0	8.0	.065																
1643	1631	0	3																							
1630	1631	0	3																							
1631	1628	0	4	CHANNEL	10.0	7611.	.0730	4.0	4.0	.040																
				OVERFLOW	40.0	7611.	.0730	10.0	10.0	.045																
1625	1626	0	3																							
1635	1636	0	3																							
1636	1626	0	1	CHANNEL	2.0	4200.	.0840	8.0	8.0	.040																
1626	1628	0	4	CHANNEL	25.0	1908.	.0205	4.0	4.0	.070																
				OVERFLOW	100.0	1908.	.0205	75.0	75.0	.075																
1628	1611	0	3																							
1610	1611	0	3																							
1611	1928	0	4	CHANNEL	30.0	4400.	.0290	4.0	4.0	.060																
				OVERFLOW	150.0	4400.	.0290	75.0	75.0	.070																
1605	1606	0	3																							
1665	1666	0	3																							
1666	1606	0	4	CHANNEL	3.0	6900.	.2130	3.0	3.0	.050																
				OVERFLOW	20.0	6900.	.2130	2.0	2.0	.055																
1606	1928	0	4	CHANNEL	5.0	5987.	.0812	4.0	4.0	.045																
				OVERFLOW	25.0	5987.	.0812	3.0	3.0	.060																
1928	1601	0	3																							
1600	1601	0	3																							
1601	1603	0	4	CHANNEL	25.0	1264.	.0290	6.0	6.0	.060																
				OVERFLOW	85.0	1264.	.0290	80.0	80.0	.070																
1710	1711	0	3																							
1711	1712	0	4	CHANNEL	5.0	5430.	.0479	4.0	4.0	.035																
				OVERFLOW	30.0	5430.	.0479	5.0	5.0	.035																
1615	1616	0	3																							
1616	1623	0	4	CHANNEL	2.0	6409.	.0620	3.0	3.0	.040																
				OVERFLOW	20.0	6409.	.0620	5.0	5.0	.045																
1660	1661	0	3																							
1661	1651	0	4	CHANNEL	3.0	9600.	.1670	4.0	4.0	.060																
				OVERFLOW	25.0	9600.	.1670	3.0	3.0	.065																
1650	1651	0	3																							
1651	1653	0	4	CHANNEL	5.0	4100.	.0860	4.0	4.0	.050																
				OVERFLOW	25.0	4100.	.0860	3.0	3.0	.055																
1655	1656	0	3																							
1656	1653	0	4	CHANNEL	3.0	10800.	.1170	4.0	4.0	.050																
				OVERFLOW	25.0	10800.	.1170	3.0	3.0	.055																
1653	1621	0	3																							
1620	1621	0	3																							
1621	1623	0	4	CHANNEL	5.0	10100.	.0320	5.0	5.0	.045																
				OVERFLOW	35.0	10100.	.0320	2.0	2.0																	

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		.0	.0	500.0	1.0	999.0	125.0	1886.0	841.0	2765.0	1456.0	3403.0	1937.0
1509	1800	4421.0	2668.0	7425.0	5187.0	13357.0	10368.0						
1490	1491	0	3					.0010	.0	.0	.001	10.00	0
1455	1456	0	3					.0010	.0	.0	.001	10.00	0
1938	1480	0	3					.0010	.0	.0	.001	10.00	0
1480	1481	0	4					.0010	.0	.0	.001	10.00	0
				CHANNEL	5.0	2400.		.0500	2.0	2.0	.040	2.00	0
				OVERFLOW	20.0	2400.		.0500	10.0	10.0	.045	10.00	0
1481	1482	7	2					.0010	.0	.0	.030	.10	0
				PIPE	.0	1.							
				RESERVOIR STORAGE IN ACRE- FEET VS SPILLWAY OUTFLOW									
		.0	.0	308.0	18.0	624.0	76.0	947.0	179.0	1279.0	318.0	1618.0	1676.0
		1965.0	4700.0										
1482	1456	0	3					.0010	.0	.0	.001	10.00	0
1456	1457	0	1	CHANNEL	2.0	4450.		.0363	80.0	80.0	.030	20.00	0
1457	1491	0	3					.0010	.0	.0	.001	10.00	0
1491	1931	0	4	CHANNEL	5.0	10236.		.0090	4.0	4.0	.050	2.00	0
				OVERFLOW	25.0	10236.		.0090	60.0	60.0	.065	15.00	0
1460	1461	0	3					.0010	.0	.0	.001	10.00	0
1461	1931	0	4	CHANNEL	3.0	2286.		.0280	4.0	4.0	.050	2.00	0
				OVERFLOW	20.0	2286.		.0280	24.0	24.0	.055	15.00	0
1931	1933	0	3					.0010	.0	.0	.001	10.00	0
1933	1467	0	4	CHANNEL	5.0	403.		.0099	2.0	2.0	.020	2.00	0
				OVERFLOW	25.0	403.		.0099	10.0	10.0	.025	15.00	0
1465	1932	0	3					.0010	.0	.0	.001	10.00	0
1932	1467	0	4	CHANNEL	4.0	1591.		.0289	8.0	8.0	.035	.50	0
				OVERFLOW	25.0	1591.		.0289	4.0	4.0	.035	15.00	0
1467	1468	0	3					.0010	.0	.0	.001	10.00	0
1468	1800	0	4	CHANNEL	5.0	2357.		.0180	2.0	2.0	.020	2.00	0
				OVERFLOW	25.0	2357.		.0180	10.0	10.0	.025	15.00	0
1800	1506	0	3					.0010	.0	.0	.001	10.00	0
1506	1507	0	4	CHANNEL	33.0	8099.		.0054	4.0	4.0	.060	2.50	0
				OVERFLOW	800.0	8099.		.0054	10.0	10.0	.065	15.00	0
1508	1507	0	3					.0010	.0	.0	.001	10.00	0
1507	1512	0	3					.0010	.0	.0	.001	10.00	0
1512	44	0	4	CHANNEL	33.0	1367.		.0064	4.0	4.0	.060	2.50	0
				OVERFLOW	308.0	1367.		.0064	80.0	80.0	.065	15.00	0
1500	1501	0	3					.0010	.0	.0	.001	10.00	0
1501	44	0	4	CHANNEL	5.0	8609.		.0212	2.0	2.0	.040	2.00	0
				OVERFLOW	20.0	8609.		.0212	10.0	10.0	.045	15.00	0
44	261	0	3					.0010	.0	.0	.001	10.00	0
261	1427	9	3					.0010	.0	.0	.001	10.00	1262
				DIVERSION TO GUTTER NUMBER1262 - TOTAL Q VS DIVERTED Q IN CFS									
		.0	.0	500.0	1.0	875.0	35.0	1920.0	315.0	2709.0	660.0	3916.0	1323.0
		5586.0	2377.0	9768.0	5344.0	18394.0	11928.0						
1427	243	0	3					.0010	.0	.0	.001	10.00	0
243	242	0	4	CHANNEL	65.0	2991.		.0112	2.0	2.0	.043	2.50	0
				OVERFLOW	650.0	2991.		.0112	100.0	100.0	.055	15.00	0
242	241	0	3					.0010	.0	.0	.001	10.00	0
241	240	0	4	CHANNEL	65.0	5732.		.0100	2.0	2.0	.043	3.00	0
				OVERFLOW	1200.0	5732.		.0100	200.0	200.0	.055	20.00	0
240	238	0	4	CHANNEL	65.0	2861.		.0100	2.0	2.0	.050	3.00	0
				OVERFLOW	1200.0	2861.		.0100	200.0	200.0	.075	20.00	0
238	237	0	3					.0010	.0	.0	.001	10.00	0
237	251	5	3					.0010	.0	.0	.001	10.00	389
				DIVERSION TO GUTTER NUMBER 389 - TOTAL Q VS DIVERTED Q IN CFS									
		.0	.0	2060.0	1.0	4980.0	2580.0	6630.0	3530.0	11150.0	7500.0		
389	1906	0	3					.0010	.0	.0	.001	10.00	0
1906	1909	0	4	CHANNEL	10.0	3340.		.0042	8.0	8.0	.025	15.00	0
				OVERFLOW	1200.0	3340.		.0042	80.0	80.0	.025	15.00	0
251	233	0	3					.0010	.0	.0	.001	10.00	0
235	239	0	1	CHANNEL	1.0	3509.		.0050	50.0	50.0	.020	10.00	0
239	234	0	3					.0010	.0	.0	.001	10.00	0
234	232	0	4	CHANNEL	2.0	2072.		.0044	3.0	3.0	.050	2.00	0
				OVERFLOW	50.0	2072.		.0044	50.0	50.0	.035	10.00	0
233	232	0	4	CHANNEL	65.0	3076.		.0100	2.0	2.0	.050	4.00	0
				OVERFLOW	600.0	3076.		.0100	200.0	200.0	.080	20.00	0
232	236	0	3					.0010	.0	.0	.001	10.00	0
236	252	5	3					.0010	.0	.0	.001	10.00	1403
				DIVERSION TO GUTTER NUMBER1403 - TOTAL Q VS DIVERTED Q IN CFS									
		.0	.0	2060.0	1.0	2400.0	100.0	3100.0	500.0	10000.0	2500.0		
1403	1599	0	3					.0010	.0	.0	.001	10.00	0
252	231	0	3					.0010	.0	.0	.001	10.00	0
1357	357	0	3					.0010	.0	.0	.001	10.00	0
357	1401	6	3					.0010	.0	.0	.001	10.00	1325
				DIVERSION TO GUTTER NUMBER1325 - TOTAL Q VS DIVERTED Q IN CFS									
		.0	.0	26.0	.1	263.0	235.0	391.0	361.0	995.0	960.0	5000.0	4950.0
1401	1387	0	3					.0010	.0	.0	.001	10.00	0
1387	387	0	3					.0010	.0	.0	.001	10.00	0
387	1908	0	3					.0010	.0	.0	.001	10.00	0
1908	1320	0	4	CHANNEL	2.0	1718.		.0076	3.0	3.0	.025	2.00	0
				OVERFLOW	600.0	1718.		.0076	80.0	80.0	.025	10.00	0
266	376	0	3					.0010	.0	.0	.001	10.00	0
376	375	0	1	CHANNEL	4.0	1569.		.0041	4.0	4.0	.050	10.00	0
375	1374	4	3					.0010	.0	.0	.001	10.00	1404
				DIVERSION TO GUTTER NUMBER1404 - TOTAL Q VS DIVERTED Q IN CFS									
		.0	.0	24.0	.1	135.0	100.0	540.0	500.0				
1374	374	0	3					.0010	.0	.0	.001	10.00	0
374	372	0	4	CHANNEL	4.0	2538.		.0115	3.0	3.0	.045	2.00	0
				OVERFLOW	20.0	2538.		.0115	20.0	20.0	.035	10.00	0
373	372	0	4	CHANNEL	3.0	1779.		.0075	4.0	4.0	.045	1.00	0
				OVERFLOW	20.0	1779.		.0075	20.0	20.0	.035	10.00	0
1367	367	0	3					.0010	.0	.0	.001	10.00	0
367	372	0	4	CHANNEL	.5	2663.		.0103	12.0	12.0	.016	.50	0
				OVERFLOW	10.0	2663.		.0103	20.0	20.0	.020	10.00	0
372	371	0	3					.0010	.0	.0	.001	10.00	0
371	311	0	4	CHANNEL	10.0	2893.		.0078	2.0	2.0	.045	1.00	0
				OVERFLOW	10.0	2893.		.0078	50.0	50.0	.035	10.00	0
1339	1822	0	3					.0010	.0	.0	.001	10.00	0
1348	348	0	3					.0010	.0	.0	.001	10.00	0
348	1937	5	3					.0010	.0	.0	.001	10.00	1331
				DIVERSION TO GUTTER NUMBER1331 - TOTAL Q VS DIVERTED Q IN CFS									

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		.0	.0	40.0	.1	314.0	77.0	1075.0	357.0	2228.0	783.0	4144.0	1719.0
1814	351	6379.0	2711.0										
351	1913	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1915	1816	0	3			2.0	2056.	.0117	.0	.0	.015	2.00	0
1818	1817	0	4	CHANNEL		40.0	2056.	.0117	8.0	8.0	.035	15.00	0
1816	1817	0	4	CHANNEL		2.0	354.	.0100	4.0	4.0	.020	1.00	0
1817	354	0	3	OVERFLOW		12.0	354.	.0100	10.0	10.0	.030	10.00	0
354	1913	0	5	OVERFLOW		6.0	837.	.0037	12.0	12.0	.015	1.00	0
1913	1914	0	3	OVERFLOW		30.0	837.	.0037	8.0	3.0	.030	15.00	0
1914	1915	0	5	PIPE		.0	1.	.0010	.0	.0	.001	10.00	0
1915	347	0	5	OVERFLOW		1.5	1345.	.2800	.0	.0	.015	1.50	0
347	359	0	5	OVERFLOW		24.0	1345.	.2800	20.0	5.0	.035	15.00	0
349	359	0	1	PIPE		.0	1.	.0010	.0	.0	.001	10.00	0
355	359	0	5	OVERFLOW		2.0	756.	.0066	.0	.0	.016	2.00	0
359	356	0	3	OVERFLOW		1.0	756.	.0066	20.0	20.0	.020	15.00	0
356	1343	10	2	PIPE		.0	1.	.0010	.0	.0	.001	10.00	0
		9.7	332.0	14.5	1712.0	18.2	2617.0	23.4	5064.0	6.6	210.0	7.7	230.0
1343	343	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
343	1342	7	3			.0	1.	.0010	.0	.0	.001	10.00	1362
		9890.0	1680.0	230.0	229.0	332.0	260.0	1712.0	360.0	2617.0	510.0	5064.0	893.0
1342	342	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
342	1335	6	3			.0	1.	.0010	.0	.0	.001	10.00	1341
		72.0	71.0	1352.0	1120.0	2107.0	1616.0	4171.0	2776.0	8280.0	5110.0		
1341	341	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1335	335	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
335	1301	0	1	CHANNEL		10.0	3343.	.0047	18.0	5.0	.045	20.00	0
1301	1302	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1302	1303	4	3			.0	1.	.0010	.0	.0	.001	10.00	1304
		585.0	1.0	1973.0	1149.0	3964.0	2984.0						
1303	330	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1304	1305	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1305	1599	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
330	329	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
329	328	0	1	CHANNEL		8.0	1804.	.0012	3.5	3.5	.024	20.00	0
1309	1311	6	3			.0	1.	.0010	.0	.0	.001	10.00	1312
		725.2	.1	824.2	.2	981.0	51.0	3918.0	1261.0	6125.0	2048.0		
1311	327	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
368	1330	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1312	1330	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1330	1332	0	5	PIPE		1.5	3079.	.0078	10.0	10.0	.025	1.50	0
1332	1368	0	3	OVERFLOW		28.0	3079.	.0078	5.0	5.0	.040	5.00	0
1368	1369	3	3			.0	1.	.0010	.0	.0	.001	10.00	0
		245.0	.1	3280.0	418.6								
1369	1370	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1370	1365	0	5	PIPE		1.5	1286.	.0030	.0	.0	.025	1.50	0
1371	1372	0	3	OVERFLOW		30.0	1286.	.0030	10.0	10.0	.025	15.00	0
1372	1599	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
328	1309	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
327	326	0	4	CHANNEL		8.0	1305.	.0008	3.5	3.5	.024	4.00	0
1409	310	0	3	OVERFLOW		40.0	1305.	.0008	5.7	7.5	.028	20.00	0
1336	336	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
336	1310	4	3			.0	1.	.0010	.0	.0	.001	10.00	1942
		20.0	10.0	200.0	100.0	2000.0	1000.0						
1942	1940	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1310	310	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
310	315	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
315	317	0	4	CHANNEL		.5	3664.	.0088	12.0	12.0	.016	.50	0
316	317	0	4	OVERFLOW		10.0	3664.	.0088	20.0	20.0	.020	10.00	0
317	326	0	3	CHANNEL		.5	2903.	.0079	12.0	12.0	.016	.50	0
326	325	0	4	OVERFLOW		10.0	2903.	.0079	20.0	20.0	.020	10.00	0
325	324	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
324	1392	7	3			.0	1.	.0010	.0	.0	.001	10.00	1402
		725.1	.1	824.0	98.0	930.0	180.0	2657.0	1833.0	4077.0	3077.0		
1402	1323	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1323	323	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
323	1321	7	3			.0	1.	.0010	.0	.0	.001	10.00	1387
		50.0	49.9	254.0	60.0	1565.0	100.0	2841.0	150.0	4250.0	200.0		
1392	392	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
392	391	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
391	1911	0	4	CHANNEL		15.0	1048.	.0012	3.5	3.5	.045	5.00	0
338	318	0	4	OVERFLOW		55.0	1048.	.0012	4.0	7.5	.055	20.00	0
318	1911	0	4	CHANNEL		1.0	2263.	.0089	1.0	1.0	.045	1.00	0
		8.0		2821.		.0012	3.0	3.0	.045	1.50			

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20	0	0	0	0	0	0	0	0	0	0	19	0	0	0	0	0	0	0	0	0	606.0
21	0	0	0	0	0	0	0	0	0	0	20	0	0	0	0	0	0	0	0	0	379.0
22	23	24	0	0	0	0	0	0	0	0	21	0	0	0	0	0	0	0	0	0	4784.0
23	37	34	31	0	0	0	0	0	0	0	22	0	0	0	0	0	0	0	0	0	2671.0
24	25	26	0	0	0	0	0	0	0	0	23	0	0	0	0	0	0	0	0	0	1666.0
25	0	0	0	0	0	0	0	0	0	0	24	0	0	0	0	0	0	0	0	0	363.0
26	27	28	0	0	0	0	0	0	0	0	25	0	0	0	0	0	0	0	0	0	1199.0
27	0	0	0	0	0	0	0	0	0	0	26	0	0	0	0	0	0	0	0	0	107.0
28	29	30	0	0	0	0	0	0	0	0	27	0	0	0	0	0	0	0	0	0	998.0
29	0	0	0	0	0	0	0	0	0	0	28	0	0	0	0	0	0	0	0	0	152.0
30	0	0	0	0	0	0	0	0	0	0	29	0	0	0	0	0	0	0	0	0	546.0
31	32	33	0	0	0	0	0	0	0	0	30	0	0	0	0	0	0	0	0	0	508.0
32	0	0	0	0	0	0	0	0	0	0	31	0	0	0	0	0	0	0	0	0	144.0
33	0	0	0	0	0	0	0	0	0	0	32	0	0	0	0	0	0	0	0	0	257.0
34	35	36	0	0	0	0	0	0	0	0	33	0	0	0	0	0	0	0	0	0	844.0
35	0	0	0	0	0	0	0	0	0	0	34	0	0	0	0	0	0	0	0	0	148.0
36	0	0	0	0	0	0	0	0	0	0	35	0	0	0	0	0	0	0	0	0	251.0
37	38	39	0	0	0	0	0	0	0	0	36	0	0	0	0	0	0	0	0	0	1124.0
38	0	0	0	0	0	0	0	0	0	0	37	0	0	0	0	0	0	0	0	0	368.0
39	0	0	0	0	0	0	0	0	0	0	38	0	0	0	0	0	0	0	0	0	290.0
40	41	42	0	0	0	0	0	0	0	0	39	0	0	0	0	0	0	0	0	0	51645.0
41	0	0	0	0	0	0	0	0	0	0	40	0	0	0	0	0	0	0	0	0	205.0
42	46	62	68	0	0	0	0	0	0	0	41	0	0	0	0	0	0	0	0	0	51084.0
44	1512	1501	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30179.0
46	59	60	0	0	0	0	0	0	0	0	42	0	0	0	0	0	0	0	0	0	47929.0
48	50	49	0	0	0	0	0	0	0	0	69	0	0	0	0	0	0	0	0	0	72077.0
49	0	0	0	0	0	0	0	0	0	0	72	0	0	0	0	0	0	0	0	0	220.0
50	51	52	56	0	0	0	0	0	0	0	71	0	0	0	0	0	0	0	0	0	71466.0
51	0	0	0	0	0	0	0	0	0	0	82	0	0	0	0	0	0	0	0	0	362.0
52	244	245	53	0	0	0	0	0	0	0	73	0	0	0	0	0	0	0	0	0	59055.0
53	54	55	0	0	0	0	0	0	0	0	75	0	0	0	0	0	0	0	0	0	536.0
54	0	0	0	0	0	0	0	0	0	0	76	0	0	0	0	0	0	0	0	0	213.0
55	0	0	0	0	0	0	0	0	0	0	77	0	0	0	0	0	0	0	0	0	297.0
56	57	58	0	0	0	0	0	0	0	0	78	79	0	0	0	0	0	0	0	0	1842.0
57	0	0	0	0	0	0	0	0	0	0	81	0	0	0	0	0	0	0	0	0	776.0
58	0	0	0	0	0	0	0	0	0	0	80	0	0	0	0	0	0	0	0	0	220.0
59	74	71	0	0	0	0	0	0	0	0	43	0	0	0	0	0	0	0	0	0	47507.0
60	0	0	0	0	0	0	0	0	0	0	44	0	0	0	0	0	0	0	0	0	225.0
61	63	64	0	0	0	0	0	0	0	0	45	0	0	0	0	0	0	0	0	0	1044.0
62	61	65	0	0	0	0	0	0	0	0	46	0	0	0	0	0	0	0	0	0	2039.0
63	0	0	0	0	0	0	0	0	0	0	47	0	0	0	0	0	0	0	0	0	234.0
64	0	0	0	0	0	0	0	0	0	0	48	0	0	0	0	0	0	0	0	0	258.0
65	66	67	0	0	0	0	0	0	0	0	49	0	0	0	0	0	0	0	0	0	956.0
66	0	0	0	0	0	0	0	0	0	0	50	0	0	0	0	0	0	0	0	0	108.0
67	0	0	0	0	0	0	0	0	0	0	51	0	0	0	0	0	0	0	0	0	636.0
68	69	70	0	0	0	0	0	0	0	0	52	0	0	0	0	0	0	0	0	0	523.0
69	0	0	0	0	0	0	0	0	0	0	53	0	0	0	0	0	0	0	0	0	197.0
70	0	0	0	0	0	0	0	0	0	0	54	0	0	0	0	0	0	0	0	0	246.0
71	72	73	0	0	0	0	0	0	0	0	55	0	0	0	0	0	0	0	0	0	1094.0
72	0	0	0	0	0	0	0	0	0	0	56	0	0	0	0	0	0	0	0	0	197.0
73	0	0	0	0	0	0	0	0	0	0	57	0	0	0	0	0	0	0	0	0	636.0

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74	77	76	94	0	0	0	0	0	0	0	58	0	0	0	0	0	0	0	0	0	46117.0
75	79	78	0	0	0	0	0	0	0	0	61	0	0	0	0	0	0	0	0	0	3945.0
76	0	0	0	0	0	0	0	0	0	0	63	0	0	0	0	0	0	0	0	0	379.0
77	75	88	0	0	0	0	0	0	0	0	65	0	0	0	0	0	0	0	0	0	4793.0
78	0	0	0	0	0	0	0	0	0	0	66	0	0	0	0	0	0	0	0	0	256.0
79	80	121	0	0	0	0	0	0	0	0	70	0	0	0	0	0	0	0	0	0	3627.0
80	82	81	0	0	0	0	0	0	0	0	83	0	0	0	0	0	0	0	0	0	2668.0
81	87	0	0	0	0	0	0	0	0	0	84	0	0	0	0	0	0	0	0	0	958.0
82	84	83	0	0	0	0	0	0	0	0	85	0	0	0	0	0	0	0	0	0	848.0
83	0	0	0	0	0	0	0	0	0	0	86	0	0	0	0	0	0	0	0	0	197.0
84	85	86	0	0	0	0	0	0	0	0	87	0	0	0	0	0	0	0	0	0	555.0
85	0	0	0	0	0	0	0	0	0	0	88	0	0	0	0	0	0	0	0	0	118.0
86	0	0	0	0	0	0	0	0	0	0	89	0	0	0	0	0	0	0	0	0	331.0
87	0	0	0	0	0	0	0	0	0	0	90	0	0	0	0	0	0	0	0	0	655.0
88	89	93	0	0	0	0	0	0	0	0	91	0	0	0	0	0	0	0	0	0	782.0
89	0	0	0	0	0	0	0	0	0	0	228	0	0	0	0	0	0	0	0	0	319.0
93	0	0	0	0	0	0	0	0	0	0	229	0	0	0	0	0	0	0	0	0	111.0
94	95	97	0	0	0	0	0	0	0	0	92	0	0	0	0	0	0	0	0	0	40534.0
95	96	116	0	0	0	0	0	0	0	0	230	0	0	0	0	0	0	0	0	0	34430.0
96	129	122	0	0	0	0	0	0	0	0	93	0	0	0	0	0	0	0	0	0	33528.0
97	99	98	0	0	0	0	0	0	0	0	94	0	0	0	0	0	0	0	0	0	5629.0
98	0	0	0	0	0	0	0	0	0	0	95	0	0	0	0	0	0	0	0	0	309.0
99	101	100	0	0	0	0	0	0	0	0	96	0	0	0	0	0	0	0	0	0	4848.0
100	0	0	0	0	0	0	0	0	0	0	97	0	0	0	0	0	0	0	0	0	458.0
101	102	107	0	0	0	0	0	0	0	0	98	0	0	0	0	0	0	0	0	0	4335.0
102	106	103	0	0	0	0	0	0	0	0	99	0	0	0	0	0	0	0	0	0	2382.0
103	104	105	0	0	0	0	0	0	0	0	100	0	0	0	0	0	0	0	0	0	1795.0
104	119	117	0	0	0	0	0	0	0	0	101	0	0	0	0	0	0	0	0	0	1302.0
105	0	0	0	0	0	0	0	0	0	0	102	0	0	0	0	0	0	0	0	0	343.0
106	0	0	0	0	0	0	0	0	0	0	103	0	0	0	0	0	0	0	0	0	273.0
107	108	109	0	0	0	0	0	0	0	0	104	0	0	0	0	0	0	0	0	0	1871.0
108	0	0	0	0	0	0	0	0	0	0	105	0	0	0	0	0	0	0	0	0	202.0
109	110	111	0	0	0	0	0	0	0	0	106	0	0	0	0	0	0	0	0	0	1563.0
110	112	113	0	0	0	0	0	0	0	0	107	0	0	0	0	0	0	0	0	0	1148.0
111	0	0	0	0	0	0	0	0	0	0	108	0	0	0	0	0	0	0	0	0	199.0
112	114	115	0	0	0	0	0	0	0	0	109	0	0	0	0	0	0	0	0	0	540.0
113	0	0	0	0	0	0	0	0	0	0	110	0	0	0	0	0	0	0	0	0	209.0
114	0	0	0	0	0	0	0	0	0	0	111	0	0	0	0	0	0	0	0	0	230.0
115	0	0	0	0	0	0	0	0	0	0	112	0	0	0	0	0	0	0	0	0	102.0
116	0	0	0	0	0	0	0	0	0	0	113	0	0	0	0	0	0	0	0	0	702.0
117	0	0	0	0	0	0	0	0	0	0	114	0	0	0	0	0	0	0	0	0	390.0
118	0	0	0	0	0	0	0	0	0	0	115	0	0	0	0	0	0	0	0	0	453.0
119	120	118	0	0	0	0	0	0	0	0	116	0	0	0	0	0	0	0	0	0	707.0
120	0	0	0	0	0	0	0	0	0	0	117	0	0	0	0	0	0	0	0	0	220.0
121	0	0	0	0	0	0	0	0	0	0	74	0	0	0	0	0	0	0	0	0	326.0
122	124	123	0	0	0	0	0	0	0	0	118	0	0	0	0	0	0	0	0	0	2595.0
123	127	128	0	0	0	0	0	0	0	0	119	0	0	0	0	0	0	0	0	0	1409.0
124	125	126	0	0	0	0	0	0	0	0	120	0	0	0	0	0	0	0	0	0	705.0
125	0	0	0	0	0	0	0	0	0	0	124	0	0	0	0	0	0	0	0	0	220.0
126	0	0	0	0	0	0	0	0	0	0	125	0	0	0	0	0	0	0	0	0	88.0
127	0	0	0	0	0	0	0	0	0	0	126	0	0	0	0	0	0	0	0	0	548.0

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179	0	0	0	0	0	0	0	0	0	0	178	0	0	0	0	0	0	0	0	0	211.0
180	181	182	0	0	0	0	0	0	0	0	179	0	0	0	0	0	0	0	0	0	2955.0
181	0	0	0	0	0	0	0	0	0	0	180	0	0	0	0	0	0	0	0	0	438.0
182	183	184	0	0	0	0	0	0	0	0	181	0	0	0	0	0	0	0	0	0	2016.0
183	0	0	0	0	0	0	0	0	0	0	182	0	0	0	0	0	0	0	0	0	599.0
184	186	185	0	0	0	0	0	0	0	0	183	0	0	0	0	0	0	0	0	0	910.0
185	0	0	0	0	0	0	0	0	0	0	184	0	0	0	0	0	0	0	0	0	232.0
186	0	0	0	0	0	0	0	0	0	0	185	0	0	0	0	0	0	0	0	0	461.0
187	192	193	0	0	0	0	0	0	0	0	186	0	0	0	0	0	0	0	0	0	14569.0
192	194	205	0	0	0	0	0	0	0	0	187	0	0	0	0	0	0	0	0	0	13278.0
193	0	0	0	0	0	0	0	0	0	0	188	0	0	0	0	0	0	0	0	0	273.0
194	198	199	196	195	0	0	0	0	0	0	189	0	0	0	0	0	0	0	0	0	5663.0
195	0	0	0	0	0	0	0	0	0	0	190	0	0	0	0	0	0	0	0	0	251.0
196	0	0	0	0	0	0	0	0	0	0	195	0	0	0	0	0	0	0	0	0	387.0
198	201	200	202	0	0	0	0	0	0	0	196	0	0	0	0	0	0	0	0	0	3544.0
199	0	0	0	0	0	0	0	0	0	0	197	0	0	0	0	0	0	0	0	0	634.0
200	0	0	0	0	0	0	0	0	0	0	198	0	0	0	0	0	0	0	0	0	542.0
201	204	203	0	0	0	0	0	0	0	0	199	0	0	0	0	0	0	0	0	0	1955.0
202	0	0	0	0	0	0	0	0	0	0	200	0	0	0	0	0	0	0	0	0	250.0
203	0	0	0	0	0	0	0	0	0	0	203	0	0	0	0	0	0	0	0	0	258.0
204	0	0	0	0	0	0	0	0	0	0	204	0	0	0	0	0	0	0	0	0	854.0
205	207	206	0	0	0	0	0	0	0	0	205	0	0	0	0	0	0	0	0	0	7500.0
206	0	0	0	0	0	0	0	0	0	0	206	0	0	0	0	0	0	0	0	0	250.0
207	211	208	0	0	0	0	0	0	0	0	207	0	0	0	0	0	0	0	0	0	6855.0
208	0	0	0	0	0	0	0	0	0	0	208	0	0	0	0	0	0	0	0	0	275.0
211	212	215	0	0	0	0	0	0	0	0	209	0	0	0	0	0	0	0	0	0	5808.0
212	214	213	0	0	0	0	0	0	0	0	210	0	0	0	0	0	0	0	0	0	1581.0
213	0	0	0	0	0	0	0	0	0	0	211	0	0	0	0	0	0	0	0	0	511.0
214	0	0	0	0	0	0	0	0	0	0	212	0	0	0	0	0	0	0	0	0	482.0
215	219	216	217	0	0	0	0	0	0	0	213	0	0	0	0	0	0	0	0	0	3943.0
216	0	0	0	0	0	0	0	0	0	0	214	0	0	0	0	0	0	0	0	0	505.0
217	0	0	0	0	0	0	0	0	0	0	215	0	0	0	0	0	0	0	0	0	245.0
218	222	221	0	0	0	0	0	0	0	0	219	0	0	0	0	0	0	0	0	0	1711.0
219	220	218	0	0	0	0	0	0	0	0	220	0	0	0	0	0	0	0	0	0	2654.0
220	0	0	0	0	0	0	0	0	0	0	221	0	0	0	0	0	0	0	0	0	506.0
221	0	0	0	0	0	0	0	0	0	0	222	0	0	0	0	0	0	0	0	0	250.0
222	224	223	0	0	0	0	0	0	0	0	223	0	0	0	0	0	0	0	0	0	1417.0
223	0	0	0	0	0	0	0	0	0	0	224	0	0	0	0	0	0	0	0	0	309.0
224	226	225	0	0	0	0	0	0	0	0	225	0	0	0	0	0	0	0	0	0	926.0
225	0	0	0	0	0	0	0	0	0	0	226	0	0	0	0	0	0	0	0	0	152.0
226	0	0	0	0	0	0	0	0	0	0	227	0	0	0	0	0	0	0	0	0	286.0
231	252	0	0	0	0	0	0	0	0	0	231	0	0	0	0	0	0	0	0	0	86054.0
232	234	233	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
233	251	0	0	0	0	0	0	0	0	0	233	0	0	0	0	0	0	0	0	0	85477.0
234	239	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	187.0
235	0	0	0	0	0	0	0	0	0	0	235	0	0	0	0	0	0	0	0	0	187.0
236	232	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
237	238	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
238	1927	240	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
239	235	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	187.0
240	241	0	0	0	0	0	0	0	0	0	240	0	0	0	0	0	0	0	0	0	84397.0

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241	242	0	0	0	0	0	0	0	0	0	241	0	0	0	0	0	0	0	0	0	84351.0
242	377	289	243	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	84008.0
243	1427	0	0	0	0	0	0	0	0	0	243	0	0	0	0	0	0	0	0	0	80261.0
244	0	0	0	0	0	0	0	0	0	0	253	0	0	0	0	0	0	0	0	0	848.0
245	1	246	0	0	0	0	0	0	0	0	254	0	0	0	0	0	0	0	0	0	67230.0
246	247	250	0	0	0	0	0	0	0	0	255	0	0	0	0	0	0	0	0	0	2389.0
247	0	0	0	0	0	0	0	0	0	0	256	0	0	0	0	0	0	0	0	0	808.0
248	0	0	0	0	0	0	0	0	0	0	257	0	0	0	0	0	0	0	0	0	645.0
249	0	0	0	0	0	0	0	0	0	0	258	0	0	0	0	0	0	0	0	0	377.0
250	248	249	0	0	0	0	0	0	0	0	259	0	0	0	0	0	0	0	0	0	1131.0
251	237	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
252	236	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
261	44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	80179.0
262	1935	0	0	0	0	0	0	0	0	0	262	0	0	0	0	0	0	0	0	0	2758.0
263	262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2758.0
264	1905	0	0	0	0	0	0	0	0	0	264	0	0	0	0	0	0	0	0	0	2784.0
265	264	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
266	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
267	293	1267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
268	267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
269	265	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
270	271	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86842.0
271	319	231	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86842.0
280	294	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
289	1924	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3653.0
290	1290	0	0	0	0	0	0	0	0	0	290	0	0	0	0	0	0	0	0	0	3653.0
291	1291	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
292	1923	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
293	1293	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
294	1294	304	1920	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
295	1295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
296	1296	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
297	298	0	0	0	0	0	0	0	0	0	297	0	0	0	0	0	0	0	0	0	587.0
298	303	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	249.0
299	0	0	0	0	0	0	0	0	0	0	299	0	0	0	0	0	0	0	0	0	72.0
300	301	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	177.0
301	0	0	0	0	0	0	0	0	0	0	301	0	0	0	0	0	0	0	0	0	177.0
303	299	1922	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	249.0
304	0	0	0	0	0	0	0	0	0	0	304	0	0	0	0	0	0	0	0	0	150.0
308	396	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
310	1409	1310	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
311	371	312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	247.0
312	1940	0	0	0	0	0	0	0	0	0	312	0	0	0	0	0	0	0	0	0	100.0
313	1939	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
314	308	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
315	310	0	0	0	0	0	0	0	0	0	315	0	0	0	0	0	0	0	0	0	28.0
316	0	0	0	0	0	0	0	0	0	0	316	0	0	0	0	0	0	0	0	0	43.0
317	315	316	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	71.0
318	338	0	0	0	0	0	0	0	0	0	318	0	0	0	0	0	0	0	0	0	230.0
319	1946	0	0	0	0	0	0	0	0	0	319	0	0	0	0	0	0	0	0	0	788.0
320	1320	0	0	0	0	0	0	0	0	0	320	0	0	0	0	0	0	0	0	0	454.0

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321	1321	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
322	1909	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
323	1323	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9.0
324	325	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
325	1325	326	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
326	327	317	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
327	1311	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
328	337	1329	329	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
329	330	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
330	1306	1303	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
331	1331	1407	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
332	333	334	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
333	1333	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.0
334	1334	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.0
335	1335	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
336	1336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
337	331	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	50.0
338	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73.0
339	1822	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
340	1340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
341	1341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
342	1342	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
343	1343	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
344	366	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
345	346	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	149.0
346	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	71.0
347	1915	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	212.0
348	1348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
349	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	13.0
350	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	51.0
351	1814	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	100.0
352	1919	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
353	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
354	1817	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.0
355	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
356	359	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
357	1357	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
358	311	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
359	345	347	349	355	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
360	1360	292	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
361	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30.0
362	1362	363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
366	1366	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
367	1367	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	23.0
368	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
369	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	17.0
370	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
371	372	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	147.0
372	374	373	367	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	64.0
373	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	38.0

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374	1374	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
375	376	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
376	266	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
377	1925	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
378	1378	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
379	380	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
380	1821	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
381	382	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
382	1381	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
383	1820	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
384	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
385	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
386	1386	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
387	1387	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
388	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
389	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
390	1912	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
391	392	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
392	1941 1392	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
393	358	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
394	395	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
395	386	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
396	1396	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
397	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	59647.0
398	362	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
399	270	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	36842.0
1238	390	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1289	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1290	291	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
1291	268	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
1293	280	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
1294	269	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
1295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1296	295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1301	335	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
1302	1301	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
1303	1302	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
1304	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1305	1307 1304	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
1306	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1307	1308	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
1308	332	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
1309	328	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
1310	336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1311	1309	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
1312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1313	339	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1320	1908 1907 1361	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	293.0
1321	323	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9.0

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1406	379	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1407	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1408	344	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
1409	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1410	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	195.0
1411	1410	1424	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1412	1411	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1413	1412	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1414	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1415	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	307.0
1416	1415	1553	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1203.0
1420	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	59.0
1421	1420	1426	1441	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1423	1421	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1424	1423	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1425	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	68.0
1426	1438	1425	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	382.0
1427	261	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	80179.0
1428	1528	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1429	1428	1416	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1203.0
1430	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	82.0
1431	1430	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	82.0
1435	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	232.0
1436	1435	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	232.0
1438	1436	1431	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	314.0
1440	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	66.0
1441	1453	1440	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76465.0
1442	1514	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2719.0
1445	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	164.0
1446	1445	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	164.0
1450	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	198.0
1451	1603	1450	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76235.0
1453	1446	1451	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76399.0
1455	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	542.0
1456	1455	1482	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1274.0
1457	1456	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1274.0
1460	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	286.0
1461	1460	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	286.0
1465	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	93.0
1467	1933	1932	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2351.0
1468	1467	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2351.0
1480	1938	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1481	1480	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1482	1481	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1490	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	698.0
1491	1490	1457	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1972.0
1500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	465.0
1501	1500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	465.0
1505	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	262.0
1506	1505	1800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79714.0
1507	1506	1508	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79714.0

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1620	0	0	0	0	0	0	0	0	0	0	1620	0	0	0	0	0	0	0	0	324.0
1621	1653	1620	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1816.0
1623	1616	1621	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2044.0
1624	1623	1705	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2111.0
1625	0	0	0	0	0	0	0	0	0	0	1625	0	0	0	0	0	0	0	0	197.0
1626	48	1625	1636	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	72591.0
1628	1631	1626	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73076.0
1630	0	0	0	0	0	0	0	0	0	0	1630	0	0	0	0	0	0	0	0	159.0
1631	1643	1630	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	485.0
1635	0	0	0	0	0	0	0	0	0	0	1635	0	0	0	0	0	0	0	0	317.0
1636	1635	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	317.0
1640	0	0	0	0	0	0	0	0	0	0	1640	0	0	0	0	0	0	0	0	200.0
1641	1640	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	200.0
1643	1646	1641	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	326.0
1645	0	0	0	0	0	0	0	0	0	0	1645	0	0	0	0	0	0	0	0	126.0
1646	1645	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	126.0
1650	0	0	0	0	0	0	0	0	0	0	1650	0	0	0	0	0	0	0	0	382.0
1651	1661	1650	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	934.0
1653	1651	1656	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1492.0
1655	0	0	0	0	0	0	0	0	0	0	1655	0	0	0	0	0	0	0	0	558.0
1656	1655	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	558.0
1660	0	0	0	0	0	0	0	0	0	0	1660	0	0	0	0	0	0	0	0	552.0
1661	1660	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	552.0
1665	0	0	0	0	0	0	0	0	0	0	1665	0	0	0	0	0	0	0	0	390.0
1666	1665	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	390.0
1705	0	0	0	0	0	0	0	0	0	0	1705	0	0	0	0	0	0	0	0	67.0
1710	0	0	0	0	0	0	0	0	0	0	1710	0	0	0	0	0	0	0	0	245.0
1711	1710	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	245.0
1712	1711	1624	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2356.0
1715	0	0	0	0	0	0	0	0	0	0	1715	0	0	0	0	0	0	0	0	115.0
1716	1715	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	115.0
1800	1509	1468	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79452.0
1812	352	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1813	1812	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1814	1813	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1815	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1816	1815	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1817	1818	1816	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.0
1818	0	0	0	0	0	0	0	0	0	0	354	0	0	0	0	0	0	0	0	6.0
1820	384	1383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1821	369	1926	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1822	1339	394	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1905	263	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2758.0
1906	389	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1907	388	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1908	387	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1909	1906	320	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
1910	313	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1911	391	318	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1912	1911	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1913	351	354	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	106.0

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1914	1913	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	106.0
1915	350	1914	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	157.0
1916	1262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1917	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	103.0
1919	1934	353	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1920	1921	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	690.0
1921	297	1917	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	690.0
1922	300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	177.0
1923	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1924	290	1289	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3653.0
1925	378	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1926	381	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1927	1238	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1928	1611	1606	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73656.0
1929	1712	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2356.0
1931	1491	1461	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2258.0
1932	1465	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	93.0
1933	1931	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2258.0
1934	360	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1935	1442	1916	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2719.0
1937	348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1938	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1939	1313	314	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1940	1910	1408	1942	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	88.0
1941	1393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1942	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1943	322	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
1944	1365	370	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1945	1944	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1946	1376	1943	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	624.0
1947	1599	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85952.0
ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER											359	TO GUTTER	266	COMP THROUGH DIVERSION WILL LAG ONE						
TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.																				
ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER											428	TO GUTTER	385	COMP THROUGH DIVERSION WILL LAG ONE						
TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.																				
ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER											541	TO GUTTER	388	COMP THROUGH DIVERSION WILL LAG ONE						
TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.																				
ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER											565	TO GUTTER	389	COMP THROUGH DIVERSION WILL LAG ONE						
TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.																				

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*** PEAK FLOWS, STAGES AND STORAGES OF GUTTERS AND DETENTION DAMS ***

CONVEYANCE ELEMENT	PEAK (CFS)	STAGE (FT)	STORAGE (AC-FT)	TIME (HR/MIN)				
1	1299.	3.9		13 5.	103	224.	1.3	8 20.
2	668.	3.7		8 50.	104	178.	1.7	8 20.
3	275.	1.0		8 35.	105	44.	.8	8 10.
4	261.	.9		8 40.	106	24.	.6	8 10.
5	1203.	3.7		13 5.	107	119.	1.3	8 25.
6	1176.	3.1		13 5.	108	12.	.4	8 10.
7	149.	2.1		8 30.	109	107.	1.1	8 20.
8	2933.	(DIRECT FLOW)		9 35.	110	84.	1.0	8 15.
9	76.	1.3		8 25.	111	13.	.3	8 5.
10	33.	.3		8 20.	112	38.	.7	8 10.
11	61.	.6		8 10.	113	19.	.5	8 10.
12	27.	.3		8 25.	114	12.	.4	8 10.
13	118.	.7		8 20.	115	8.	.3	8 5.
14	64.	.5		8 15.	116	34.	.8	8 15.
15	2256.	(DIRECT FLOW)		9 55.	117	67.	1.2	8 15.
16	2239.	(DIRECT FLOW)		9 55.	118	30.	.7	8 10.
17	262.	1.4		8 30.	119	76.	1.4	8 15.
18	175.	1.5		8 35.	120	43.	.9	8 10.
19	59.	.8		8 15.	121	43.	.8	8 45.
20	31.	.5		8 20.	122	171.	1.1	8 35.
21	593.	2.7		8 35.	123	111.	1.0	8 25.
22	240.	2.1		8 45.	124	63.	.8	8 20.
23	225.	1.9		8 30.	125	14.	.4	8 10.
24	64.	.8		8 30.	126	6.	.2	8 10.
25	148.	1.6		8 25.	127	43.	.6	8 15.
26	9.	.2		8 5.	128	35.	.5	8 15.
27	120.	.9		8 25.	129	1338.	4.1	10 25.
28	23.	.5		8 35.	130	133.	1.0	8 25.
29	73.	.8		8 25.	131	43.	.5	8 10.
30	57.	.8		8 30.	132	19.	.5	8 10.
31	11.	.3		8 10.	133	74.	.8	8 25.
32	45.	.7		8 30.	134	56.	.7	8 20.
33	72.	.9		8 45.	135	8.	.3	8 10.
34	26.	.4		8 35.	136	15.	.4	8 10.
35	34.	.5		8 50.	137	1312.	3.4	10 15.
36	71.	1.0		8 45.	138	45.	.7	9 30.
37	27.	.4		8 15.	139	1284.	3.3	10 10.
38	46.	.6		8 45.	140	100.	.9	8 35.
39	2124.	4.9		10 5.	141	21.	.6	8 45.
40	29.	.4		8 30.	142	83.	1.0	8 20.
41	2100.	4.5		10 0.	143	30.	.6	8 15.
42	2618.	(DIRECT FLOW)		11 15.	144	18.	.5	8 10.
43	1952.	4.7		10 0.	145	6.	.3	8 5.
44	2755.	6.4		9 20.	146	52.	.7	8 20.
45	161.	1.0		8 5.	147	16.	.4	8 10.
46	2753.	4.4		9 5.	148	29.	.5	8 10.
47	306.	2.1		8 15.	149	1254.	3.2	10 5.
48	2492.	4.8		9 5.	150	14.	.4	8 30.
49	91.	1.3		8 10.	151	32.	.6	8 40.
50	34.	.7		8 10.	152	1243.	3.3	9 50.
51	40.	.8		8 10.	153	15.	.3	8 10.
52	298.	1.4		8 15.	154	1318.	3.3	9 25.
53	100.	.6		8 10.	155	15.	.2	8 25.
54	31.	.7		8 5.	156	1314.	3.4	9 20.
55	1922.	4.6		10 0.	157	1304.	3.5	9 5.
56	29.	.4		8 40.	158	83.	.7	8 25.
57	82.	1.0		8 35.	159	20.	.4	8 15.
58	162.	1.0		8 40.	160	59.	.7	8 15.
59	13.	.4		8 15.	161	22.	.5	8 10.
60	19.	.7		8 10.	162	18.	.4	8 10.
61	73.	1.3		8 50.	163	63.	.5	8 20.
62	9.	.2		8 5.	164	4.	.1	8 10.
63	68.	.8		8 35.	165	38.	.6	8 15.
64	103.	.9		8 35.	166	58.	.6	8 15.
65	35.	.5		8 20.	167	16.	.4	8 10.
66	57.	.7		8 35.	168	14.	.4	8 10.
67	100.	1.1		8 40.	169	9.	.3	8 10.
68	33.	.6		8 40.	170	45.	.7	8 40.
69	43.	.8		8 20.	171	29.	.5	8 40.
70	1867.	4.6		9 55.	172	1198.	3.9	9 5.
71	329.	2.1		9 15.	173	331.	1.1	8 50.
72	57.	.7		8 40.	174	20.	.5	8 10.
73	370.	1.8		9 20.	175	285.	1.1	8 45.
74	13.	.3		8 15.	176	259.	1.4	8 45.
75	324.	1.8		9 10.	177	33.	.6	8 20.
76	248.	1.0		8 50.	178	24.	.6	8 10.
77	100.	1.0		9 0.	179	11.	.1	8 10.
78	45.	.6		8 25.	180	178.	1.5	8 30.
79	11.	.4		8 10.	181	23.	.5	8 15.
80	29.	.5		8 15.	182	127.	1.0	8 25.
81	7.	.4		8 10.	183	27.	.5	8 20.
82	19.	.4		8 10.	184	80.	.7	8 20.
83	61.	.9		8 55.	185	17.	.6	8 10.
84	49.	.6		8 30.	186	57.	.7	8 15.
85	35.	.8		8 45.	187	886.	3.0	9 10.
86	7.	.3		8 10.	192	887.	2.9	8 55.
87	1521.	3.8		10 40.	193	54.	.3	8 30.
88	1382.	3.6		10 40.	194	328.	1.4	8 40.
89	1384.	4.6		10 30.	195	12.	.3	8 10.
90	491.	2.7		8 45.	196	16.	.5	8 15.
91	72.	.9		8 20.	198	263.	1.4	8 40.
92	444.	2.7		8 35.	199	25.	.6	8 15.
93	75.	1.0		8 45.	200	24.	.5	8 15.
94	367.	2.5		8 30.	201	240.	1.3	8 25.
95	244.	1.7		8 30.	202	13.	.4	8 10.
96					203	62.	.8	8 10.
97					204	178.	1.1	8 20.
98					205	565.	2.2	8 55.
99					206	14.	.1	8 10.
100					207	561.	2.2	8 50.
101					208	14.	.3	8 10.
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211	624.	2.8	8 35.	345	175.	1.2	8 15.
212	156.	.9	8 25.	346	99.	.9	8 10.
213	84.	.8	8 20.	347	253.	4.6	8 15.
214	64.	.6	8 15.	348	29.	(DIRECT FLOW)	8 40.
215	471.	2.3	8 30.	349	4.	.2	8 20.
216	84.	.5	8 15.	350	75.	2.9	8 15.
217	13.	.1	8 10.	351	149.	2.8	12 50.
218	309.	2.2	8 20.	352	192.	.1	9.9 12 45.
219	405.	1.9	8 20.	353	46.	.9	8 10.
220	92.	.8	8 15.	354	43.	1.1	12 50.
221	49.	.7	8 10.	355	13.	1.3	8 10.
222	262.	2.0	8 20.	356	324.	.1	9.5 8 30.
223	57.	.5	8 15.	357	384.	(DIRECT FLOW)	8 35.
224	201.	1.9	8 15.	358	427.	3.6	8 35.
225	48.	.8	8 10.	359	443.	(DIRECT FLOW)	8 15.
226	75.	.5	8 15.	360	250.	(DIRECT FLOW)	12 5.
231	2119.	3.2	13 55.	361	41.	(DIRECT FLOW)	8 5.
232	2126.	(DIRECT FLOW)	13 45.	362	263.	(DIRECT FLOW)	8 30.
233	2122.	4.1	13 50.	363	7.	.4	8 15.
234	70.	2.3	8 40.	366	76.	.9	8 15.
235	84.	.8	8 20.	367	35.	.7	8 10.
236	2126.	(DIRECT FLOW)	13 45.	368	86.	(DIRECT FLOW)	8 10.
237	2595.	(DIRECT FLOW)	13 20.	369	28.	.6	8 10.
238	2595.	(DIRECT FLOW)	13 20.	370	90.	(DIRECT FLOW)	8 5.
239	84.	(DIRECT FLOW)	8 20.	371	130.	1.6	8 20.
240	2507.	3.5	13 0.	372	61.	(DIRECT FLOW)	8 15.
241	2552.	3.4	12 35.	373	7.	.7	8 25.
242	2722.	(DIRECT FLOW)	11 50.	374	36.	1.4	11 45.
243	1961.	2.9	11 35.	375	201.	(DIRECT FLOW)	11 35.
244	662.	2.1	8 20.	376	201.	3.6	11 35.
245	2104.	4.9	8 55.	377	96.	2.9	11 40.
246	865.	2.5	8 40.	378	170.	(DIRECT FLOW)	11 30.
247	292.	1.2	8 35.	379	102.	(DIRECT FLOW)	8 15.
248	248.	1.1	8 35.	380	102.	2.9	8 15.
249	165.	1.0	8 25.	381	81.	(DIRECT FLOW)	8 15.
250	409.	1.8	8 35.	382	81.	2.7	8 15.
251	2121.	(DIRECT FLOW)	13 20.	383	82.	(DIRECT FLOW)	8 15.
252	2106.	(DIRECT FLOW)	13 45.	384	82.	3.5	8 15.
261	2618.	(DIRECT FLOW)	11 15.	385	1.	(DIRECT FLOW)	8 40.
262	1115.	1.8	11 25.	386	2.	(DIRECT FLOW)	8 40.
263	1115.	(DIRECT FLOW)	11 25.	387	39.	(DIRECT FLOW)	8 10.
264	906.	1.4	11 35.	388	408.	(DIRECT FLOW)	8 50.
265	906.	(DIRECT FLOW)	11 35.	389	473.	(DIRECT FLOW)	13 20.
266	201.	(DIRECT FLOW)	11 25.	390	611.	(DIRECT FLOW)	8 50.
267	939.	(DIRECT FLOW)	11 40.	391	550.	5.6	8 45.
268	909.	.1	21.3 11 55.	392	561.	(DIRECT FLOW)	8 35.
269	243.	(DIRECT FLOW)	11 35.	393	427.	(DIRECT FLOW)	8 35.
270	2598.	5.0	14 10.	394	1.	.2	8 45.
271	2600.	(DIRECT FLOW)	14 5.	395	2.	(DIRECT FLOW)	8 40.
280	437.	(DIRECT FLOW)	8 20.	396	261.	(DIRECT FLOW)	8 35.
289	723.	4.8	12 10.	397	1172.	.1	755.5 13 0.
290	654.	4.5	12 0.	398	261.	.1	2.4 8 35.
291	909.	(DIRECT FLOW)	11 55.	399	2598.	(DIRECT FLOW)	14 10.
292	250.	1.2	12 5.	1238	203.	(DIRECT FLOW)	8 50.
293	334.	5.8	8 20.	1262	620.	(DIRECT FLOW)	11 20.
294	437.	(DIRECT FLOW)	8 20.	1267	663.	(DIRECT FLOW)	11 35.
295	0.	.1	3.0 17 25.	1289	74.	(DIRECT FLOW)	11 35.
296	0.	(DIRECT FLOW)	16 25.	1290	656.	(DIRECT FLOW)	11 55.
297	394.	3.2	8 15.	1291	909.	(DIRECT FLOW)	11 55.
298	72.	.1	1.0 8 20.	1293	334.	(DIRECT FLOW)	8 20.
299	79.	.7	8 10.	1294	240.	1.4	11 45.
300	10.	.1	11.4 10 5.	1295	104.	(DIRECT FLOW)	8 25.
301	166.	.8	8 10.	1296	0.	(DIRECT FLOW)	16 25.
303	89.	(DIRECT FLOW)	8 10.	1301	28.	(DIRECT FLOW)	8 25.
304	34.	1.0	8 25.	1302	28.	(DIRECT FLOW)	8 25.
308	260.	(DIRECT FLOW)	8 35.	1303	28.	(DIRECT FLOW)	8 25.
310	17.	(DIRECT FLOW)	8 40.	1304	0.	(DIRECT FLOW)	8 25.
311	424.	(DIRECT FLOW)	8 30.	1305	0.	(DIRECT FLOW)	8 45.
312	306.	4.1	8 35.	1306	30.	(DIRECT FLOW)	8 50.
313	268.	(DIRECT FLOW)	8 35.	1307	0.	(DIRECT FLOW)	8 45.
314	260.	5.0	8 35.	1308	30.	(DIRECT FLOW)	8 45.
315	34.	.7	8 20.	1309	121.	(DIRECT FLOW)	8 15.
316	47.	.8	8 15.	1310	9.	(DIRECT FLOW)	8 45.
317	80.	(DIRECT FLOW)	8 15.	1311	121.	(DIRECT FLOW)	8 15.
318	74.	2.3	8 40.	1312	0.	(DIRECT FLOW)	8 15.
319	540.	3.3	9 20.	1313	9.	(DIRECT FLOW)	8 40.
320	448.	2.3	9 10.	1320	420.	(DIRECT FLOW)	9 5.
321	44.	.7	8 10.	1321	0.	(DIRECT FLOW)	8 5.
322	477.	(DIRECT FLOW)	13 45.	1323	11.	(DIRECT FLOW)	8 5.
323	11.	(DIRECT FLOW)	8 5.	1325	354.	(DIRECT FLOW)	8 40.
324	520.	(DIRECT FLOW)	8 35.	1329	36.	.7	9 15.
325	520.	(DIRECT FLOW)	8 35.	1330	70.	2.3	8 25.
326	188.	3.4	8 25.	1331	28.	(DIRECT FLOW)	8 40.
327	114.	2.7	8 25.	1332	70.	(DIRECT FLOW)	8 25.
328	121.	(DIRECT FLOW)	8 15.	1333	32.	(DIRECT FLOW)	8 35.
329	47.	1.6	8 55.	1334	5.	(DIRECT FLOW)	8 30.
330	50.	(DIRECT FLOW)	8 50.	1335	1.	(DIRECT FLOW)	8 30.
331	28.	(DIRECT FLOW)	8 40.	1336	17.	(DIRECT FLOW)	8 45.
332	30.	(DIRECT FLOW)	8 45.	1337	44.	(DIRECT FLOW)	8 10.
333	23.	.6	8 45.	1338	25.	(DIRECT FLOW)	8 10.
334	7.	.4	8 15.	1339	25.	(DIRECT FLOW)	8 20.
335	28.	.9	8 25.	1340	61.	(DIRECT FLOW)	8 35.
336	17.	(DIRECT FLOW)	8 45.	1341	66.	(DIRECT FLOW)	8 30.
337	60.	.9	8 15.	1342	67.	(DIRECT FLOW)	8 30.
338	37.	1.5	8 30.	1343	324.	(DIRECT FLOW)	8 30.
339	26.	(DIRECT FLOW)	8 40.	1348	29.	(DIRECT FLOW)	8 40.
340	61.	(DIRECT FLOW)	8 35.	1357	384.	(DIRECT FLOW)	8 35.
341	66.	(DIRECT FLOW)	8 30.	1360	1.	(DIRECT FLOW)	8 20.
342	67.	(DIRECT FLOW)	8 30.	1361	22.	1.7	8 15.
343	324.	(DIRECT FLOW)	8 30.	1362	258.	(DIRECT FLOW)	8 30.
344	76.	(DIRECT FLOW)	8 15.	1363	19.	(DIRECT FLOW)	8 10.

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1364	44.	2.1	8 20.	1542	82.	1.4	8 25.
1365	107.	(DIRECT FLOW)	8 30.	1544	1984.	(DIRECT FLOW)	10 46.
1366	1.	(DIRECT FLOW)	8 20.	1545	51.	(DIRECT FLOW)	8 16.
1367	0.	(DIRECT FLOW)	8 20.	1546	133.	1.5	8 35.
1368	70.	(DIRECT FLOW)	8 25.	1548	1979.	1.7	10 45.
1369	70.	(DIRECT FLOW)	8 25.	1550	201.	(DIRECT FLOW)	8 20.
1370	68.	2.2	8 35.	1551	267.	2.1	8 40.
1371	0.	(DIRECT FLOW)	8 25.	1553	320.	(DIRECT FLOW)	8 40.
1372	0.	(DIRECT FLOW)	8 25.	1556	19.	(DIRECT FLOW)	8 16.
1373	139.	(DIRECT FLOW)	8 25.	1557	53.	1.2	8 40.
1374	36.	(DIRECT FLOW)	11 35.	1560	68.	(DIRECT FLOW)	8 15.
1375	139.	(DIRECT FLOW)	8 25.	1561	64.	1.0	8 20.
1376	139.	2.2	8 30.	1563	108.	(DIRECT FLOW)	8 20.
1377	0.	(DIRECT FLOW)	8 25.	1565	47.	(DIRECT FLOW)	8 15.
1378	170.	(DIRECT FLOW)	11 30.	1566	44.	.8	8 20.
1381	81.	(DIRECT FLOW)	8 15.	1570	47.	(DIRECT FLOW)	8 15.
1382	0.	(DIRECT FLOW)	16 30.	1571	46.	.4	8 20.
1383	0.	(DIRECT FLOW)	16 30.	1575	131.	(DIRECT FLOW)	8 15.
1386	2.	(DIRECT FLOW)	8 40.	1576	112.	2.0	8 25.
1387	39.	(DIRECT FLOW)	8 10.	1599	2617.	(DIRECT FLOW)	14 10.
1392	520.	(DIRECT FLOW)	8 35.	1600	5.	(DIRECT FLOW)	8 0.
1393	43.	(DIRECT FLOW)	8 40.	1601	2995.	4.1	9 35.
1396	261.	(DIRECT FLOW)	8 35.	1603	3323.	(DIRECT FLOW)	9 30.
1401	30.	(DIRECT FLOW)	8 35.	1605	18.	(DIRECT FLOW)	8 10.
1402	0.	(DIRECT FLOW)	8 35.	1606	311.	2.1	8 25.
1403	20.	(DIRECT FLOW)	13 45.	1610	24.	(DIRECT FLOW)	8 5.
1404	165.	(DIRECT FLOW)	11 35.	1611	2914.	3.9	9 35.
1405	81.	(DIRECT FLOW)	8 15.	1615	39.	(DIRECT FLOW)	8 0.
1406	102.	(DIRECT FLOW)	8 15.	1616	28.	.9	8 10.
1407	0.	(DIRECT FLOW)	8 40.	1620	53.	(DIRECT FLOW)	8 5.
1408	51.	(DIRECT FLOW)	8 15.	1621	410.	2.8	8 45.
1409	8.	(DIRECT FLOW)	8 40.	1623	422.	(DIRECT FLOW)	8 45.
1410	24.	(DIRECT FLOW)	8 5.	1624	422.	2.7	8 50.
1411	2781.	4.5	10 20.	1625	144.	(DIRECT FLOW)	8 15.
1412	2781.	(DIRECT FLOW)	10 20.	1626	2849.	4.1	9 25.
1413	2781.	(DIRECT FLOW)	10 20.	1628	2971.	(DIRECT FLOW)	9 20.
1414	1468.	(DIRECT FLOW)	10 25.	1630	66.	(DIRECT FLOW)	8 15.
1415	38.	(DIRECT FLOW)	8 10.	1631	187.	1.3	8 45.
1416	318.	2.6	8 55.	1635	169.	(DIRECT FLOW)	8 15.
1420	24.	(DIRECT FLOW)	8 20.	1636	155.	1.4	8 20.
1421	3199.	4.9	10 0.	1640	132.	(DIRECT FLOW)	8 15.
1423	3199.	(DIRECT FLOW)	10 0.	1641	91.	2.5	8 35.
1424	2835.	(DIRECT FLOW)	10 0.	1643	141.	(DIRECT FLOW)	8 35.
1425	11.	(DIRECT FLOW)	8 0.	1645	57.	(DIRECT FLOW)	8 25.
1426	35.	.9	8 15.	1646	50.	.9	8 35.
1427	1998.	(DIRECT FLOW)	11 15.	1650	250.	(DIRECT FLOW)	8 15.
1428	356.	2.2	10 15.	1651	308.	2.2	8 25.
1429	505.	(DIRECT FLOW)	10 10.	1653	462.	(DIRECT FLOW)	8 30.
1430	12.	(DIRECT FLOW)	8 0.	1655	199.	(DIRECT FLOW)	8 25.
1431	11.	.5	8 5.	1656	170.	1.7	8 40.
1435	30.	(DIRECT FLOW)	8 5.	1660	112.	(DIRECT FLOW)	8 10.
1436	22.	1.0	8 10.	1661	87.	1.3	8 25.
1438	32.	(DIRECT FLOW)	8 10.	1665	361.	(DIRECT FLOW)	8 5.
1440	13.	(DIRECT FLOW)	8 0.	1666	324.	2.1	8 15.
1441	3197.	5.0	10 0.	1705	8.	(DIRECT FLOW)	8 5.
1442	499.	1.7	11 20.	1710	39.	(DIRECT FLOW)	8 5.
1445	22.	(DIRECT FLOW)	8 0.	1711	34.	.7	8 25.
1446	15.	.7	8 10.	1712	450.	(DIRECT FLOW)	8 50.
1450	24.	(DIRECT FLOW)	8 5.	1715	31.	(DIRECT FLOW)	8 15.
1451	3274.	4.7	9 45.	1716	19.	.6	8 50.
1453	3276.	(DIRECT FLOW)	9 45.	1800	1411.	(DIRECT FLOW)	10 15.
1455	111.	(DIRECT FLOW)	8 10.	1812	192.	(DIRECT FLOW)	12 45.
1456	89.	.5	8 25.	1813	192.	(DIRECT FLOW)	12 45.
1457	89.	(DIRECT FLOW)	8 25.	1814	149.	(DIRECT FLOW)	12 45.
1460	65.	(DIRECT FLOW)	8 5.	1815	43.	(DIRECT FLOW)	12 50.
1461	57.	1.4	8 10.	1816	42.	.8	12 50.
1465	32.	(DIRECT FLOW)	8 10.	1817	43.	(DIRECT FLOW)	12 50.
1467	166.	(DIRECT FLOW)	8 20.	1818	16.	.7	8 5.
1468	166.	1.8	8 20.	1820	82.	(DIRECT FLOW)	8 15.
1480	497.	2.8	8 15.	1821	104.	(DIRECT FLOW)	8 15.
1481	5.	.0	79.5	1822	26.	(DIRECT FLOW)	8 40.
1482	5.	(DIRECT FLOW)	24 40.	1905	914.	(DIRECT FLOW)	11 25.
1490	146.	(DIRECT FLOW)	8 10.	1906	442.	.7	13 45.
1491	121.	2.3	8 55.	1907	380.	2.3	9 5.
1500	179.	(DIRECT FLOW)	8 10.	1908	39.	1.4	8 15.
1501	131.	2.1	8 30.	1909	477.	(DIRECT FLOW)	13 45.
1505	178.	(DIRECT FLOW)	8 10.	1910	260.	(DIRECT FLOW)	8 35.
1506	1206.	3.2	11 25.	1911	622.	(DIRECT FLOW)	8 45.
1507	2595.	(DIRECT FLOW)	11 5.	1912	611.	5.4	8 50.
1508	1405.	(DIRECT FLOW)	11 5.	1913	192.	(DIRECT FLOW)	12 50.
1509	1313.	(DIRECT FLOW)	10 20.	1914	191.	3.3	12 55.
1510	29.	(DIRECT FLOW)	8 15.	1915	194.	(DIRECT FLOW)	12 55.
1511	1912.	3.4	11 5.	1916	616.	1.6	11 25.
1512	2585.	4.2	11 15.	1917	23.	.8	8 20.
1513	1912.	(DIRECT FLOW)	11 5.	1919	248.	(DIRECT FLOW)	12 15.
1514	507.	(DIRECT FLOW)	11 5.	1920	403.	3.7	8 20.
1515	18.	(DIRECT FLOW)	8 5.	1921	416.	(DIRECT FLOW)	8 15.
1517	23.	.8	8 25.	1922	10.	.3	10 5.
1520	74.	(DIRECT FLOW)	8 10.	1923	253.	(DIRECT FLOW)	12 0.
1521	1965.	3.3	10 40.	1924	727.	(DIRECT FLOW)	12 0.
1522	1991.	(DIRECT FLOW)	10 45.	1925	96.	(DIRECT FLOW)	11 30.
1525	35.	(DIRECT FLOW)	8 15.	1926	80.	(DIRECT FLOW)	8 15.
1526	501.	2.6	10 15.	1927	203.	3.6	9 0.
1528	364.	(DIRECT FLOW)	10 5.	1928	2997.	(DIRECT FLOW)	9 30.
1530	61.	(DIRECT FLOW)	8 10.	1929	444.	2.0	8 55.
1531	166.	1.5	8 40.	1931	139.	(DIRECT FLOW)	8 20.
1532	558.	(DIRECT FLOW)	10 15.	1932	28.	.6	8 15.
1533	1994.	(DIRECT FLOW)	10 30.	1933	139.	1.9	8 20.
1534	1450.	2.3	10 35.	1934	246.	1.2	12 15.
1537	555.	2.6	10 20.	1935	1115.	(DIRECT FLOW)	11 25.
1541	127.	(DIRECT FLOW)	8 5.	1937	1.	(DIRECT FLOW)	8 40.

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1938	504.	(DIRECT FLOW)	8	10.
1939	268.	(DIRECT FLOW)	8	35.
1940	305.	(DIRECT FLOW)	8	30.
1941	43.	.8	8	40.
1942	9.	(DIRECT FLOW)	8	45.
1943	476.	3.0	13	50.
1944	139.	4.9	8	25.
1945	139.	(DIRECT FLOW)	8	25.
1946	516.	(DIRECT FLOW)	9	10.
1947	2617.	(DIRECT FLOW)	14	10.

UDSWMM
50-YEAR MODEL

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URBAN DRAINAGE STORM WATER MANAGEMENT MODEL - 32 BIT VERSION 1998
 REVISED BY UNIVERSITY OF COLORADO AT DENVER

*** ENTRY MADE TO RUNOFF MODEL ***

model sbc_ltd
 50-year model

NUMBER OF TIME STEPS 865
 DINTERGRATION TIME INTERVAL (MINUTES) 5.00

1.0 PERCENT OF IMPERVIOUS AREA HAS ZERO DETENTION DEPTH
 OFOR 288 RAINFALL STEPS, THE TIME INTERVAL IS 5.00 MINUTES
 OFOR RAINGAGE NUMBER 1 RAINFALL HISTORY IN INCHES PER HOUR

.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.08	.08	.08	.08
.08	.08	.08	.08	.09	.09	.09	.09	.09	.09
.09	.10	.10	.10	.10	.10	.11	.11	.11	.11
.12	.12	.12	.13	.13	.13	.14	.14	.15	.15
.16	.16	.17	.18	.18	.19	.20	.21	.23	.24
.26	.28	.30	.33	.36	.41	.46	.52	.61	.73
.89	1.13	1.49	2.06	2.99	3.88	3.58	2.47	1.74	1.29
1.00	.80	.66	.56	.49	.43	.38	.35	.32	.29
.27	.25	.23	.22	.21	.20	.19	.18	.17	.17
.16	.15	.15	.14	.14	.14	.13	.13	.12	.12
.12	.12	.11	.11	.11	.11	.10	.10	.10	.10
.10	.09	.09	.09	.09	.09	.09	.08	.08	.08
.08	.08	.08	.08	.08	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03

OFOR RAINGAGE NUMBER 2 RAINFALL HISTORY IN INCHES PER HOUR

.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.09
.09	.09	.09	.09	.09	.09	.09	.09	.10	.10
.10	.10	.10	.10	.11	.11	.11	.11	.11	.11
.12	.12	.12	.12	.13	.13	.13	.14	.14	.14
.15	.15	.16	.16	.17	.18	.19	.19	.20	.22
.23	.25	.27	.29	.32	.35	.39	.45	.52	.62
.76	.96	1.28	1.79	2.66	3.66	3.26	2.17	1.50	1.10
.85	.68	.57	.48	.42	.37	.33	.30	.28	.26
.24	.22	.21	.20	.19	.18	.17	.17	.16	.16
.15	.15	.14	.14	.13	.13	.13	.13	.12	.12
.12	.12	.11	.11	.11	.11	.11	.10	.10	.10
.10	.10	.10	.10	.09	.09	.09	.09	.09	.09
.09	.09	.09	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04

OFOR RAINGAGE NUMBER 3 RAINFALL HISTORY IN INCHES PER HOUR

.06	.06	.06	.06	.06	.06	.06	.06	.06	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.09	.09	.09	.09	.09	.09
.09	.09	.09	.10	.10	.10	.10	.10	.10	.11
.11	.11	.11	.11	.11	.12	.12	.12	.12	.13
.13	.13	.13	.14	.14	.14	.15	.15	.16	.16
.17	.17	.18	.19	.19	.20	.21	.22	.23	.25
.26	.28	.30	.32	.35	.39	.43	.48	.54	.62
.73	.88	1.09	1.42	1.98	3.24	2.46	1.65	1.23	.97
.80	.67	.58	.51	.45	.40	.37	.34	.31	.29
.27	.25	.24	.23	.22	.21	.20	.19	.18	.18
.17	.16	.16	.16	.15	.15	.14	.14	.14	.13
.13	.13	.12	.12	.12	.12	.12	.11	.11	.11
.11	.11	.10	.10	.10	.10	.10	.10	.10	.09
.09	.09	.09	.09	.09	.09	.09	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06

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.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
OFOR RAINGAGE NUMBER	4	RAINFALL HISTORY IN INCHES PER HOUR							
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.09	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.10	.10	.10	.10	.10	.10	.10	.10
.11	.11	.11	.11	.11	.11	.12	.12	.12	.12
.13	.13	.13	.13	.14	.14	.14	.15	.15	.15
.16	.16	.17	.18	.18	.19	.20	.21	.22	.23
.24	.26	.28	.30	.32	.35	.39	.43	.49	.56
.66	.79	.97	1.26	1.74	2.78	2.14	1.46	1.10	.87
.72	.60	.52	.46	.41	.37	.34	.31	.29	.27
.25	.24	.22	.21	.20	.19	.19	.18	.17	.17
.16	.16	.15	.15	.14	.14	.14	.13	.13	.13
.13	.12	.12	.12	.12	.12	.11	.11	.11	.11
.11	.11	.10	.10	.10	.10	.10	.10	.10	.10
.09	.09	.09	.09	.09	.09	.09	.09	.09	.09
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.08	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
OFOR RAINGAGE NUMBER	5	RAINFALL HISTORY IN INCHES PER HOUR							
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.07	.07	.07	.07	.07	.07	.07	.07
.08	.08	.08	.08	.08	.08	.09	.09	.09	.09
.09	.10	.10	.10	.11	.11	.11	.12	.12	.12
.13	.13	.14	.14	.15	.16	.16	.17	.18	.19
.20	.22	.23	.25	.27	.29	.32	.36	.41	.47
.54	.65	.80	1.02	1.39	2.13	1.68	1.18	.90	.72
.59	.50	.44	.38	.34	.31	.28	.26	.24	.22
.21	.20	.18	.18	.17	.16	.15	.15	.14	.13
.13	.13	.12	.12	.11	.11	.11	.10	.10	.10
.10	.09	.09	.09	.09	.09	.08	.08	.08	.08
.08	.08	.07	.07	.07	.07	.07	.07	.07	.07
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

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model sbc_ltd
50-year model

SUBAREA NUMBER	GUTTER OR MANHOLE	WIDTH (FT)	AREA (AC)	PERCENT IMPERV.	SLOPE (FT/FT)	RESISTANCE FACTOR		SURFACE STORAGE(IN)		INFILTRATION RATE(IN/HR)			GAGE NC
						IMPERV.	PERV.	IMPERV.	PERV.	MAXIMUM	MINIMUM	DECAY RATE	
227	226	7480.	286.0	30.0	.4076	.300	.500	.300	.470	3.90	.50	.00024	5
226	225	6240.	152.0	30.0	.5701	.300	.500	.300	.470	3.90	.50	.00024	5
225	224	8440.	488.0	20.0	.3704	.300	.500	.300	.470	4.50	.60	.00010	5
224	223	11920.	309.0	20.0	.2882	.300	.500	.300	.450	3.50	.20	.00100	5
222	221	13040.	250.0	20.0	.5139	.300	.500	.300	.450	3.90	.50	.00024	5
221	220	15160.	506.0	20.0	.4510	.300	.500	.300	.450	3.50	.20	.00100	5
219	218	3320.	44.0	6.0	.2945	.300	.500	.300	.470	3.90	.50	.00024	5
220	219	10200.	437.0	5.0	.3544	.300	.500	.300	.480	4.50	.60	.00010	5
223	222	2280.	182.0	6.0	.4444	.300	.500	.300	.470	4.80	.50	.00010	5
214	216	16320.	505.0	20.0	.4409	.300	.500	.300	.450	3.90	.50	.00024	5
212	214	13760.	482.0	15.0	.4325	.300	.500	.300	.450	3.90	.50	.00024	5
211	213	11800.	511.0	20.0	.3390	.300	.500	.300	.440	3.50	.20	.00100	5
210	212	12200.	588.0	5.0	.2915	.300	.500	.300	.420	4.80	.50	.00010	5
213	215	6480.	539.0	6.0	.3847	.300	.400	.150	.420	3.90	.50	.00024	5
215	217	9720.	245.0	5.0	.2985	.250	.450	.300	.500	3.90	.50	.00024	5
209	211	6800.	284.0	6.0	.4718	.300	.400	.150	.460	3.90	.50	.00024	5
185	186	8520.	461.0	15.0	.2842	.300	.500	.300	.450	4.80	.50	.00010	5
184	185	7440.	232.0	8.0	.3661	.300	.500	.300	.400	3.90	.50	.00024	5
182	183	16000.	599.0	6.0	.1690	.300	.500	.300	.450	4.50	.60	.00010	5
180	181	13280.	438.0	6.0	.2725	.300	.500	.300	.450	4.50	.60	.00010	5

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183	184	7080.	217.0	6.0	.2820	.300	.500	.300	.400	3.90	.50	.00024	5
181	182	9200.	507.0	7.0	.2836	.300	.500	.300	.450	4.50	.60	.00010	5
179	180	9040.	501.0	5.0	.2840	.250	.450	.300	.500	3.50	.20	.00100	4
204	204	13440.	854.0	30.0	.3985	.300	.500	.300	.470	3.90	.50	.00024	5
203	203	7000.	258.0	25.0	.4793	.300	.500	.300	.470	3.90	.50	.00024	5
199	201	15400.	843.0	5.0	.3343	.300	.500	.300	.470	4.50	.60	.00010	5
198	200	14440.	542.0	5.0	.2842	.300	.500	.300	.450	3.90	.50	.00024	5
200	202	7640.	250.0	5.0	.2900	.300	.500	.300	.500	4.80	.50	.00010	5
196	198	14440.	797.0	5.0	.4198	.250	.450	.300	.450	3.90	.50	.00024	5
195	196	14640.	387.0	5.0	.2370	.250	.450	.300	.500	4.50	.60	.00010	5
197	199	18040.	634.0	5.0	.2744	.250	.450	.300	.450	3.90	.50	.00024	5
190	195	9520.	251.0	5.0	.2833	.250	.450	.300	.470	3.90	.50	.00024	5
189	194	15120.	847.0	9.0	.3487	.150	.400	.300	.500	4.50	.50	.00010	4
208	208	8520.	275.0	5.0	.3120	.250	.450	.300	.450	3.90	.50	.00024	5
207	207	8560.	772.0	6.0	.4592	.150	.400	.300	.430	3.50	.20	.00100	5
206	206	7720.	250.0	5.0	.3693	.250	.450	.300	.470	3.90	.50	.00024	5
205	205	9800.	395.0	7.0	.4113	.150	.400	.300	.450	3.90	.50	.00024	4
187	192	1540.	115.0	6.0	.5495	.150	.400	.300	.430	3.50	.20	.00100	4
188	193	8960.	273.0	9.0	.3629	.150	.400	.300	.400	3.50	.20	.00100	4
186	187	19200.	1018.0	8.0	.3200	.150	.400	.300	.450	3.90	.50	.00024	4
177	178	13000.	392.0	7.0	.2685	.150	.400	.300	.450	3.90	.50	.00024	5
178	179	7720.	211.0	5.0	.3191	.250	.450	.300	.420	3.50	.20	.00100	5
175	176	15040.	716.0	5.0	.3492	.250	.450	.300	.400	3.50	.20	.00100	4
176	177	12040.	233.0	6.0	.2396	.250	.450	.300	.450	3.90	.50	.00024	4
174	175	3800.	78.0	5.0	.2684	.250	.450	.300	.450	3.90	.50	.00024	4
173	174	8120.	188.0	8.0	.3071	.150	.400	.300	.430	3.90	.50	.00024	4
172	173	11520.	230.0	5.0	.3401	.250	.450	.300	.400	3.50	.20	.00100	4
171	172	3720.	73.0	7.0	.2083	.150	.400	.300	.450	3.90	.50	.00024	4
167	168	7240.	259.0	5.0	.2386	.300	.500	.300	.500	3.90	.50	.00024	5
168	169	6280.	175.0	5.0	.2720	.300	.500	.300	.500	3.90	.50	.00024	5
164	165	13840.	350.0	6.0	.3519	.300	.500	.300	.470	3.90	.50	.00024	4
166	167	10720.	215.0	6.0	.3188	.300	.500	.300	.500	3.90	.50	.00024	4
165	166	1040.	99.0	5.0	.2782	.300	.500	.300	.500	3.90	.50	.00024	4
170	171	8840.	139.0	5.0	.2244	.250	.450	.300	.400	3.50	.20	.00100	4
169	170	9680.	332.0	5.0	.2538	.250	.450	.300	.400	3.50	.20	.00100	4
162	163	5280.	112.0	5.0	.2935	.250	.450	.300	.470	3.90	.50	.00100	4
163	164	8000.	76.0	5.0	.3938	.300	.500	.300	.450	3.90	.50	.00024	4
156	157	1660.	103.0	7.0	.3821	.250	.450	.300	.460	3.50	.20	.00100	4
160	161	8760.	341.0	5.0	.3148	.300	.500	.300	.470	3.90	.50	.00100	4
161	162	11600.	362.0	5.0	.3269	.300	.500	.300	.470	3.90	.50	.00100	5
158	159	12760.	476.0	5.0	.2852	.300	.500	.300	.470	3.90	.50	.00100	5
159	160	6720.	342.0	6.0	.3021	.300	.500	.300	.470	3.90	.50	.00100	4
155	156	9960.	523.0	6.0	.3280	.250	.450	.300	.400	3.90	.50	.00024	4
157	158	11400.	344.0	5.0	.2728	.250	.450	.300	.460	3.90	.50	.00024	4
152	153	8760.	249.0	5.0	.2831	.300	.500	.300	.500	3.90	.50	.00024	4
153	154	5760.	249.0	6.0	.3299	.250	.450	.300	.450	3.90	.50	.00024	4
154	155	2180.	161.0	5.0	.3792	.300	.500	.300	.400	3.50	.20	.00100	4
148	149	6440.	214.0	6.0	.3001	.250	.450	.300	.400	3.50	.20	.00100	4
149	150	5560.	58.0	6.0	.1610	.250	.450	.300	.400	3.50	.20	.00100	4
150	151	8240.	189.0	5.0	.2338	.250	.450	.300	.400	3.50	.20	.00100	4
151	152	13960.	501.0	8.0	.3572	.250	.450	.300	.450	3.90	.50	.00024	4
145	146	6930.	318.0	5.0	.2782	.300	.500	.300	.460	3.90	.50	.00024	4
146	147	11200.	283.0	5.0	.2727	.250	.450	.300	.500	3.90	.50	.00024	4
147	148	5440.	453.0	5.0	.3306	.250	.450	.300	.470	3.90	.50	.00024	4
141	142	4160.	103.0	6.0	.2843	.250	.450	.300	.450	3.90	.50	.00024	4
142	143	9680.	187.0	5.0	.3565	.250	.450	.300	.470	3.90	.50	.00024	4
143	144	4400.	274.0	5.0	.3218	.300	.500	.300	.460	3.90	.50	.00024	4
144	145	4320.	79.0	5.0	.2164	.300	.500	.300	.500	3.90	.50	.00024	4
139	140	8640.	184.0	6.0	.3125	.250	.450	.300	.460	3.90	.50	.00024	4
140	141	7600.	132.0	5.0	.2104	.250	.450	.300	.450	3.50	.20	.00100	4
136	137	6200.	142.0	15.0	.2104	.150	.400	.300	.470	3.50	.20	.00100	4
137	138	8780.	383.0	10.0	.0823	.150	.400	.150	.420	3.50	.20	.00100	4
138	139	3760.	70.0	15.0	.1898	.250	.450	.150	.450	3.90	.50	.00024	4
133	134	20040.	530.0	8.0	.3229	.250	.450	.300	.460	3.90	.50	.00024	4
134	135	8160.	160.0	5.0	.2440	.250	.450	.300	.450	3.90	.50	.00024	5
135	136	6000.	282.0	5.0	.2300	.250	.450	.300	.460	3.90	.50	.00024	5
130	131	9720.	290.0	12.0	.3042	.150	.400	.150	.500	3.90	.50	.00024	4
131	132	9120.	213.0	8.0	.1964	.250	.450	.300	.470	3.90	.50	.00024	4
132	133	15440.	496.0	7.0	.1806	.250	.450	.300	.470	3.90	.50	.00024	4
128	129	7040.	151.0	12.0	.5988	.300	.500	.200	.450	3.90	.50	.00024	4
129	130	6720.	110.0	15.0	.2077	.150	.400	.150	.450	3.90	.50	.00024	4
124	125	7600.	220.0	5.0	.1948	.300	.500	.300	.500	3.90	.50	.00024	4
125	126	6840.	88.0	5.0	.2679	.300	.500	.300	.500	3.90	.50	.00024	4
126	127	16000.	548.0	8.0	.2341	.250	.450	.300	.480	3.90	.50	.00024	4
120	124	15040.	397.0	13.0	.1127	.150	.400	.150	.500	3.90	.50	.00024	4
127	128	17320.	472.0	8.0	.2160	.250	.450	.300	.470	3.90	.50	.00024	4
118	122	18880.	481.0	8.0	.2138	.150	.400	.200	.450	3.90	.50	.00024	4
119	123	8320.	389.0	12.0	.1613	.150	.400	.200	.450	3.90	.50	.00024	4
113	116	19040.	702.0	5.0	.1137	.300	.500	.300	.500	3.90	.50	.00024	4
93	96	12640.	579.0	5.0	.2560	.250	.450	.300	.460	3.90	.50	.00024	4
230	95	8000.	200.0	5.0	.2312	.250	.450	.300	.450	3.90	.50	.00024	4
88	85	3840.	118.0	5.0	.2369	.250	.450	.300	.400	3.90	.50	.00024	4
89	86	11760.	331.0	5.0	.2521	.250	.450	.300	.400	3.90	.50	.00024	4
90	87	16080.	655.0	5.0	.1364	.250	.450	.300	.400	3.50	.20	.00100	4
84	81	12440.	303.0	5.0	.2148	.250	.450	.300	.400	3.50	.20	.00100	4
85	82	2220.	96.0	5.0	.1143	.250	.450	.300	.400	3.50	.20	.00100	4
86	83	4760.	197.0	5.0	.1438	.250	.450	.300	.400	3.90	.50	.00024	4
87	84	5440.	106.0	5.0	.1919	.250	.450	.300	.400	3.90	.50	.00024	4
83	80	31300.	862.0	9.0	.1050	.150	.400	.200	.400	3.50	.20	.00100	4
74	121	9400.	326.0	6.0	.1923	.150	.400	.200	.400	3.50	.20	.00024	4
70	79	16040.	633.0	7.0	.1589	.250	.450	.300	.400	3.50	.20	.00100	4
61	75	3200.	62.0	5.0	.3363	.250	.450	.300	.400	3.90	.50	.00024	4
63	76	12840.	379.0	8.0	.1972	.250	.450	.300	.400	3.50	.20	.00100	4
65	77	4040.	66.0	8.0	.2100	.250	.450	.300	.430	3.90	.50	.00024	4
66	78	7560.	256.0	5.0	.1250	.250	.450	.300	.450	3.90	.50	.00024	4
58	74	9400.	411.0	8.0	.3384	.250	.450	.300	.400	3.50	.20	.00100	4
228	89	8480.	319.0	8.0	.1659	.150	.400	.150	.450	3.50	.20	.00100	4
229	93	4880.	111.0	5.0	.2059	.250	.450	.300	.450	4.50	.60	.00010	4
91	88	16520.	352.0	6.0	.1576	.250	.450	.300	.450	3.90	.50	.00024	4
114	117	12000.	390.0	15.0	.1571	.150	.400	.150	.430	3.90	.50	.00024	4
115	118	16440.	453.0	6.0	.1736	.250	.450	.300	.460	3.90	.50	.00024	4

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116	119	2600.	34.0	15.0	.1472	.150	.400	.150	.500	3.90	.50	.00024	4
117	120	7960.	220.0	15.0	.1331	.150	.400	.150	.470	3.90	.50	.00024	4
101	104	6880.	205.0	15.0	.1564	.150	.400	.150	.450	3.50	.20	.00100	4
102	105	9120.	343.0	10.0	.1175	.150	.400	.150	.500	3.90	.50	.00024	4
103	106	12760.	273.0	8.0	.1121	.250	.450	.300	.500	3.90	.50	.00024	4
99	102	10440.	314.0	10.0	.1275	.150	.400	.150	.480	3.90	.50	.00024	4
100	103	8170.	150.0	8.0	.1343	.150	.400	.150	.450	3.90	.50	.00100	4
109	112	7280.	208.0	7.0	.4086	.250	.450	.300	.470	3.90	.50	.00024	4
110	113	10120.	209.0	7.0	.2899	.250	.450	.300	.500	3.90	.50	.00024	4
111	114	9000.	230.0	5.0	.2973	.300	.500	.300	.470	3.90	.50	.00024	5
112	115	6480.	102.0	6.0	.4123	.250	.450	.300	.460	3.90	.50	.00024	4
107	110	4140.	399.0	8.0	.3550	.250	.450	.300	.470	3.90	.50	.00024	4
105	108	12480.	202.0	5.0	.3863	.300	.500	.300	.470	3.90	.50	.00024	4
106	109	5520.	216.0	7.0	.1680	.250	.450	.300	.500	3.90	.50	.00024	4
108	111	11200.	199.0	5.0	.4732	.300	.500	.300	.460	3.90	.50	.00024	4
104	107	5440.	106.0	8.0	.2557	.250	.450	.300	.480	3.90	.50	.00024	4
97	100	19960.	458.0	7.0	.5159	.250	.450	.300	.480	3.50	.20	.00100	4
95	98	14000.	309.0	18.0	.1544	.250	.450	.200	.470	3.50	.20	.00100	4
96	99	2880.	55.0	10.0	.3003	.250	.450	.300	.480	3.50	.20	.00100	4
98	101	1380.	82.0	8.0	.1629	.250	.450	.200	.470	3.50	.20	.00100	4
94	97	11440.	472.0	8.0	.3012	.250	.450	.300	.470	3.90	.50	.00024	4
92	94	5120.	475.0	7.0	.1426	.250	.450	.300	.500	3.90	.50	.00024	4
56	72	8960.	197.0	7.0	.1792	.150	.400	.150	.420	3.50	.20	.00100	4
57	73	16000.	636.0	8.0	.1300	.150	.400	.150	.440	3.90	.50	.00024	4
55	71	9640.	261.0	7.0	.1967	.250	.450	.300	.470	3.50	.20	.00100	4
43	59	8040.	296.0	9.0	.1912	.150	.400	.150	.400	3.90	.50	.00024	4
47	63	7960.	234.0	6.0	.4083	.250	.450	.300	.470	3.90	.50	.00024	4
48	64	7480.	258.0	6.0	.3750	.250	.450	.300	.500	3.90	.50	.00024	4
45	61	15000.	552.0	8.0	.2077	.250	.450	.200	.470	3.50	.20	.00100	4
42	46	6440.	197.0	7.0	.3799	.250	.450	.200	.400	3.50	.20	.00100	4
44	60	8160.	225.0	7.0	.2515	.250	.450	.200	.470	3.50	.20	.00100	4
46	62	2800.	39.0	5.0	.3963	.250	.450	.300	.470	3.50	.20	.00100	4
50	66	6120.	108.0	6.0	.4444	.250	.450	.300	.500	3.90	.50	.00024	4
51	67	13240.	636.0	7.0	.3651	.250	.450	.300	.470	3.50	.20	.00100	4
53	69	7480.	197.0	12.0	.2552	.150	.400	.150	.470	3.50	.20	.00100	4
54	70	13920.	246.0	12.0	.2827	.150	.400	.150	.420	3.50	.20	.00100	4
49	65	7920.	212.0	5.0	.3375	.250	.450	.300	.480	3.90	.50	.00024	4
52	68	4240.	80.0	7.0	.3917	.250	.450	.300	.500	3.50	.20	.00100	4
41	42	15160.	593.0	8.0	.4922	.250	.450	.200	.450	3.90	.50	.00024	4
39	40	13160.	356.0	20.0	.4570	.250	.450	.100	.450	3.90	.50	.00024	4
40	41	6200.	205.0	9.0	.5172	.250	.450	.200	.500	3.50	.20	.00100	4
18	18	15200.	565.0	7.0	.3792	.250	.450	.200	.420	3.50	.20	.00100	3
19	20	10680.	606.0	9.0	.1670	.150	.400	.150	.470	3.90	.50	.00024	4
20	21	13920.	379.0	6.0	.3275	.250	.450	.300	.400	3.90	.50	.00024	3
14	14	6160.	132.0	25.0	.4006	.250	.450	.100	.500	3.50	.20	.00100	5
15	15	3000.	36.0	25.0	.3169	.250	.450	.100	.450	3.50	.20	.00100	5
16	16	3840.	117.0	25.0	.2094	.250	.450	.100	.400	3.50	.20	.00100	5
17	17	5640.	156.0	20.0	.3423	.250	.450	.100	.400	3.50	.20	.00100	5
8	8	14200.	1227.0	67.0	.2919	.250	.450	.050	.450	3.50	.20	.00100	5
37	38	5060.	368.0	7.0	.2400	.250	.450	.200	.420	3.90	.50	.00024	4
38	39	10280.	290.0	7.0	.3153	.250	.450	.300	.420	3.50	.20	.00100	4
36	37	16320.	466.0	5.0	.1439	.250	.450	.300	.480	3.90	.50	.00024	4
33	34	13680.	445.0	8.0	.1186	.150	.400	.200	.410	3.90	.50	.00024	4
34	35	6280.	148.0	7.0	.2940	.250	.450	.300	.420	3.50	.20	.00100	4
35	36	10680.	251.0	6.0	.1368	.250	.450	.300	.400	3.50	.20	.00100	4
31	32	6520.	144.0	6.0	.2938	.250	.450	.300	.420	3.90	.50	.00024	4
32	33	10360.	257.0	12.0	.1275	.150	.400	.150	.420	3.50	.20	.00100	4
30	31	5440.	107.0	7.0	.2363	.150	.400	.150	.450	4.50	.60	.00010	3
22	23	9840.	195.0	8.0	.1920	.250	.450	.200	.460	3.50	.20	.00100	3
29	30	11560.	546.0	12.0	.0980	.150	.400	.150	.450	3.50	.20	.00100	4
26	27	5080.	107.0	5.0	.2510	.250	.450	.300	.450	3.90	.50	.00024	3
27	28	5040.	300.0	9.0	.1461	.150	.400	.150	.430	3.90	.50	.00024	3
28	29	6120.	152.0	7.0	.2020	.150	.400	.150	.450	3.50	.20	.00100	4
24	25	5920.	363.0	9.0	.3292	.250	.450	.300	.450	3.50	.20	.00100	3
25	26	3720.	94.0	8.0	.1772	.150	.400	.150	.450	3.50	.20	.00100	3
23	24	1740.	104.0	7.0	.1530	.250	.450	.300	.450	3.50	.20	.00100	3
21	22	12000.	447.0	20.0	.2822	.150	.400	.200	.400	3.50	.20	.00100	3
9	9	20640.	411.0	8.0	.2894	.250	.450	.300	.470	3.90	.50	.00024	2
10	10	7520.	202.0	6.0	.3773	.250	.450	.300	.480	3.90	.50	.00024	2
7	7	9880.	373.0	7.0	.2911	.300	.500	.300	.500	3.90	.50	.00024	2
3	3	22000.	929.0	8.0	.3243	.250	.450	.200	.450	3.50	.20	.00100	2
4	4	25560.	960.0	8.0	.2675	.250	.450	.200	.500	3.50	.20	.00100	2
2	2	14480.	519.0	7.0	.4504	.300	.500	.300	.420	3.50	.20	.00100	2
6	6	16100.	296.0	10.0	.4790	.300	.500	.300	.450	3.50	.20	.00100	2
5	5	18300.	336.0	6.0	.2506	.300	.500	.300	.420	5.00	.60	.00006	2
1	1	30900.	567.0	7.0	.5000	.300	.500	.300	.420	3.00	.20	.00100	2
11	11	6000.	113.0	25.0	.3243	.250	.450	.200	.500	3.90	.50	.00024	2
12	12	8360.	159.0	6.0	.3715	.300	.500	.300	.500	3.90	.50	.00024	2
13	13	10480.	229.0	7.0	.3542	.300	.500	.300	.500	3.90	.50	.00024	2
256	247	39100.	808.0	7.0	.1652	.250	.450	.200	.450	3.50	.20	.00100	2
257	248	31200.	645.0	8.0	.2217	.250	.450	.200	.450	3.50	.20	.00100	2
258	249	18300.	377.0	7.0	.1984	.250	.450	.300	.420	3.50	.20	.00100	2
259	250	5300.	109.0	5.0	.1627	.250	.450	.300	.450	3.50	.20	.00100	2
253	244	36900.	848.0	50.0	.2354	.300	.500	.300	.350	3.90	.50	.00024	2
254	245	7300.	100.0	7.0	.2934	.250	.450	.200	.450	3.50	.20	.00100	2
255	246	21800.	450.0	8.0	.2396	.250	.450	.300	.450	3.50	.20	.00100	2
76	54	10300.	213.0	8.0	.3735	.300	.500	.300	.500	5.00	.60	.00006	2
77	55	25900.	297.0	7.0	.4316	.300	.500	.300	.500	5.00	.60	.00006	2
75	53	2400.	26.0	6.0	.4875	.300	.500	.300	.460	3.50	.20	.00024	2
73	52	38400.	441.0	18.0	.3662	.300	.500	.300	.400	3.50	.20	.00100	2
82	51	19700.	362.0	25.0	.3938	.250	.450	.300	.400	3.50	.20	.00100	2
71	50	11300.	207.0	25.0	.4627	.300	.500	.400	.450	3.50	.20	.00100	2
80	58	12000.	220.0	6.0	.3854	.300	.500	.300	.480	5.00	.60	.00006	2
81	57	42200.	776.0	8.0	.5226	.250	.450	.200	.470	4.50	.60	.00010	2
78	56	22000.	404.0	18.0	.4013	.250	.450	.300	.500	4.80	.50	.00010	2
79	56	21400.	442.0	15.0	.3303	.300	.500	.300	.450	4.50	.50	.00010	2
72	49	16000.	220.0	35.0	.5698	.300	.500	.300	.500	4.50	.50	.00010	2
69	48	9400.	391.0	35.0	.2301	.250	.450	.300	.400	3.90	.50	.00024	2
1635	1635	12865.	317.0	12.0	.3700	.300	.500	.300	.450	3.50	.20	.00100	2
1645	1645	5640.	126.0	5.0	.2900	.250	.450	.150	.450	3.50	.20	.00100	2
1640	1640	8667.	200.0	10.0	.2900	.300	.300	.320	.450	3.50	.20	.00100	2

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1630	1630	8660.	159.0	6.0	.1300	.400	.450	.150	.450	3.50	.20	.00100	2
1625	1625	10700.	197.0	9.0	.2100	.200	.400	.150	.450	3.50	.20	.00100	1
1610	1610	6780.	109.0	9.0	.0200	.200	.400	.150	.450	4.80	.50	.00010	1
1665	1665	14692.	390.0	35.0	.2870	.200	.400	.150	.450	3.50	.20	.00100	2
1605	1605	7689.	81.0	6.0	.1100	.200	.400	.150	.450	4.80	.50	.00010	1
1660	1660	23764.	552.0	7.0	.2000	.200	.450	.150	.460	3.90	.50	.00024	2
1650	1650	13676.	382.0	7.0	.2300	.200	.200	.150	.450	3.50	.20	.00100	2
1655	1655	22832.	558.0	6.0	.1600	.200	.450	.150	.460	3.50	.20	.00100	2
1620	1620	17977.	324.0	7.0	.0500	.200	.400	.150	.470	4.80	.50	.00010	2
1615	1615	11967.	228.0	7.0	.1200	.200	.400	.150	.470	4.50	.60	.00010	2
1710	1710	9974.	245.0	5.0	.0100	.200	.400	.150	.350	3.90	.50	.00024	1
1600	1600	3273.	25.0	7.0	.0500	.200	.450	.150	.600	5.00	.70	.00002	1
1705	1705	2245.	67.0	5.0	.0100	.200	.400	.150	.350	3.90	.50	.00024	2
1450	1450	4800.	198.0	5.0	.0200	.150	.450	.150	.600	3.90	.50	.00024	1
1445	1445	6714.	164.0	5.0	.0800	.200	.400	.150	.350	5.00	.60	.00006	1
1440	1440	12663.	66.0	7.0	.0100	.150	.450	.150	.600	3.90	.50	.00024	1
1480	1480	34034.	732.0	35.0	.0200	.200	.400	.150	.300	3.90	.50	.00024	1
1435	1435	6984.	232.0	5.0	.0800	.200	.400	.150	.460	5.00	.60	.00006	1
1430	1430	6338.	82.0	5.0	.0700	.200	.400	.150	.460	5.00	.60	.00006	1
1425	1425	4940.	68.0	6.0	.0400	.200	.400	.150	.600	5.00	.70	.00002	1
1420	1420	26178.	59.0	9.0	.0220	.200	.450	.150	.600	3.90	.50	.00024	1
1570	1570	3089.	171.0	6.0	.3540	.200	.450	.150	.450	3.50	.20	.00100	2
1555	1555	7055.	83.0	7.0	.1300	.200	.450	.150	.450	4.80	.50	.00010	1
1565	1565	4112.	95.0	9.0	.3200	.200	.450	.150	.470	3.50	.20	.00100	2
1560	1560	5353.	123.0	8.0	.4400	.200	.450	.150	.450	3.50	.20	.00100	2
1550	1550	20321.	424.0	7.0	.0700	.200	.400	.150	.450	3.50	.20	.00100	1
1415	1415	5148.	307.0	5.0	.0260	.200	.400	.150	.500	3.90	.50	.00024	1
1410	1410	5300.	195.0	5.0	.0100	.150	.450	.150	.500	3.90	.50	.00024	1
1455	1455	19899.	542.0	11.0	.0037	.200	.400	.150	.350	4.80	.50	.00010	1
1490	1490	8100.	698.0	10.0	.0620	.200	.400	.150	.350	4.50	.50	.00010	1
1465	1465	19569.	93.0	10.0	.0348	.150	.500	.150	.350	4.50	.60	.00010	1
1460	1460	12745.	286.0	9.0	.0603	.200	.400	.150	.350	5.00	.60	.00006	1
1575	1575	10554.	222.0	10.0	.4060	.200	.450	.150	.450	3.50	.20	.00100	2
1545	1545	15603.	253.0	7.0	.0890	.200	.400	.150	.450	4.80	.50	.00010	1
1530	1530	8269.	345.0	6.0	.1080	.200	.400	.150	.350	4.80	.50	.00010	1
1525	1525	14343.	53.0	10.0	.0200	.150	.400	.150	.350	3.90	.50	.00024	1
1505	1505	49306.	262.0	10.0	.0100	.150	.450	.150	.350	3.50	.20	.00100	1
1520	1520	21460.	99.0	10.0	.0100	.200	.450	.150	.350	3.50	.20	.00100	1
1715	1715	3131.	115.0	7.0	.1200	.150	.400	.150	.350	3.90	.50	.00024	1
1515	1515	3666.	8.0	60.0	.0200	.150	.400	.150	.350	3.50	.20	.00100	1
1540	1540	19881.	345.0	15.0	.0300	.200	.400	.150	.350	4.50	.60	.00010	1
1510	1510	16588.	76.0	3.0	.0100	.150	.400	.150	.350	3.90	.50	.00024	1
1500	1500	21483.	465.0	10.0	.0400	.200	.400	.150	.250	3.90	.50	.00024	1
299	299	20092.	72.0	40.0	.1300	.150	.500	.150	.350	4.80	.50	.00010	1
301	301	38137.	177.0	31.0	.1600	.150	.500	.150	.350	4.80	.50	.00010	1
297	297	84806.	338.0	40.0	.1200	.150	.500	.150	.350	4.80	.50	.00010	1
305	1917	1795.	103.0	10.0	.0240	.150	.350	.150	.250	3.90	.50	.00024	1
304	304	2970.	150.0	10.0	.0240	.150	.350	.150	.250	3.90	.50	.00024	1
262	262	3964.	39.0	5.0	.0200	.200	.400	.150	.250	3.90	.50	.00024	1
264	264	1734.	26.0	5.0	.0200	.200	.400	.150	.250	3.90	.50	.00024	1
243	243	46293.	82.0	7.0	.0200	.200	.350	.150	.350	3.90	.50	.00024	1
384	384	27915.	77.0	45.0	.0900	.150	.500	.150	.350	4.80	.50	.00010	1
290	290	4748.	29.0	5.0	.0250	.300	.400	.150	.400	3.90	.50	.00024	1
353	353	12867.	41.0	50.0	.0700	.150	.500	.150	.350	5.00	.60	.00006	1
350	350	13939.	51.0	70.0	.0550	.150	.400	.150	.350	4.80	.50	.00010	1
351	351	17043.	59.0	70.0	.0600	.150	.450	.150	.350	5.00	.60	.00006	1
376	376	1390.	3.0	10.0	.0100	.150	.450	.150	.350	4.80	.50	.00010	1
368	368	7225.	99.0	50.0	.0070	.150	.450	.150	.350	3.90	.50	.00024	1
361	361	6400.	30.0	60.0	.0060	.150	.450	.150	.350	3.90	.50	.00024	2
369	369	7449.	17.0	60.0	.0400	.150	.450	.150	.350	4.80	.50	.00010	1
354	1818	6316.	6.0	95.0	.0400	.150	.350	.150	.250	4.80	.50	.00010	1
355	355	9583.	7.0	65.0	.0400	.150	.350	.150	.250	4.80	.50	.00010	1
363	363	9583.	7.0	33.0	.0550	.150	.350	.150	.250	4.80	.50	.00010	1
366	366	26706.	81.0	45.0	.0550	.150	.500	.150	.350	4.80	.50	.00010	1
367	367	9047.	23.0	65.0	.0450	.150	.500	.150	.350	4.80	.50	.00010	1
373	373	4140.	38.0	6.0	.0200	.150	.400	.150	.350	4.80	.50	.00010	1
241	241	45665.	343.0	45.0	.0200	.150	.400	.150	.450	3.90	.50	.00024	1
346	346	21083.	71.0	40.0	.0600	.150	.450	.150	.350	3.90	.50	.00024	1
345	345	20528.	78.0	50.0	.0600	.150	.450	.150	.350	4.80	.50	.00010	1
349	349	1951.	13.0	15.0	.0200	.150	.450	.150	.350	4.80	.50	.00010	1
347	347	11476.	55.0	65.0	.0500	.150	.400	.150	.350	4.80	.50	.00010	1
371	371	12050.	83.0	50.0	.0500	.150	.450	.150	.250	4.80	.50	.00010	1
338	338	14259.	73.0	8.0	.0250	.150	.350	.150	.250	3.90	.50	.00024	1
333	333	6300.	5.0	60.0	.0400	.200	.450	.150	.550	3.50	.20	.00100	1
334	334	6300.	5.0	60.0	.0400	.150	.350	.150	.250	3.50	.20	.00100	1
240	240	2500.	46.0	25.0	.1100	.150	.450	.150	.600	3.90	.50	.00024	1
318	318	20255.	157.0	20.0	.0300	.150	.550	.150	.500	3.90	.50	.00024	1
335	335	8868.	36.0	45.0	.0500	.150	.450	.150	.450	3.90	.50	.00024	1
336	1329	10002.	31.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
337	337	14520.	50.0	50.0	.0350	.150	.450	.150	.450	3.90	.50	.00024	1
312	312	7094.	12.0	70.0	.0400	.150	.450	.150	.250	3.90	.50	.00024	1
315	315	8712.	28.0	45.0	.0400	.150	.450	.150	.450	3.90	.50	.00024	1
316	316	12777.	43.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
358	358	4084.	12.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
320	320	22099.	161.0	50.0	.0250	.250	.450	.250	.600	3.90	.50	.00024	1
1323	1323	2406.	9.0	50.0	.0080	.150	.450	.150	.450	3.90	.50	.00024	1
321	321	47509.	25.0	60.0	.0450	.150	.450	.150	.350	3.90	.50	.00024	1
319	319	43000.	164.0	70.0	.0250	.150	.400	.150	.250	3.90	.50	.00024	1
370	370	14400.	41.0	70.0	.0250	.150	.400	.150	.250	3.90	.50	.00024	1
233	233	42776.	281.0	25.0	.0500	.150	.500	.150	.500	3.90	.50	.00024	1
235	235	20400.	187.0	20.0	.1100	.150	.500	.150	.500	3.90	.50	.00024	1
231	231	58487.	390.0	55.0	.0200	.150	.400	.150	.250	3.90	.50	.00024	1

OTOTAL NUMBER OF SUBCATCHMENTS, 314
 OTOTAL TRIBUTARY AREA (ACRES), 86852.00
 1

model sbc_ltd
 50-year model

50_1td.wpd July 12, 2000 50-YR SWMM MODEL

*** CONTINUITY CHECK FOR SUBCATCHMENT ROUTING IN UDSWM386 MODEL ***

WATERSHED AREA (ACRES) 86852.000
 TOTAL RAINFALL (INCHES) 3.645
 TOTAL INFILTRATION (INCHES) 2.709
 TOTAL WATERSHED OUTFLOW (INCHES) .908
 TOTAL SURFACE STORAGE AT END OF STORM (INCHES) .028
 ERROR IN CONTINUITY, PERCENTAGE OF RAINFALL -.023

1

model sbc_1td
 50-year model

GUTTER NUMBER	GUTTER CONNECTION	NDP	NP		WIDTH OR DIAM (FT)	LENGTH (FT)	INVERT SLOPE (FT/FT)	SIDE SLOPES		MANNING N	OVERBANK/SURCHARGE		JK
								HORIZ L	VERT R		DEPTH (FT)		
226	224	0	1	CHANNEL	20.0	3740.	.1337	4.0	4.0	.040	15.00	0	
225	224	0	1	CHANNEL	5.0	1862.	.0600	10.0	10.0	.043	15.00	0	
224	222	0	1	CHANNEL	4.0	4220.	.1300	3.0	3.0	.055	15.00	0	
223	222	0	1	CHANNEL	10.0	5960.	.1406	10.0	10.0	.040	15.00	0	
222	218	0	1	CHANNEL	5.0	2280.	.1000	4.0	4.0	.055	15.00	0	
221	218	0	1	CHANNEL	5.0	6520.	.1992	5.0	5.0	.055	15.00	0	
220	219	0	1	CHANNEL	8.0	7580.	.2107	7.0	7.0	.050	15.00	0	
218	219	0	1	CHANNEL	5.0	1660.	.0900	4.0	4.0	.055	15.00	0	
219	215	0	1	CHANNEL	10.0	2531.	.1000	7.0	7.0	.055	15.00	0	
216	215	0	1	CHANNEL	20.0	8160.	.1875	10.0	10.0	.055	15.00	0	
214	212	0	1	CHANNEL	10.0	6880.	.1727	10.0	10.0	.055	15.00	0	
213	212	0	1	CHANNEL	10.0	5900.	.1268	10.0	10.0	.055	15.00	0	
212	211	0	1	CHANNEL	15.0	6100.	.1511	7.0	7.0	.060	15.00	0	
215	211	0	4	CHANNEL	10.0	5210.	.0600	4.0	4.0	.050	2.00	0	
				OVERFLOW	50.0	5210.	.0600	6.0	6.0	.055	25.00	0	
217	215	0	1	CHANNEL	20.0	4860.	.3560	5.0	5.0	.040	15.00	0	
211	207	0	4	CHANNEL	8.0	2390.	.0500	3.0	3.0	.050	2.00	0	
				OVERFLOW	25.0	2390.	.0500	5.0	5.0	.055	25.00	0	
186	184	0	1	CHANNEL	10.0	4260.	.1002	9.0	9.0	.060	15.00	0	
185	184	0	1	CHANNEL	5.0	3720.	.0594	6.0	6.0	.060	15.00	0	
183	182	0	1	CHANNEL	10.0	8000.	.1050	6.0	6.0	.060	15.00	0	
181	180	0	1	CHANNEL	5.0	6640.	.1583	7.0	7.0	.060	15.00	0	
184	182	0	1	CHANNEL	15.0	3540.	.1158	8.0	8.0	.055	15.00	0	
182	180	0	4	CHANNEL	15.0	4600.	.0720	4.0	4.0	.050	2.50	0	
				OVERFLOW	100.0	4370.	.0758	15.0	15.0	.055	20.00	0	
180	176	0	4	CHANNEL	10.0	4520.	.0507	4.0	4.0	.045	3.00	0	
				OVERFLOW	35.0	4294.	.0534	3.0	3.0	.060	20.00	0	
204	201	0	1	CHANNEL	15.0	6720.	.0911	6.0	6.0	.050	15.00	0	
203	201	0	1	CHANNEL	5.0	3500.	.2286	5.0	5.0	.055	15.00	0	
201	198	0	4	CHANNEL	15.0	7700.	.0835	4.0	4.0	.050	3.00	0	
				OVERFLOW	50.0	7315.	.0879	7.0	7.0	.060	20.00	0	
200	198	0	1	CHANNEL	5.0	7220.	.1722	7.0	7.0	.055	15.00	0	
202	198	0	1	CHANNEL	5.0	3820.	.1971	5.0	5.0	.060	15.00	0	
198	194	0	4	CHANNEL	25.0	7220.	.0370	4.0	4.0	.050	3.00	0	
				OVERFLOW	200.0	6860.	.0389	7.0	7.0	.060	20.00	0	
199	194	0	1	CHANNEL	5.0	9020.	.1233	6.0	6.0	.060	15.00	0	
196	194	0	1	CHANNEL	5.0	7320.	.1243	5.0	5.0	.060	15.00	0	
195	194	0	1	CHANNEL	10.0	4760.	.1513	5.0	5.0	.060	15.00	0	
194	192	0	4	CHANNEL	20.0	7560.	.0921	4.0	4.0	.055	3.00	0	
				OVERFLOW	80.0	7182.	.0969	10.0	10.0	.060	20.00	0	
208	207	0	1	CHANNEL	10.0	4260.	.2230	8.0	8.0	.060	15.00	0	
207	205	0	4	CHANNEL	25.0	5000.	.0150	4.0	4.0	.040	2.00	0	
				OVERFLOW	200.0	5000.	.0150	10.0	10.0	.050	25.00	0	
206	205	0	1	CHANNEL	25.0	3860.	.2591	5.0	5.0	.040	15.00	0	
205	192	0	4	CHANNEL	20.0	4900.	.0349	4.0	4.0	.045	3.00	0	
				OVERFLOW	100.0	4900.	.0349	8.0	8.0	.055	25.00	0	
192	187	0	4	CHANNEL	32.0	1540.	.0120	4.0	4.0	.040	3.00	0	
				OVERFLOW	250.0	1540.	.0120	20.0	20.0	.050	25.00	0	
193	187	0	1	CHANNEL	25.0	4480.	.1897	4.0	4.0	.040	15.00	0	
187	172	0	4	CHANNEL	32.0	7388.	.0100	4.0	4.0	.040	3.00	0	
				OVERFLOW	250.0	7388.	.0100	20.0	20.0	.050	25.00	0	
178	177	0	1	CHANNEL	5.0	6500.	.1186	8.0	8.0	.060	15.00	0	
177	175	0	1	CHANNEL	8.0	6020.	.0862	7.0	7.0	.055	15.00	0	
179	176	0	1	CHANNEL	20.0	3860.	.2383	5.0	5.0	.045	15.00	0	
176	175	0	4	CHANNEL	20.0	7520.	.0386	4.0	4.0	.045	3.00	0	
				OVERFLOW	100.0	7144.	.0406	5.0	5.0	.060	20.00	0	
174	173	0	1	CHANNEL	5.0	4060.	.1421	6.0	6.0	.055	15.00	0	
175	173	0	4	CHANNEL	30.0	1900.	.0353	4.0	4.0	.035	3.00	0	
				OVERFLOW	150.0	1805.	.0372	15.0	15.0	.045	20.00	0	
173	172	0	4	CHANNEL	25.0	5760.	.0587	4.0	4.0	.035	3.00	0	
				OVERFLOW	200.0	5472.	.0618	15.0	15.0	.045	20.00	0	
172	157	0	4	CHANNEL	25.0	1860.	.0100	3.0	3.0	.045	3.00	0	
				OVERFLOW	75.0	1860.	.0100	5.0	5.0	.050	25.00	0	
168	165	0	1	CHANNEL	5.0	3620.	.1740	7.0	7.0	.060	15.00	0	
169	165	0	1	CHANNEL	5.0	3140.	.1720	7.0	7.0	.060	15.00	0	
165	166	0	1	CHANNEL	10.0	6920.	.1026	5.0	5.0	.060	15.00	0	
167	166	0	1	CHANNEL	5.0	5360.	.1940	6.0	6.0	.060	15.00	0	
166	163	0	1	CHANNEL	15.0	1040.	.0673	10.0	10.0	.055	15.00	0	
164	163	0	1	CHANNEL	10.0	4000.	.1263	8.0	8.0	.050	15.00	0	
163	157	0	1	CHANNEL	25.0	2640.	.0568	5.0	5.0	.050	15.00	0	
170	157	0	1	CHANNEL	5.0	4840.	.1543	5.0	5.0	.055	15.00	0	
171	157	0	1	CHANNEL	5.0	4420.	.1837	7.0	7.0	.055	15.00	0	
157	156	0	4	CHANNEL	25.0	1660.	.0220	3.0	3.0	.045	3.00	0	
				OVERFLOW	75.0	1660.	.0220	4.0	4.0	.050	25.00	0	
161	160	0	1	CHANNEL	5.0	4380.	.1667	5.0	5.0	.060	15.00	0	

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162	160	0	1	CHANNEL	5.0	5800.	.2121	5.0	5.0	.060	15.00	0
160	158	0	1	CHANNEL	10.0	3360.	.0908	10.0	10.0	.055	15.00	0
159	158	0	1	CHANNEL	10.0	6380.	.1293	6.0	6.0	.060	15.00	0
158	156	0	1	CHANNEL	20.0	5700.	.0619	5.0	5.0	.050	15.00	0
156	154	0	4	CHANNEL	35.0	4980.	.0190	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	4980.	.0190	3.0	3.0	.055	25.00	0
155	154	0	1	CHANNEL	12.0	2180.	.2683	4.0	4.0	.050	15.00	0
153	152	0	1	CHANNEL	12.0	4380.	.1530	4.0	4.0	.060	15.00	0
154	152	0	4	CHANNEL	35.0	2880.	.0200	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	2880.	.0200	3.0	3.0	.055	25.00	0
152	149	0	4	CHANNEL	30.0	6980.	.0150	4.0	4.0	.045	3.00	0
				OVERFLOW	200.0	6980.	.0150	5.0	5.0	.050	25.00	0
150	149	0	1	CHANNEL	5.0	2780.	.1691	4.0	4.0	.055	15.00	0
151	149	0	1	CHANNEL	6.0	4120.	.1286	4.0	4.0	.055	15.00	0
149	139	0	4	CHANNEL	35.0	3220.	.0140	4.0	4.0	.045	3.00	0
				OVERFLOW	300.0	3220.	.0140	5.0	5.0	.050	25.00	0
147	146	0	1	CHANNEL	8.0	5600.	.1625	6.0	6.0	.060	15.00	0
148	146	0	1	CHANNEL	8.0	2720.	.1048	8.0	8.0	.060	15.00	0
146	142	0	1	CHANNEL	10.0	5540.	.0727	8.0	8.0	.055	15.00	0
144	143	0	1	CHANNEL	5.0	2200.	.1568	8.0	8.0	.060	15.00	0
145	143	0	1	CHANNEL	3.0	2160.	.1574	5.0	5.0	.060	15.00	0
143	142	0	1	CHANNEL	8.0	4840.	.1184	5.0	5.0	.060	15.00	0
142	140	0	1	CHANNEL	10.0	2080.	.0514	8.0	5.0	.055	15.00	0
141	140	0	1	CHANNEL	5.0	3800.	.1237	5.0	5.0	.060	15.00	0
140	139	0	1	CHANNEL	15.0	4320.	.0505	8.0	7.0	.055	15.00	0
138	137	0	1	CHANNEL	10.0	5440.	.0432	10.0	10.0	.055	15.00	0
139	137	0	4	CHANNEL	30.0	1880.	.0160	4.0	4.0	.045	3.00	0
				OVERFLOW	200.0	1880.	.0160	5.0	5.0	.050	25.00	0
137	129	0	4	CHANNEL	30.0	2009.	.0130	4.0	4.0	.040	3.00	0
				OVERFLOW	200.0	2009.	.0130	5.0	5.0	.050	25.00	0
135	134	0	1	CHANNEL	5.0	4080.	.1716	5.0	5.0	.060	15.00	0
136	134	0	1	CHANNEL	5.0	3000.	.1433	6.0	6.0	.060	15.00	0
134	133	0	1	CHANNEL	10.0	10020.	.0868	5.0	5.0	.055	15.00	0
133	130	0	1	CHANNEL	15.0	7720.	.0505	5.0	5.0	.055	15.00	0
131	130	0	4	CHANNEL	15.0	4860.	.1008	3.0	3.0	.055	3.00	0
				OVERFLOW	100.0	4617.	.1061	10.0	10.0	.060	20.00	0
132	130	0	1	CHANNEL	8.0	4560.	.0789	6.0	6.0	.060	15.00	0
130	129	0	1	CHANNEL	25.0	3360.	.0363	7.0	7.0	.055	15.00	0
129	96	0	4	CHANNEL	30.0	3520.	.0160	3.5	3.5	.055	4.00	0
				OVERFLOW	100.0	3520.	.0160	4.0	4.0	.060	25.00	0
125	124	0	1	CHANNEL	5.0	3800.	.1842	8.0	8.0	.055	15.00	0
126	124	0	1	CHANNEL	5.0	3420.	.1871	6.0	6.0	.060	15.00	0
124	122	0	1	CHANNEL	10.0	7520.	.0535	8.0	8.0	.055	15.00	0
127	123	0	1	CHANNEL	10.0	8000.	.1056	10.0	10.0	.055	15.00	0
128	123	0	1	CHANNEL	10.0	8660.	.1236	15.0	15.0	.055	15.00	0
123	122	0	1	CHANNEL	15.0	4160.	.0317	15.0	15.0	.055	15.00	0
122	96	0	1	CHANNEL	20.0	9440.	.0607	5.0	5.0	.060	15.00	0
96	95	0	4	CHANNEL	25.0	6320.	.0170	2.0	2.0	.055	4.00	0
				OVERFLOW	50.0	6320.	.0170	2.0	2.0	.060	25.00	0
116	95	0	4	CHANNEL	5.0	9520.	.0772	3.0	3.0	.050	2.50	0
				OVERFLOW	70.0	9044.	.0813	8.0	8.0	.055	20.00	0
95	94	0	4	CHANNEL	30.0	4000.	.0120	3.0	3.0	.040	3.00	0
				OVERFLOW	150.0	4000.	.0120	5.0	5.0	.050	25.00	0
85	84	0	1	CHANNEL	5.0	2220.	.0396	4.0	4.0	.060	15.00	0
86	84	0	1	CHANNEL	8.0	5880.	.1259	4.0	4.0	.060	15.00	0
84	82	0	1	CHANNEL	10.0	2720.	.0890	10.0	10.0	.060	15.00	0
83	82	0	1	CHANNEL	10.0	2380.	.0450	12.0	12.0	.060	15.00	0
82	80	0	1	CHANNEL	20.0	2220.	.0396	12.0	12.0	.060	15.00	0
87	81	0	1	CHANNEL	10.0	8040.	.0796	5.0	5.0	.065	15.00	0
81	80	0	1	CHANNEL	15.0	6220.	.0691	7.0	7.0	.065	15.00	0
80	79	0	1	CHANNEL	20.0	6380.	.1993	10.0	10.0	.065	15.00	0
121	79	0	4	CHANNEL	8.0	4700.	.0660	4.0	4.0	.055	2.50	0
				OVERFLOW	60.0	4465.	.0695	12.0	12.0	.057	20.00	0
79	75	0	1	CHANNEL	25.0	8020.	.0212	10.0	10.0	.060	15.00	0
78	75	0	1	CHANNEL	8.0	3780.	.0688	20.0	20.0	.060	15.00	0
75	77	0	1	CHANNEL	25.0	1600.	.0188	3.0	5.0	.060	15.00	0
77	74	0	1	CHANNEL	40.0	2020.	.0198	3.0	3.0	.060	15.00	0
76	74	0	4	CHANNEL	10.0	6420.	.0779	4.0	4.0	.050	2.00	0
				OVERFLOW	60.0	6420.	.0779	8.0	8.0	.055	20.00	0
74	59	0	4	CHANNEL	30.0	4700.	.0130	4.0	4.0	.050	4.00	0
				OVERFLOW	75.0	4700.	.0130	4.0	3.0	.055	25.00	0
89	88	0	1	CHANNEL	8.0	4240.	.0217	10.0	10.0	.055	15.00	0
93	88	0	1	CHANNEL	5.0	2440.	.0984	10.0	10.0	.055	15.00	0
88	77	0	4	CHANNEL	11.0	7200.	.1380	10.0	10.0	.060	3.00	0
				OVERFLOW	100.0	7200.	.1380	50.0	50.0	.045	20.00	0
120	119	0	4	CHANNEL	5.0	3980.	.0879	3.0	3.0	.050	3.00	0
				OVERFLOW	200.0	3781.	.0925	10.0	10.0	.055	20.00	0
118	119	0	4	CHANNEL	5.0	8220.	.1095	3.0	3.0	.050	3.00	0
				OVERFLOW	150.0	7809.	.1153	10.0	10.0	.055	20.00	0
119	104	0	4	CHANNEL	5.0	1300.	.0400	3.0	3.0	.050	3.00	0
				OVERFLOW	150.0	1235.	.0421	10.0	10.0	.055	20.00	0
117	104	0	4	CHANNEL	5.0	6000.	.0587	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	5700.	.0618	10.0	10.0	.055	20.00	0
104	103	0	4	CHANNEL	10.0	3440.	.0343	3.0	3.0	.045	3.00	0
				OVERFLOW	150.0	3268.	.0361	10.0	10.0	.050	20.00	0
105	103	0	4	CHANNEL	5.0	4560.	.0811	3.0	3.0	.045	3.00	0
				OVERFLOW	100.0	4332.	.0854	10.0	10.0	.050	20.00	0
106	102	0	4	CHANNEL	5.0	6380.	.0690	3.0	3.0	.045	3.00	0
				OVERFLOW	70.0	6061.	.0726	10.0	10.0	.050	20.00	0
103	102	0	4	CHANNEL	8.0	1380.	.0362	4.0	40.0	.050	3.00	0
				OVERFLOW	68.0	1311.	.0381	25.0	25.0	.055	20.00	0
102	101	0	4	CHANNEL	11.0	5220.	.0383	8.0	8.0	.055	3.00	0
				OVERFLOW	100.0	4959.	.0403	5.0	5.0	.060	20.00	0
114	112	0	1	CHANNEL	5.0	4500.	.1467	5.0	5.0	.060	8.00	0
115	112	0	1	CHANNEL	5.0	3240.	.1759	5.0	5.0	.060	8.00	0
112	110	0	4	CHANNEL	5.0	3640.	.1745	3.0	3.0	.055	2.50	0
				OVERFLOW	40.0	3458.	.1837	10.0	8.0	.060	20.00	0
113	110	0	4	CHANNEL	5.0	5060.	.1690	3.0	3.0	.055	3.00	0
				OVERFLOW	40.0	4807.	.1779	10.0	10.0	.060	20.00	0
110	109	0	4	CHANNEL	11.0	4140.	.0531	4.0	4.0	.055	3.00	0
				OVERFLOW	60.0	3933.	.0559	50.0	50.0	.060	20.00	0

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111	109	0	4	CHANNEL	5.0	5600.	.2348	3.0	3.0	.050	2.00	0	
				OVERFLOW	20.0	5320.	.2472	6.0	6.0	.055	20.00	0	
108	107	0	4	CHANNEL	5.0	6240.	.1875	3.0	3.0	.050	2.00	0	
				OVERFLOW	20.0	5928.	.1974	6.0	6.0	.055	20.00	0	
109	107	0	4	CHANNEL	11.0	2760.	.0525	4.0	4.0	.050	3.00	0	
				OVERFLOW	60.0	2622.	.0553	6.0	6.0	.055	20.00	0	
107	101	0	4	CHANNEL	11.0	2720.	.0368	4.0	4.0	.050	3.00	0	
				OVERFLOW	45.0	2584.	.0387	6.0	6.0	.055	20.00	0	
101	99	0	4	CHANNEL	11.0	1380.	.0268	4.0	4.0	.050	3.00	0	
				OVERFLOW	50.0	1311.	.0282	5.0	5.0	.055	20.00	0	
100	99	0	4	CHANNEL	5.0	9980.	.1735	3.0	3.0	.050	2.00	0	
				OVERFLOW	25.0	9481.	.1826	5.0	5.0	.055	20.00	0	
99	97	0	4	CHANNEL	11.0	1440.	.0299	4.0	4.0	.050	3.00	0	
				OVERFLOW	50.0	1368.	.0315	5.0	5.0	.055	20.00	0	
98	97	0	4	CHANNEL	8.0	7000.	.1179	3.0	3.0	.050	2.00	0	
				OVERFLOW	35.0	6650.	.1241	6.0	6.0	.055	20.00	0	
97	94	0	4	CHANNEL	11.0	5720.	.0332	4.0	4.0	.050	2.50	0	
				OVERFLOW	50.0	5434.	.0349	4.0	4.0	.055	20.00	0	
94	74	0	4	CHANNEL	32.0	2560.	.0120	4.0	4.0	.040	3.50	0	
				OVERFLOW	150.0	2560.	.0120	8.0	8.0	.050	25.00	0	
72	71	0	1	CHANNEL	10.0	4480.	.0808	5.0	5.0	.055	15.00	0	
73	71	0	1	CHANNEL	10.0	8000.	.0303	8.0	8.0	.055	15.00	0	
71	59	0	1	CHANNEL	12.0	4820.	.0664	5.0	5.0	.060	15.00	0	
59	46	0	4	CHANNEL	30.0	4020.	.0140	4.0	4.0	.050	4.00	0	
				OVERFLOW	60.0	4020.	.0140	3.0	3.0	.055	25.00	0	
63	61	0	1	CHANNEL	9.0	6420.	.0779	5.0	5.0	.070	20.00	0	
64	61	0	1	CHANNEL	9.0	2020.	.0198	5.0	5.0	.070	20.00	0	
61	62	0	1	CHANNEL	12.0	7500.	.0633	5.0	5.0	.070	20.00	0	
60	46	0	1	CHANNEL	12.0	4080.	.1262	5.0	5.0	.060	20.00	0	
46	42	0	4	CHANNEL	25.0	3220.	.0300	3.0	3.0	.055	5.00	0	
				OVERFLOW	50.0	3220.	.0300	4.0	4.0	.060	25.00	0	
66	65	0	1	CHANNEL	9.0	3060.	.2026	4.0	4.0	.060	15.00	0	
67	65	0	4	CHANNEL	10.0	6620.	.0853	3.0	3.0	.050	4.00	0	
				OVERFLOW	45.0	6289.	.0898	3.0	3.0	.060	25.00	0	
65	62	0	4	CHANNEL	15.0	3960.	.0088	3.0	3.0	.050	4.00	0	
				OVERFLOW	50.0	3762.	.0093	3.0	3.0	.060	25.00	0	
62	42	0	1	CHANNEL	12.0	1400.	.2629	5.0	5.0	.070	20.00	0	
69	68	0	1	CHANNEL	10.0	3740.	.1056	6.0	6.0	.055	15.00	0	
70	68	0	1	CHANNEL	12.0	6960.	.0912	6.0	6.0	.055	15.00	0	
68	42	0	1	CHANNEL	12.0	2120.	.1203	5.0	5.0	.060	15.00	0	
41	40	0	1	CHANNEL	12.0	3100.	.2423	5.0	5.0	.060	20.00	0	
42	40	0	4	CHANNEL	20.0	7580.	.0500	3.0	3.0	.055	4.00	0	
				OVERFLOW	50.0	7580.	.0500	2.0	2.0	.060	25.00	0	
40	16	0	4	CHANNEL	20.0	3000.	.0330	3.0	3.0	.055	4.00	0	
				OVERFLOW	50.0	3000.	.0330	2.0	2.0	.060	25.00	0	
20	18	0	1	CHANNEL	10.0	5340.	.0534	8.0	8.0	.050	15.00	0	
18	17	0	4	CHANNEL	11.0	7600.	.0605	3.0	3.0	.050	3.00	0	
				OVERFLOW	40.0	7220.	.0637	5.0	5.0	.055	20.00	0	
21	17	0	1	CHANNEL	10.0	6960.	.1042	5.0	5.0	.060	15.00	0	
17	16	0	4	CHANNEL	11.0	1000.	.0493	10.0	10.0	.040	3.00	0	
				OVERFLOW	40.0	1000.	.0493	8.0	8.0	.055	20.00	0	
14	15	0	1	CHANNEL	15.0	3080.	.2662	3.0	3.0	.060	15.00	0	
15	8	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
16	15	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
8	397	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
397	6	14	2	PIPE	.1	1.	.0050	.0	.0	.013	.10	0	
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW													
		.0	.0	207.0	170.0	415.0	476.0	833.0	1330.0	1254.0	2417.0	1677.0	3673.0
		2104.0	5078.0	2535.0	6591.0	2968.0	8200.0	3405.0	9896.0	3847.0	12853.0	4292.0	16870.0
		6098.0	37861.0	7880.0	91713.0								
38	37	0	1	CHANNEL	12.0	5060.	.1146	15.0	15.0	.050	15.00	0	
39	37	0	1	CHANNEL	10.0	5140.	.0807	10.0	10.0	.050	20.00	0	
37	23	0	4	CHANNEL	11.0	8160.	.0386	4.0	4.0	.050	3.00	0	
				OVERFLOW	60.0	7752.	.0406	25.0	25.0	.055	20.00	0	
35	34	0	1	CHANNEL	10.0	3140.	.0930	10.0	10.0	.050	15.00	0	
36	34	0	1	CHANNEL	12.0	5340.	.0549	15.0	15.0	.050	15.00	0	
34	23	0	4	CHANNEL	11.0	6840.	.0450	4.0	4.0	.050	3.00	0	
				OVERFLOW	50.0	6498.	.0474	25.0	25.0	.055	20.00	0	
32	31	0	1	CHANNEL	8.0	3260.	.0883	8.0	8.0	.055	15.00	0	
33	31	0	1	CHANNEL	8.0	5180.	.0788	8.0	8.0	.055	15.00	0	
31	23	0	1	CHANNEL	12.0	2720.	.0393	10.0	10.0	.055	15.00	0	
23	22	0	4	CHANNEL	11.0	4920.	.0315	3.0	3.0	.050	3.00	0	
				OVERFLOW	50.0	4674.	.0332	10.0	10.0	.055	20.00	0	
29	28	0	1	CHANNEL	5.0	3060.	.1471	6.0	6.0	.055	15.00	0	
30	28	0	1	CHANNEL	12.0	5780.	.0484	15.0	15.0	.050	15.00	0	
27	26	0	1	CHANNEL	10.0	2540.	.1693	10.0	10.0	.040	15.00	0	
28	26	0	4	CHANNEL	11.0	2520.	.0595	10.0	10.0	.040	3.00	0	
				OVERFLOW	80.0	2394.	.0626	25.0	25.0	.045	15.00	0	
25	24	0	1	CHANNEL	6.0	5920.	.1309	8.0	8.0	.050	15.00	0	
26	24	0	4	CHANNEL	12.0	1860.	.0242	4.0	4.0	.050	3.00	0	
				OVERFLOW	80.0	1767.	.0255	10.0	10.0	.055	15.00	0	
24	22	0	4	CHANNEL	12.0	1740.	.0287	4.0	4.0	.050	3.00	0	
				OVERFLOW	100.0	1653.	.0302	10.0	10.0	.055	20.00	0	
22	8	0	4	CHANNEL	11.0	3600.	.0658	3.0	3.0	.050	3.00	0	
				OVERFLOW	40.0	3600.	.0658	6.0	6.0	.055	20.00	0	
9	7	0	4	CHANNEL	3.0	10320.	.1556	3.0	3.0	.060	2.00	0	
				OVERFLOW	20.0	9804.	.1638	2.0	2.0	.080	25.00	0	
10	7	0	1	CHANNEL	15.0	3760.	.1293	3.0	3.0	.040	15.00	0	
7	5	0	4	CHANNEL	5.0	4940.	.0656	2.0	2.0	.060	2.50	0	
				OVERFLOW	25.0	4693.	.0691	2.0	2.0	.080	20.00	0	
3	2	0	1	CHANNEL	25.0	11000.	.0682	4.0	4.0	.040	15.00	0	
4	2	0	1	CHANNEL	25.0	12780.	.1033	4.0	4.0	.040	15.00	0	
2	1	0	4	CHANNEL	8.0	7240.	.0631	2.0	2.0	.070	3.00	0	
				OVERFLOW	30.0	6878.	.0664	2.0	2.0	.080	20.00	0	
6	5	0	4	CHANNEL	35.0	4840.	.0340	2.0	2.0	.055	4.00	0	
				OVERFLOW	60.0	4840.	.0340	2.0	2.0	.065	25.00	0	
5	1	0	4	CHANNEL	30.0	4960.	.0240	2.0	2.0	.055	4.00	0	
				OVERFLOW	55.0	4960.	.0240	2.0	2.0	.065	25.00	0	
1	245	0	4	CHANNEL	30.0	10240.	.0240	2.0	2.0	.055	4.00	0	
				OVERFLOW	55.0	10240.	.0240	2.0	2.0	.065	25.00	0	
11	13	0	1	CHANNEL	12.0	3000.	.1200	3.0	3.0	.040	15.00	0	

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12	13	0	1	CHANNEL	12.0	4180.	.1340	3.0	3.0	.040	15.00	0	
13	5	0	4	CHANNEL	15.0	5240.	.1202	4.0	4.0	.040	5.00	0	
				OVERFLOW	100.0	4978.	.1265	40.0	40.0	.045	20.00	0	
248	250	0	4	CHANNEL	25.0	9340.	.0931	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	8973.	.0980	40.0	40.0	.080	20.00	0	
249	250	0	4	CHANNEL	20.0	3940.	.0964	4.0	4.0	.060	5.00	0	
				OVERFLOW	80.0	3743.	.1015	40.0	40.0	.080	20.00	0	
247	246	0	4	CHANNEL	25.0	8120.	.0924	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	7714.	.0973	40.0	40.0	.080	20.00	0	
250	246	0	4	CHANNEL	25.0	2060.	.0485	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	1957.	.0511	40.0	40.0	.080	20.00	0	
246	245	0	4	CHANNEL	25.0	4650.	.0676	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	4427.	.0712	40.0	40.0	.080	20.00	0	
244	52	0	4	CHANNEL	25.0	8700.	.0989	4.0	4.0	.070	5.00	0	
				OVERFLOW	100.0	8265.	.1041	40.0	40.0	.080	20.00	0	
245	52	0	4	CHANNEL	30.0	3060.	.0300	3.0	3.0	.070	4.00	0	
				OVERFLOW	60.0	3060.	.0300	2.0	2.0	.080	20.00	0	
54	53	0	1	CHANNEL	5.0	4000.	.1500	3.0	3.0	.060	15.00	0	
55	53	0	1	CHANNEL	5.0	5500.	.1382	3.0	3.0	.060	15.00	0	
53	52	0	1	CHANNEL	5.0	1200.	.1083	3.0	3.0	.060	15.00	0	
51	50	0	4	CHANNEL	5.0	5200.	.1327	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	4940.	.1397	40.0	40.0	.080	20.00	0	
52	50	0	4	CHANNEL	35.0	9160.	.0218	3.0	3.0	.055	4.00	0	
				OVERFLOW	65.0	9160.	.0218	2.0	2.0	.065	25.00	0	
50	48	0	4	CHANNEL	40.0	3400.	.0294	5.0	5.0	.060	4.00	0	
				OVERFLOW	150.0	3400.	.0294	75.0	75.0	.080	25.00	0	
57	56	0	4	CHANNEL	25.0	8400.	.1262	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	7980.	.1328	40.0	40.0	.080	20.00	0	
58	56	0	1	CHANNEL	5.0	2200.	.1636	3.0	3.0	.060	15.00	0	
56	50	0	4	CHANNEL	25.0	10000.	.0930	4.0	4.0	.070	5.00	0	
				OVERFLOW	100.0	9500.	.0979	40.0	40.0	.080	20.00	0	
49	48	0	1	CHANNEL	12.0	3200.	.2594	3.0	3.0	.060	8.00	0	
48	1626	0	4	CHANNEL	30.0	4700.	.0133	2.0	2.0	.070	5.00	0	
				OVERFLOW	200.0	4700.	.0133	2.0	2.0	.085	25.00	0	
1238	1927	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1927	238	0	4	CHANNEL	15.0	964.	.0012	3.5	3.5	.045	4.00	0	
				OVERFLOW	70.0	964.	.0012	7.5	5.0	.055	20.00	0	
1295	295	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
295	1296	10	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0	
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW													
		.0	.0	8.3	.5	17.8	1.0	28.1	10.5	39.4	18.2	52.5	23.5
1296	296	68.3	278.0	86.7	1321.5	107.1	5035.0	150.0	10000.0	.0	.0	10.00	0
296	1382	0	3		.0	1.	.0010	.0	.0	.001	10.00	1383	
					.0	1.	.0010	.0	.0	.001	10.00	1383	
DIVERSION TO GUTTER NUMBER1383 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	24.0	.1	278.0	250.0	1321.0	1290.0	5035.0	5000.0	10000.0	9964.0
1382	1381	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
384	1820	0	5	PIPE	3.0	4047.	.0176	.0	.0	.020	3.00	0	
				OVERFLOW	1.0	4047.	.0176	20.0	20.0	.020	50.00	0	
1820	383	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1383	1820	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
383	1405	8	3		.0	1.	.0010	.0	.0	.001	10.00	1360	
DIVERSION TO GUTTER NUMBER1360 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	150.0	1.0	223.0	23.0	285.0	75.0	426.0	201.0	1592.0	1342.0
1405	3953.0	3653.0	10000.0	9680.0									
1381	1381	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
382	382	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
382	381	0	5	PIPE	7.5	1142.	.0020	.0	.0	.015	7.50	0	
				OVERFLOW	7.5	1142.	.0020	20.0	20.0	.015	50.00	0	
381	1926	4	3		.0	1.	.0010	.0	.0	.001	10.00	1366	
DIVERSION TO GUTTER NUMBER1366 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	150.0	1.0	342.0	182.0	2438.0	2050.0				
369	1821	0	4	CHANNEL	.5	1030.	.0089	12.0	12.0	.016	.50	0	
				OVERFLOW	10.0	1030.	.0089	20.0	20.0	.020	10.00	0	
1926	1821	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1821	380	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
380	379	0	1	CHANNEL	8.0	754.	.0040	1.5	1.5	.050	10.00	0	
379	1406	4	3		.0	1.	.0010	.0	.0	.001	10.00	1367	
DIVERSION TO GUTTER NUMBER1367 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	180.0	.1	629.0	354.0	3656.0	3293.0				
1406	1378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1404	1378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1378	378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
378	1925	5	3		.0	1.	.0010	.0	.0	.001	10.00	1289	
DIVERSION TO GUTTER NUMBER1289 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	90.0	1.0	95.0	5.0	363.0	253.0	528.0	390.0		
1925	377	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
377	242	0	1	CHANNEL	8.0	2090.	.0040	1.5	1.5	.055	10.00	0	
1715	1716	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1716	1517	0	4	CHANNEL	10.0	3321.	.0032	8.0	8.0	.035	.50	0	
				OVERFLOW	30.0	3321.	.0032	80.0	80.0	.035	15.00	0	
1515	1517	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1517	1522	0	4	CHANNEL	4.0	851.	.0035	8.0	8.0	.035	.50	0	
				OVERFLOW	20.0	851.	.0035	60.0	60.0	.035	15.00	0	
1541	1542	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1542	1544	0	4	CHANNEL	5.0	10122.	.0260	4.0	4.0	.040	2.00	0	
				OVERFLOW	30.0	10122.	.0260	80.0	80.0	.045	15.00	0	
1520	1521	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1525	1526	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1528	1428	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1428	1429	0	4	CHANNEL	4.0	1682.	.0131	2.0	2.0	.025	2.00	0	
				OVERFLOW	400.0	1682.	.0131	40.0	40.0	.035	15.00	0	
1415	1416	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1550	1551	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1560	1561	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1561	1563	0	4	CHANNEL	3.0	2480.	.1940	4.0	4.0	.050	2.00	0	
				OVERFLOW	25.0	2480.	.1940	50.0	50.0	.055	15.00	0	
1565	1566	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1566	1563	0	4	CHANNEL	3.0	2240.	.2140	4.0	4.0	.050	2.00	0	
				OVERFLOW	25.0	2240.	.2140	6.0	6.0	.055	15.00	0	
1563	1551	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	

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1551	1553	0	4	CHANNEL	3.0	8900.	.0560	5.0	5.0	.040	2.00	0
				OVERFLOW	30.0	8900.	.0560	50.0	50.0	.045	10.00	0
1570	1571	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1571	1557	0	1	CHANNEL	5.0	1200.	.2670	40.0	40.0	.055	10.00	0
1556	1557	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1557	1553	0	4	CHANNEL	3.0	5620.	.0240	5.0	5.0	.040	2.00	0
				OVERFLOW	25.0	5620.	.0240	40.0	40.0	.045	15.00	0
1553	1416	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1416	1429	0	4	CHANNEL	5.0	4085.	.0225	4.0	4.0	.050	2.00	0
				OVERFLOW	25.0	4085.	.0225	40.0	40.0	.055	15.00	0
1429	1526	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1526	1532	0	4	CHANNEL	2.0	1410.	.0136	2.0	2.0	.055	2.00	0
				OVERFLOW	400.0	1410.	.0136	40.0	40.0	.065	15.00	0
1530	1531	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1545	1546	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1575	1576	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1576	1546	0	4	CHANNEL	2.0	3500.	.0229	5.0	5.0	.050	2.00	0
				OVERFLOW	30.0	3500.	.0229	50.0	50.0	.055	15.00	0
1546	1531	0	4	CHANNEL	5.0	7763.	.0840	4.0	4.0	.050	2.00	0
				OVERFLOW	30.0	7763.	.0840	75.0	75.0	.055	15.00	0
1531	1532	0	4	CHANNEL	5.0	5288.	.0872	4.0	4.0	.040	2.00	0
				OVERFLOW	30.0	5288.	.0872	80.0	80.0	.045	15.00	0
1532	1537	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1537	1533	0	4	CHANNEL	2.0	1127.	.0035	2.0	2.0	.035	2.00	0
				OVERFLOW	400.0	1127.	.0035	5.0	40.0	.035	15.00	0
1414	1534	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1534	1533	0	4	CHANNEL	10.0	1966.	.0080	5.0	5.0	.050	1.00	0
				OVERFLOW	400.0	1966.	.0080	50.0	3.0	.065	15.00	0
1533	1521	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1521	1544	0	4	CHANNEL	4.0	2633.	.0093	2.0	2.0	.050	2.00	0
				OVERFLOW	500.0	2633.	.0093	25.0	25.0	.065	10.00	0
1544	1548	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1548	1522	0	4	CHANNEL	4.0	1054.	.0038	8.0	8.0	.035	.50	0
				OVERFLOW	500.0	1054.	.0038	60.0	60.0	.035	15.00	0
1522	1511	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1510	1511	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1511	1513	0	4	CHANNEL	4.0	3213.	.0057	2.0	2.0	.050	2.00	0
				OVERFLOW	512.0	3213.	.0057	50.0	50.0	.060	10.00	0
1513	1514	8	3		.0	1.	.0010	.0	.0	.001	10.00	1508
DIVERSION TO GUTTER NUMBER1508 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	50.0	.1	140.0	48.0	415.0	192.0	1791.0	1299.0	3930.0 3176.0
1514	1442	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1442	1935	0	4	CHANNEL	2.0	2252.	.0097	4.0	4.0	.040	1.00	0
				OVERFLOW	300.0	2252.	.0097	80.0	80.0	.060	15.00	0
1262	1916	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1916	1935	0	4	CHANNEL	2.0	1211.	.0046	5.0	3.0	.035	1.00	0
				OVERFLOW	400.0	1211.	.0046	100.0	3.0	.035	20.00	0
1935	262	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
262	263	0	4	CHANNEL	2.0	529.	.0058	5.0	3.0	.035	1.00	0
				OVERFLOW	500.0	529.	.0058	150.0	3.0	.035	20.00	0
263	1905	8	3		.0	1.	.0010	.0	.0	.001	10.00	266
DIVERSION TO GUTTER NUMBER 266 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	175.0	174.9	412.0	185.0	908.0	198.0	1902.0	212.0	3161.0 228.0
1905	264	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
264	265	0	4	CHANNEL	2.0	1138.	.0017	5.0	3.0	.035	.50	0
				OVERFLOW	600.0	1138.	.0017	150.0	3.0	.035	20.00	0
265	269	8	3		.0	1.	.0010	.0	.0	.001	10.00	1267
DIVERSION TO GUTTER NUMBER1267 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	170.0	169.9	227.0	195.0	710.0	516.0	1689.0	1249.0	2933.0 1956.0
269	1294	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1294	294	0	4	CHANNEL	2.0	1043.	.0027	4.0	4.0	.025	1.00	0
				OVERFLOW	375.0	1043.	.0027	80.0	3.0	.035	15.00	0
304	294	0	1	CHANNEL	8.0	2370.	.0060	5.0	5.0	.035	10.00	0
299	303	0	4	CHANNEL	.5	3612.	.0400	12.0	12.0	.016	.50	0
				OVERFLOW	24.0	3612.	.0400	20.0	20.0	.020	10.00	0
301	300	0	4	CHANNEL	.5	3743.	.0800	12.0	12.0	.016	.50	0
				OVERFLOW	24.0	3743.	.0800	20.0	20.0	.020	10.00	0
300	1922	5	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	5.4	10.0	28.7	11.0	36.6	32.0	39.3	468.0	
1922	303	0	4	CHANNEL	.5	899.	.0667	12.0	12.0	.016	.50	0
				OVERFLOW	10.0	899.	.0667	20.0	20.0	.020	10.00	0
303	298	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
298	297	11	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	.1	15.0	.5	45.0	1.4	94.0	2.9	130.0	5.3 158.0
		9.3	182.0	12.2	192.0	15.9	225.0	20.4	286.0	25.0	827.0	
297	1921	0	4	CHANNEL	6.0	5106.	.0250	3.0	3.0	.045	6.00	0
				OVERFLOW	50.0	6800.	.0188	3.0	3.0	.035	10.00	0
1917	1921	0	4	CHANNEL	5.0	1894.	.0079	8.0	8.0	.035	1.00	0
				OVERFLOW	40.0	1894.	.0079	80.0	80.0	.035	15.00	0
1921	1920	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1920	294	0	4	CHANNEL	18.0	785.	.0013	6.0	6.0	.035	6.00	0
				OVERFLOW	100.0	785.	.0013	12.0	12.0	.035	15.00	0
294	280	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
280	1293	6	3		.0	1.	.0010	.0	.0	.001	10.00	1295
DIVERSION TO GUTTER NUMBER1295 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	295.0	1.0	370.0	42.0	1046.0	661.0	2827.0	2327.0	8734.0 8169.0
1293	293	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
293	267	0	5	PIPE	8.5	757.	.0020	.0	.0	.015	8.50	0
				OVERFLOW	8.5	757.	.0020	.0	.0	.015	20.00	0
1267	267	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
267	268	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
268	1291	8	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	1.4	81.0	5.0	267.0	10.4	465.0	16.9	632.0	25.0 1145.0
		35.1	1888.0	140.0	10000.0							
1291	291	0	3		.0	1.	.0010	.0	.0	.001	10.00	0

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291	1290	6	3	NUMBER1923	- TOTAL Q VS	1.	.0010	.0	.0	.001	10.00	1923	
		DIVERSION TO GUTTER		NUMBER1923 - TOTAL Q VS		DIVERTED Q IN CFS							
1290	290	.0	.0	515.0	1.0	1249.0	471.0	1956.0	1098.0	6585.0	5685.0	10000.0	9000.0
1290	290	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1290	290	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1290	290	0	4	CHANNEL		30.0	1375.	.0017	4.0	4.0	.045	6.00	0
				OVERFLOW		100.0	1375.	.0017	20.0	20.0	.050	15.00	0
1289	1924	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1924	289	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
289	242	0	4	CHANNEL		30.0	1962.	.0017	4.0	4.0	.045	6.00	0
				OVERFLOW		100.0	1962.	.0017	20.0	20.0	.050	15.00	0
1505	1506	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1410	1411	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1420	1421	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1435	1436	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1436	1438	0	4	CHANNEL		2.0	3730.	.0350	4.0	4.0	.050	3.00	0
				OVERFLOW		30.0	3730.	.0350	16.0	16.0	.055	15.00	0
1430	1431	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1431	1438	0	4	CHANNEL		2.0	1670.	.0820	4.0	4.0	.040	1.00	0
				OVERFLOW		12.0	1670.	.0820	15.0	15.0	.045	15.00	0
1438	1426	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1425	1426	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1426	1421	0	4	CHANNEL		5.0	2319.	.0190	8.0	8.0	.040	2.00	0
				OVERFLOW		40.0	2319.	.0190	75.0	75.0	.045	15.00	0
1445	1446	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1446	1453	0	4	CHANNEL		2.0	6667.	.0606	3.0	3.0	.040	3.00	0
				OVERFLOW		25.0	6667.	.0606	6.0	6.0	.045	15.00	0
1645	1646	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1646	1643	0	4	CHANNEL		5.0	5300.	.1450	4.0	4.0	.060	2.00	0
				OVERFLOW		25.0	5300.	.1450	15.0	15.0	.065	15.00	0
1640	1641	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1641	1643	0	4	CHANNEL		2.0	5800.	.0160	3.0	3.0	.060	3.00	0
				OVERFLOW		25.0	5800.	.0160	8.0	8.0	.065	15.00	0
1643	1631	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1630	1631	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1631	1629	0	4	CHANNEL		10.0	7611.	.0730	4.0	4.0	.040	3.00	0
				OVERFLOW		40.0	7611.	.0730	10.0	10.0	.045	15.00	0
1625	1626	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1635	1636	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1636	1626	0	1	CHANNEL		2.0	4200.	.0840	8.0	8.0	.040	10.00	0
1626	1628	0	4	CHANNEL		25.0	1908.	.0205	4.0	4.0	.070	2.00	0
				OVERFLOW		100.0	1908.	.0205	75.0	75.0	.075	15.00	0
1628	1611	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1610	1611	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1611	1928	0	4	CHANNEL		30.0	4400.	.0290	4.0	4.0	.060	2.50	0
				OVERFLOW		150.0	4400.	.0290	75.0	75.0	.070	15.00	0
1605	1606	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1665	1666	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1666	1606	0	4	CHANNEL		3.0	6900.	.2130	3.0	3.0	.050	2.00	0
				OVERFLOW		20.0	6900.	.2130	2.0	2.0	.055	10.00	0
1606	1928	0	4	CHANNEL		5.0	5987.	.0812	4.0	4.0	.045	2.00	0
				OVERFLOW		25.0	5987.	.0812	3.0	3.0	.060	15.00	0
1928	1601	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1600	1601	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1601	1603	0	4	CHANNEL		25.0	1264.	.0290	6.0	6.0	.060	2.50	0
				OVERFLOW		85.0	1264.	.0290	80.0	80.0	.070	15.00	0
1710	1711	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1711	1712	0	4	CHANNEL		5.0	5430.	.0479	4.0	4.0	.035	1.00	0
				OVERFLOW		30.0	5430.	.0479	5.0	5.0	.035	15.00	0
1615	1616	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1616	1623	0	4	CHANNEL		2.0	6409.	.0620	3.0	3.0	.040	3.00	0
				OVERFLOW		20.0	6409.	.0620	5.0	5.0	.045	15.00	0
1660	1661	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1661	1651	0	4	CHANNEL		3.0	9600.	.1670	4.0	4.0	.060	3.00	0
				OVERFLOW		25.0	9600.	.1670	3.0	3.0	.065	15.00	0
1650	1651	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1651	1653	0	4	CHANNEL		5.0	4100.	.0860	4.0	4.0	.050	3.00	0
				OVERFLOW		25.0	4100.	.0860	3.0	3.0	.055	15.00	0
1655	1656	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1656	1653	0	4	CHANNEL		3.0	10800.	.1170	4.0	4.0	.050	3.00	0
				OVERFLOW		25.0	10800.	.1170	3.0	3.0	.055	15.00	0
1653	1621	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1620	1621	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1621	1623	0	4	CHANNEL		5.0	10100.	.0320	5.0	5.0	.045	3.00	0
				OVERFLOW		35.0	10100.	.0320	2.0	2.0	.060	15.00	0
1623	1624	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1705	1624	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1624	1712	0	4	CHANNEL		2.0	2490.	.0390	5.0	5.0	.050	2.00	0
				OVERFLOW		25.0	2490.	.0390	5.0	5.0	.050	10.00	0
1712	1929	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1929	1603	0	4	CHANNEL		10.0	1172.	.0043	10.0	10.0	.035	.50	0
				OVERFLOW		20.0	1172.	.0043	40.0	40.0	.035	15.00	0
1603	1451	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1450	1451	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1451	1453	0	4	CHANNEL		30.0	2963.	.0110	6.0	6.0	.060	2.50	0
				OVERFLOW		110.0	2963.	.0110	80.0	80.0	.070	15.00	0
1453	1441	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1440	1441	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1441	1421	0	4	CHANNEL		30.0	3235.	.0078	4.0	4.0	.060	2.50	0
				OVERFLOW		110.0	3235.	.0078	75.0	75.0	.070	15.00	0
1421	1423	0	4	CHANNEL		30.0	800.	.0120	4.0	4.0	.060	2.50	0
				OVERFLOW		120.0	800.	.0120	75.0	75.0	.090	15.00	0
1423	1424	8	3			.0	1.	.0010	.0	.0	.001	10.00	1528
		DIVERSION TO GUTTER		NUMBER1528 - TOTAL Q VS		DIVERTED Q IN CFS							
1424	1411	.0	.0	1000.0	1.0	2000.0	114.0	3100.0	335.0	4000.0	597.0	5683.0	1262.0
1411	1412	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
				CHANNEL		30.0	3369.	.0084	4.0	4.0	.060	2.50	0
				OVERFLOW		160.0	3369.	.0084	75.0	75.0	.065	15.00	0
1412	1413	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1413	1509	9	3			.0	1.	.0010	.0	.0	.001	10.00	1414
		DIVERSION TO GUTTER		NUMBER1414 - TOTAL Q VS		DIVERTED Q IN CFS							

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		.0	.0	500.0	1.0	999.0	125.0	1886.0	841.0	2765.0	1456.0	3403.0	1937.0		
		4421.0	2668.0	7425.0	5187.0	13357.0	10368.0								
1509	1800	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1490	1491	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1455	1456	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1938	1480	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1480	1481	0	4			.0	1.0	.0010	.0	.0	.001	10.00	0		
				CHANNEL		5.0	2400.0	.0500	2.0	2.0	.040	2.00	0		
				OVERFLOW		20.0	2400.0	.0500	10.0	10.0	.045	10.00	0		
1481	1482	7	2	PIPE		.0	1.0	.0010	.0	.0	.030	.10	0		
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW															
		.0	.0	308.0	18.0	624.0	76.0	947.0	179.0	1279.0	318.0	1618.0	1676.0		
		1965.0	4700.0												
1482	1456	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1456	1457	0	1	CHANNEL		2.0	4450.0	.0363	80.0	80.0	.030	20.00	0		
1457	1491	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1491	1931	0	4	CHANNEL		5.0	10236.0	.0090	4.0	4.0	.050	2.00	0		
				OVERFLOW		25.0	10236.0	.0090	60.0	60.0	.065	15.00	0		
1460	1461	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1461	1931	0	4	CHANNEL		3.0	2286.0	.0280	4.0	4.0	.050	2.00	0		
				OVERFLOW		20.0	2286.0	.0280	24.0	24.0	.055	15.00	0		
1931	1933	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1933	1467	0	4	CHANNEL		5.0	403.0	.0099	2.0	2.0	.020	2.00	0		
				OVERFLOW		25.0	403.0	.0099	10.0	10.0	.025	15.00	0		
1465	1932	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1932	1467	0	4	CHANNEL		4.0	1591.0	.0289	8.0	8.0	.035	.50	0		
				OVERFLOW		25.0	1591.0	.0289	4.0	4.0	.035	15.00	0		
1467	1468	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1468	1800	0	4	CHANNEL		5.0	2357.0	.0180	2.0	2.0	.020	2.00	0		
				OVERFLOW		25.0	2357.0	.0180	10.0	10.0	.025	15.00	0		
1800	1506	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1506	1507	0	4	CHANNEL		33.0	8099.0	.0054	4.0	4.0	.060	2.50	0		
				OVERFLOW		800.0	8099.0	.0054	10.0	10.0	.065	15.00	0		
1508	1507	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1507	1512	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1512	44	0	4	CHANNEL		33.0	1367.0	.0064	4.0	4.0	.060	2.50	0		
				OVERFLOW		308.0	1367.0	.0064	80.0	80.0	.065	15.00	0		
1500	1501	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1501	44	0	4	CHANNEL		5.0	8609.0	.0212	2.0	2.0	.040	2.00	0		
				OVERFLOW		20.0	8609.0	.0212	10.0	10.0	.045	15.00	0		
44	261	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
261	1427	9	3			.0	1.0	.0010	.0	.0	.001	10.00	1262		
DIVERSION TO GUTTER NUMBER1262 - TOTAL Q VS DIVERTED Q IN CFS															
		.0	.0	500.0	1.0	875.0	35.0	1920.0	315.0	2709.0	660.0	3916.0	1323.3		
		5586.0	2377.0	9768.0	5344.0	18394.0	11928.0								
1427	243	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
243	242	0	4	CHANNEL		65.0	2991.0	.0112	2.0	2.0	.043	2.50	0		
				OVERFLOW		650.0	2991.0	.0112	100.0	100.0	.055	15.00	0		
242	241	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
241	240	0	4	CHANNEL		65.0	5732.0	.0100	2.0	2.0	.043	3.00	0		
				OVERFLOW		1200.0	5732.0	.0100	200.0	200.0	.055	20.00	0		
240	238	0	4	CHANNEL		65.0	2861.0	.0100	2.0	2.0	.050	3.00	0		
				OVERFLOW		1200.0	2861.0	.0100	200.0	200.0	.075	20.00	0		
238	237	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
237	251	5	3			.0	1.0	.0010	.0	.0	.001	10.00	389		
DIVERSION TO GUTTER NUMBER389 - TOTAL Q VS DIVERTED Q IN CFS															
		.0	.0	2060.0	1.0	4980.0	2580.0	6630.0	3530.0	11150.0	7500.0				
		389	1906	0	3	.0	1.0	.0010	.0	.0	.001	10.00	0		
1906	1909	0	4	CHANNEL		10.0	3340.0	.0042	8.0	8.0	.025	.50	0		
				OVERFLOW		1200.0	3340.0	.0042	80.0	80.0	.025	15.00	0		
251	233	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
235	239	0	1	CHANNEL		1.0	3509.0	.0050	50.0	50.0	.020	10.00	0		
239	234	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
234	232	0	4	CHANNEL		2.0	2072.0	.0044	3.0	3.0	.050	2.00	0		
				OVERFLOW		50.0	2072.0	.0044	50.0	50.0	.035	10.00	0		
233	232	0	4	CHANNEL		65.0	3076.0	.0100	2.0	2.0	.050	4.00	0		
				OVERFLOW		600.0	3076.0	.0100	200.0	200.0	.080	20.00	0		
232	236	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
236	252	5	3			.0	1.0	.0010	.0	.0	.001	10.00	1403		
DIVERSION TO GUTTER NUMBER1403 - TOTAL Q VS DIVERTED Q IN CFS															
		.0	.0	2060.0	1.0	2400.0	100.0	3100.0	500.0	10000.0	2500.0				
1403	1599	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
252	231	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1357	357	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
357	1401	6	3			.0	1.0	.0010	.0	.0	.001	10.00	1325		
DIVERSION TO GUTTER NUMBER1325 - TOTAL Q VS DIVERTED Q IN CFS															
		.0	.0	26.0	.1	263.0	235.0	391.0	361.0	995.0	960.0	5000.0	4950.0		
1401	1387	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1387	387	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
387	1908	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1908	1320	0	4	CHANNEL		2.0	1718.0	.0076	3.0	3.0	.025	2.00	0		
				OVERFLOW		600.0	1718.0	.0076	80.0	80.0	.025	10.00	0		
266	376	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
376	375	0	1	CHANNEL		4.0	1569.0	.0041	4.0	4.0	.050	10.00	0		
375	1374	4	3			.0	1.0	.0010	.0	.0	.001	10.00	1404		
DIVERSION TO GUTTER NUMBER1404 - TOTAL Q VS DIVERTED Q IN CFS															
		.0	.0	24.0	.1	135.0	100.0	540.0	500.0						
1374	374	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
374	372	0	4	CHANNEL		4.0	2538.0	.0115	3.0	3.0	.045	2.00	0		
				OVERFLOW		20.0	2538.0	.0115	20.0	20.0	.035	10.00	0		
373	372	0	4	CHANNEL		3.0	1779.0	.0075	4.0	4.0	.045	1.00	0		
				OVERFLOW		20.0	1779.0	.0075	20.0	20.0	.035	10.00	0		
1367	367	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
367	372	0	4	CHANNEL		.5	2663.0	.0103	12.0	12.0	.016	.50	0		
				OVERFLOW		10.0	2663.0	.0103	20.0	20.0	.020	10.00	0		
372	371	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
371	311	0	4	CHANNEL		10.0	2893.0	.0078	2.0	2.0	.045	1.00	0		
				OVERFLOW		10.0	2893.0	.0078	50.0	50.0	.035	10.00	0		
1339	1822	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
1348	348	0	3			.0	1.0	.0010	.0	.0	.001	10.00	0		
348	1937	5	3			.0	1.0	.0010	.0	.0	.001	10.00	1331		
DIVERSION TO GUTTER NUMBER1331 - TOTAL Q VS DIVERTED Q IN CFS															

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1937	1386	.0	.0	31.0	30.0	542.0	335.0	795.0	466.0	1394.0	766.0			
385	1386	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
1386	386	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
386	395	6	3			.0	1.	.0010	.0	.0	.001	10.00	1407	
DIVERSION TO GUTTER NUMBER1407 - TOTAL Q VS DIVERTED Q IN CFS														
395	394	.0	.0	206.0	1.0	394.0	64.0	902.0	273.0	2616.0	572.0	5000.0	1100.0	
394	1822	0	4	CHANNEL		.5	1000.	.0061	12.0	12.0	.016	.50	0	
				OVERFLOW		10.0	1000.	.0061	20.0	20.0	.020	10.00	0	
1822	339	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
339	1313	4	3			.0	1.	.0010	.0	.0	.001	10.00	1336	
DIVERSION TO GUTTER NUMBER1336 - TOTAL Q VS DIVERTED Q IN CFS														
1313	1939	.0	.0	30.0	20.0	300.0	200.0	3000.0	2000.0					
1362	362	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
363	362	0	1	CHANNEL		1.0	4078.	.0121	20.0	5.0	.020	10.00	0	
362	398	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
398	1396	10	2	PIPE		.1	1.	.0010	.0	.0	.030	.10	0	
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW														
		.0	.0	.4	26.0	1.3	138.0	2.1	200.0	2.4	260.0	2.8	360.0	
		3.4	510.0	4.0	893.0	5.0	1809.0	15.0	10000.0					
1396	396	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
396	308	7	3			.0	1.	.0010	.0	.0	.001	10.00	385	
DIVERSION TO GUTTER NUMBER 385 - TOTAL Q VS DIVERTED Q IN CFS														
		.0	.0	260.0	.1	360.0	60.0	510.0	190.0	893.0	545.0	1909.0	1388.0	
		10000.0	9550.0											
308	314	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
314	1939	0	1	CHANNEL		8.0	600.	.0048	.1	2.0	.050	15.00	0	
1939	313	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
313	1910	6	3			.0	1.	.0010	.0	.0	.001	10.00	1409	
DIVERSION TO GUTTER NUMBER1409 - TOTAL Q VS DIVERTED Q IN CFS														
1910	1940	.0	.0	260.0	.1	389.0	129.0	470.0	195.0	648.0	358.0	10000.0	9500.0	
1366	366	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
366	344	0	4	CHANNEL		.5	5533.	.0079	12.0	12.0	.016	.50	0	
				OVERFLOW		10.0	5533.	.0079	20.0	20.0	.020	10.00	0	
344	1408	4	3			.0	1.	.0010	.0	.0	.001	10.00	1339	
DIVERSION TO GUTTER NUMBER1339 - TOTAL Q VS DIVERTED Q IN CFS														
1408	1940	.0	.0	25.0	.1	50.0	25.0	2000.0	35.0					
1940	312	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
312	311	0	1	CHANNEL		8.0	1520.	.0068	2.0	2.0	.050	10.00	0	
311	358	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
358	393	0	4	CHANNEL		8.0	2401.	.0100	1.5	1.5	.030	4.50	0	
				OVERFLOW		20.0	2401.	.0100	50.0	50.0	.020	10.00	0	
393	1357	8	3			.0	1.	.0010	.0	.0	.001	10.00	1393	
DIVERSION TO GUTTER NUMBER1393 - TOTAL Q VS DIVERTED Q IN CFS														
		.0	.0	240.0	1.0	588.0	79.0	874.0	150.0	1822.0	391.0	2281.0	509.0	
		3048.0	704.0	4515.0	1075.0									
1393	1941	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
1941	392	0	4	CHANNEL		4.0	423.	.0142	4.0	4.0	.030	.50	0	
				OVERFLOW		30.0	423.	.0142	12.0	12.0	.032	15.00	0	
1325	325	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
1331	331	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
1407	331	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
331	337	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
337	328	0	4	CHANNEL		.5	2862.	.0066	12.0	12.0	.016	.50	0	
				OVERFLOW		10.0	2862.	.0066	20.0	20.0	.020	10.00	0	
1329	328	0	4	CHANNEL		.5	2288.	.0088	12.0	12.0	.016	.50	0	
				OVERFLOW		10.0	2288.	.0088	20.0	20.0	.020	10.00	0	
1340	340	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
340	1333	6	3			.0	1.	.0010	.0	.0	.001	10.00	1348	
DIVERSION TO GUTTER NUMBER1348 - TOTAL Q VS DIVERTED Q IN CFS														
		.0	.0	66.0	31.0	833.0	542.0	1194.0	795.0	2037.0	1394.0	3730.0	2560.0	
1333	333	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
333	332	0	1	CHANNEL		1.0	2969.	.0047	50.0	5.0	.020	20.00	0	
341	1334	6	3			.0	1.	.0010	.0	.0	.001	10.00	1340	
DIVERSION TO GUTTER NUMBER1340 - TOTAL Q VS DIVERTED Q IN CFS														
		.0	.0	71.0	66.0	1120.0	833.0	1616.0	1194.0	2776.0	2037.0	5110.0	3730.0	
1334	334	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
334	332	0	1	CHANNEL		1.0	2967.	.0047	5.0	50.0	.020	20.00	0	
332	1308	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
1308	1307	4	3			.0	1.	.0010	.0	.0	.001	10.00	1306	
DIVERSION TO GUTTER NUMBER1306 - TOTAL Q VS DIVERTED Q IN CFS														
		.0	.0	56.2	56.1	1080.0	60.5	2500.0	65.0					
1307	1305	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
1306	330	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
346	345	0	4	CHANNEL		.5	1855.	.0179	12.0	12.0	.016	.50	0	
				OVERFLOW		10.0	1855.	.0179	20.0	20.0	.020	10.00	0	
345	359	0	4	CHANNEL		.5	3689.	.0097	12.0	12.0	.016	.50	0	
				OVERFLOW		10.0	3689.	.0097	20.0	20.0	.020	10.00	0	
350	1915	0	5	PIPE		2.0	2980.	.0074	.0	.0	.015	2.00	0	
				OVERFLOW		1.0	2980.	.0074	20.0	20.0	.020	20.00	0	
1360	360	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
1923	292	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
292	360	0	4	CHANNEL		1.0	1500.	.0027	50.0	50.0	.020	1.00	0	
				OVERFLOW		15.0	1500.	.0027	4.0	4.0	.020	10.00	0	
360	1934	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
1934	1919	0	4	CHANNEL		1.0	1500.	.0027	50.0	50.0	.020	1.00	0	
				OVERFLOW		15.0	1500.	.0027	4.0	4.0	.020	10.00	0	
353	1919	0	4	CHANNEL		.5	1591.	.0037	12.0	12.0	.016	.50	0	
				OVERFLOW		10.0	1591.	.0037	20.0	20.0	.020	10.00	0	
1919	352	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
352	1812	7	2	PIPE		.1	1.	.0010	.0	.0	.030	.10	0	
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW														
		.0	.0	.7	20.0	2.2	31.0	5.8	39.0	12.8	300.0	23.3	3986.0	
		50.0	10000.0											
1812	1813	0	3			.0	1.	.0010	.0	.0	.001	10.00	0	
1813	1814	7	3			.0	1.	.0010	.0	.0	.001	10.00	1815	
DIVERSION TO GUTTER NUMBER1815 - TOTAL Q VS DIVERTED Q IN CFS														

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1911	1912	0	3	OVERFLOW	10.0	2821.	.0012	20.0	20.0	.035	10.00			
1912	390	0	4	CHANNEL	.0	1.	.0010	.0	.0	.001	10.00	0		
				OVERFLOW	15.0	1048.	.0012	3.5	3.5	.045	4.00	0		
390	1238	7	3	OVERFLOW	70.0	1048.	.0012	7.5	5.0	.055	20.00			
					.0	1.	.0010	.0	.0	.001	10.00	388		
DIVERSION TO GUTTER NUMBER 388 - TOTAL Q VS DIVERTED Q IN CFS														
		.0	.0		200.0	1.0	205.0	5.0	274.0	73.0	431.0	229.0	726.0	523.0
		5000.0	4795.0											
388	1907	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1907	1320	0	4	CHANNEL	4.0	2175.	.0064	3.0	3.0	.025	2.00	0		
				OVERFLOW	300.0	2175.	.0064	80.0	80.0	.025	15.00	0		
1320	320	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
320	1909	0	4	CHANNEL	6.0	1412.	.0087	3.0	3.0	.035	2.00	0		
				OVERFLOW	700.0	1412.	.0087	100.0	100.0	.035	10.00	0		
1909	322	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1322	321	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
321	1337	0	1	CHANNEL	10.0	1092.	.0080	50.0	50.0	.045	15.00	0		
1337	1338	3	3		.0	1.	.0010	.0	.0	.001	10.00	1363		
DIVERSION TO GUTTER NUMBER 1363 - TOTAL Q VS DIVERTED Q IN CFS														
		.0	.0		10.0	.1	3500.0	1910.4						
1338	1361	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1361	1320	0	5	PIPE	1.5	823.	.0100	.0	.0	.025	1.50	0		
				OVERFLOW	50.0	823.	.0100	20.0	20.0	.045	15.00	0		
361	1364	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1363	1364	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1364	1365	0	5	PIPE	1.5	1547.	.0078	.0	.0	.025	1.50	0		
				OVERFLOW	10.0	1547.	.0078	50.0	50.0	.045	20.00	0		
1365	1944	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
370	1944	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1944	1945	0	5	PIPE	4.5	1283.	.0109	.0	.0	.025	4.50	0		
				OVERFLOW	10.0	1283.	.0109	50.0	50.0	.035	20.00	0		
1945	1373	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1373	1375	3	3		.0	1.	.0010	.0	.0	.001	10.00	1377		
DIVERSION TO GUTTER NUMBER 1377 - TOTAL Q VS DIVERTED Q IN CFS														
		.0	.0		195.7	.1	5200.0	3985.2						
1377	1372	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1375	1376	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1376	1946	0	4	CHANNEL	8.0	750.	.0100	3.0	3.0	.045	6.00	0		
				OVERFLOW	50.0	750.	.0100	20.0	20.0	.050	5.00	0		
322	1943	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1943	1946	0	4	CHANNEL	20.0	1443.	.0083	4.0	4.0	.045	6.00	0		
				OVERFLOW	400.0	1443.	.0083	50.0	50.0	.060	10.00	0		
1946	319	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
319	271	0	4	CHANNEL	30.0	4190.	.0086	4.0	4.0	.065	7.00	0		
				OVERFLOW	500.0	4190.	.0086	50.0	50.0	.060	10.00	0		
231	271	0	4	CHANNEL	130.0	5118.	.0074	4.0	4.0	.055	8.00	0		
				OVERFLOW	600.0	5118.	.0074	50.0	50.0	.050	20.00	0		
271	270	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
270	399	0	4	CHANNEL	70.0	2605.	.0074	3.0	3.0	.055	8.00	0		
				OVERFLOW	700.0	2605.	.0074	100.0	100.0	.040	20.00	0		
399	1599	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1599	1947	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		
1947	0	0	3		.0	1.	.0010	.0	.0	.001	10.00	0		

OTOTAL NUMBER OF GUTTERS/PIPES, 610

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model sbc_1td
50-year model

ARRANGEMENT OF SUBCATCHMENTS AND GUTTERS/PIPES

GUTTER	TRIBUTARY GUTTER/PIPE										TRIBUTARY SUBAREA										D.A. (AC)	
1	2	5	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	64741.0
2	3	4	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0	0	0	2408.0
3	0	0	0	0	0	0	0	0	0	0	3	0	0	0	0	0	0	0	0	0	0	929.0
4	0	0	0	0	0	0	0	0	0	0	4	0	0	0	0	0	0	0	0	0	0	960.0
5	7	6	13	0	0	0	0	0	0	0	5	0	0	0	0	0	0	0	0	0	0	61766.0
6	397	0	0	0	0	0	0	0	0	0	6	0	0	0	0	0	0	0	0	0	0	59943.0
7	9	10	0	0	0	0	0	0	0	0	7	0	0	0	0	0	0	0	0	0	0	986.0
8	15	22	0	0	0	0	0	0	0	0	8	0	0	0	0	0	0	0	0	0	0	59647.0
9	0	0	0	0	0	0	0	0	0	0	9	0	0	0	0	0	0	0	0	0	0	411.0
10	0	0	0	0	0	0	0	0	0	0	10	0	0	0	0	0	0	0	0	0	0	202.0
11	0	0	0	0	0	0	0	0	0	0	11	0	0	0	0	0	0	0	0	0	0	113.0
12	0	0	0	0	0	0	0	0	0	0	12	0	0	0	0	0	0	0	0	0	0	159.0
13	11	12	0	0	0	0	0	0	0	0	13	0	0	0	0	0	0	0	0	0	0	501.0
14	0	0	0	0	0	0	0	0	0	0	14	0	0	0	0	0	0	0	0	0	0	132.0
15	14	16	0	0	0	0	0	0	0	0	15	0	0	0	0	0	0	0	0	0	0	53636.0
16	40	17	0	0	0	0	0	0	0	0	16	0	0	0	0	0	0	0	0	0	0	53468.0
17	18	21	0	0	0	0	0	0	0	0	17	0	0	0	0	0	0	0	0	0	0	1706.0
18	20	0	0	0	0	0	0	0	0	0	18	0	0	0	0	0	0	0	0	0	0	1171.0

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20	0	0	0	0	0	0	0	0	0	0	19	0	0	0	0	0	0	0	0	0	606.0
21	0	0	0	0	0	0	0	0	0	0	20	0	0	0	0	0	0	0	0	0	379.0
22	23	24	0	0	0	0	0	0	0	0	21	0	0	0	0	0	0	0	0	0	4784.0
23	37	34	31	0	0	0	0	0	0	0	22	0	0	0	0	0	0	0	0	0	2671.0
24	25	26	0	0	0	0	0	0	0	0	23	0	0	0	0	0	0	0	0	0	1666.0
25	0	0	0	0	0	0	0	0	0	0	24	0	0	0	0	0	0	0	0	0	363.0
26	27	28	0	0	0	0	0	0	0	0	25	0	0	0	0	0	0	0	0	0	1199.0
27	0	0	0	0	0	0	0	0	0	0	26	0	0	0	0	0	0	0	0	0	107.0
28	29	30	0	0	0	0	0	0	0	0	27	0	0	0	0	0	0	0	0	0	998.0
29	0	0	0	0	0	0	0	0	0	0	28	0	0	0	0	0	0	0	0	0	152.0
30	0	0	0	0	0	0	0	0	0	0	29	0	0	0	0	0	0	0	0	0	546.0
31	32	33	0	0	0	0	0	0	0	0	30	0	0	0	0	0	0	0	0	0	508.0
32	0	0	0	0	0	0	0	0	0	0	31	0	0	0	0	0	0	0	0	0	144.0
33	0	0	0	0	0	0	0	0	0	0	32	0	0	0	0	0	0	0	0	0	257.0
34	35	36	0	0	0	0	0	0	0	0	33	0	0	0	0	0	0	0	0	0	844.0
35	0	0	0	0	0	0	0	0	0	0	34	0	0	0	0	0	0	0	0	0	148.0
36	0	0	0	0	0	0	0	0	0	0	35	0	0	0	0	0	0	0	0	0	251.0
37	38	39	0	0	0	0	0	0	0	0	36	0	0	0	0	0	0	0	0	0	1124.0
38	0	0	0	0	0	0	0	0	0	0	37	0	0	0	0	0	0	0	0	0	368.0
39	0	0	0	0	0	0	0	0	0	0	38	0	0	0	0	0	0	0	0	0	290.0
40	41	42	0	0	0	0	0	0	0	0	39	0	0	0	0	0	0	0	0	0	51645.0
41	0	0	0	0	0	0	0	0	0	0	40	0	0	0	0	0	0	0	0	0	205.0
42	46	62	68	0	0	0	0	0	0	0	41	0	0	0	0	0	0	0	0	0	31084.0
44	1512	1501	0	0	0	0	0	0	0	0	42	0	0	0	0	0	0	0	0	0	40179.0
46	59	60	0	0	0	0	0	0	0	0	69	0	0	0	0	0	0	0	0	0	47929.0
48	50	49	0	0	0	0	0	0	0	0	72	0	0	0	0	0	0	0	0	0	72077.0
49	0	0	0	0	0	0	0	0	0	0	71	0	0	0	0	0	0	0	0	0	220.0
50	51	52	56	0	0	0	0	0	0	0	77	0	0	0	0	0	0	0	0	0	1466.0
51	0	0	0	0	0	0	0	0	0	0	78	79	0	0	0	0	0	0	0	0	362.0
52	244	245	53	0	0	0	0	0	0	0	81	0	0	0	0	0	0	0	0	0	69055.0
53	54	55	0	0	0	0	0	0	0	0	75	0	0	0	0	0	0	0	0	0	536.0
54	0	0	0	0	0	0	0	0	0	0	76	0	0	0	0	0	0	0	0	0	213.0
55	0	0	0	0	0	0	0	0	0	0	77	0	0	0	0	0	0	0	0	0	297.0
56	57	58	0	0	0	0	0	0	0	0	78	79	0	0	0	0	0	0	0	0	1842.0
57	0	0	0	0	0	0	0	0	0	0	80	0	0	0	0	0	0	0	0	0	776.0
58	0	0	0	0	0	0	0	0	0	0	43	0	0	0	0	0	0	0	0	0	220.0
59	74	71	0	0	0	0	0	0	0	0	44	0	0	0	0	0	0	0	0	0	47507.0
60	0	0	0	0	0	0	0	0	0	0	45	0	0	0	0	0	0	0	0	0	225.0
61	63	64	0	0	0	0	0	0	0	0	46	0	0	0	0	0	0	0	0	0	1044.0
62	61	65	0	0	0	0	0	0	0	0	47	0	0	0	0	0	0	0	0	0	2039.0
63	0	0	0	0	0	0	0	0	0	0	48	0	0	0	0	0	0	0	0	0	234.0
64	0	0	0	0	0	0	0	0	0	0	49	0	0	0	0	0	0	0	0	0	258.0
65	66	67	0	0	0	0	0	0	0	0	50	0	0	0	0	0	0	0	0	0	956.0
66	0	0	0	0	0	0	0	0	0	0	51	0	0	0	0	0	0	0	0	0	108.0
67	0	0	0	0	0	0	0	0	0	0	52	0	0	0	0	0	0	0	0	0	636.0
68	69	70	0	0	0	0	0	0	0	0	53	0	0	0	0	0	0	0	0	0	523.0
69	0	0	0	0	0	0	0	0	0	0	54	0	0	0	0	0	0	0	0	0	197.0
70	0	0	0	0	0	0	0	0	0	0	55	0	0	0	0	0	0	0	0	0	246.0
71	72	73	0	0	0	0	0	0	0	0	56	0	0	0	0	0	0	0	0	0	1094.0
72	0	0	0	0	0	0	0	0	0	0	57	0	0	0	0	0	0	0	0	0	197.0
73	0	0	0	0	0	0	0	0	0	0	57	0	0	0	0	0	0	0	0	0	636.0

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74	77	76	94	0	0	0	0	0	0	0	58	0	0	0	0	0	0	0	0	46117.0
75	79	78	0	0	0	0	0	0	0	0	61	0	0	0	0	0	0	0	0	3945.0
76	0	0	0	0	0	0	0	0	0	0	63	0	0	0	0	0	0	0	0	379.0
77	75	88	0	0	0	0	0	0	0	0	65	0	0	0	0	0	0	0	0	4793.0
78	0	0	0	0	0	0	0	0	0	0	66	0	0	0	0	0	0	0	0	256.0
79	80	121	0	0	0	0	0	0	0	0	70	0	0	0	0	0	0	0	0	3627.0
80	92	81	0	0	0	0	0	0	0	0	83	0	0	0	0	0	0	0	0	2669.0
81	87	0	0	0	0	0	0	0	0	0	84	0	0	0	0	0	0	0	0	958.0
82	84	83	0	0	0	0	0	0	0	0	85	0	0	0	0	0	0	0	0	848.0
83	0	0	0	0	0	0	0	0	0	0	86	0	0	0	0	0	0	0	0	197.0
84	85	86	0	0	0	0	0	0	0	0	87	0	0	0	0	0	0	0	0	555.0
85	0	0	0	0	0	0	0	0	0	0	88	0	0	0	0	0	0	0	0	118.0
86	0	0	0	0	0	0	0	0	0	0	89	0	0	0	0	0	0	0	0	331.0
87	0	0	0	0	0	0	0	0	0	0	90	0	0	0	0	0	0	0	0	655.0
88	89	93	0	0	0	0	0	0	0	0	91	0	0	0	0	0	0	0	0	782.0
89	0	0	0	0	0	0	0	0	0	0	228	0	0	0	0	0	0	0	0	319.0
93	0	0	0	0	0	0	0	0	0	0	229	0	0	0	0	0	0	0	0	111.0
94	95	97	0	0	0	0	0	0	0	0	92	0	0	0	0	0	0	0	0	40534.0
95	96	116	0	0	0	0	0	0	0	0	230	0	0	0	0	0	0	0	0	34430.0
96	129	122	0	0	0	0	0	0	0	0	93	0	0	0	0	0	0	0	0	33528.0
97	99	98	0	0	0	0	0	0	0	0	94	0	0	0	0	0	0	0	0	5629.0
98	0	0	0	0	0	0	0	0	0	0	95	0	0	0	0	0	0	0	0	309.0
99	101	100	0	0	0	0	0	0	0	0	96	0	0	0	0	0	0	0	0	4848.0
100	0	0	0	0	0	0	0	0	0	0	97	0	0	0	0	0	0	0	0	458.0
101	102	107	0	0	0	0	0	0	0	0	98	0	0	0	0	0	0	0	0	4335.0
102	106	103	0	0	0	0	0	0	0	0	99	0	0	0	0	0	0	0	0	2382.0
103	104	105	0	0	0	0	0	0	0	0	100	0	0	0	0	0	0	0	0	1795.0
104	119	117	0	0	0	0	0	0	0	0	101	0	0	0	0	0	0	0	0	1302.0
105	0	0	0	0	0	0	0	0	0	0	102	0	0	0	0	0	0	0	0	343.0
106	0	0	0	0	0	0	0	0	0	0	103	0	0	0	0	0	0	0	0	273.0
107	108	109	0	0	0	0	0	0	0	0	104	0	0	0	0	0	0	0	0	1871.0
108	0	0	0	0	0	0	0	0	0	0	105	0	0	0	0	0	0	0	0	202.0
109	110	111	0	0	0	0	0	0	0	0	106	0	0	0	0	0	0	0	0	1563.0
110	112	113	0	0	0	0	0	0	0	0	107	0	0	0	0	0	0	0	0	1148.0
111	0	0	0	0	0	0	0	0	0	0	108	0	0	0	0	0	0	0	0	199.0
112	114	115	0	0	0	0	0	0	0	0	109	0	0	0	0	0	0	0	0	540.0
113	0	0	0	0	0	0	0	0	0	0	110	0	0	0	0	0	0	0	0	209.0
114	0	0	0	0	0	0	0	0	0	0	111	0	0	0	0	0	0	0	0	230.0
115	0	0	0	0	0	0	0	0	0	0	112	0	0	0	0	0	0	0	0	102.0
116	0	0	0	0	0	0	0	0	0	0	113	0	0	0	0	0	0	0	0	702.0
117	0	0	0	0	0	0	0	0	0	0	114	0	0	0	0	0	0	0	0	390.0
118	0	0	0	0	0	0	0	0	0	0	115	0	0	0	0	0	0	0	0	453.0
119	120	118	0	0	0	0	0	0	0	0	116	0	0	0	0	0	0	0	0	707.0
120	0	0	0	0	0	0	0	0	0	0	117	0	0	0	0	0	0	0	0	220.0
121	0	0	0	0	0	0	0	0	0	0	74	0	0	0	0	0	0	0	0	326.0
122	124	123	0	0	0	0	0	0	0	0	118	0	0	0	0	0	0	0	0	2595.0
123	127	128	0	0	0	0	0	0	0	0	119	0	0	0	0	0	0	0	0	1409.0
124	125	126	0	0	0	0	0	0	0	0	120	0	0	0	0	0	0	0	0	705.0
125	0	0	0	0	0	0	0	0	0	0	124	0	0	0	0	0	0	0	0	220.0
126	0	0	0	0	0	0	0	0	0	0	125	0	0	0	0	0	0	0	0	88.0
127	0	0	0	0	0	0	0	0	0	0	126	0	0	0	0	0	0	0	0	548.0

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128	0	0	0	0	0	0	0	0	0	0	127	0	0	0	0	0	0	0	0	0	472.0
129	137	130	0	0	0	0	0	0	0	0	128	0	0	0	0	0	0	0	0	0	30354.0
130	133	131	132	0	0	0	0	0	0	0	129	0	0	0	0	0	0	0	0	0	2081.0
131	0	0	0	0	0	0	0	0	0	0	130	0	0	0	0	0	0	0	0	0	290.0
132	0	0	0	0	0	0	0	0	0	0	131	0	0	0	0	0	0	0	0	0	213.0
133	134	0	0	0	0	0	0	0	0	0	132	0	0	0	0	0	0	0	0	0	1468.0
134	135	136	0	0	0	0	0	0	0	0	133	0	0	0	0	0	0	0	0	0	972.0
135	0	0	0	0	0	0	0	0	0	0	134	0	0	0	0	0	0	0	0	0	160.0
136	0	0	0	0	0	0	0	0	0	0	135	0	0	0	0	0	0	0	0	0	282.0
137	138	139	0	0	0	0	0	0	0	0	136	0	0	0	0	0	0	0	0	0	28122.0
138	0	0	0	0	0	0	0	0	0	0	137	0	0	0	0	0	0	0	0	0	383.0
139	149	140	0	0	0	0	0	0	0	0	138	0	0	0	0	0	0	0	0	0	27597.0
140	142	141	0	0	0	0	0	0	0	0	139	0	0	0	0	0	0	0	0	0	2013.0
141	0	0	0	0	0	0	0	0	0	0	140	0	0	0	0	0	0	0	0	0	132.0
142	146	143	0	0	0	0	0	0	0	0	141	0	0	0	0	0	0	0	0	0	1697.0
143	144	145	0	0	0	0	0	0	0	0	142	0	0	0	0	0	0	0	0	0	540.0
144	0	0	0	0	0	0	0	0	0	0	143	0	0	0	0	0	0	0	0	0	274.0
145	0	0	0	0	0	0	0	0	0	0	144	0	0	0	0	0	0	0	0	0	79.0
146	147	148	0	0	0	0	0	0	0	0	145	0	0	0	0	0	0	0	0	0	1054.0
147	0	0	0	0	0	0	0	0	0	0	146	0	0	0	0	0	0	0	0	0	283.0
148	0	0	0	0	0	0	0	0	0	0	147	0	0	0	0	0	0	0	0	0	453.0
149	152	150	151	0	0	0	0	0	0	0	148	0	0	0	0	0	0	0	0	0	25514.0
150	0	0	0	0	0	0	0	0	0	0	149	0	0	0	0	0	0	0	0	0	58.0
151	0	0	0	0	0	0	0	0	0	0	150	0	0	0	0	0	0	0	0	0	189.0
152	153	154	0	0	0	0	0	0	0	0	151	0	0	0	0	0	0	0	0	0	25053.0
153	0	0	0	0	0	0	0	0	0	0	152	0	0	0	0	0	0	0	0	0	249.0
154	156	155	0	0	0	0	0	0	0	0	153	0	0	0	0	0	0	0	0	0	24303.0
155	0	0	0	0	0	0	0	0	0	0	154	0	0	0	0	0	0	0	0	0	161.0
156	157	158	0	0	0	0	0	0	0	0	155	0	0	0	0	0	0	0	0	0	23893.0
157	172	163	170	171	0	0	0	0	0	0	156	0	0	0	0	0	0	0	0	0	21505.0
158	160	159	0	0	0	0	0	0	0	0	157	0	0	0	0	0	0	0	0	0	1865.0
159	0	0	0	0	0	0	0	0	0	0	158	0	0	0	0	0	0	0	0	0	476.0
160	161	162	0	0	0	0	0	0	0	0	159	0	0	0	0	0	0	0	0	0	1045.0
161	0	0	0	0	0	0	0	0	0	0	160	0	0	0	0	0	0	0	0	0	341.0
162	0	0	0	0	0	0	0	0	0	0	161	0	0	0	0	0	0	0	0	0	362.0
163	166	164	0	0	0	0	0	0	0	0	162	0	0	0	0	0	0	0	0	0	1286.0
164	0	0	0	0	0	0	0	0	0	0	163	0	0	0	0	0	0	0	0	0	76.0
165	168	169	0	0	0	0	0	0	0	0	164	0	0	0	0	0	0	0	0	0	784.0
166	165	167	0	0	0	0	0	0	0	0	165	0	0	0	0	0	0	0	0	0	1098.0
167	0	0	0	0	0	0	0	0	0	0	166	0	0	0	0	0	0	0	0	0	215.0
168	0	0	0	0	0	0	0	0	0	0	167	0	0	0	0	0	0	0	0	0	259.0
169	0	0	0	0	0	0	0	0	0	0	168	0	0	0	0	0	0	0	0	0	175.0
170	0	0	0	0	0	0	0	0	0	0	169	0	0	0	0	0	0	0	0	0	332.0
171	0	0	0	0	0	0	0	0	0	0	170	0	0	0	0	0	0	0	0	0	139.0
172	187	173	0	0	0	0	0	0	0	0	171	0	0	0	0	0	0	0	0	0	19645.0
173	174	175	0	0	0	0	0	0	0	0	172	0	0	0	0	0	0	0	0	0	5003.0
174	0	0	0	0	0	0	0	0	0	0	173	0	0	0	0	0	0	0	0	0	188.0
175	177	176	0	0	0	0	0	0	0	0	174	0	0	0	0	0	0	0	0	0	4585.0
176	180	179	0	0	0	0	0	0	0	0	175	0	0	0	0	0	0	0	0	0	3882.0
177	178	0	0	0	0	0	0	0	0	0	176	0	0	0	0	0	0	0	0	0	625.0
178	0	0	0	0	0	0	0	0	0	0	177	0	0	0	0	0	0	0	0	0	392.0

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179	0	0	0	0	0	0	0	0	0	0	178	0	0	0	0	0	0	0	0	0	211.0
180	181	182	0	0	0	0	0	0	0	0	179	0	0	0	0	0	0	0	0	0	2955.0
181	0	0	0	0	0	0	0	0	0	0	180	0	0	0	0	0	0	0	0	0	438.0
182	183	184	0	0	0	0	0	0	0	0	181	0	0	0	0	0	0	0	0	0	2016.0
183	0	0	0	0	0	0	0	0	0	0	182	0	0	0	0	0	0	0	0	0	599.0
184	186	185	0	0	0	0	0	0	0	0	183	0	0	0	0	0	0	0	0	0	910.0
185	0	0	0	0	0	0	0	0	0	0	184	0	0	0	0	0	0	0	0	0	232.0
186	0	0	0	0	0	0	0	0	0	0	185	0	0	0	0	0	0	0	0	0	461.0
187	192	193	0	0	0	0	0	0	0	0	186	0	0	0	0	0	0	0	0	0	14569.0
192	194	205	0	0	0	0	0	0	0	0	187	0	0	0	0	0	0	0	0	0	13278.0
193	0	0	0	0	0	0	0	0	0	0	188	0	0	0	0	0	0	0	0	0	273.0
194	198	199	196	195	0	0	0	0	0	0	189	0	0	0	0	0	0	0	0	0	5663.0
195	0	0	0	0	0	0	0	0	0	0	190	0	0	0	0	0	0	0	0	0	251.0
196	0	0	0	0	0	0	0	0	0	0	195	0	0	0	0	0	0	0	0	0	387.0
198	201	200	202	0	0	0	0	0	0	0	196	0	0	0	0	0	0	0	0	0	3544.0
199	0	0	0	0	0	0	0	0	0	0	197	0	0	0	0	0	0	0	0	0	634.0
200	0	0	0	0	0	0	0	0	0	0	198	0	0	0	0	0	0	0	0	0	542.0
201	204	203	0	0	0	0	0	0	0	0	199	0	0	0	0	0	0	0	0	0	1955.0
202	0	0	0	0	0	0	0	0	0	0	200	0	0	0	0	0	0	0	0	0	250.0
203	0	0	0	0	0	0	0	0	0	0	203	0	0	0	0	0	0	0	0	0	258.0
204	0	0	0	0	0	0	0	0	0	0	204	0	0	0	0	0	0	0	0	0	854.0
205	207	206	0	0	0	0	0	0	0	0	205	0	0	0	0	0	0	0	0	0	7500.0
206	0	0	0	0	0	0	0	0	0	0	206	0	0	0	0	0	0	0	0	0	250.0
207	211	208	0	0	0	0	0	0	0	0	207	0	0	0	0	0	0	0	0	0	6855.0
208	0	0	0	0	0	0	0	0	0	0	208	0	0	0	0	0	0	0	0	0	275.0
211	212	215	0	0	0	0	0	0	0	0	209	0	0	0	0	0	0	0	0	0	5808.0
212	214	213	0	0	0	0	0	0	0	0	210	0	0	0	0	0	0	0	0	0	1581.0
213	0	0	0	0	0	0	0	0	0	0	211	0	0	0	0	0	0	0	0	0	511.0
214	0	0	0	0	0	0	0	0	0	0	212	0	0	0	0	0	0	0	0	0	482.0
215	219	216	217	0	0	0	0	0	0	0	213	0	0	0	0	0	0	0	0	0	3943.0
216	0	0	0	0	0	0	0	0	0	0	214	0	0	0	0	0	0	0	0	0	505.0
217	0	0	0	0	0	0	0	0	0	0	215	0	0	0	0	0	0	0	0	0	245.0
218	222	221	0	0	0	0	0	0	0	0	219	0	0	0	0	0	0	0	0	0	1711.0
219	220	218	0	0	0	0	0	0	0	0	220	0	0	0	0	0	0	0	0	0	2654.0
220	0	0	0	0	0	0	0	0	0	0	221	0	0	0	0	0	0	0	0	0	506.0
221	0	0	0	0	0	0	0	0	0	0	222	0	0	0	0	0	0	0	0	0	250.0
222	224	223	0	0	0	0	0	0	0	0	223	0	0	0	0	0	0	0	0	0	1417.0
223	0	0	0	0	0	0	0	0	0	0	224	0	0	0	0	0	0	0	0	0	309.0
224	226	225	0	0	0	0	0	0	0	0	225	0	0	0	0	0	0	0	0	0	926.0
225	0	0	0	0	0	0	0	0	0	0	226	0	0	0	0	0	0	0	0	0	152.0
226	0	0	0	0	0	0	0	0	0	0	227	0	0	0	0	0	0	0	0	0	286.0
231	252	0	0	0	0	0	0	0	0	0	231	0	0	0	0	0	0	0	0	0	86054.0
232	234	233	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
233	251	0	0	0	0	0	0	0	0	0	233	0	0	0	0	0	0	0	0	0	85477.0
234	239	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	187.0
235	0	0	0	0	0	0	0	0	0	0	235	0	0	0	0	0	0	0	0	0	187.0
236	232	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
237	238	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
238	1927	240	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
239	235	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	187.0
240	241	0	0	0	0	0	0	0	0	0	240	0	0	0	0	0	0	0	0	0	84397.0

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241	242	0	0	0	0	0	0	0	0	0	241	0	0	0	0	0	0	0	0	84351.0
242	377	289	243	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	84008.0
243	1427	0	0	0	0	0	0	0	0	0	243	0	0	0	0	0	0	0	0	80261.0
244	0	0	0	0	0	0	0	0	0	0	253	0	0	0	0	0	0	0	0	848.0
245	1	246	0	0	0	0	0	0	0	0	254	0	0	0	0	0	0	0	0	67230.0
246	247	250	0	0	0	0	0	0	0	0	255	0	0	0	0	0	0	0	0	2389.0
247	0	0	0	0	0	0	0	0	0	0	256	0	0	0	0	0	0	0	0	808.0
248	0	0	0	0	0	0	0	0	0	0	257	0	0	0	0	0	0	0	0	645.0
249	0	0	0	0	0	0	0	0	0	0	258	0	0	0	0	0	0	0	0	377.0
250	248	249	0	0	0	0	0	0	0	0	259	0	0	0	0	0	0	0	0	1131.0
251	237	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
252	236	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
261	44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	80179.0
262	1935	0	0	0	0	0	0	0	0	0	262	0	0	0	0	0	0	0	0	2758.0
263	262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2758.0
264	1905	0	0	0	0	0	0	0	0	0	264	0	0	0	0	0	0	0	0	2784.0
265	264	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
266	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
267	293	1267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
268	267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
269	265	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
270	271	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86842.0
271	319	231	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86842.0
280	294	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
289	1924	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3653.0
290	1290	0	0	0	0	0	0	0	0	0	290	0	0	0	0	0	0	0	0	3653.0
291	1291	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
292	1923	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
293	1293	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
294	1294	304	1920	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
295	1295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
296	1296	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
297	298	0	0	0	0	0	0	0	0	0	297	0	0	0	0	0	0	0	0	587.0
298	303	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	249.0
299	0	0	0	0	0	0	0	0	0	0	299	0	0	0	0	0	0	0	0	72.0
300	301	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	177.0
301	0	0	0	0	0	0	0	0	0	0	301	0	0	0	0	0	0	0	0	177.0
303	299	1922	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	249.0
304	0	0	0	0	0	0	0	0	0	0	304	0	0	0	0	0	0	0	0	150.0
308	396	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
310	1409	1310	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
311	371	312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	247.0
312	1940	0	0	0	0	0	0	0	0	0	312	0	0	0	0	0	0	0	0	100.0
313	1939	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
314	308	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
315	310	0	0	0	0	0	0	0	0	0	315	0	0	0	0	0	0	0	0	28.0
316	0	0	0	0	0	0	0	0	0	0	316	0	0	0	0	0	0	0	0	43.0
317	315	316	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	71.0
318	338	0	0	0	0	0	0	0	0	0	318	0	0	0	0	0	0	0	0	230.0
319	1946	0	0	0	0	0	0	0	0	0	319	0	0	0	0	0	0	0	0	788.0
320	1320	0	0	0	0	0	0	0	0	0	320	0	0	0	0	0	0	0	0	454.0

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321	1321	0	0	0	0	0	0	0	0	0	321	0	0	0	0	0	0	0	0	0	34.0
322	1909	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
323	1323	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9.0
324	325	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
325	1325	326	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
326	327	317	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
327	1311	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
328	337	1329	329	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
329	330	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
330	1306	1303	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
331	1331	1407	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
332	333	334	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
333	1333	0	0	0	0	0	0	0	0	0	333	0	0	0	0	0	0	0	0	0	5.0
334	1334	0	0	0	0	0	0	0	0	0	334	0	0	0	0	0	0	0	0	0	5.0
335	1335	0	0	0	0	0	0	0	0	0	335	0	0	0	0	0	0	0	0	0	417.0
336	1336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
337	331	0	0	0	0	0	0	0	0	0	337	0	0	0	0	0	0	0	0	0	50.0
338	0	0	0	0	0	0	0	0	0	0	338	0	0	0	0	0	0	0	0	0	73.0
339	1822	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
340	1340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
341	1341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
342	1342	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
343	1343	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
344	366	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
345	346	0	0	0	0	0	0	0	0	0	345	0	0	0	0	0	0	0	0	0	149.0
346	0	0	0	0	0	0	0	0	0	0	346	0	0	0	0	0	0	0	0	0	71.0
347	1915	0	0	0	0	0	0	0	0	0	347	0	0	0	0	0	0	0	0	0	212.0
348	1348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
349	0	0	0	0	0	0	0	0	0	0	349	0	0	0	0	0	0	0	0	0	13.0
350	0	0	0	0	0	0	0	0	0	0	350	0	0	0	0	0	0	0	0	0	51.0
351	1814	0	0	0	0	0	0	0	0	0	351	0	0	0	0	0	0	0	0	0	100.0
352	1919	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
353	0	0	0	0	0	0	0	0	0	0	353	0	0	0	0	0	0	0	0	0	41.0
354	1817	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.0
355	0	0	0	0	0	0	0	0	0	0	355	0	0	0	0	0	0	0	0	0	7.0
356	359	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
357	1357	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
358	311	0	0	0	0	0	0	0	0	0	358	0	0	0	0	0	0	0	0	0	259.0
359	345	347	349	355	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
360	1360	292	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
361	0	0	0	0	0	0	0	0	0	0	361	0	0	0	0	0	0	0	0	0	30.0
362	1362	363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
363	0	0	0	0	0	0	0	0	0	0	363	0	0	0	0	0	0	0	0	0	7.0
366	1366	0	0	0	0	0	0	0	0	0	366	0	0	0	0	0	0	0	0	0	81.0
367	1367	0	0	0	0	0	0	0	0	0	367	0	0	0	0	0	0	0	0	0	23.0
368	0	0	0	0	0	0	0	0	0	0	368	0	0	0	0	0	0	0	0	0	99.0
369	0	0	0	0	0	0	0	0	0	0	369	0	0	0	0	0	0	0	0	0	17.0
370	0	0	0	0	0	0	0	0	0	0	370	0	0	0	0	0	0	0	0	0	41.0
371	372	0	0	0	0	0	0	0	0	0	371	0	0	0	0	0	0	0	0	0	147.0
372	374	373	367	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	64.0
373	0	0	0	0	0	0	0	0	0	0	373	0	0	0	0	0	0	0	0	0	38.0

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1323	1402	0	0	0	0	0	0	0	0	0	1323	0	0	0	0	0	0	0	0	0	9.0
1325	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1329	0	0	0	0	0	0	0	0	0	0	336	0	0	0	0	0	0	0	0	0	31.0
1330	368 1312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1331	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1332	1330	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1333	340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1334	341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1335	342	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
1336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1337	321	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
1338	1337	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
1339	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1342	343	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
1343	356	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
1348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1357	393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1360	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1361	1338	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
1362	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1364	361 1363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30.0
1365	1370 1364	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	129.0
1366	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1367	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1368	1332	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1369	1368	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1370	1369	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1371	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1372	1371 1377	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1373	1945	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1374	375	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
1375	1373	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1376	1375	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1377	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1378	1406 1404	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1381	1382 1405	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1382	296	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1386	1937 385	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1387	1401	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1392	324	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
1393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1396	398	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1401	357	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1402	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1403	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1404	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1405	383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0

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1406	379	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1407	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1408	344	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
1409	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1410	0	0	0	0	0	0	0	0	0	0	1410	0	0	0	0	0	0	0	195.0
1411	1410	1424	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1412	1411	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1413	1412	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1414	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1415	0	0	0	0	0	0	0	0	0	0	1415	0	0	0	0	0	0	0	307.0
1416	1415	1553	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1203.0
1420	0	0	0	0	0	0	0	0	0	0	1420	0	0	0	0	0	0	0	59.0
1421	1420	1426	1441	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1423	1421	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1424	1423	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1425	0	0	0	0	0	0	0	0	0	0	1425	0	0	0	0	0	0	0	68.0
1426	1438	1425	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	382.0
1427	261	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	80179.0
1428	1528	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1429	1428	1416	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1203.0
1430	0	0	0	0	0	0	0	0	0	0	1430	0	0	0	0	0	0	0	82.0
1431	1430	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	82.0
1435	0	0	0	0	0	0	0	0	0	0	1435	0	0	0	0	0	0	0	232.0
1436	1435	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	232.0
1438	1436	1431	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	314.0
1440	0	0	0	0	0	0	0	0	0	0	1440	0	0	0	0	0	0	0	66.0
1441	1453	1440	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76465.0
1442	1514	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2719.0
1445	0	0	0	0	0	0	0	0	0	0	1445	0	0	0	0	0	0	0	164.0
1446	1445	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	164.0
1450	0	0	0	0	0	0	0	0	0	0	1450	0	0	0	0	0	0	0	198.0
1451	1603	1450	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76235.0
1453	1446	1451	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76399.0
1455	0	0	0	0	0	0	0	0	0	0	1455	0	0	0	0	0	0	0	542.0
1456	1455	1482	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1274.0
1457	1456	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1274.0
1460	0	0	0	0	0	0	0	0	0	0	1460	0	0	0	0	0	0	0	286.0
1461	1460	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	286.0
1465	0	0	0	0	0	0	0	0	0	0	1465	0	0	0	0	0	0	0	93.0
1467	1933	1932	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2351.0
1468	1467	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2351.0
1480	1938	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1481	1480	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1482	1481	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1490	0	0	0	0	0	0	0	0	0	0	1490	0	0	0	0	0	0	0	698.0
1491	1490	1457	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1972.0
1500	0	0	0	0	0	0	0	0	0	0	1500	0	0	0	0	0	0	0	465.0
1501	1500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	465.0
1505	0	0	0	0	0	0	0	0	0	0	1505	0	0	0	0	0	0	0	262.0
1506	1505	1800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79714.0
1507	1506	1508	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79714.0

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1620	0	0	0	0	0	0	0	0	0	0	1620	0	0	0	0	0	0	0	0	0	0	324.0
1621	1653	1620	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1816.0
1623	1616	1621	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2044.0
1624	1623	1705	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2111.0
1625	0	0	0	0	0	0	0	0	0	0	1625	0	0	0	0	0	0	0	0	0	0	197.0
1626	48	1625	1636	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	72591.0
1628	1631	1626	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73076.0
1630	0	0	0	0	0	0	0	0	0	0	1630	0	0	0	0	0	0	0	0	0	0	159.0
1631	1643	1630	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	485.0
1635	0	0	0	0	0	0	0	0	0	0	1635	0	0	0	0	0	0	0	0	0	0	317.0
1636	1635	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	317.0
1640	0	0	0	0	0	0	0	0	0	0	1640	0	0	0	0	0	0	0	0	0	0	200.0
1641	1640	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	200.0
1643	1646	1641	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	326.0
1645	0	0	0	0	0	0	0	0	0	0	1645	0	0	0	0	0	0	0	0	0	0	126.0
1646	1645	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	126.0
1650	0	0	0	0	0	0	0	0	0	0	1650	0	0	0	0	0	0	0	0	0	0	382.0
1651	1661	1650	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	934.0
1653	1651	1656	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1492.0
1655	0	0	0	0	0	0	0	0	0	0	1655	0	0	0	0	0	0	0	0	0	0	558.0
1656	1655	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	558.0
1660	0	0	0	0	0	0	0	0	0	0	1660	0	0	0	0	0	0	0	0	0	0	552.0
1661	1660	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	552.0
1665	0	0	0	0	0	0	0	0	0	0	1665	0	0	0	0	0	0	0	0	0	0	390.0
1666	1665	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	390.0
1705	0	0	0	0	0	0	0	0	0	0	1705	0	0	0	0	0	0	0	0	0	0	67.0
1710	0	0	0	0	0	0	0	0	0	0	1710	0	0	0	0	0	0	0	0	0	0	245.0
1711	1710	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	245.0
1712	1711	1624	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2356.0
1715	0	0	0	0	0	0	0	0	0	0	1715	0	0	0	0	0	0	0	0	0	0	115.0
1716	1715	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	115.0
1800	1509	1468	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79452.0
1812	352	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1813	1812	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1814	1813	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1815	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1816	1815	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1817	1818	1816	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.0
1818	0	0	0	0	0	0	0	0	0	0	354	0	0	0	0	0	0	0	0	0	0	6.0
1820	384	1383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1821	369	1926	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1822	1339	394	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1905	263	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2758.0
1906	389	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1907	388	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1908	387	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1909	1906	320	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
1910	313	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1911	391	318	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1912	1911	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1913	351	354	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	106.0

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1914	1913	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	106.0
1915	350 1914	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	157.0
1916	1262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1917	0	0	0	0	0	0	0	0	0	0	305	0	0	0	0	0	0	0	0	103.0
1919	1934 353	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1920	1921	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	690.0
1921	297 1917	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	690.0
1922	300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	177.0
1923	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1924	290 1289	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3653.0
1925	378	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1926	381	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1927	1238	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1928	1611 1606	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73656.0
1929	1712	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2356.0
1931	1491 1461	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2258.0
1932	1465	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	93.0
1933	1931	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2258.0
1934	360	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1935	1442 1916	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2719.0
1937	348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1938	0	0	0	0	0	0	0	0	0	0	1480	0	0	0	0	0	0	0	0	732.0
1939	1313 314	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1940	1910 1408 1942	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	88.0
1941	1393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1942	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1943	322	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
1944	1365 370	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1945	1944	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1946	1376 1943	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	624.0
1947	1599	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86852.0

ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER 359 TO GUTTER 266 COMP THROUGH DIVERSION WILL LAG ONE TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.
 ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER 420 TO GUTTER 385 COMP THROUGH DIVERSION WILL LAG ONE TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.
 ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER 541 TO GUTTER 388 COMP THROUGH DIVERSION WILL LAG ONE TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.
 ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER 565 TO GUTTER 389 COMP THROUGH DIVERSION WILL LAG ONE TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.

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*** PEAK FLOWS, STAGES AND STORAGES OF GUTTERS AND DETENTION DAMS ***

CONVEYANCE ELEMENT	PEAK (CFS)	STAGE (FT)	STORAGE (AC-FT)	TIME (HR/MIN)				
1	3342.	5.8		12 45.	104	332.	2.3	8 20.
2	1556.	5.0		8 40.	105	67.	1.1	8 10.
3	622.	1.7		8 30.	106	41.	.9	8 20.
4	617.	1.5		8 30.	107	267.	2.0	8 35.
5	3190.	5.7		12 45.	108	38.	.7	8 30.
6	3140.	5.0		12 45.	109	215.	1.6	8 30.
7	443.	3.2		8 35.	110	153.	1.4	8 25.
8	7265.	(DIRECT FLOW)		9 25.	111	40.	.6	8 30.
9	223.	2.1		8 30.	112	72.	1.0	8 25.
10	112.	.7		8 20.	113	35.	.7	8 25.
11	123.	.8		8 10.	114	16.	.5	8 10.
12	97.	.7		8 20.	115	23.	.5	8 25.
13	332.	1.3		8 20.	116	60.	1.1	8 25.
14	139.	.8		8 10.	117	112.	1.6	8 15.
15	5697.	(DIRECT FLOW)		9 45.	118	60.	1.0	8 30.
16	5666.	(DIRECT FLOW)		9 45.	119	129.	1.9	8 20.
17	631.	2.1		8 30.	120	67.	1.1	8 10.
18	405.	2.3		8 30.	121	123.	1.4	8 35.
20	96.	1.0		8 15.	122	359.	1.7	8 45.
21	112.	1.1		8 35.	123	205.	1.3	8 35.
22	1417.	3.8		8 45.	124	108.	1.1	8 25.
23	649.	3.3		8 50.	125	24.	.5	8 20.
24	554.	3.0		8 35.	126	15.	.4	8 30.
25	152.	1.2		8 30.	127	78.	.8	8 25.
26	370.	2.5		8 30.	128	70.	.7	8 30.
27	32.	.4		8 25.	129	3065.	5.5	9 55.
28	285.	1.4		8 30.	130	270.	1.4	8 35.
29	70.	.9		8 25.	131	68.	.7	8 10.
30	160.	1.1		8 35.	132	36.	.7	8 25.
31	153.	1.3		8 35.	133	161.	1.3	8 40.
32	28.	.5		8 30.	134	112.	1.1	8 30.
33	116.	1.1		8 30.	135	11.	.4	8 10.
34	219.	1.7		8 45.	136	21.	.5	8 10.
35	76.	.7		8 30.	137	2921.	4.3	9 50.
36	97.	.8		8 40.	138	106.	1.1	8 40.
37	203.	1.7		8 45.	139	2832.	4.2	9 45.
38	48.	.5		8 20.	140	275.	1.6	8 40.
39	133.	1.0		8 35.	141	67.	1.0	8 30.
40	5412.	6.9		10 5.	142	190.	1.5	8 35.
41	96.	.7		8 25.	143	71.	.9	8 30.
42	5352.	6.4		10 5.	144	30.	.6	8 10.
44	6357.	(DIRECT FLOW)		10 40.	145	11.	.5	8 25.
46	4977.	6.9		10 5.	146	104.	1.0	8 35.
48	6168.	8.3		9 10.	147	35.	.5	8 30.
49	293.	1.4		8 10.	148	47.	.7	8 15.
50	6142.	5.7		9 0.	149	2673.	3.9	9 45.
51	580.	2.8		8 15.	150	41.	.7	8 20.
52	5431.	6.6		8 55.	151	92.	1.1	8 30.
53	149.	1.7		8 10.	152	2603.	4.1	9 35.
54	50.	.9		8 5.	153	29.	.4	8 30.
55	57.	1.0		8 5.	154	2648.	4.3	9 20.
56	710.	2.2		8 25.	155	42.	.4	8 30.
57	323.	1.2		8 25.	156	2602.	4.3	9 15.
58	45.	.8		8 5.	157	2462.	4.4	9 5.
59	4921.	6.7		10 5.	158	165.	1.0	8 30.
60	93.	.9		8 30.	159	29.	.5	8 10.
61	235.	1.8		8 45.	160	101.	.9	8 20.
62	496.	1.8		8 45.	161	40.	.7	8 25.
63	32.	.7		8 35.	162	25.	.5	8 10.
64	34.	1.0		8 25.	163	150.	.9	8 35.
65	243.	2.6		8 45.	164	20.	.3	8 30.
66	20.	.4		8 25.	165	75.	.9	8 25.
67	212.	1.5		8 35.	166	114.	.9	8 30.
68	294.	1.6		8 30.	167	32.	.6	8 30.
69	100.	.9		8 25.	168	19.	.5	8 10.
70	152.	1.1		8 30.	169	13.	.4	8 10.
71	269.	1.8		8 40.	170	130.	1.3	8 35.
72	95.	1.0		8 30.	171	82.	.9	8 25.
73	80.	1.1		8 30.	172	2183.	4.8	9 10.
74	4785.	6.6		10 0.	173	827.	1.9	8 45.
75	970.	3.7		9 10.	174	42.	.7	8 25.
76	157.	1.3		8 35.	175	686.	1.8	8 40.
77	1114.	3.3		9 10.	176	612.	2.3	8 40.
78	27.	.5		8 30.	177	69.	.9	8 30.
79	944.	3.0		9 5.	178	34.	.7	8 10.
80	720.	1.7		8 50.	179	53.	.3	8 35.
81	289.	1.7		8 55.	180	336.	2.0	8 30.
82	135.	1.0		8 40.	181	33.	.6	8 10.
83	24.	.5		8 25.	182	186.	1.2	8 25.
84	90.	.9		8 35.	183	40.	.6	8 15.
85	19.	.7		8 30.	184	119.	.8	8 20.
86	54.	.8		8 30.	185	25.	.7	8 15.
87	179.	1.5		8 50.	186	83.	.9	8 15.
88	147.	1.0		8 50.	187	1499.	3.5	9 20.
89	103.	1.4		8 45.	192	1498.	3.5	8 55.
93	11.	.4		8 5.	193	149.	.5	8 25.
94	3838.	5.1		10 5.	194	505.	1.8	8 35.
95	3297.	4.7		10 10.	195	17.	.3	8 10.
96	3282.	6.5		10 0.	196	23.	.6	8 10.
97	1176.	3.6		8 45.	198	401.	1.7	8 35.
98	166.	1.4		8 25.	199	36.	.7	8 15.
99	1019.	3.7		8 40.	200	34.	.6	8 10.
100	242.	1.8		8 30.	201	360.	1.7	8 25.
101	757.	3.4		8 35.	202	19.	.5	8 10.
102	476.	2.4		8 35.	203	89.	1.0	8 10.
103	419.	1.7		8 25.	204	265.	1.3	8 20.

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205	1019.	3.0	9	0.	341	1308.	(DIRECT FLOW)	11	55.	
206	19.	.1	8	10.	342	1638.	(DIRECT FLOW)	11	55.	
207	999.	2.6	8	50.	343	2055.	(DIRECT FLOW)	11	55.	
208	20.	.3	8	10.	344	136.	(DIRECT FLOW)	8	15.	
211	1021.	3.4	8	35.	345	309.	1.5	8	15.	
212	256.	1.2	8	25.	346	175.	1.1	8	10.	
213	160.	1.0	8	25.	347	2051.	6.5	11	50.	
214	91.	.7	8	15.	348	638.	(DIRECT FLOW)	12	5.	
215	764.	2.6	8	30.	349	9.	.3	8	25.	
216	121.	.6	8	15.	350	123.	3.1	8	10.	
217	18.	.1	8	10.	351	1334.	4.8	11	45.	
218	468.	2.7	8	20.	352	2055.	.1	17.8	11	45.
219	655.	2.3	8	25.	353	72.	1.0	8	10.	
220	178.	1.1	8	25.	354	720.	2.5	11	50.	
221	69.	.9	8	10.	355	18.	2.1	8	10.	
222	402.	2.5	8	20.	356	2055.	.1	15.9	11	55.
223	111.	.7	8	20.	357	520.	(DIRECT FLOW)	8	25.	
224	289.	2.3	8	15.	358	603.	4.4	8	25.	
225	67.	.9	8	10.	359	2060.	(DIRECT FLOW)	11	50.	
226	110.	.6	8	10.	360	2062.	(DIRECT FLOW)	11	40.	
231	2279.	3.3	12	40.	361	66.	(DIRECT FLOW)	8	5.	
232	2342.	(DIRECT FLOW)	12	30.	362	417.	(DIRECT FLOW)	11	55.	
233	2334.	4.2	12	30.	363	13.	.5	8	10.	
234	157.	2.6	8	40.	366	136.	1.1	8	15.	
235	186.	1.0	8	20.	367	58.	.8	8	10.	
236	2342.	(DIRECT FLOW)	12	30.	368	140.	(DIRECT FLOW)	8	10.	
237	4434.	(DIRECT FLOW)	12	0.	369	47.	.8	8	5.	
238	4434.	(DIRECT FLOW)	12	0.	370	137.	(DIRECT FLOW)	8	5.	
239	186.	(DIRECT FLOW)	8	20.	371	212.	1.9	8	20.	
240	4231.	3.9	12	0.	372	96.	(DIRECT FLOW)	8	10.	
241	4282.	3.8	11	40.	373	18.	1.1	8	30.	
242	4458.	(DIRECT FLOW)	10	55.	374	36.	1.4	11	10.	
243	3392.	3.4	10	55.	375	229.	(DIRECT FLOW)	10	55.	
244	1148.	2.8	8	20.	376	229.	3.8	10	55.	
245	4691.	6.7	8	50.	377	109.	3.1	11	50.	
246	1969.	3.9	8	30.	378	348.	(DIRECT FLOW)	11	30.	
247	663.	2.0	8	30.	379	182.	(DIRECT FLOW)	8	15.	
248	558.	1.8	8	30.	380	182.	3.9	8	15.	
249	363.	1.6	8	20.	381	261.	(DIRECT FLOW)	11	45.	
250	936.	2.8	8	30.	382	261.	5.4	11	45.	
251	2336.	(DIRECT FLOW)	12	0.	383	726.	(DIRECT FLOW)	11	40.	
252	2259.	(DIRECT FLOW)	12	30.	384	150.	3.9	8	10.	
261	6357.	(DIRECT FLOW)	10	40.	385	108.	(DIRECT FLOW)	12	5.	
262	3830.	2.6	10	50.	386	361.	(DIRECT FLOW)	12	5.	
263	3830.	(DIRECT FLOW)	10	50.	387	103.	(DIRECT FLOW)	12	20.	
264	3583.	2.5	10	55.	388	754.	(DIRECT FLOW)	8	45.	
265	3583.	(DIRECT FLOW)	10	55.	389	2098.	(DIRECT FLOW)	12	0.	
266	229.	(DIRECT FLOW)	10	50.	390	957.	(DIRECT FLOW)	8	45.	
267	2639.	(DIRECT FLOW)	10	55.	391	830.	6.4	12	30.	
268	2602.	.1	44.3	11	5.	392	831.	(DIRECT FLOW)	12	20.
269	1351.	(DIRECT FLOW)	10	55.	393	603.	(DIRECT FLOW)	8	25.	
270	5354.	7.6	13	10.	394	307.	1.6	12	5.	
271	5358.	(DIRECT FLOW)	13	5.	395	308.	(DIRECT FLOW)	12	5.	
280	1411.	(DIRECT FLOW)	11	0.	396	416.	(DIRECT FLOW)	12	0.	
289	1100.	5.9	11	50.	397	3134.	.1	1494.4	12	40.
290	865.	5.3	11	10.	398	416.	.1	3.0	12	0.
291	2602.	(DIRECT FLOW)	11	5.	399	5354.	(DIRECT FLOW)	13	10.	
292	1736.	2.8	11	15.	1238	203.	(DIRECT FLOW)	8	45.	
293	408.	6.8	11	0.	1262	2924.	(DIRECT FLOW)	10	45.	
294	1411.	(DIRECT FLOW)	11	0.	1267	2231.	(DIRECT FLOW)	10	55.	
295	751.	.1	76.6	11	35.	1289	239.	(DIRECT FLOW)	11	35.
296	751.	(DIRECT FLOW)	11	35.	1290	864.	(DIRECT FLOW)	11	5.	
297	727.	4.2	8	10.	1291	2602.	(DIRECT FLOW)	11	5.	
298	111.	.1	2.1	8	25.	1293	409.	(DIRECT FLOW)	11	0.
299	154.	.8	8	10.	1294	1341.	2.2	11	0.	
300	11.	.1	20.2	10	30.	1295	1002.	(DIRECT FLOW)	11	5.
301	345.	1.0	8	10.	1296	751.	(DIRECT FLOW)	11	35.	
303	164.	(DIRECT FLOW)	8	10.	1301	303.	(DIRECT FLOW)	12	5.	
304	62.	1.4	8	25.	1302	303.	(DIRECT FLOW)	12	5.	
308	307.	(DIRECT FLOW)	12	0.	1303	302.	(DIRECT FLOW)	12	5.	
310	263.	(DIRECT FLOW)	12	10.	1304	1.	(DIRECT FLOW)	12	5.	
311	593.	(DIRECT FLOW)	8	20.	1305	599.	(DIRECT FLOW)	12	5.	
312	454.	5.0	12	15.	1306	59.	(DIRECT FLOW)	12	10.	
313	418.	(DIRECT FLOW)	12	5.	1307	599.	(DIRECT FLOW)	12	5.	
314	307.	5.4	12	0.	1308	657.	(DIRECT FLOW)	12	5.	
315	260.	1.4	12	20.	1309	792.	(DIRECT FLOW)	12	10.	
316	84.	1.0	8	15.	1310	111.	(DIRECT FLOW)	12	10.	
317	262.	(DIRECT FLOW)	12	20.	1311	792.	(DIRECT FLOW)	12	10.	
318	161.	2.9	8	40.	1312	0.	(DIRECT FLOW)	12	10.	
319	3086.	7.4	13	5.	1313	111.	(DIRECT FLOW)	12	5.	
320	1001.	2.5	12	40.	1320	1002.	(DIRECT FLOW)	12	30.	
321	602.	1.9	12	25.	1321	608.	(DIRECT FLOW)	12	20.	
322	3037.	(DIRECT FLOW)	12	30.	1323	681.	(DIRECT FLOW)	12	20.	
323	681.	(DIRECT FLOW)	12	20.	1325	489.	(DIRECT FLOW)	8	30.	
324	1454.	(DIRECT FLOW)	12	20.	1329	65.	.9	8	10.	
325	1454.	(DIRECT FLOW)	12	20.	1330	117.	2.6	8	25.	
326	1046.	6.2	12	20.	1331	385.	(DIRECT FLOW)	12	5.	
327	784.	5.6	12	15.	1332	117.	(DIRECT FLOW)	8	25.	
328	792.	(DIRECT FLOW)	12	10.	1333	332.	(DIRECT FLOW)	12	0.	
329	357.	4.1	12	15.	1334	338.	(DIRECT FLOW)	11	55.	
330	361.	(DIRECT FLOW)	12	5.	1335	330.	(DIRECT FLOW)	11	55.	
331	438.	(DIRECT FLOW)	12	5.	1336	222.	(DIRECT FLOW)	12	10.	
332	657.	(DIRECT FLOW)	12	5.	1337	602.	(DIRECT FLOW)	12	25.	
333	326.	1.6	12	10.	1338	278.	(DIRECT FLOW)	12	25.	
334	331.	1.6	12	5.	1339	25.	(DIRECT FLOW)	8	20.	
335	303.	2.6	12	5.	1340	970.	(DIRECT FLOW)	12	0.	
336	222.	(DIRECT FLOW)	12	10.	1341	1308.	(DIRECT FLOW)	11	55.	
337	435.	1.8	12	10.	1342	1638.	(DIRECT FLOW)	11	55.	
338	81.	1.7	8	25.	1343	2055.	(DIRECT FLOW)	11	55.	
339	333.	(DIRECT FLOW)	12	5.	1348	638.	(DIRECT FLOW)	12	5.	
340	970.	(DIRECT FLOW)	12	0.	1357	520.	(DIRECT FLOW)	8	25.	

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1360	494.	(DIRECT FLOW)	11	45.	1533	5569.	(DIRECT FLOW)	10	5.	
1361	276.	2.7	12	25.	1534	3412.	3.2	10	10.	
1362	417.	(DIRECT FLOW)	11	55.	1537	2218.	3.5	9	55.	
1363	324.	(DIRECT FLOW)	12	25.	1541	239.	(DIRECT FLOW)	8	5.	
1364	314.	3.0	12	30.	1542	166.	1.9	8	25.	
1365	324.	(DIRECT FLOW)	12	30.	1544	5567.	(DIRECT FLOW)	10	15.	
1366	105.	(DIRECT FLOW)	11	50.	1545	155.	(DIRECT FLOW)	8	15.	
1367	2.	(DIRECT FLOW)	8	20.	1546	308.	2.1	8	35.	
1368	117.	(DIRECT FLOW)	8	25.	1548	5551.	2.7	10	15.	
1369	117.	(DIRECT FLOW)	8	25.	1550	421.	(DIRECT FLOW)	8	15.	
1370	114.	2.5	8	30.	1551	533.	2.5	8	35.	
1371	0.	(DIRECT FLOW)	8	25.	1553	673.	(DIRECT FLOW)	8	35.	
1372	100.	(DIRECT FLOW)	12	40.	1556	65.	(DIRECT FLOW)	8	15.	
1373	321.	(DIRECT FLOW)	12	40.	1557	141.	1.9	8	35.	
1374	36.	(DIRECT FLOW)	10	55.	1560	143.	(DIRECT FLOW)	8	10.	
1375	221.	(DIRECT FLOW)	12	40.	1561	142.	1.4	8	15.	
1376	221.	2.8	12	40.	1563	242.	(DIRECT FLOW)	8	15.	
1377	100.	(DIRECT FLOW)	12	40.	1565	101.	(DIRECT FLOW)	8	10.	
1378	348.	(DIRECT FLOW)	11	30.	1566	100.	1.2	8	15.	
1381	261.	(DIRECT FLOW)	11	40.	1570	105.	(DIRECT FLOW)	8	20.	
1382	29.	(DIRECT FLOW)	11	35.	1571	105.	.6	8	20.	
1383	722.	(DIRECT FLOW)	11	40.	1575	276.	(DIRECT FLOW)	8	10.	
1386	361.	(DIRECT FLOW)	12	5.	1576	221.	2.4	8	25.	
1387	103.	(DIRECT FLOW)	12	20.	1599	5828.	(DIRECT FLOW)	12	55.	
1392	772.	(DIRECT FLOW)	12	20.	1600	7.	(DIRECT FLOW)	8	0.	
1393	83.	(DIRECT FLOW)	8	30.	1601	6642.	5.2	9	25.	
1396	416.	(DIRECT FLOW)	12	0.	1603	7485.	(DIRECT FLOW)	9	20.	
1401	31.	(DIRECT FLOW)	8	25.	1605	67.	(DIRECT FLOW)	8	15.	
1402	681.	(DIRECT FLOW)	12	20.	1606	586.	2.6	8	25.	
1403	83.	(DIRECT FLOW)	12	30.	1610	50.	(DIRECT FLOW)	8	5.	
1404	193.	(DIRECT FLOW)	10	55.	1611	6475.	4.9	9	20.	
1405	231.	(DIRECT FLOW)	11	40.	1615	81.	(DIRECT FLOW)	8	10.	
1406	180.	(DIRECT FLOW)	8	15.	1616	68.	1.4	8	20.	
1407	53.	(DIRECT FLOW)	12	5.	1620	105.	(DIRECT FLOW)	8	10.	
1408	111.	(DIRECT FLOW)	8	15.	1621	972.	3.7	8	45.	
1409	153.	(DIRECT FLOW)	12	10.	1623	1025.	(DIRECT FLOW)	8	40.	
1410	45.	(DIRECT FLOW)	8	5.	1624	1033.	3.6	8	45.	
1411	5350.	5.5	10	0.	1625	291.	(DIRECT FLOW)	8	10.	
1412	5350.	(DIRECT FLOW)	10	0.	1626	6353.	5.2	9	15.	
1413	5350.	(DIRECT FLOW)	10	0.	1628	6628.	(DIRECT FLOW)	9	10.	
1414	3447.	(DIRECT FLOW)	10	5.	1630	144.	(DIRECT FLOW)	8	15.	
1415	72.	(DIRECT FLOW)	8	15.	1631	407.	1.9	8	35.	
1416	678.	3.2	8	50.	1635	350.	(DIRECT FLOW)	8	10.	
1420	81.	(DIRECT FLOW)	8	15.	1636	330.	1.9	8	20.	
1421	7190.	6.3	9	45.	1640	273.	(DIRECT FLOW)	8	10.	
1423	7190.	(DIRECT FLOW)	9	45.	1641	183.	3.2	8	30.	
1424	5470.	(DIRECT FLOW)	9	45.	1643	297.	(DIRECT FLOW)	8	30.	
1425	16.	(DIRECT FLOW)	8	0.	1645	126.	(DIRECT FLOW)	8	15.	
1426	54.	1.1	8	15.	1646	116.	1.3	8	25.	
1427	3433.	(DIRECT FLOW)	10	40.	1650	524.	(DIRECT FLOW)	8	10.	
1428	1713.	2.8	9	55.	1651	696.	3.1	8	20.	
1429	2080.	(DIRECT FLOW)	9	50.	1653	1075.	(DIRECT FLOW)	8	25.	
1430	16.	(DIRECT FLOW)	8	0.	1655	441.	(DIRECT FLOW)	8	20.	
1431	15.	.6	8	5.	1656	393.	2.5	8	30.	
1435	43.	(DIRECT FLOW)	8	0.	1660	318.	(DIRECT FLOW)	8	15.	
1436	34.	1.2	8	10.	1661	261.	2.1	8	30.	
1438	49.	(DIRECT FLOW)	8	10.	1665	651.	(DIRECT FLOW)	8	5.	
1440	43.	(DIRECT FLOW)	8	15.	1666	593.	2.5	8	15.	
1441	7177.	6.4	9	45.	1705	16.	(DIRECT FLOW)	8	10.	
1442	914.	2.0	10	45.	1710	81.	(DIRECT FLOW)	8	10.	
1445	35.	(DIRECT FLOW)	8	10.	1711	72.	1.0	8	35.	
1446	27.	.9	8	20.	1712	1103.	(DIRECT FLOW)	8	45.	
1450	46.	(DIRECT FLOW)	8	5.	1715	69.	(DIRECT FLOW)	8	10.	
1451	7366.	6.0	9	30.	1716	45.	.8	8	50.	
1453	7378.	(DIRECT FLOW)	9	30.	1800	2121.	(DIRECT FLOW)	9	55.	
1455	186.	(DIRECT FLOW)	8	10.	1812	2055.	(DIRECT FLOW)	11	45.	
1456	156.	.6	8	25.	1813	2055.	(DIRECT FLOW)	11	45.	
1457	156.	(DIRECT FLOW)	8	25.	1814	1336.	(DIRECT FLOW)	11	45.	
1460	100.	(DIRECT FLOW)	8	5.	1815	719.	(DIRECT FLOW)	11	50.	
1461	91.	1.8	8	10.	1816	720.	2.4	11	50.	
1465	85.	(DIRECT FLOW)	8	15.	1817	720.	(DIRECT FLOW)	11	50.	
1467	296.	(DIRECT FLOW)	8	20.	1818	23.	.9	8	0.	
1468	293.	2.2	8	25.	1820	726.	(DIRECT FLOW)	11	40.	
1480	841.	3.3	8	15.	1821	184.	(DIRECT FLOW)	8	15.	
1481	7.	.0	121.3	24	40.	1822	333.	(DIRECT FLOW)	12	5.
1482	7.	(DIRECT FLOW)	24	20.	1905	3601.	(DIRECT FLOW)	10	50.	
1490	251.	(DIRECT FLOW)	8	10.	1906	2065.	1.1	12	20.	
1491	209.	2.6	9	10.	1907	732.	2.5	9	0.	
1500	346.	(DIRECT FLOW)	9	10.	1908	98.	2.0	12	45.	
1501	261.	2.6	8	35.	1909	3037.	(DIRECT FLOW)	12	30.	
1505	345.	(DIRECT FLOW)	8	10.	1910	265.	(DIRECT FLOW)	12	5.	
1506	1874.	3.5	10	55.	1911	969.	(DIRECT FLOW)	8	40.	
1507	6310.	(DIRECT FLOW)	10	35.	1912	957.	6.2	8	45.	
1508	4490.	(DIRECT FLOW)	10	30.	1913	2051.	(DIRECT FLOW)	11	50.	
1509	1903.	(DIRECT FLOW)	10	0.	1914	2052.	5.4	11	50.	
1510	70.	(DIRECT FLOW)	8	20.	1915	2056.	(DIRECT FLOW)	11	50.	
1511	5422.	4.6	10	30.	1916	2913.	2.6	10	50.	
1512	6286.	5.5	10	40.	1917	39.	1.0	8	25.	
1513	5422.	(DIRECT FLOW)	10	30.	1919	2061.	(DIRECT FLOW)	11	40.	
1514	932.	(DIRECT FLOW)	10	30.	1920	749.	4.9	8	15.	
1515	27.	(DIRECT FLOW)	8	5.	1921	761.	(DIRECT FLOW)	8	10.	
1517	48.	1.0	8	55.	1922	11.	.3	10	30.	
1520	142.	(DIRECT FLOW)	8	10.	1923	1738.	(DIRECT FLOW)	11	10.	
1521	5516.	4.5	10	15.	1924	1103.	(DIRECT FLOW)	11	30.	
1522	5580.	(DIRECT FLOW)	10	15.	1925	109.	(DIRECT FLOW)	11	30.	
1525	77.	(DIRECT FLOW)	8	10.	1926	155.	(DIRECT FLOW)	11	45.	
1526	2073.	3.4	9	55.	1927	203.	3.6	8	55.	
1528	1720.	(DIRECT FLOW)	9	50.	1928	6655.	(DIRECT FLOW)	9	20.	
1530	139.	(DIRECT FLOW)	8	15.	1929	1093.	2.8	8	50.	
1531	402.	2.1	8	40.	1931	238.	(DIRECT FLOW)	8	55.	
1532	2224.	(DIRECT FLOW)	9	50.	1932	81.	.9	8	15.	

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1933	238.	2.3	8	55.
1934	2059.	3.0	11	40.
1935	3826.	(DIRECT FLOW)	10	45.
1937	253.	(DIRECT FLOW)	12	5.
1938	856.	(DIRECT FLOW)	8	10.
1939	418.	(DIRECT FLOW)	12	5.
1940	454.	(DIRECT FLOW)	12	10.
1941	82.	1.0	8	30.
1942	111.	(DIRECT FLOW)	12	10.
1943	3022.	6.7	12	40.
1944	321.	5.6	12	40.
1945	321.	(DIRECT FLOW)	12	40.
1946	3243.	(DIRECT FLOW)	12	40.
1947	5828.	(DIRECT FLOW)	12	55.

UDSWMM
100-YEAR MODEL

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URBAN DRAINAGE STORM WATER MANAGEMENT MODEL - 32 BIT VERSION 1998
 REVISED BY UNIVERSITY OF COLORADO AT DENVER

*** ENTRY MADE TO RUNOFF MODEL ***

SBC CHANGES FROM DRAFT REPORT MODEL SBC_IN.SWI - ASSORTED MODIFICATIONS
 model sbc_ltc.swi with narrowing of conveyance 1330 overflow channel from 50' to

NUMBER OF TIME STEPS 865
 INTEGRATION TIME INTERVAL (MINUTES) 5.00

1.0 PERCENT OF IMPERVIOUS AREA HAS ZERO DETENTION DEPTH
 OFOR 288 RAINFALL STEPS, THE TIME INTERVAL IS 5.00 MINUTES
 OFOR RAINGAGE NUMBER 1 RAINFALL HISTORY IN INCHES PER HOUR

.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.09	.09	.09	.09	.09
.09	.09	.09	.10	.10	.10	.10	.10	.10	.11
.11	.11	.11	.11	.12	.12	.12	.12	.12	.13
.13	.13	.14	.14	.14	.15	.15	.16	.16	.17
.17	.18	.19	.20	.20	.21	.22	.24	.25	.27
.29	.31	.34	.37	.41	.45	.51	.59	.69	.82
1.01	1.28	1.69	2.34	3.39	4.36	4.04	2.80	1.97	1.46
1.13	.91	.75	.63	.55	.48	.43	.38	.35	.32
.30	.28	.26	.24	.23	.22	.21	.20	.19	.18
.18	.17	.17	.16	.15	.15	.15	.14	.14	.14
.13	.13	.13	.12	.12	.12	.12	.11	.11	.11
.11	.11	.10	.10	.10	.10	.10	.10	.09	.09
.09	.09	.09	.09	.09	.09	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04

OFOR RAINGAGE NUMBER 2 RAINFALL HISTORY IN INCHES PER HOUR

.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.09	.09	.09	.10	.10	.10
.10	.10	.10	.10	.10	.11	.11	.11	.11	.11
.11	.12	.12	.12	.12	.13	.13	.13	.14	.14
.14	.15	.15	.16	.17	.17	.18	.19	.20	.22
.23	.25	.27	.30	.33	.37	.41	.48	.56	.68
.84	1.07	1.43	2.03	3.02	4.11	3.68	2.46	1.69	1.23
.94	.75	.61	.52	.44	.39	.34	.31	.28	.26
.24	.22	.21	.20	.19	.18	.17	.16	.16	.15
.15	.14	.14	.13	.13	.13	.12	.12	.12	.12
.11	.11	.11	.11	.11	.11	.10	.10	.10	.10
.10	.10	.10	.10	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.09	.09	.09	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06

OFOR RAINGAGE NUMBER 3 RAINFALL HISTORY IN INCHES PER HOUR

.07	.07	.07	.07	.07	.07	.07	.07	.07	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.09	.09
.09	.09	.09	.09	.09	.09	.09	.09	.09	.09
.10	.10	.10	.10	.10	.10	.10	.10	.10	.11
.11	.11	.11	.11	.11	.12	.12	.12	.12	.12
.13	.13	.13	.14	.14	.14	.15	.15	.16	.16
.17	.17	.18	.19	.19	.20	.21	.22	.24	.25
.27	.29	.31	.34	.37	.41	.46	.51	.59	.68
.81	.98	.22	1.60	2.24	3.64	2.78	1.87	1.39	1.09
.89	.74	.63	.55	.48	.43	.39	.35	.32	.30
.28	.26	.24	.23	.22	.21	.20	.19	.18	.17
.17	.16	.16	.15	.15	.14	.14	.14	.13	.13
.13	.13	.12	.12	.12	.12	.12	.11	.11	.11
.11	.11	.11	.10	.10	.10	.10	.10	.10	.10
.10	.09	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07

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.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06

OFOR RAINGAGE NUMBER 4 RAINFALL HISTORY IN INCHES PER HOUR

.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.10	.10	.10	.10	.10	.10
.10	.10	.11	.11	.11	.11	.11	.11	.11	.12
.12	.12	.12	.12	.13	.13	.13	.13	.14	.14
.14	.14	.15	.15	.15	.16	.16	.17	.17	.17
.18	.19	.19	.20	.21	.21	.22	.23	.25	.26
.27	.29	.31	.33	.36	.39	.43	.48	.54	.62
.73	.87	.08	1.40	1.95	3.20	2.42	1.63	1.22	.97
.80	.67	.58	.51	.46	.41	.38	.35	.32	.30
.28	.27	.25	.24	.23	.22	.21	.20	.20	.19
.18	.18	.17	.17	.16	.16	.16	.15	.15	.15
.14	.14	.14	.13	.13	.13	.13	.13	.12	.12
.12	.12	.12	.11	.11	.11	.11	.11	.11	.10
.10	.10	.10	.10	.10	.10	.10	.10	.09	.09
.09	.09	.09	.09	.09	.09	.09	.09	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.07	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.07
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.06	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05

OFOR RAINGAGE NUMBER 5 RAINFALL HISTORY IN INCHES PER HOUR

.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.07	.07	.07	.07	.07	.07	.07	.07
.07	.07	.07	.08	.08	.08	.08	.08	.08	.08
.08	.09	.09	.09	.09	.09	.09	.10	.10	.10
.10	.10	.11	.11	.11	.12	.12	.12	.13	.13
.13	.14	.14	.15	.16	.16	.17	.18	.19	.20
.21	.23	.24	.26	.29	.32	.35	.39	.44	.51
.60	.72	.89	1.15	1.58	2.47	1.93	1.34	1.01	.80
.66	.55	.48	.42	.37	.33	.30	.28	.25	.24
.22	.21	.19	.18	.17	.17	.16	.15	.15	.14
.14	.13	.13	.12	.12	.12	.11	.11	.11	.11
.10	.10	.10	.10	.09	.09	.09	.09	.09	.09
.08	.08	.08	.08	.08	.08	.08	.08	.07	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03

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SBC CHANGES FROM DRAFT REPORT MODEL SBC_IN.SWI - ASSORTED MODIFICATIONS
 model sbc_ltc.swi with narrowing of conveyance 1330 overflow channel from 50' to

SUBAREA NUMBER	GUTTER OR MANHOLE	WIDTH (FT)	AREA (AC)	PERCENT IMPERV.	SLOPE (FT/FT)	RESISTANCE FACTOR		SURFACE STORAGE (IN)		INFILTRATION RATE (IN/HR)			GAGH NO
						IMPERV.	PERV.	IMPERV.	PERV.	MAXIMUM	MINIMUM	DECAY RATE	
227	226	7480.	286.0	30.0	.4076	.300	.500	.300	.470	3.90	.50	.00024	5
226	225	6240.	152.0	30.0	.5701	.300	.500	.300	.470	3.90	.50	.00024	5
225	224	8440.	488.0	20.0	.3704	.300	.500	.300	.470	4.50	.60	.00010	5
224	223	11920.	309.0	20.0	.2882	.300	.500	.300	.450	3.50	.20	.00100	5
222	221	13040.	250.0	20.0	.5139	.300	.500	.300	.450	3.90	.50	.00024	5
221	220	15160.	506.0	20.0	.4510	.300	.500	.300	.450	3.50	.20	.00100	5
219	218	3320.	44.0	6.0	.2945	.300	.500	.300	.470	3.90	.50	.00024	5
220	219	10200.	437.0	5.0	.3544	.300	.500	.300	.480	4.50	.60	.00010	5
223	222	2280.	182.0	6.0	.4444	.300	.500	.300	.470	4.80	.50	.00010	5
214	216	16320.	505.0	20.0	.4409	.300	.500	.300	.450	3.90	.50	.00024	5
212	214	13760.	492.0	15.0	.4325	.300	.500	.300	.450	3.90	.50	.00024	5
211	213	11800.	511.0	20.0	.3390	.300	.500	.300	.440	3.50	.20	.00100	5
210	212	12200.	588.0	5.0	.2915	.300	.500	.300	.420	4.80	.50	.00010	5
213	215	6480.	539.0	6.0	.3847	.300	.400	.150	.420	3.90	.50	.00024	5
215	217	9720.	245.0	5.0	.2985	.250	.450	.300	.500	3.90	.50	.00024	5
209	211	6800.	284.0	6.0	.4718	.300	.400	.150	.460	3.90	.50	.00024	5
185	186	8520.	461.0	15.0	.2842	.300	.500	.300	.450	4.50	.50	.00010	5
184	185	7440.	232.0	8.0	.3661	.300	.500	.300	.400	3.90	.50	.00024	5
182	183	16000.	599.0	6.0	.1690	.300	.500	.300	.450	4.50	.60	.00010	5
180	181	13280.	439.0	6.0	.2725	.300	.500	.300	.450	4.50	.60	.00010	5

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183	184	7080.	217.0	6.0	.2820	.300	.500	.300	.400	3.90	.50	.00024	5
181	182	9200.	507.0	7.0	.2836	.300	.500	.300	.450	4.50	.60	.00010	5
179	180	9040.	501.0	5.0	.2840	.250	.450	.300	.500	3.50	.20	.00100	4
204	204	13440.	854.0	30.0	.3985	.300	.500	.300	.470	3.90	.50	.00024	5
203	203	7000.	258.0	25.0	.4793	.300	.500	.300	.470	3.90	.50	.00024	5
199	201	15400.	843.0	5.0	.3343	.300	.500	.300	.470	4.50	.60	.00010	5
198	200	14440.	542.0	5.0	.2842	.300	.500	.300	.450	3.90	.50	.00024	5
200	202	7640.	250.0	5.0	.2900	.300	.500	.300	.500	4.80	.50	.00010	5
196	198	14440.	797.0	5.0	.4198	.250	.450	.300	.450	3.90	.50	.00024	5
195	196	14640.	387.0	5.0	.2370	.250	.450	.300	.500	4.50	.60	.00010	5
197	199	18040.	634.0	5.0	.2744	.250	.450	.300	.450	3.90	.50	.00024	5
190	195	9520.	251.0	5.0	.2833	.250	.450	.300	.470	3.90	.50	.00024	5
189	194	15120.	847.0	9.0	.3487	.150	.400	.300	.500	4.50	.50	.00010	4
208	208	8520.	275.0	5.0	.3120	.250	.450	.300	.450	3.90	.50	.00024	5
207	207	8560.	772.0	6.0	.4592	.150	.400	.300	.430	3.50	.20	.00100	5
206	206	7720.	250.0	5.0	.3693	.250	.450	.300	.470	3.90	.50	.00024	5
205	205	9800.	395.0	7.0	.4113	.150	.400	.300	.450	3.90	.50	.00024	4
187	192	1540.	115.0	6.0	.5495	.150	.400	.300	.430	3.50	.20	.00100	4
188	193	8960.	273.0	9.0	.3629	.150	.400	.300	.400	3.50	.20	.00100	4
186	187	19200.	1018.0	8.0	.3200	.150	.400	.300	.450	3.90	.50	.00024	4
177	178	13000.	392.0	7.0	.2685	.150	.400	.300	.450	3.90	.50	.00024	5
178	179	7720.	211.0	5.0	.3191	.250	.450	.300	.420	3.50	.20	.00100	5
175	176	15040.	716.0	5.0	.3492	.250	.450	.300	.400	3.50	.20	.00100	4
176	177	12040.	233.0	6.0	.2396	.250	.450	.300	.450	3.90	.50	.00024	4
174	175	3800.	78.0	5.0	.2684	.250	.450	.300	.450	3.90	.50	.00024	4
173	174	8120.	188.0	8.0	.3071	.150	.400	.300	.430	3.90	.50	.00024	4
172	173	11520.	230.0	5.0	.3401	.250	.450	.300	.400	3.50	.20	.00100	4
171	172	3720.	73.0	7.0	.2083	.150	.400	.300	.450	3.90	.50	.00024	4
167	168	7240.	259.0	5.0	.2386	.300	.500	.300	.500	3.90	.50	.00024	5
168	169	6280.	175.0	5.0	.2720	.300	.500	.300	.500	3.90	.50	.00024	5
164	165	13840.	350.0	6.0	.3519	.300	.500	.300	.470	3.90	.50	.00024	4
166	167	10720.	215.0	6.0	.3188	.300	.500	.300	.500	3.90	.50	.00024	4
165	166	1040.	99.0	5.0	.2782	.300	.500	.300	.500	3.90	.50	.00024	4
170	171	8840.	139.0	5.0	.2244	.250	.450	.300	.400	3.50	.20	.00100	4
169	170	9680.	332.0	5.0	.2538	.250	.450	.300	.400	3.50	.20	.00100	4
162	163	5280.	112.0	5.0	.2935	.250	.450	.300	.470	3.90	.50	.00100	4
163	164	8000.	76.0	5.0	.3938	.300	.500	.300	.450	3.90	.50	.00024	4
156	157	1660.	103.0	7.0	.3821	.250	.450	.300	.460	3.50	.20	.00100	4
160	161	8760.	341.0	5.0	.3148	.300	.500	.300	.470	3.90	.50	.00100	4
161	162	11600.	362.0	5.0	.3269	.300	.500	.300	.470	3.90	.50	.00100	5
158	159	12760.	476.0	5.0	.2852	.300	.500	.300	.470	3.90	.50	.00100	5
159	160	6720.	342.0	6.0	.3021	.300	.500	.300	.470	3.90	.50	.00100	4
155	156	9960.	523.0	6.0	.3280	.250	.450	.300	.400	3.90	.50	.00024	4
157	158	11400.	344.0	5.0	.2728	.250	.450	.300	.460	3.90	.50	.00024	4
152	153	8760.	249.0	5.0	.2831	.300	.500	.300	.500	3.90	.50	.00024	4
153	154	5760.	249.0	6.0	.3299	.250	.450	.300	.450	3.90	.50	.00024	4
154	155	2180.	161.0	5.0	.3792	.300	.500	.300	.400	3.50	.20	.00100	4
148	149	6440.	214.0	6.0	.3001	.250	.450	.300	.400	3.50	.20	.00100	4
149	150	5560.	58.0	6.0	.1610	.250	.450	.300	.400	3.50	.20	.00100	4
150	151	8240.	189.0	5.0	.2338	.250	.450	.300	.400	3.50	.20	.00100	4
151	152	13960.	501.0	8.0	.3572	.250	.450	.300	.450	3.90	.50	.00024	4
145	146	6930.	318.0	5.0	.2782	.300	.500	.300	.460	3.90	.50	.00024	4
146	147	11200.	283.0	5.0	.2727	.250	.450	.300	.500	3.90	.50	.00024	4
147	148	5440.	453.0	5.0	.3306	.250	.450	.300	.470	3.90	.50	.00024	4
141	142	4160.	103.0	6.0	.2843	.250	.450	.300	.450	3.90	.50	.00024	4
142	143	9680.	187.0	5.0	.3565	.250	.450	.300	.470	3.90	.50	.00024	4
143	144	4400.	274.0	5.0	.3218	.300	.500	.300	.460	3.90	.50	.00024	4
144	145	4320.	79.0	5.0	.2164	.300	.500	.300	.500	3.90	.50	.00024	4
139	140	8640.	184.0	6.0	.3125	.250	.450	.300	.460	3.90	.50	.00024	4
140	141	7600.	132.0	5.0	.2104	.250	.450	.300	.450	3.50	.20	.00100	4
136	137	6200.	142.0	15.0	.2104	.150	.400	.150	.470	3.50	.20	.00100	4
137	138	8780.	383.0	10.0	.0823	.150	.400	.150	.420	3.50	.20	.00100	4
138	139	3760.	70.0	15.0	.1898	.250	.450	.150	.450	3.90	.50	.00024	4
133	134	20040.	530.0	8.0	.3229	.250	.450	.300	.460	3.90	.50	.00024	4
134	135	8160.	160.0	5.0	.2440	.250	.450	.300	.450	3.90	.50	.00024	5
135	136	6000.	282.0	5.0	.2300	.250	.450	.300	.460	3.90	.50	.00024	5
130	131	9720.	290.0	12.0	.3042	.150	.400	.150	.500	3.90	.50	.00024	4
131	132	9120.	213.0	8.0	.1964	.250	.450	.300	.470	3.90	.50	.00024	4
132	133	15440.	496.0	7.0	.1806	.250	.450	.300	.470	3.90	.50	.00024	4
128	129	7040.	151.0	12.0	.5988	.300	.500	.200	.450	3.90	.50	.00024	4
129	130	6720.	110.0	15.0	.2077	.150	.400	.150	.450	3.90	.50	.00024	4
124	125	7600.	220.0	5.0	.1948	.300	.500	.300	.500	3.90	.50	.00024	4
125	126	6840.	88.0	5.0	.2679	.300	.500	.300	.500	3.90	.50	.00024	4
126	127	16000.	548.0	8.0	.2341	.250	.450	.300	.460	3.90	.50	.00024	4
120	124	15040.	397.0	13.0	.1127	.150	.400	.150	.500	3.90	.50	.00024	4
127	128	17320.	472.0	8.0	.2160	.250	.450	.300	.470	3.90	.50	.00024	4
118	122	18880.	481.0	8.0	.2138	.150	.400	.200	.450	3.90	.50	.00024	4
119	123	8320.	389.0	12.0	.1613	.150	.400	.200	.450	3.90	.50	.00024	4
113	116	19040.	702.0	5.0	.1137	.300	.500	.300	.500	3.90	.50	.00024	4
93	96	12640.	579.0	5.0	.2560	.250	.450	.300	.460	3.90	.50	.00024	4
230	95	8000.	200.0	5.0	.2312	.250	.450	.300	.450	3.90	.50	.00024	4
88	85	3840.	118.0	5.0	.2369	.250	.450	.300	.400	3.90	.50	.00024	4
89	86	11760.	331.0	5.0	.2521	.250	.450	.300	.400	3.90	.50	.00024	4
90	87	16080.	655.0	5.0	.1364	.250	.450	.300	.400	3.50	.20	.00100	4
84	81	12440.	303.0	5.0	.2148	.250	.450	.300	.400	3.50	.20	.00100	4
85	82	2220.	96.0	5.0	.1143	.250	.450	.300	.400	3.50	.20	.00100	4
86	83	4760.	197.0	5.0	.1438	.250	.450	.300	.400	3.90	.50	.00024	4
87	84	5440.	106.0	5.0	.1919	.250	.450	.300	.400	3.90	.50	.00024	4
83	80	31300.	862.0	9.0	.1050	.150	.400	.200	.400	3.50	.20	.00100	4
74	121	9400.	326.0	6.0	.1923	.150	.400	.200	.400	3.50	.20	.00024	4
70	79	16040.	633.0	7.0	.1589	.250	.450	.300	.400	3.50	.20	.00100	4
61	75	3200.	62.0	5.0	.3363	.250	.450	.300	.400	3.90	.50	.00024	4
63	76	12840.	379.0	8.0	.1972	.250	.450	.300	.400	3.50	.20	.00100	4
65	77	4040.	66.0	8.0	.2100	.250	.450	.300	.430	3.90	.50	.00024	4
66	78	7560.	256.0	5.0	.1250	.250	.450	.300	.450	3.90	.50	.00024	4
58	74	9400.	411.0	8.0	.3384	.250	.450	.300	.400	3.50	.20	.00100	4
228	89	8480.	319.0	8.0	.1659	.150	.400	.150	.450	3.50	.20	.00100	4
229	93	4880.	111.0	5.0	.2059	.250	.450	.300	.450	4.50	.60	.00010	4
91	88	16520.	352.0	6.0	.1576	.250	.450	.300	.450	3.90	.50	.00024	4
114	117	12000.	390.0	15.0	.1571	.150	.400	.150	.430	3.90	.50	.00024	4
115	118	16440.	453.0	6.0	.1736	.250	.450	.300	.460	3.90	.50	.00024	4

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116	119	2600.	34.0	15.0	.1472	.150	.400	.150	.500	3.90	.50	.00024	4
117	120	7960.	220.0	15.0	.1331	.150	.400	.150	.470	3.90	.50	.00024	4
101	104	6880.	205.0	15.0	.1564	.150	.400	.150	.450	3.50	.20	.00100	4
102	105	9120.	343.0	10.0	.1175	.150	.400	.150	.500	3.90	.50	.00024	4
103	106	12760.	273.0	8.0	.1121	.250	.450	.300	.500	3.90	.50	.00024	4
99	102	10440.	314.0	10.0	.1275	.150	.400	.150	.480	3.90	.50	.00024	4
100	103	8170.	150.0	8.0	.1343	.150	.400	.150	.450	3.90	.50	.00100	4
109	112	7280.	208.0	7.0	.4086	.250	.450	.300	.470	3.90	.50	.00024	4
110	113	10120.	209.0	7.0	.2899	.250	.450	.300	.500	3.90	.50	.00024	4
111	114	9000.	230.0	5.0	.2973	.300	.500	.300	.470	3.90	.50	.00024	5
112	115	6480.	102.0	6.0	.4123	.250	.450	.300	.460	3.90	.50	.00024	4
107	110	4140.	399.0	8.0	.3550	.250	.450	.300	.470	3.90	.50	.00024	4
105	108	12480.	202.0	5.0	.3863	.300	.500	.300	.470	3.90	.50	.00024	4
106	109	5520.	216.0	7.0	.1680	.250	.450	.300	.500	3.90	.50	.00024	4
108	111	11200.	199.0	5.0	.4732	.300	.500	.300	.460	3.90	.50	.00024	4
104	107	5440.	106.0	8.0	.2557	.250	.450	.300	.480	3.90	.50	.00024	4
97	100	19960.	458.0	7.0	.5159	.250	.450	.300	.480	3.50	.20	.00100	4
95	98	14000.	309.0	18.0	.1544	.250	.450	.200	.470	3.50	.20	.00100	4
96	99	2880.	55.0	10.0	.3003	.250	.450	.300	.480	3.50	.20	.00100	4
98	101	1380.	82.0	8.0	.1629	.250	.450	.200	.470	3.50	.20	.00100	4
94	97	11440.	472.0	8.0	.3012	.250	.450	.300	.470	3.90	.50	.00024	4
92	94	5120.	475.0	7.0	.1426	.250	.450	.300	.500	3.90	.50	.00024	4
56	72	8960.	197.0	7.0	.1792	.150	.400	.150	.420	3.50	.20	.00100	4
57	73	16000.	636.0	8.0	.1300	.150	.400	.150	.440	3.90	.50	.00024	4
55	71	9640.	261.0	7.0	.1967	.250	.450	.300	.470	3.50	.20	.00100	4
43	59	8040.	296.0	9.0	.1912	.150	.400	.150	.400	3.90	.50	.00024	4
47	63	7960.	234.0	6.0	.4083	.250	.450	.300	.470	3.90	.50	.00024	4
48	64	7480.	258.0	6.0	.3750	.250	.450	.300	.500	3.90	.50	.00024	4
45	61	15000.	552.0	8.0	.2077	.250	.450	.200	.470	3.50	.20	.00100	4
42	46	6440.	197.0	7.0	.3799	.250	.450	.200	.400	3.50	.20	.00100	4
44	60	8160.	225.0	7.0	.2515	.250	.450	.200	.470	3.50	.20	.00100	4
46	62	2800.	39.0	5.0	.3963	.250	.450	.300	.470	3.50	.20	.00100	4
50	66	6120.	108.0	6.0	.4444	.250	.450	.300	.500	3.90	.50	.00024	4
51	67	13240.	636.0	7.0	.3651	.250	.450	.300	.470	3.50	.20	.00100	4
53	69	7480.	197.0	12.0	.2552	.150	.400	.150	.470	3.50	.20	.00100	4
54	70	13920.	246.0	12.0	.2827	.150	.400	.150	.420	3.50	.20	.00100	4
49	65	7920.	212.0	5.0	.3375	.250	.450	.300	.480	3.90	.50	.00024	4
52	68	4240.	80.0	7.0	.3917	.250	.450	.300	.500	3.50	.20	.00100	4
41	42	15160.	593.0	8.0	.4922	.250	.450	.200	.450	3.90	.50	.00024	4
39	40	13160.	356.0	20.0	.4570	.250	.450	.100	.450	3.90	.50	.00024	4
40	41	6200.	205.0	9.0	.5172	.250	.450	.200	.500	3.50	.20	.00100	4
18	18	15200.	565.0	7.0	.3792	.250	.450	.200	.420	3.50	.20	.00100	4
19	20	10680.	606.0	9.0	.1670	.150	.400	.150	.470	3.90	.50	.00024	4
20	21	13920.	379.0	6.0	.3275	.250	.450	.300	.400	3.90	.50	.00024	4
14	14	6160.	132.0	25.0	.4006	.250	.450	.100	.500	3.50	.20	.00100	3
15	15	3000.	36.0	25.0	.3169	.250	.450	.100	.450	3.50	.20	.00100	3
16	16	3840.	117.0	25.0	.2094	.250	.450	.100	.400	3.50	.20	.00100	3
17	17	5640.	156.0	20.0	.3423	.250	.450	.100	.400	3.50	.20	.00100	3
8	8	14200.	1227.0	67.0	.2919	.250	.450	.050	.450	3.50	.20	.00100	3
37	38	5060.	368.0	7.0	.2400	.250	.450	.200	.420	3.90	.50	.00024	4
38	39	10280.	290.0	7.0	.3153	.250	.450	.300	.420	3.50	.20	.00100	4
36	37	16320.	466.0	5.0	.1439	.250	.450	.300	.480	3.90	.50	.00024	4
33	34	13680.	445.0	8.0	.1186	.150	.400	.200	.410	3.90	.50	.00024	4
34	35	6280.	148.0	7.0	.2940	.250	.450	.300	.420	3.50	.20	.00100	4
35	36	10680.	251.0	6.0	.1368	.250	.450	.300	.400	3.50	.20	.00100	4
31	32	6520.	144.0	6.0	.2938	.250	.450	.300	.420	3.90	.50	.00024	4
32	33	10360.	257.0	12.0	.1275	.150	.400	.150	.420	3.50	.20	.00100	4
30	31	5440.	107.0	7.0	.2363	.150	.400	.150	.450	4.50	.60	.00010	5
22	23	9840.	195.0	8.0	.1920	.250	.450	.200	.460	3.50	.20	.00100	5
29	30	11560.	546.0	12.0	.0980	.150	.400	.150	.450	3.50	.20	.00100	5
26	27	5080.	107.0	5.0	.2510	.250	.450	.300	.450	3.90	.50	.00024	5
27	28	5040.	300.0	9.0	.1461	.150	.400	.150	.430	3.90	.50	.00024	5
28	29	6120.	152.0	7.0	.2020	.150	.400	.150	.450	3.50	.20	.00100	5
24	25	5920.	363.0	9.0	.3292	.250	.450	.300	.450	3.50	.20	.00100	5
25	26	3720.	94.0	8.0	.1772	.150	.400	.150	.450	3.50	.20	.00100	5
23	24	1740.	104.0	7.0	.1530	.250	.450	.300	.450	3.50	.20	.00100	5
21	22	12000.	447.0	20.0	.2822	.150	.400	.200	.400	3.50	.20	.00100	5
9	9	20640.	411.0	8.0	.2894	.250	.450	.300	.470	3.90	.50	.00024	5
10	10	7520.	202.0	6.0	.3773	.250	.450	.300	.480	3.90	.50	.00024	5
7	7	9880.	373.0	7.0	.2911	.300	.500	.300	.500	3.90	.50	.00024	5
3	3	22000.	929.0	8.0	.3243	.250	.450	.200	.450	3.50	.20	.00100	5
4	4	25560.	960.0	8.0	.2675	.250	.450	.200	.500	3.50	.20	.00100	5
2	2	14480.	519.0	7.0	.4504	.300	.500	.300	.420	3.50	.20	.00100	5
6	6	16100.	296.0	10.0	.4790	.300	.500	.300	.450	3.50	.20	.00100	5
5	5	18300.	336.0	6.0	.2506	.300	.500	.300	.420	5.00	.60	.00006	5
1	1	30900.	567.0	7.0	.5000	.300	.500	.300	.420	3.50	.20	.00100	5
11	11	6000.	113.0	25.0	.3243	.250	.450	.200	.500	3.90	.50	.00024	5
12	12	8360.	159.0	6.0	.3715	.300	.500	.300	.500	3.90	.50	.00024	5
13	13	10480.	229.0	7.0	.3542	.300	.500	.300	.500	3.90	.50	.00024	5
256	247	39100.	808.0	7.0	.1652	.250	.450	.200	.450	3.50	.20	.00100	5
257	248	31200.	645.0	8.0	.2217	.250	.450	.200	.450	3.50	.20	.00100	5
258	249	18300.	377.0	7.0	.1984	.250	.450	.300	.420	3.50	.20	.00100	5
259	250	5300.	109.0	5.0	.1627	.250	.450	.300	.450	4.80	.50	.00010	5
253	244	36900.	848.0	50.0	.2354	.300	.500	.300	.350	3.90	.50	.00024	5
254	245	7300.	100.0	7.0	.2934	.250	.450	.200	.450	3.50	.20	.00100	5
255	246	21800.	450.0	8.0	.2396	.250	.450	.300	.450	3.50	.20	.00100	5
76	54	10300.	213.0	8.0	.3735	.300	.500	.300	.500	5.00	.60	.00006	5
77	55	25900.	297.0	7.0	.4316	.300	.500	.300	.500	5.00	.60	.00006	5
75	53	2400.	26.0	6.0	.4875	.300	.500	.300	.460	3.50	.20	.00024	5
73	52	38400.	441.0	18.0	.3662	.300	.500	.300	.400	3.50	.20	.00100	5
82	51	19700.	362.0	25.0	.3938	.250	.450	.300	.400	3.50	.20	.00100	5
71	50	11300.	207.0	25.0	.4627	.300	.500	.400	.450	3.50	.20	.00100	5
80	58	12000.	220.0	6.0	.3854	.300	.500	.300	.480	5.00	.60	.00006	5
81	57	42200.	776.0	8.0	.5226	.250	.450	.200	.470	4.50	.60	.00010	5
78	56	22000.	404.0	18.0	.4013	.250	.450	.300	.500	4.80	.50	.00010	5
79	56	21400.	442.0	15.0	.3303	.300	.500	.300	.450	4.50	.60	.00010	5
72	49	16000.	220.0	35.0	.5698	.300	.500	.300	.500	4.50	.50	.00010	5
69	48	9400.	391.0	35.0	.2301	.250	.450	.300	.400	3.90	.50	.00024	5
1635	1635	12865.	317.0	12.0	.3700	.300	.500	.300	.450	3.50	.20	.00100	5
1645	1645	5640.	126.0	5.0	.2900	.250	.450	.150	.450	3.50	.20	.00100	5
1640	1640	8667.	200.0	10.0	.2900	.300	.320	.450	.450	3.50	.20	.00100	5

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1630	1630	8660.	159.0	6.0	.1300	.400	.450	.150	.450	3.50	.20	.00100	2
1625	1625	10700.	197.0	9.0	.2100	.200	.400	.150	.450	3.50	.20	.00100	1
1610	1610	6780.	109.0	9.0	.0200	.200	.400	.150	.450	4.80	.50	.00010	1
1665	1665	14692.	390.0	35.0	.2870	.200	.400	.150	.450	3.50	.20	.00100	2
1605	1605	7689.	81.0	6.0	.1100	.200	.400	.150	.450	4.80	.50	.00010	1
1660	1660	23764.	552.0	7.0	.2000	.200	.450	.150	.460	3.90	.50	.00024	2
1650	1650	13676.	382.0	7.0	.2300	.200	.200	.150	.450	3.50	.20	.00100	2
1655	1655	22832.	558.0	6.0	.1600	.200	.450	.150	.460	3.50	.20	.00100	2
1620	1620	17977.	324.0	7.0	.0500	.200	.400	.150	.470	4.80	.50	.00010	2
1615	1615	11967.	228.0	7.0	.1200	.200	.400	.150	.470	4.50	.60	.00010	2
1710	1710	9974.	245.0	5.0	.0100	.200	.400	.150	.350	3.90	.50	.00024	1
1600	1600	3273.	25.0	7.0	.0500	.200	.450	.150	.600	5.00	.70	.00002	1
1705	1705	2245.	67.0	5.0	.0100	.200	.400	.150	.350	3.90	.50	.00024	2
1450	1450	4800.	198.0	5.0	.0200	.150	.450	.150	.600	3.90	.50	.00024	1
1445	1445	6714.	164.0	5.0	.0800	.200	.400	.150	.350	5.00	.60	.00006	1
1440	1440	12663.	66.0	7.0	.0100	.150	.450	.150	.600	3.90	.50	.00024	1
1480	1938	34034.	732.0	35.0	.0200	.200	.400	.150	.300	3.90	.50	.00024	1
1435	1435	6984.	232.0	5.0	.0800	.200	.400	.150	.460	5.00	.60	.00006	1
1430	1430	6338.	82.0	5.0	.0700	.200	.400	.150	.460	5.00	.60	.00006	1
1425	1425	4940.	68.0	6.0	.0400	.200	.400	.150	.600	5.00	.70	.00002	1
1420	1420	26178.	59.0	9.0	.0220	.200	.450	.150	.600	3.90	.50	.00024	1
1570	1570	3089.	171.0	6.0	.3540	.200	.450	.150	.450	3.50	.20	.00100	2
1555	1555	7055.	83.0	7.0	.1300	.200	.450	.150	.450	4.80	.50	.00010	1
1565	1565	4112.	95.0	9.0	.3200	.200	.450	.150	.470	3.50	.20	.00100	2
1560	1560	5353.	123.0	8.0	.4400	.200	.450	.150	.450	3.50	.20	.00100	2
1550	1550	20321.	424.0	7.0	.0700	.200	.400	.150	.450	3.50	.20	.00100	1
1415	1415	5148.	307.0	5.0	.0260	.200	.400	.150	.500	3.90	.50	.00024	1
1410	1410	5300.	195.0	5.0	.0100	.150	.450	.150	.500	3.90	.50	.00024	1
1455	1455	19899.	542.0	11.0	.0037	.200	.400	.150	.350	4.80	.50	.00010	1
1490	1490	8100.	698.0	10.0	.0620	.200	.400	.150	.350	4.50	.50	.00010	1
1465	1465	19569.	93.0	10.0	.0348	.150	.350	.150	.350	4.50	.60	.00010	1
1460	1460	12745.	286.0	9.0	.0603	.200	.400	.150	.350	5.00	.60	.00006	1
1575	1575	10554.	222.0	10.0	.4060	.200	.450	.150	.450	3.50	.20	.00100	2
1545	1545	15603.	253.0	7.0	.0890	.200	.400	.150	.450	4.80	.50	.00010	1
1530	1530	8269.	345.0	6.0	.1080	.200	.400	.150	.350	4.80	.50	.00010	1
1525	1525	14343.	53.0	10.0	.0200	.150	.400	.150	.350	3.90	.50	.00024	1
1505	1505	49306.	262.0	10.0	.0100	.150	.450	.150	.350	3.50	.20	.00100	1
1520	1520	21460.	99.0	10.0	.0100	.200	.450	.150	.350	3.50	.20	.00100	1
1715	1715	3131.	115.0	7.0	.1200	.150	.400	.150	.350	3.90	.50	.00024	1
1515	1515	3666.	8.0	60.0	.0200	.150	.400	.150	.350	3.50	.20	.00100	1
1540	1541	19881.	345.0	15.0	.0300	.200	.400	.150	.350	4.50	.60	.00010	1
1510	1510	16588.	76.0	3.0	.0100	.150	.400	.150	.350	3.90	.50	.00024	1
1500	1500	21483.	465.0	10.0	.0400	.200	.400	.150	.250	3.90	.50	.00024	1
299	299	20092.	72.0	40.0	.1300	.150	.500	.150	.350	4.80	.50	.00010	1
301	301	38137.	177.0	31.0	.1600	.150	.500	.150	.350	4.80	.50	.00010	1
297	297	84806.	338.0	40.0	.1200	.150	.500	.150	.350	4.80	.50	.00010	1
305	1917	1795.	103.0	10.0	.0240	.150	.350	.150	.250	3.90	.50	.00024	1
304	304	2970.	150.0	10.0	.0240	.150	.350	.150	.250	3.90	.50	.00024	1
262	262	3964.	39.0	5.0	.0200	.200	.400	.150	.250	3.90	.50	.00024	1
264	264	1734.	26.0	5.0	.0200	.200	.400	.150	.250	3.90	.50	.00024	1
243	243	46293.	82.0	7.0	.0200	.200	.350	.150	.350	3.90	.50	.00024	1
384	384	27915.	77.0	45.0	.0900	.150	.500	.150	.350	4.80	.50	.00010	1
290	290	4748.	29.0	5.0	.0250	.300	.400	.150	.400	3.90	.50	.00024	1
353	353	12867.	41.0	50.0	.0700	.150	.500	.150	.350	5.00	.60	.00006	1
350	350	13939.	51.0	70.0	.0550	.150	.400	.150	.350	4.80	.50	.00010	1
351	351	17043.	59.0	70.0	.0600	.150	.450	.150	.350	5.00	.60	.00006	1
376	376	1390.	3.0	10.0	.0100	.150	.450	.150	.350	4.80	.50	.00010	1
368	368	7225.	99.0	50.0	.0070	.150	.450	.150	.350	3.90	.50	.00024	1
361	361	6400.	30.0	60.0	.0060	.150	.450	.150	.350	3.90	.50	.00024	1
369	369	7449.	17.0	60.0	.0400	.150	.450	.150	.350	4.80	.50	.00010	1
354	1818	6316.	6.0	95.0	.0400	.150	.350	.150	.250	4.80	.50	.00010	1
355	355	9583.	7.0	65.0	.0400	.150	.350	.150	.250	4.80	.50	.00010	1
363	363	9583.	7.0	33.0	.0550	.150	.350	.150	.250	4.80	.50	.00010	1
366	366	26706.	81.0	45.0	.0550	.150	.500	.150	.350	4.80	.50	.00010	1
367	367	9047.	23.0	65.0	.0450	.150	.500	.150	.350	4.80	.50	.00010	1
373	373	4140.	38.0	6.0	.0200	.150	.400	.150	.350	4.80	.50	.00010	1
241	241	45665.	343.0	45.0	.0200	.150	.400	.150	.450	3.90	.50	.00024	1
346	346	21083.	71.0	40.0	.0600	.150	.450	.150	.350	3.90	.50	.00024	1
345	345	20528.	78.0	50.0	.0600	.150	.450	.150	.350	4.80	.50	.00010	1
349	349	1951.	13.0	15.0	.0200	.150	.450	.150	.350	4.80	.50	.00010	1
347	347	11476.	55.0	65.0	.0500	.150	.400	.150	.350	4.80	.50	.00010	1
371	371	12050.	83.0	50.0	.0500	.150	.450	.150	.250	4.80	.50	.00010	1
338	338	14259.	73.0	8.0	.0250	.150	.350	.150	.250	3.90	.50	.00024	1
333	333	6300.	5.0	60.0	.0400	.200	.450	.150	.550	3.50	.20	.00100	1
334	334	6300.	5.0	60.0	.0400	.150	.350	.150	.250	3.50	.20	.00100	1
240	240	2500.	46.0	25.0	.1100	.150	.450	.150	.600	3.90	.50	.00024	1
318	318	20255.	157.0	20.0	.0300	.150	.550	.150	.500	3.90	.50	.00024	1
335	335	8868.	36.0	45.0	.0500	.150	.450	.150	.450	3.90	.50	.00024	1
336	1329	10002.	31.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
337	337	14520.	50.0	50.0	.0350	.150	.450	.150	.450	3.90	.50	.00024	1
312	312	7094.	12.0	70.0	.0400	.150	.450	.150	.250	3.90	.50	.00024	1
315	315	8712.	28.0	45.0	.0400	.150	.450	.150	.450	3.90	.50	.00024	1
316	316	12777.	43.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
358	358	4084.	12.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
320	320	22099.	161.0	50.0	.0250	.250	.450	.250	.600	3.90	.50	.00024	1
1323	1323	2406.	9.0	50.0	.0080	.150	.450	.150	.450	3.90	.50	.00024	1
321	321	47509.	25.0	60.0	.0450	.150	.450	.150	.350	3.90	.50	.00024	1
319	319	43000.	164.0	70.0	.0250	.150	.400	.150	.250	3.90	.50	.00024	1
370	370	14400.	41.0	70.0	.0250	.150	.400	.150	.250	3.90	.50	.00024	1
233	233	42776.	281.0	25.0	.0500	.150	.500	.150	.500	3.90	.50	.00024	1
235	235	20400.	187.0	20.0	.1100	.150	.500	.150	.500	3.90	.50	.00024	1
231	231	58487.	390.0	55.0	.0200	.150	.400	.150	.250	3.90	.50	.00024	1

OTOTAL NUMBER OF SUBCATCHMENTS, 314
 OTOTAL TRIBUTARY AREA (ACRES), 86852.00
 1

SBC CHANGES FROM DRAFT REPORT MODEL SBC_IN.SWI - ASSORTED MODIFICATIONS
 model sbct_ltc.swi with narrowing of conveyance 1330 overflow channel from 50' to

sbc_ltd.wpd July 12, 2000 100-YR SWMM MODEL

*** CONTINUITY CHECK FOR SUBCATCHMENT ROUTING IN UDSWM386 MODEL ***

WATERSHED AREA (ACRES) 86852.000
 TOTAL RAINFALL (INCHES) 4.002
 TOTAL INFILTRATION (INCHES) 2.881
 TOTAL WATERSHED OUTFLOW (INCHES) 1.094
 TOTAL SURFACE STORAGE AT END OF STORM (INCHES) .028
 ERROR IN CONTINUITY, PERCENTAGE OF RAINFALL -.023

SBC CHANGES FROM DRAFT REPORT MODEL SBC_IN.SWI - ASSORTED MODIFICATIONS
 model sbc_ltc.swi with narrowing of conveyance 1330 overflow channel from 50' to

GUTTER NUMBER	GUTTER CONNECTION	NDP	NP		WIDTH OR DIAM (FT)	LENGTH (FT)	INVERT SLOPE (FT/FT)	SIDE SLOPES		MANNING N	OVERBANK/SURCHAPGE DEPTH (FT)	JK
								HORIZ L	TO VERT R			
226	224	0	1	CHANNEL	20.0	3740.	.1337	4.0	4.0	.040	15.00	0
225	224	0	1	CHANNEL	5.0	1862.	.0600	10.0	10.0	.045	15.00	0
224	222	0	1	CHANNEL	4.0	4220.	.1300	3.0	3.0	.055	15.00	0
223	222	0	1	CHANNEL	10.0	5960.	.1406	10.0	10.0	.040	15.00	0
222	218	0	1	CHANNEL	5.0	2280.	.1000	4.0	4.0	.055	15.00	0
221	218	0	1	CHANNEL	5.0	6520.	.1992	5.0	5.0	.055	15.00	0
220	219	0	1	CHANNEL	8.0	7580.	.2107	7.0	7.0	.050	15.00	0
218	219	0	1	CHANNEL	5.0	1660.	.0900	4.0	4.0	.055	15.00	0
219	215	0	1	CHANNEL	10.0	2531.	.1000	7.0	7.0	.055	15.00	0
216	215	0	1	CHANNEL	20.0	8160.	.1875	10.0	10.0	.055	15.00	0
214	212	0	1	CHANNEL	10.0	6880.	.1727	10.0	10.0	.055	15.00	0
213	212	0	1	CHANNEL	10.0	5900.	.1268	10.0	10.0	.055	15.00	0
212	211	0	1	CHANNEL	15.0	6100.	.1511	7.0	7.0	.060	15.00	0
215	211	0	4	CHANNEL	10.0	5210.	.0600	4.0	4.0	.050	2.00	0
				OVERFLOW	50.0	5210.	.0600	6.0	6.0	.055	25.00	0
217	215	0	1	CHANNEL	20.0	4860.	.3560	5.0	5.0	.040	15.00	0
211	207	0	4	CHANNEL	8.0	2390.	.0500	3.0	3.0	.050	2.00	0
				OVERFLOW	25.0	2390.	.0500	5.0	5.0	.055	25.00	0
186	184	0	1	CHANNEL	10.0	4260.	.1002	9.0	9.0	.060	15.00	0
185	184	0	1	CHANNEL	5.0	3720.	.0594	6.0	6.0	.060	15.00	0
183	182	0	1	CHANNEL	10.0	8000.	.1050	6.0	6.0	.060	15.00	0
181	180	0	1	CHANNEL	5.0	6640.	.1583	7.0	7.0	.060	15.00	0
184	182	0	1	CHANNEL	15.0	3540.	.1158	8.0	8.0	.055	15.00	0
182	180	0	4	CHANNEL	15.0	4600.	.0720	4.0	4.0	.050	2.50	0
				OVERFLOW	100.0	4370.	.0758	15.0	15.0	.055	20.00	0
180	176	0	4	CHANNEL	10.0	4520.	.0507	4.0	4.0	.045	3.00	0
				OVERFLOW	35.0	4294.	.0534	3.0	3.0	.060	20.00	0
204	201	0	1	CHANNEL	15.0	6720.	.0911	6.0	6.0	.050	15.00	0
203	201	0	1	CHANNEL	5.0	3500.	.2286	5.0	5.0	.055	15.00	0
201	198	0	4	CHANNEL	15.0	7700.	.0835	4.0	4.0	.050	3.00	0
				OVERFLOW	50.0	7315.	.0879	7.0	7.0	.060	20.00	0
200	198	0	1	CHANNEL	5.0	7220.	.1722	7.0	7.0	.055	15.00	0
202	198	0	1	CHANNEL	5.0	3820.	.1971	5.0	5.0	.060	15.00	0
198	194	0	4	CHANNEL	25.0	7220.	.0370	4.0	4.0	.050	3.00	0
				OVERFLOW	200.0	6860.	.0389	7.0	7.0	.060	20.00	0
199	194	0	1	CHANNEL	5.0	9020.	.1233	6.0	6.0	.060	15.00	0
196	194	0	1	CHANNEL	5.0	7320.	.1243	5.0	5.0	.060	15.00	0
195	194	0	1	CHANNEL	10.0	4760.	.1513	5.0	5.0	.060	15.00	0
194	192	0	4	CHANNEL	20.0	7560.	.0921	4.0	4.0	.055	3.00	0
				OVERFLOW	80.0	7182.	.0969	10.0	10.0	.060	20.00	0
208	207	0	1	CHANNEL	10.0	4260.	.2230	8.0	8.0	.060	15.00	0
207	205	0	4	CHANNEL	25.0	5000.	.0150	4.0	4.0	.040	2.00	0
				OVERFLOW	200.0	5000.	.0150	10.0	10.0	.050	25.00	0
206	205	0	1	CHANNEL	25.0	3860.	.2591	5.0	5.0	.040	15.00	0
205	192	0	4	CHANNEL	20.0	4900.	.0349	4.0	4.0	.045	3.00	0
				OVERFLOW	100.0	4900.	.0349	8.0	8.0	.055	25.00	0
192	187	0	4	CHANNEL	32.0	1540.	.0120	4.0	4.0	.040	3.00	0
				OVERFLOW	250.0	1540.	.0120	20.0	20.0	.050	25.00	0
193	187	0	1	CHANNEL	25.0	4480.	.1897	4.0	4.0	.040	15.00	0
187	172	0	4	CHANNEL	32.0	7388.	.0100	4.0	4.0	.040	3.00	0
				OVERFLOW	250.0	7388.	.0100	20.0	20.0	.050	25.00	0
178	177	0	1	CHANNEL	5.0	6500.	.1186	8.0	8.0	.060	15.00	0
177	175	0	1	CHANNEL	8.0	6020.	.0862	7.0	7.0	.055	15.00	0
179	176	0	1	CHANNEL	20.0	3860.	.2383	5.0	5.0	.045	15.00	0
176	175	0	4	CHANNEL	20.0	7520.	.0386	4.0	4.0	.045	3.00	0
				OVERFLOW	100.0	7144.	.0406	5.0	5.0	.060	20.00	0
174	173	0	1	CHANNEL	5.0	4060.	.1421	6.0	6.0	.055	15.00	0
175	173	0	4	CHANNEL	30.0	1900.	.0353	4.0	4.0	.035	3.00	0
				OVERFLOW	150.0	1805.	.0372	15.0	15.0	.045	20.00	0
173	172	0	4	CHANNEL	25.0	5760.	.0587	4.0	4.0	.035	3.00	0
				OVERFLOW	200.0	5472.	.0618	15.0	15.0	.045	20.00	0
172	157	0	4	CHANNEL	25.0	1860.	.0100	3.0	3.0	.045	3.00	0
				OVERFLOW	75.0	1860.	.0100	5.0	5.0	.050	25.00	0
168	165	0	1	CHANNEL	5.0	3620.	.1740	7.0	7.0	.060	15.00	0
169	165	0	1	CHANNEL	5.0	3140.	.1720	7.0	7.0	.060	15.00	0
165	166	0	1	CHANNEL	10.0	6920.	.1026	5.0	5.0	.060	15.00	0
167	166	0	1	CHANNEL	5.0	5360.	.1940	6.0	6.0	.060	15.00	0
166	163	0	1	CHANNEL	15.0	1040.	.0673	10.0	10.0	.055	15.00	0
164	163	0	1	CHANNEL	10.0	4000.	.1263	8.0	8.0	.050	15.00	0
163	157	0	1	CHANNEL	25.0	2640.	.0568	5.0	5.0	.050	15.00	0
170	157	0	1	CHANNEL	5.0	4840.	.1543	5.0	5.0	.055	15.00	0
171	157	0	1	CHANNEL	5.0	4420.	.1837	7.0	7.0	.055	15.00	0
157	156	0	4	CHANNEL	25.0	1660.	.0220	3.0	3.0	.045	3.00	0
				OVERFLOW	75.0	1660.	.0220	4.0	4.0	.050	25.00	0
161	160	0	1	CHANNEL	5.0	4380.	.1667	5.0	5.0	.060	15.00	0

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162	160	0	1	CHANNEL	5.0	5800.	.2121	5.0	5.0	.060	15.00	0
160	158	0	1	CHANNEL	10.0	3360.	.0908	10.0	10.0	.055	15.00	0
159	158	0	1	CHANNEL	10.0	6380.	.1293	6.0	6.0	.060	15.00	0
158	156	0	1	CHANNEL	20.0	5700.	.0619	5.0	5.0	.050	15.00	0
156	154	0	4	CHANNEL	35.0	4980.	.0190	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	4980.	.0190	3.0	3.0	.055	25.00	0
155	154	0	1	CHANNEL	12.0	2190.	.2683	4.0	4.0	.050	15.00	0
153	152	0	1	CHANNEL	12.0	4380.	.1530	4.0	4.0	.060	15.00	0
154	152	0	4	CHANNEL	35.0	2880.	.0200	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	2880.	.0200	3.0	3.0	.055	25.00	0
152	149	0	4	CHANNEL	30.0	6980.	.0150	4.0	4.0	.045	3.00	0
				OVERFLOW	200.0	6980.	.0150	5.0	5.0	.050	25.00	0
150	149	0	1	CHANNEL	5.0	2780.	.1691	4.0	4.0	.055	15.00	0
151	149	0	1	CHANNEL	6.0	4120.	.1286	4.0	4.0	.055	15.00	0
149	139	0	4	CHANNEL	35.0	3220.	.0140	4.0	4.0	.045	3.00	0
				OVERFLOW	300.0	3220.	.0140	5.0	5.0	.050	25.00	0
147	146	0	1	CHANNEL	8.0	5600.	.1625	6.0	6.0	.060	15.00	0
148	146	0	1	CHANNEL	8.0	2720.	.1048	8.0	8.0	.060	15.00	0
146	142	0	1	CHANNEL	10.0	5540.	.0727	8.0	8.0	.055	15.00	0
144	143	0	1	CHANNEL	5.0	2200.	.1568	8.0	8.0	.060	15.00	0
145	143	0	1	CHANNEL	3.0	2160.	.1574	5.0	5.0	.060	15.00	0
143	142	0	1	CHANNEL	8.0	4840.	.1184	5.0	5.0	.060	15.00	0
142	140	0	1	CHANNEL	10.0	2080.	.0514	8.0	5.0	.055	15.00	0
141	140	0	1	CHANNEL	5.0	3800.	.1237	5.0	5.0	.060	15.00	0
140	139	0	1	CHANNEL	15.0	4320.	.0505	8.0	7.0	.055	15.00	0
138	137	0	1	CHANNEL	10.0	5440.	.0432	10.0	10.0	.055	15.00	0
139	137	0	4	CHANNEL	30.0	1880.	.0160	4.0	4.0	.045	3.00	0
				OVERFLOW	200.0	1880.	.0160	5.0	5.0	.050	25.00	0
137	129	0	4	CHANNEL	30.0	2009.	.0130	4.0	4.0	.040	3.00	0
				OVERFLOW	200.0	2009.	.0130	5.0	5.0	.050	25.00	0
135	134	0	1	CHANNEL	5.0	4080.	.1716	5.0	5.0	.060	15.00	0
136	134	0	1	CHANNEL	5.0	3000.	.1433	6.0	6.0	.060	15.00	0
134	133	0	1	CHANNEL	10.0	10020.	.0868	5.0	5.0	.055	15.00	0
133	130	0	1	CHANNEL	15.0	7720.	.0505	5.0	5.0	.055	15.00	0
131	130	0	4	CHANNEL	15.0	4860.	.1008	3.0	3.0	.055	3.00	0
				OVERFLOW	100.0	4617.	.1061	10.0	10.0	.060	20.00	0
132	130	0	1	CHANNEL	8.0	4560.	.0789	6.0	6.0	.060	15.00	0
130	129	0	1	CHANNEL	25.0	3360.	.0363	7.0	7.0	.055	15.00	0
129	96	0	4	CHANNEL	30.0	3520.	.0160	3.5	3.5	.055	4.00	0
				OVERFLOW	100.0	3520.	.0160	4.0	4.0	.060	25.00	0
125	124	0	1	CHANNEL	5.0	3800.	.1842	8.0	8.0	.055	15.00	0
126	124	0	1	CHANNEL	5.0	3420.	.1871	6.0	6.0	.060	15.00	0
124	122	0	1	CHANNEL	10.0	7520.	.0535	8.0	8.0	.055	15.00	0
127	123	0	1	CHANNEL	10.0	8000.	.1056	10.0	10.0	.055	15.00	0
128	123	0	1	CHANNEL	10.0	8660.	.1236	15.0	15.0	.055	15.00	0
123	122	0	1	CHANNEL	15.0	4160.	.0317	15.0	15.0	.055	15.00	0
122	96	0	1	CHANNEL	20.0	9440.	.0607	5.0	5.0	.060	15.00	0
96	95	0	4	CHANNEL	25.0	6320.	.0170	2.0	2.0	.055	4.00	0
				OVERFLOW	50.0	6320.	.0170	2.0	2.0	.060	25.00	0
116	95	0	4	CHANNEL	5.0	9520.	.0772	3.0	3.0	.050	2.50	0
				OVERFLOW	70.0	9044.	.0813	8.0	8.0	.055	20.00	0
95	94	0	4	CHANNEL	30.0	4000.	.0120	3.0	3.0	.040	3.00	0
				OVERFLOW	150.0	4000.	.0120	5.0	5.0	.050	25.00	0
85	84	0	1	CHANNEL	5.0	2220.	.0396	4.0	4.0	.060	15.00	0
86	84	0	1	CHANNEL	8.0	5880.	.1259	4.0	4.0	.060	15.00	0
84	82	0	1	CHANNEL	10.0	2720.	.0890	10.0	10.0	.060	15.00	0
83	82	0	1	CHANNEL	10.0	2380.	.0450	12.0	12.0	.060	15.00	0
82	80	0	1	CHANNEL	20.0	2220.	.0396	12.0	12.0	.060	15.00	0
87	81	0	1	CHANNEL	10.0	8040.	.0796	5.0	5.0	.065	15.00	0
81	80	0	1	CHANNEL	15.0	6220.	.0691	7.0	7.0	.065	15.00	0
80	79	0	1	CHANNEL	20.0	6380.	.1993	10.0	10.0	.065	15.00	0
121	79	0	4	CHANNEL	8.0	4700.	.0660	4.0	4.0	.055	2.50	0
				OVERFLOW	60.0	4465.	.0695	12.0	12.0	.057	20.00	0
79	75	0	1	CHANNEL	25.0	8020.	.0212	10.0	10.0	.060	15.00	0
78	75	0	1	CHANNEL	8.0	3780.	.0688	20.0	20.0	.060	15.00	0
75	77	0	1	CHANNEL	25.0	1600.	.0188	3.0	5.0	.060	15.00	0
77	74	0	1	CHANNEL	40.0	2020.	.0198	3.0	3.0	.060	15.00	0
76	74	0	4	CHANNEL	10.0	6420.	.0779	4.0	4.0	.050	2.00	0
				OVERFLOW	60.0	6420.	.0779	8.0	8.0	.055	20.00	0
74	59	0	4	CHANNEL	30.0	4700.	.0130	4.0	4.0	.050	4.00	0
				OVERFLOW	75.0	4700.	.0130	4.0	3.0	.055	25.00	0
89	88	0	1	CHANNEL	8.0	4240.	.0217	10.0	10.0	.055	15.00	0
93	88	0	1	CHANNEL	5.0	2440.	.0984	10.0	10.0	.055	15.00	0
88	77	0	4	CHANNEL	11.0	7200.	.1380	10.0	10.0	.060	3.00	0
				OVERFLOW	100.0	7200.	.1360	50.0	50.0	.045	20.00	0
120	119	0	4	CHANNEL	5.0	3980.	.0879	3.0	3.0	.050	3.00	0
				OVERFLOW	200.0	3781.	.0925	10.0	10.0	.055	20.00	0
118	119	0	4	CHANNEL	5.0	8220.	.1095	3.0	3.0	.050	3.00	0
				OVERFLOW	150.0	7809.	.1153	10.0	10.0	.055	20.00	0
119	104	0	4	CHANNEL	5.0	1300.	.0400	3.0	3.0	.050	3.00	0
				OVERFLOW	150.0	1235.	.0421	10.0	10.0	.055	20.00	0
117	104	0	4	CHANNEL	5.0	6000.	.0587	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	5700.	.0618	10.0	10.0	.055	20.00	0
104	103	0	4	CHANNEL	10.0	3440.	.0343	3.0	3.0	.045	3.00	0
				OVERFLOW	150.0	3268.	.0361	10.0	10.0	.050	20.00	0
105	103	0	4	CHANNEL	5.0	4560.	.0811	3.0	3.0	.045	3.00	0
				OVERFLOW	100.0	4332.	.0854	10.0	10.0	.050	20.00	0
106	102	0	4	CHANNEL	5.0	6380.	.0690	3.0	3.0	.045	3.00	0
				OVERFLOW	70.0	6061.	.0726	10.0	10.0	.050	20.00	0
103	102	0	4	CHANNEL	8.0	1380.	.0362	4.0	40.0	.050	3.00	0
				OVERFLOW	68.0	1311.	.0381	25.0	25.0	.055	20.00	0
102	101	0	4	CHANNEL	11.0	5220.	.0383	8.0	8.0	.055	3.00	0
				OVERFLOW	100.0	4959.	.0403	5.0	5.0	.060	20.00	0
114	112	0	1	CHANNEL	5.0	4500.	.1467	5.0	5.0	.060	8.00	0
115	112	0	1	CHANNEL	5.0	3240.	.1759	5.0	5.0	.060	8.00	0
112	110	0	4	CHANNEL	5.0	3640.	.1745	3.0	3.0	.055	2.50	0
				OVERFLOW	40.0	3458.	.1837	10.0	8.0	.060	20.00	0
113	110	0	4	CHANNEL	5.0	5060.	.1690	3.0	3.0	.055	3.00	0
				OVERFLOW	40.0	4807.	.1779	10.0	10.0	.060	20.00	0
110	109	0	4	CHANNEL	11.0	4140.	.0531	4.0	4.0	.055	3.00	0
				OVERFLOW	60.0	3933.	.0559	5.0	5.0	.060	20.00	0

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111	109	0	4	CHANNEL	5.0	5600.	.2348	3.0	3.0	.050	2.00	0
				OVERFLOW	20.0	5320.	.2472	6.0	6.0	.055	20.00	0
108	107	0	4	CHANNEL	5.0	6240.	.1875	3.0	3.0	.050	2.00	0
				OVERFLOW	20.0	5928.	.1974	6.0	6.0	.055	20.00	0
109	107	0	4	CHANNEL	11.0	2760.	.0525	4.0	4.0	.050	3.00	0
				OVERFLOW	60.0	2622.	.0553	6.0	6.0	.055	20.00	0
107	101	0	4	CHANNEL	11.0	2720.	.0368	4.0	4.0	.050	3.00	0
				OVERFLOW	45.0	2584.	.0387	6.0	6.0	.055	20.00	0
101	99	0	4	CHANNEL	11.0	1380.	.0268	4.0	4.0	.050	3.00	0
				OVERFLOW	50.0	1311.	.0282	5.0	5.0	.055	20.00	0
100	99	0	4	CHANNEL	5.0	9980.	.1735	3.0	3.0	.050	2.00	0
				OVERFLOW	25.0	9481.	.1826	5.0	5.0	.055	20.00	0
99	97	0	4	CHANNEL	11.0	1440.	.0299	4.0	4.0	.050	3.00	0
				OVERFLOW	50.0	1368.	.0315	5.0	5.0	.055	20.00	0
98	97	0	4	CHANNEL	8.0	7000.	.1179	3.0	3.0	.050	2.00	0
				OVERFLOW	35.0	6650.	.1241	6.0	6.0	.055	20.00	0
97	94	0	4	CHANNEL	11.0	5720.	.0332	4.0	4.0	.050	2.50	0
				OVERFLOW	50.0	5434.	.0349	4.0	4.0	.055	20.00	0
94	74	0	4	CHANNEL	32.0	2560.	.0120	4.0	4.0	.040	3.50	0
				OVERFLOW	150.0	2560.	.0120	8.0	8.0	.050	25.00	0
72	71	0	1	CHANNEL	10.0	4480.	.0808	5.0	5.0	.055	15.00	0
73	71	0	1	CHANNEL	10.0	8000.	.0303	8.0	8.0	.055	15.00	0
71	59	0	1	CHANNEL	12.0	4820.	.0664	5.0	5.0	.060	15.00	0
59	46	0	4	CHANNEL	30.0	4020.	.0140	4.0	4.0	.050	4.00	0
				OVERFLOW	60.0	4020.	.0140	3.0	3.0	.055	25.00	0
63	61	0	1	CHANNEL	9.0	6420.	.0779	5.0	5.0	.070	20.00	0
64	61	0	1	CHANNEL	9.0	2020.	.0198	5.0	5.0	.070	20.00	0
61	62	0	1	CHANNEL	12.0	7500.	.0633	5.0	5.0	.070	20.00	0
60	46	0	1	CHANNEL	12.0	4080.	.1262	5.0	5.0	.060	20.00	0
46	42	0	4	CHANNEL	25.0	3220.	.0300	3.0	3.0	.055	5.00	0
				OVERFLOW	50.0	3220.	.0300	4.0	4.0	.060	25.00	0
66	65	0	1	CHANNEL	9.0	3060.	.2026	4.0	4.0	.060	15.00	0
67	65	0	4	CHANNEL	10.0	6620.	.0853	3.0	3.0	.050	4.00	0
				OVERFLOW	45.0	6289.	.0898	3.0	3.0	.060	25.00	0
65	62	0	4	CHANNEL	15.0	3960.	.0088	3.0	3.0	.050	4.00	0
				OVERFLOW	50.0	3762.	.0093	3.0	3.0	.060	25.00	0
62	42	0	1	CHANNEL	12.0	1400.	.2629	5.0	5.0	.070	20.00	0
69	68	0	1	CHANNEL	10.0	3740.	.1056	6.0	6.0	.055	15.00	0
70	68	0	1	CHANNEL	12.0	6960.	.0912	6.0	6.0	.055	15.00	0
68	42	0	1	CHANNEL	12.0	2120.	.1203	5.0	5.0	.060	15.00	0
41	40	0	1	CHANNEL	12.0	3100.	.2423	5.0	5.0	.060	20.00	0
42	40	0	4	CHANNEL	20.0	7580.	.0500	3.0	3.0	.055	4.00	0
				OVERFLOW	50.0	7580.	.0500	2.0	2.0	.060	25.00	0
40	16	0	4	CHANNEL	20.0	3000.	.0330	3.0	3.0	.055	4.00	0
				OVERFLOW	50.0	3000.	.0330	2.0	2.0	.060	25.00	0
20	18	0	1	CHANNEL	10.0	5340.	.0534	8.0	8.0	.050	15.00	0
18	17	0	4	CHANNEL	11.0	7600.	.0605	3.0	3.0	.050	3.00	0
				OVERFLOW	40.0	7220.	.0637	5.0	5.0	.055	20.00	0
21	17	0	1	CHANNEL	10.0	6960.	.1042	5.0	5.0	.060	15.00	0
17	16	0	4	CHANNEL	11.0	1000.	.0493	10.0	10.0	.040	3.00	0
				OVERFLOW	40.0	1000.	.0493	8.0	8.0	.055	20.00	0
14	15	0	1	CHANNEL	15.0	3080.	.2662	3.0	3.0	.060	15.00	0
15	8	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
16	15	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
8	397	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
397	6	14	2	PIPE	.1	1.	.0050	.0	.0	.013	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
.0 .0 207.0 170.0 415.0 476.0 833.0 1330.0 1254.0 2417.0 1677.0 3678.0												
2104.0 5078.0 2535.0 6591.0 2968.0 8200.0 3405.0 9896.0 3847.0 12853.0 4292.0 16870.0												
6098.0 37861.0 7880.0 91713.0												
38	37	0	1	CHANNEL	12.0	5060.	.1146	15.0	15.0	.050	15.00	0
39	37	0	1	CHANNEL	10.0	5140.	.0807	10.0	10.0	.050	20.00	0
37	23	0	4	CHANNEL	11.0	8160.	.0386	4.0	4.0	.050	3.00	0
				OVERFLOW	60.0	7752.	.0406	25.0	25.0	.055	20.00	0
35	34	0	1	CHANNEL	10.0	3140.	.0930	10.0	10.0	.050	15.00	0
36	34	0	1	CHANNEL	12.0	5340.	.0549	15.0	15.0	.050	15.00	0
34	23	0	4	CHANNEL	11.0	6840.	.0450	4.0	4.0	.050	3.00	0
				OVERFLOW	50.0	6498.	.0474	25.0	25.0	.055	20.00	0
32	31	0	1	CHANNEL	8.0	3260.	.0883	8.0	8.0	.055	15.00	0
33	31	0	1	CHANNEL	8.0	5180.	.0788	8.0	8.0	.055	15.00	0
31	23	0	1	CHANNEL	12.0	2720.	.0393	10.0	10.0	.055	15.00	0
23	22	0	4	CHANNEL	11.0	4920.	.0315	3.0	3.0	.050	3.00	0
				OVERFLOW	50.0	4674.	.0332	10.0	10.0	.055	20.00	0
29	28	0	1	CHANNEL	5.0	3060.	.1471	6.0	6.0	.055	15.00	0
30	28	0	1	CHANNEL	12.0	5780.	.0484	15.0	15.0	.050	15.00	0
27	26	0	1	CHANNEL	10.0	2540.	.1693	10.0	10.0	.040	15.00	0
28	26	0	4	CHANNEL	11.0	2520.	.0595	10.0	10.0	.040	3.00	0
				OVERFLOW	80.0	2394.	.0626	25.0	25.0	.045	15.00	0
25	24	0	1	CHANNEL	6.0	5920.	.1309	8.0	8.0	.050	15.00	0
26	24	0	4	CHANNEL	12.0	1860.	.0242	4.0	4.0	.050	3.00	0
				OVERFLOW	80.0	1767.	.0255	10.0	10.0	.055	15.00	0
24	22	0	4	CHANNEL	12.0	1740.	.0287	4.0	4.0	.050	3.00	0
				OVERFLOW	100.0	1653.	.0302	10.0	10.0	.055	20.00	0
22	8	0	4	CHANNEL	11.0	3600.	.0658	3.0	3.0	.050	3.00	0
				OVERFLOW	40.0	3600.	.0658	6.0	6.0	.055	20.00	0
9	7	0	4	CHANNEL	3.0	10320.	.1556	3.0	3.0	.060	2.00	0
				OVERFLOW	20.0	9804.	.1638	2.0	2.0	.080	25.00	0
10	7	0	1	CHANNEL	15.0	3760.	.1293	3.0	3.0	.040	15.00	0
7	5	0	4	CHANNEL	5.0	4940.	.0656	2.0	2.0	.060	2.50	0
				OVERFLOW	25.0	4693.	.0691	2.0	2.0	.080	20.00	0
3	2	0	1	CHANNEL	25.0	11000.	.0682	4.0	4.0	.040	15.00	0
4	2	0	1	CHANNEL	25.0	12780.	.1033	4.0	4.0	.040	15.00	0
2	1	0	4	CHANNEL	8.0	7240.	.0631	2.0	2.0	.070	3.00	0
				OVERFLOW	30.0	6878.	.0664	2.0	2.0	.080	20.00	0
6	5	0	4	CHANNEL	35.0	4840.	.0340	2.0	2.0	.055	4.00	0
				OVERFLOW	60.0	4840.	.0340	2.0	2.0	.065	25.00	0
5	1	0	4	CHANNEL	30.0	4960.	.0240	2.0	2.0	.055	4.00	0
				OVERFLOW	55.0	4960.	.0240	2.0	2.0	.065	25.00	0
1	245	0	4	CHANNEL	30.0	10240.	.0240	2.0	2.0	.055	4.00	0
				OVERFLOW	55.0	10240.	.0240	2.0	2.0	.065	25.00	0
11	13	0	1	CHANNEL	12.0	3000.	.1200	3.0	3.0	.040	15.00	0

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12	13	0	1	CHANNEL	12.0	4180.	.1340	3.0	3.0	.040	15.00	0	
13	5	0	4	CHANNEL	15.0	5240.	.1202	4.0	4.0	.040	5.00	0	
				OVERFLOW	100.0	4978.	.1265	40.0	40.0	.045	20.00	0	
248	250	0	4	CHANNEL	25.0	9340.	.0931	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	8873.	.0980	40.0	40.0	.080	20.00	0	
249	250	0	4	CHANNEL	20.0	3940.	.0964	4.0	4.0	.060	5.00	0	
				OVERFLOW	80.0	3743.	.1015	40.0	40.0	.080	20.00	0	
247	246	0	4	CHANNEL	25.0	8120.	.0924	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	7714.	.0973	40.0	40.0	.080	20.00	0	
250	246	0	4	CHANNEL	25.0	2060.	.0485	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	1957.	.0511	40.0	40.0	.090	20.00	0	
246	245	0	4	CHANNEL	25.0	4660.	.0676	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	4427.	.0712	40.0	40.0	.080	20.00	0	
244	52	0	4	CHANNEL	25.0	8700.	.0989	4.0	4.0	.070	5.00	0	
				OVERFLOW	100.0	8265.	.1041	40.0	40.0	.080	20.00	0	
245	52	0	4	CHANNEL	30.0	3060.	.0300	3.0	3.0	.070	4.00	0	
				OVERFLOW	60.0	3060.	.0300	2.0	2.0	.080	20.00	0	
54	53	0	1	CHANNEL	5.0	4000.	.1500	3.0	3.0	.060	15.00	0	
55	53	0	1	CHANNEL	5.0	5500.	.1382	3.0	3.0	.060	15.00	0	
53	52	0	1	CHANNEL	5.0	1200.	.1083	3.0	3.0	.060	15.00	0	
51	50	0	4	CHANNEL	5.0	5200.	.1327	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	4940.	.1397	40.0	40.0	.080	20.00	0	
52	50	0	4	CHANNEL	35.0	9160.	.0218	3.0	3.0	.055	4.00	0	
				OVERFLOW	65.0	9160.	.0218	2.0	2.0	.065	25.00	0	
50	48	0	4	CHANNEL	40.0	3400.	.0294	5.0	5.0	.060	4.00	0	
				OVERFLOW	150.0	3400.	.0294	75.0	75.0	.080	25.00	0	
57	56	0	4	CHANNEL	25.0	8400.	.1262	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	7980.	.1328	40.0	40.0	.080	20.00	0	
58	56	0	1	CHANNEL	5.0	2200.	.1636	3.0	3.0	.060	15.00	0	
56	50	0	4	CHANNEL	25.0	10000.	.0930	4.0	4.0	.070	5.00	0	
				OVERFLOW	100.0	9500.	.0979	40.0	40.0	.080	20.00	0	
49	48	0	1	CHANNEL	12.0	3200.	.2594	3.0	3.0	.060	8.00	0	
48	1626	0	4	CHANNEL	30.0	4700.	.0133	2.0	2.0	.070	5.00	0	
				OVERFLOW	200.0	4700.	.0133	2.0	2.0	.085	25.00	0	
1238	1927	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1927	238	0	4	CHANNEL	15.0	964.	.0012	3.5	3.5	.045	4.00	0	
				OVERFLOW	70.0	964.	.0012	7.5	5.0	.055	20.00	0	
1295	295	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
295	1296	10	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0	
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW													
		.0	.0	8.3	.5	17.8	1.0	28.1	10.5	39.4	18.2	52.5	23.5
		68.3	278.0	86.7	1321.5	107.1	5035.0	150.0	10000.0				
1296	296	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
296	1382	6	3		.0	1.	.0010	.0	.0	.001	10.00	1383	
DIVERSION TO GUTTER NUMBER1383 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	24.0	.1	278.0	250.0	1321.0	1290.0	5035.0	5000.0	10000.0	9964.0
1382	1381	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
384	1820	0	5	PIPE	3.0	4047.	.0176	.0	.0	.020	3.00	0	
				OVERFLOW	1.0	4047.	.0176	20.0	20.0	.020	50.00	0	
1820	383	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1383	1820	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
383	1405	8	3		.0	1.	.0010	.0	.0	.001	10.00	1360	
DIVERSION TO GUTTER NUMBER1360 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	150.0	1.0	223.0	23.0	285.0	75.0	426.0	201.0	1592.0	1342.0
		3953.0	3653.0	10000.0	9680.0								
1405	1381	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1381	382	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
382	381	0	5	PIPE	7.5	1142.	.0020	.0	.0	.015	7.50	0	
				OVERFLOW	7.5	1142.	.0020	20.0	20.0	.015	50.00	0	
381	1926	4	3		.0	1.	.0010	.0	.0	.001	10.00	1366	
DIVERSION TO GUTTER NUMBER1366 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	150.0	1.0	342.0	182.0	2438.0	2050.0		.016	.50	0
369	1821	0	4	CHANNEL	.5	1030.	.0089	12.0	12.0	.020	10.00	0	
				OVERFLOW	10.0	1030.	.0089	20.0	20.0	.020	10.00	0	
1926	1821	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1821	380	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
380	379	0	1	CHANNEL	8.0	754.	.0040	1.5	1.5	.050	10.00	0	
379	1406	4	3		.0	1.	.0010	.0	.0	.001	10.00	1367	
DIVERSION TO GUTTER NUMBER1367 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	180.0	.1	629.0	354.0	3656.0	3293.0				
1406	1378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1404	1378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1378	378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
378	1925	5	3		.0	1.	.0010	.0	.0	.001	10.00	1289	
DIVERSION TO GUTTER NUMBER1289 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	90.0	1.0	95.0	5.0	363.0	253.0	528.0	390.0		
1925	377	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
377	242	0	1	CHANNEL	8.0	2080.	.0040	1.5	1.5	.055	10.00	0	
1715	1716	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1716	1517	0	4	CHANNEL	10.0	3321.	.0032	6.0	6.0	.035	.50	0	
				OVERFLOW	30.0	3321.	.0032	80.0	80.0	.035	15.00	0	
1515	1517	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1517	1522	0	4	CHANNEL	4.0	851.	.0035	8.0	8.0	.035	.50	0	
				OVERFLOW	20.0	851.	.0035	60.0	60.0	.035	15.00	0	
1541	1542	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1542	1544	0	4	CHANNEL	5.0	10122.	.0260	4.0	4.0	.040	2.00	0	
				OVERFLOW	30.0	10122.	.0260	80.0	80.0	.045	15.00	0	
1520	1521	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1525	1526	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1528	1428	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1428	1429	0	4	CHANNEL	4.0	1682.	.0131	2.0	2.0	.025	2.00	0	
				OVERFLOW	400.0	1682.	.0131	40.0	40.0	.035	15.00	0	
1415	1416	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1550	1551	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1560	1561	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1561	1563	0	4	CHANNEL	3.0	2480.	.1940	4.0	4.0	.050	2.00	0	
				OVERFLOW	25.0	2480.	.1940	50.0	50.0	.055	15.00	0	
1565	1566	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1566	1563	0	4	CHANNEL	3.0	2240.	.2140	4.0	4.0	.050	2.00	0	
				OVERFLOW	25.0	2240.	.2140	6.0	6.0	.055	15.00	0	
1563	1551	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	

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1551	1553	0	4	CHANNEL	3.0	8900.	.0560	5.0	5.0	.040	2.00	0
				OVERFLOW	30.0	8900.	.0560	50.0	50.0	.045	10.00	0
1570	1571	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1571	1557	0	1	CHANNEL	5.0	1200.	.2670	40.0	40.0	.055	10.00	0
1556	1557	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1557	1553	0	4	CHANNEL	3.0	5620.	.0240	5.0	5.0	.040	2.00	0
				OVERFLOW	25.0	5620.	.0240	40.0	40.0	.045	15.00	0
1553	1416	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1416	1429	0	4	CHANNEL	5.0	4085.	.0225	4.0	4.0	.050	2.00	0
				OVERFLOW	25.0	4085.	.0225	40.0	40.0	.055	15.00	0
1429	1526	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1526	1532	0	4	CHANNEL	2.0	1410.	.0136	2.0	2.0	.055	2.00	0
				OVERFLOW	400.0	1410.	.0136	40.0	40.0	.065	15.00	0
1530	1531	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1545	1546	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1575	1576	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1576	1546	0	4	CHANNEL	2.0	3500.	.0229	5.0	5.0	.050	2.00	0
				OVERFLOW	30.0	3500.	.0229	50.0	50.0	.055	15.00	0
1546	1531	0	4	CHANNEL	5.0	7763.	.0840	4.0	4.0	.050	2.00	0
				OVERFLOW	30.0	7763.	.0840	75.0	75.0	.055	15.00	0
1531	1532	0	4	CHANNEL	5.0	5288.	.0872	4.0	4.0	.040	2.00	0
				OVERFLOW	30.0	5288.	.0872	80.0	80.0	.045	15.00	0
1532	1537	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1537	1533	0	4	CHANNEL	2.0	1127.	.0035	2.0	2.0	.035	2.00	0
				OVERFLOW	400.0	1127.	.0035	5.0	40.0	.035	15.00	0
1414	1534	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1534	1533	0	4	CHANNEL	10.0	1966.	.0080	5.0	5.0	.050	1.00	0
				OVERFLOW	400.0	1966.	.0080	50.0	3.0	.065	15.00	0
1533	1521	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1521	1544	0	4	CHANNEL	4.0	2633.	.0093	2.0	2.0	.050	2.00	0
				OVERFLOW	500.0	2633.	.0093	25.0	25.0	.065	10.00	0
1544	1548	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1548	1522	0	4	CHANNEL	4.0	1054.	.0038	8.0	8.0	.035	.50	0
				OVERFLOW	500.0	1054.	.0038	60.0	60.0	.035	15.00	0
1522	1511	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1510	1511	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1511	1513	0	4	CHANNEL	4.0	3213.	.0057	2.0	2.0	.050	2.00	0
				OVERFLOW	512.0	3213.	.0057	50.0	50.0	.060	10.00	0
1513	1514	8	3		.0	1.	.0010	.0	.0	.001	10.00	1508
DIVERSION TO GUTTER NUMBER 1508 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	50.0	.1	140.0	48.0	415.0	192.0	1791.0	1299.0	3930.0 3176.0
		7762.0	6551.0	15011.0	13210.0							
1514	1442	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1442	1935	0	4	CHANNEL	2.0	2252.	.0097	4.0	4.0	.040	1.00	0
				OVERFLOW	300.0	2252.	.0097	80.0	80.0	.060	15.00	0
1262	1916	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1916	1935	0	4	CHANNEL	2.0	1211.	.0046	5.0	3.0	.035	1.00	0
				OVERFLOW	400.0	1211.	.0046	100.0	3.0	.035	20.00	0
1935	262	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
262	263	0	4	CHANNEL	2.0	529.	.0058	5.0	3.0	.035	1.00	0
				OVERFLOW	500.0	529.	.0058	150.0	3.0	.035	20.00	0
263	1905	8	3		.0	1.	.0010	.0	.0	.001	10.00	266
DIVERSION TO GUTTER NUMBER 266 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	175.0	174.9	412.0	185.0	908.0	198.0	1902.0	212.0	3161.0 228.0
		6477.0	233.0	13854.0	256.0							
1905	264	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
264	265	0	4	CHANNEL	2.0	1138.	.0017	5.0	3.0	.035	.50	0
				OVERFLOW	600.0	1138.	.0017	150.0	3.0	.035	20.00	0
265	269	8	3		.0	1.	.0010	.0	.0	.001	10.00	1267
DIVERSION TO GUTTER NUMBER 1267 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	170.0	169.9	227.0	195.0	710.0	516.0	1689.0	1249.0	2933.0 1956.0
		6244.0	3358.0	13598.0	6585.0							
269	1294	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1294	294	0	4	CHANNEL	2.0	1043.	.0027	4.0	4.0	.025	1.00	0
				OVERFLOW	375.0	1043.	.0027	80.0	3.0	.035	15.00	0
304	294	0	1	CHANNEL	8.0	2370.	.0060	5.0	5.0	.035	10.00	0
299	303	0	4	CHANNEL	.5	3612.	.0400	12.0	12.0	.016	.50	0
				OVERFLOW	24.0	3612.	.0400	20.0	20.0	.020	10.00	0
301	300	0	4	CHANNEL	.5	3743.	.0800	12.0	12.0	.016	.50	0
				OVERFLOW	24.0	3743.	.0800	20.0	20.0	.020	10.00	0
300	1922	5	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	5.4	10.0	28.7	11.0	36.6	32.0	39.3	468.0	
1922	303	0	4	CHANNEL	.5	899.	.0667	12.0	12.0	.016	.50	0
				OVERFLOW	10.0	899.	.0667	20.0	20.0	.020	10.00	0
303	298	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
298	297	11	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	.1	15.0	.5	45.0	1.4	94.0	2.9	130.0	5.3 158.0
		9.3	182.0	12.2	192.0	15.9	225.0	20.4	286.0	25.0	827.0	
297	1921	0	4	CHANNEL	6.0	5106.	.0250	3.0	3.0	.045	6.00	0
				OVERFLOW	50.0	6800.	.0188	3.0	3.0	.035	10.00	0
1917	1921	0	4	CHANNEL	5.0	1894.	.0079	8.0	8.0	.035	1.00	0
				OVERFLOW	40.0	1894.	.0079	80.0	80.0	.035	15.00	0
1921	1920	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1920	294	0	4	CHANNEL	18.0	785.	.0013	6.0	6.0	.035	6.00	0
				OVERFLOW	100.0	785.	.0013	12.0	12.0	.035	15.00	0
294	280	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
280	1293	6	3		.0	1.	.0010	.0	.0	.001	10.00	1295
DIVERSION TO GUTTER NUMBER 1295 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	295.0	1.0	370.0	42.0	1046.0	661.0	2827.0	2327.0	8734.0 8169.0
1293	293	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
293	267	0	5	PIPE	8.5	757.	.0020	.0	.0	.015	8.50	0
				OVERFLOW	8.5	757.	.0020	.0	.0	.015	20.00	0
1267	267	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
267	268	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
268	1291	8	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	1.4	81.0	5.0	267.0	10.4	465.0	16.9	632.0	25.0 1145.0
		35.1	1888.0	140.0	10000.0							
1291	291	0	3		.0	1.	.0010	.0	.0	.001	10.00	0

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291		1290		6		3		.0		1.		.0010		.0		.0		.001		10.00		1923	
DIVERSION TO GUTTER		NUMBER1923 - TOTAL Q VS DIVERTED Q IN CFS		.0		.0		1956.0		1098.0		6585.0		5685.0		10000.0		9000.0					
.0		.0		515.0		1.0		1249.0		471.0		1956.0		1098.0		6585.0		5685.0		10000.0		9000.0	
1290	290	0	3																				
290	1924	0	4	CHANNEL	30.0	1375.	.0017	4.0	4.0	.045	6.00	0											
				OVERFLOW	100.0	1375.	.0017	20.0	20.0	.050	15.00	0											
1289	1924	0	3																				
1924	289	0	3																				
289	242	0	4	CHANNEL	30.0	1962.	.0017	4.0	4.0	.045	6.00	0											
				OVERFLOW	100.0	1962.	.0017	20.0	20.0	.050	15.00	0											
1505	1506	0	3																				
1410	1411	0	3																				
1420	1421	0	3																				
1435	1436	0	3																				
1436	1438	0	4	CHANNEL	2.0	3730.	.0350	4.0	4.0	.050	3.00	0											
				OVERFLOW	30.0	3730.	.0350	16.0	16.0	.055	15.00	0											
1430	1431	0	3																				
1431	1438	0	4	CHANNEL	2.0	1670.	.0820	4.0	4.0	.040	1.00	0											
				OVERFLOW	12.0	1670.	.0820	15.0	15.0	.045	15.00	0											
1438	1426	0	3																				
1425	1426	0	3																				
1426	1421	0	4	CHANNEL	5.0	2319.	.0190	8.0	8.0	.040	2.00	0											
				OVERFLOW	40.0	2319.	.0190	75.0	75.0	.045	15.00	0											
1445	1446	0	3																				
1446	1443	0	4	CHANNEL	2.0	6667.	.0606	3.0	3.0	.040	3.00	0											
				OVERFLOW	25.0	6667.	.0606	6.0	6.0	.045	15.00	0											
1645	1646	0	3																				
1646	1643	0	4	CHANNEL	5.0	5300.	.1450	4.0	4.0	.060	2.00	0											
				OVERFLOW	25.0	5300.	.1450	15.0	15.0	.065	15.00	0											
1640	1641	0	3																				
1641	1643	0	4	CHANNEL	2.0	5800.	.0160	3.0	3.0	.060	3.00	0											
				OVERFLOW	25.0	5800.	.0160	8.0	8.0	.065	15.00	0											
1643	1631	0	3																				
1630	1631	0	3																				
1631	1628	0	4	CHANNEL	10.0	7611.	.0730	4.0	4.0	.040	3.00	0											
				OVERFLOW	40.0	7611.	.0730	10.0	10.0	.045	15.00	0											
1625	1626	0	3																				
1635	1636	0	3																				
1636	1626	0	1	CHANNEL	2.0	4200.	.0840	8.0	8.0	.040	10.00	0											
1626	1628	0	4	CHANNEL	25.0	1908.	.0205	4.0	4.0	.070	2.00	0											
				OVERFLOW	100.0	1908.	.0205	75.0	75.0	.075	15.00	0											
1628	1611	0	3																				
1610	1611	0	3																				
1611	1928	0	4	CHANNEL	30.0	4400.	.0290	4.0	4.0	.060	2.50	0											
				OVERFLOW	150.0	4400.	.0290	75.0	75.0	.070	15.00	0											
1605	1606	0	3																				
1665	1666	0	3																				
1666	1606	0	4	CHANNEL	3.0	6900.	.2130	3.0	3.0	.050	2.00	0											
				OVERFLOW	20.0	6900.	.2130	2.0	2.0	.055	10.00	0											
1606	1928	0	4	CHANNEL	5.0	5987.	.0812	4.0	4.0	.045	2.00	0											
				OVERFLOW	25.0	5987.	.0812	3.0	3.0	.060	15.00	0											
1928	1601	0	3																				
1600	1601	0	3																				
1601	1603	0	4	CHANNEL	25.0	1264.	.0290	6.0	6.0	.060	2.50	0											
				OVERFLOW	85.0	1264.	.0290	80.0	80.0	.070	15.00	0											
1710	1711	0	3																				
1711	1712	0	4	CHANNEL	5.0	5430.	.0479	4.0	4.0	.035	1.00	0											
				OVERFLOW	30.0	5430.	.0479	5.0	5.0	.035	15.00	0											
1615	1616	0	3																				
1616	1623	0	4	CHANNEL	2.0	6409.	.0620	3.0	3.0	.040	3.00	0											
				OVERFLOW	20.0	6409.	.0620	5.0	5.0	.045	15.00	0											
1660	1661	0	3																				
1661	1651	0	4	CHANNEL	3.0	9600.	.1670	4.0	4.0	.060	3.00	0											
				OVERFLOW	25.0	9600.	.1670	3.0	3.0	.065	15.00	0											
1650	1651	0	3																				
1651	1653	0	4	CHANNEL	5.0	4100.	.0860	4.0	4.0	.050	3.00	0											
				OVERFLOW	25.0	4100.	.0860	3.0	3.0	.055	15.00	0											
1655	1656	0	3																				
1656	1653	0	4	CHANNEL	3.0	10800.	.1170	4.0	4.0	.050	3.00	0											
				OVERFLOW	25.0	10800.	.1170	3.0	3.0	.055	15.00	0											
1653	1621	0	3																				
1620	1621	0	3																				
1621	1623	0	4	CHANNEL	5.0	10100.	.0320	5.0	5.0	.045	3.00	0											
				OVERFLOW	35.0	10100.	.0320	2.0	2.0	.060	15.00	0											
1623	1624	0	3																				
1705	1624	0	3																				
1624	1712	0	4	CHANNEL	2.0	2490.	.0380	5.0	5.0	.050	2.00	0											
				OVERFLOW	25.0	2490.	.0380																

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		.0	.0	500.0	1.0	999.0	125.0	1886.0	841.0	2765.0	1456.0	3403.0	1937.0
1509	1800	4421.0	2668.0	7425.0	5187.0	13357.0	10368.0						
1490	1491	0	3					.0010	.0	.0	.001	10.00	0
1455	1456	0	3					.0010	.0	.0	.001	10.00	0
1938	1480	0	3					.0010	.0	.0	.001	10.00	0
1480	1481	0	4	CHANNEL	5.0	2400.		.0500	2.0	2.0	.040	2.00	0
1481	1482	7	2	PIPE	.0	1.		.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW													
		.0	.0	308.0	18.0	624.0	76.0	947.0	179.0	1279.0	318.0	1618.0	1676.0
1482	1456	1965.0	4700.0					.0010	.0	.0	.001	10.00	0
1456	1457	0	1	CHANNEL	2.0	4450.		.0363	80.0	80.0	.030	20.00	0
1457	1491	0	3					.0010	.0	.0	.001	10.00	0
1491	1931	0	4	CHANNEL	5.0	10236.		.0090	4.0	4.0	.050	2.00	0
				OVERFLOW	25.0	10236.		.0090	60.0	60.0	.065	15.00	0
1460	1461	0	3					.0010	.0	.0	.001	10.00	0
1461	1931	0	4	CHANNEL	3.0	2286.		.0280	4.0	4.0	.050	2.00	0
				OVERFLOW	20.0	2286.		.0280	24.0	24.0	.055	15.00	0
1931	1933	0	3					.0010	.0	.0	.001	10.00	0
1933	1467	0	4	CHANNEL	5.0	403.		.0099	2.0	2.0	.020	2.00	0
				OVERFLOW	25.0	403.		.0099	10.0	10.0	.025	15.00	0
1465	1932	0	3					.0010	.0	.0	.001	10.00	0
1932	1467	0	4	CHANNEL	4.0	1591.		.0289	8.0	8.0	.035	.50	0
				OVERFLOW	25.0	1591.		.0289	4.0	4.0	.035	15.00	0
1467	1468	0	3					.0010	.0	.0	.001	10.00	0
1468	1800	0	4	CHANNEL	5.0	2357.		.0180	2.0	2.0	.020	2.00	0
				OVERFLOW	25.0	2357.		.0180	10.0	10.0	.025	15.00	0
1800	1506	0	3					.0010	.0	.0	.001	10.00	0
1506	1507	0	4	CHANNEL	33.0	8099.		.0054	4.0	4.0	.060	2.50	0
				OVERFLOW	800.0	8099.		.0054	10.0	10.0	.065	15.00	0
1508	1507	0	3					.0010	.0	.0	.001	10.00	0
1507	1512	0	3					.0010	.0	.0	.001	10.00	0
1512	44	0	4	CHANNEL	33.0	1367.		.0064	4.0	4.0	.060	2.50	0
				OVERFLOW	308.0	1367.		.0064	80.0	80.0	.065	15.00	0
1500	1501	0	3					.0010	.0	.0	.001	10.00	0
1501	44	0	4	CHANNEL	5.0	8609.		.0212	2.0	2.0	.040	2.00	0
				OVERFLOW	20.0	8609.		.0212	10.0	10.0	.045	15.00	0
44	261	0	3					.0010	.0	.0	.001	10.00	0
261	1427	9	3					.0010	.0	.0	.001	10.00	1262
DIVERSION TO GUTTER NUMBER1262 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	500.0	1.0	875.0	35.0	1920.0	315.0	2709.0	660.0	3916.0	1323.0
1427	243	5586.0	2377.0	9768.0	5344.0	18394.0	11928.0						
243	242	0	3					.0010	.0	.0	.001	10.00	0
				CHANNEL	65.0	2991.		.0112	2.0	2.0	.043	2.50	0
				OVERFLOW	650.0	2991.		.0112	100.0	100.0	.055	15.00	0
242	241	0	3					.0010	.0	.0	.001	10.00	0
241	240	0	4	CHANNEL	65.0	5732.		.0100	2.0	2.0	.043	3.00	0
				OVERFLOW	1200.0	5732.		.0100	200.0	200.0	.055	20.00	0
240	238	0	4	CHANNEL	65.0	2861.		.0100	2.0	2.0	.050	3.00	0
				OVERFLOW	1200.0	2861.		.0100	200.0	200.0	.075	20.00	0
238	237	0	3					.0010	.0	.0	.001	10.00	0
237	251	5	3					.0010	.0	.0	.001	10.00	389
DIVERSION TO GUTTER NUMBER389 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	2060.0	1.0	4980.0	2580.0	6630.0	3530.0	11150.0	7500.0		
389	1906	0	3					.0010	.0	.0	.001	10.00	0
1906	1909	0	4	CHANNEL	10.0	3340.		.0042	8.0	8.0	.025	.50	0
				OVERFLOW	1200.0	3340.		.0042	80.0	80.0	.025	15.00	0
251	233	0	3					.0010	.0	.0	.001	10.00	0
235	239	0	1	CHANNEL	1.0	3509.		.0050	50.0	50.0	.020	10.00	0
239	234	0	3					.0010	.0	.0	.001	10.00	0
234	232	0	4	CHANNEL	2.0	2072.		.0044	3.0	3.0	.050	2.00	0
				OVERFLOW	50.0	2072.		.0044	50.0	50.0	.035	10.00	0
233	232	0	4	CHANNEL	65.0	3076.		.0100	2.0	2.0	.050	4.00	0
				OVERFLOW	600.0	3076.		.0100	200.0	200.0	.080	20.00	0
232	236	0	3					.0010	.0	.0	.001	10.00	0
236	252	5	3					.0010	.0	.0	.001	10.00	1403
DIVERSION TO GUTTER NUMBER1403 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	2060.0	1.0	2400.0	100.0	3100.0	500.0	10000.0	2500.0		
1403	1599	0	3					.0010	.0	.0	.001	10.00	0
252	231	0	3					.0010	.0	.0	.001	10.00	0
1357	357	0	3					.0010	.0	.0	.001	10.00	0
357	1401	6	3					.0010	.0	.0	.001	10.00	1325
DIVERSION TO GUTTER NUMBER1325 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	26.0	.1	263.0	235.0	391.0	361.0	995.0	960.0	5000.0	4950.0
1401	1387	0	3					.0010	.0	.0	.001	10.00	0
1387	387	0	3					.0010	.0	.0	.001	10.00	0
387	1908	0	3					.0010	.0	.0	.001	10.00	0
1908	1320	0	4	CHANNEL	2.0	1718.		.0076	3.0	3.0	.025	2.00	0
				OVERFLOW	600.0	1718.		.0076	80.0	80.0	.025	10.00	0
266	376	0	3					.0010	.0	.0	.001	10.00	0
376	375	0	1	CHANNEL	4.0	1569.		.0041	4.0	4.0	.050	10.00	0
375	1374	4	3					.0010	.0	.0	.001	10.00	1404
DIVERSION TO GUTTER NUMBER1404 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	24.0	.1	135.0	100.0	540.0	500.0				
1374	374	0	3					.0010	.0	.0	.001	10.00	0
374	372	0	4	CHANNEL	4.0	2538.		.0115	3.0	3.0	.045	2.00	0
				OVERFLOW	20.0	2538.		.0115	20.0	20.0	.035	10.00	0
373	372	0	4	CHANNEL	3.0	1779.		.0075	4.0	4.0	.045	1.00	0
				OVERFLOW	20.0	1779.		.0075	20.0	20.0	.035	10.00	0
1367	367	0	3					.0010	.0	.0	.001	10.00	0
367	372	0	4	CHANNEL	.5	2663.		.0103	12.0	12.0	.016	.50	0
				OVERFLOW	10.0	2663.		.0103	20.0	20.0	.020	10.00	0
372	371	0	3					.0010	.0	.0	.001	10.00	0
371	311	0	4	CHANNEL	10.0	2893.		.0078	2.0	2.0	.045	1.00	0
				OVERFLOW	10.0	2893.		.0078	50.0	50.0	.035	10.00	0
1339	1822	0	3					.0010	.0	.0	.001	10.00	0
1348	348	0	3					.0010	.0	.0	.001	10.00	0
348	1937	5	3					.0010	.0	.0	.001	10.00	1331
DIVERSION TO GUTTER NUMBER1331 - TOTAL Q VS DIVERTED Q IN CFS													

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1937		.0	.0	31.0	30.0	542.0	335.0	795.0	466.0	1394.0	766.0								
1386	1386	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
385	1386	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
1386	386	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
386	395	6	3			.0	1.	.0010	.0	.0	.001	10.00	1407						
DIVERSION TO GUTTER NUMBER1407 - TOTAL Q VS DIVERTED Q IN CFS																			
395	394	.0	.0	206.0	1.0	394.0	64.0	902.0	273.0	2616.0	572.0	5000.0	1100.0						
394	1822	0	4			.5	1000.	.0061	12.0	12.0	.016	10.00	0						
CHANNEL OVERFLOW																			
1822	339	0	3			10.0	1000.	.0061	20.0	20.0	.020	10.00	0						
339	1313	4	3			.0	1.	.0010	.0	.0	.001	10.00	0						
DIVERSION TO GUTTER NUMBER1336 - TOTAL Q VS DIVERTED Q IN CFS																			
1313	1939	.0	.0	30.0	20.0	300.0	200.0	3000.0	2000.0										
1362	362	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
363	362	0	1			1.0	4078.	.0121	20.0	5.0	.020	10.00	0						
362	398	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
398	1396	10	2			.1	1.	.0010	.0	.0	.030	10.00	0						
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW																			
1396	396	.0	.0	.4	26.0	1.3	138.0	2.1	200.0	2.4	260.0	2.8	360.0						
396	308	3.4	510.0	4.0	893.0	5.0	1809.0	15.0	10000.0										
DIVERSION TO GUTTER NUMBER 385 - TOTAL Q VS DIVERTED Q IN CFS																			
308	314	10000.0	9550.0	260.0	.1	360.0	60.0	510.0	190.0	893.0	545.0	1809.0	1388.0						
314	1939	0	1			.0	1.	.0010	.0	.0	.001	10.00	0						
1939	313	0	3			8.0	600.	.0048	.1	2.0	.050	15.00	0						
313	1910	6	3			.0	1.	.0010	.0	.0	.001	10.00	0						
DIVERSION TO GUTTER NUMBER1409 - TOTAL Q VS DIVERTED Q IN CFS																			
1910	1940	.0	.0	260.0	.1	389.0	129.0	470.0	195.0	648.0	358.0	10000.0	9500.0						
1366	366	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
366	344	0	4			.5	5533.	.0079	12.0	12.0	.016	10.00	0						
CHANNEL OVERFLOW																			
344	1408	4	3			10.0	5533.	.0079	20.0	20.0	.020	10.00	0						
DIVERSION TO GUTTER NUMBER1339 - TOTAL Q VS DIVERTED Q IN CFS																			
1408	1940	.0	.0	25.0	.1	50.0	25.0	2000.0	35.0										
1940	312	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
312	311	0	1			8.0	1520.	.0068	2.0	2.0	.050	10.00	0						
311	358	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
358	393	0	4			8.0	2401.	.0100	1.5	1.5	.030	4.50	0						
CHANNEL OVERFLOW																			
393	1357	8	3			20.0	2401.	.0100	50.0	50.0	.020	10.00	0						
DIVERSION TO GUTTER NUMBER1393 - TOTAL Q VS DIVERTED Q IN CFS																			
1393	1941	.0	.0	240.0	1.0	588.0	79.0	874.0	150.0	1822.0	391.0	2281.0	509.0						
1941	392	3048.0	704.0	4515.0	1075.0	.0	1.	.0010	.0	.0	.001	10.00	0						
CHANNEL OVERFLOW																			
1325	325	0	3			4.0	423.	.0142	4.0	4.0	.030	10.00	0						
1331	331	0	3			30.0	423.	.0142	12.0	12.0	.032	15.00	0						
1407	331	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
331	337	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
337	328	0	4			.5	2862.	.0066	12.0	12.0	.016	10.00	0						
CHANNEL OVERFLOW																			
1329	328	0	4			10.0	2862.	.0066	20.0	20.0	.020	10.00	0						
CHANNEL OVERFLOW																			
1340	340	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
340	1333	6	3			.0	1.	.0010	.0	.0	.001	10.00	1348						
DIVERSION TO GUTTER NUMBER1348 - TOTAL Q VS DIVERTED Q IN CFS																			
1333	333	.0	.0	66.0	31.0	833.0	542.0	1194.0	795.0	2037.0	1394.0	3730.0	2560.0						
333	332	0	1			.0	1.	.0010	.0	.0	.001	10.00	0						
341	1334	6	3			1.0	2969.	.0047	50.0	5.0	.020	20.00	0						
DIVERSION TO GUTTER NUMBER1340 - TOTAL Q VS DIVERTED Q IN CFS																			
1334	334	.0	.0	71.0	66.0	1120.0	833.0	1616.0	1194.0	2776.0	2037.0	5110.0	3730.0						
334	332	0	1			.0	1.	.0010	.0	.0	.001	10.00	0						
332	1308	0	3			1.0	2967.	.0047	5.0	50.0	.020	20.00	0						
1308	1307	4	3			.0	1.	.0010	.0	.0	.001	10.00	1306						
DIVERSION TO GUTTER NUMBER1306 - TOTAL Q VS DIVERTED Q IN CFS																			
1307	1305	.0	.0	56.2	56.1	1080.0	60.5	2500.0	65.0										
1306	330	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
346	345	0	4			.5	1855.	.0179	12.0	12.0	.016	10.00	0						
CHANNEL OVERFLOW																			
345	359	0	4			10.0	1855.	.0179	20.0	20.0	.020	10.00	0						
CHANNEL OVERFLOW																			
350	1915	0	5			.5	3689.	.0097	12.0	12.0	.016	10.00	0						
CHANNEL OVERFLOW																			
1360	360	0	3			10.0	3689.	.0097	20.0	20.0	.020	10.00	0						
1923	292	0	3			2.0	2980.	.0074	.0	.0	.015	2.00	0						
292	360	0	4			1.0	2980.	.0074	20.0	20.0	.020	20.00	0						
CHANNEL OVERFLOW																			
360	1934	0	3			.0	1.	.0010	.0	.0	.001	10.00	0						
1934	1919	0	4			1.0	1500.	.0027	50.0	50.0	.020	10.00	0						
CHANNEL OVERFLOW																			
353	1919	0	4			1.0	1500.	.0027	4.0	4.0	.020	10.00	0						
CHANNEL OVERFLOW																			
1919	352	0	3			.5	1591.	.0037	12.0	12.0	.016	10.00	0						
352	1812	0	3			10.0	1591.	.0037	20.0	20.0	.020	10.00	0						
CHANNEL OVERFLOW																			
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW																			
1812	1813	.0	.0	.7	20.0	2.2	31.0	5.8	39.0	12.8	300.0	23.3	3986.0						
1813	1814	50.0	10000.0			.0	1.	.0010	.0	.0	.001	10.00	0						
DIVERSION TO GUTTER NUMBER1815 - TOTAL Q VS DIVERTED Q IN CFS																			

		.0	.0	40.0	.1	314.0	77.0	1075.0	357.0	2228.0	783.0	4144.0	1719.0
1814	351	6379.0	2711.0										
351	1913	0	3										
1815	1816	0	3										
1818	1817	0	4	CHANNEL	2.0	354.	.0100	4.0	4.0	.020	1.00	0	
1816	1817	0	4	CHANNEL	12.0	354.	.0100	10.0	10.0	.030	10.00	0	
1817	354	0	3	OVERFLOW	6.0	837.	.0037	12.0	12.0	.015	1.00	0	
354	1913	0	5	OVERFLOW	30.0	837.	.0037	8.0	3.0	.030	15.00	0	
1913	1914	0	3	PIPE	.0	1.	.0010	.0	.0	.001	10.00	0	
1914	1915	0	5	OVERFLOW	2.0	756.	.0066	.0	.0	.016	2.00	0	
1915	347	0	3	PIPE	1.0	756.	.0066	20.0	20.0	.020	15.00	0	
347	359	0	5	OVERFLOW	.0	1.	.0010	.0	.0	.001	10.00	0	
349	359	0	1	PIPE	4.0	2229.	.0173	.0	.0	.015	4.00	0	
355	359	0	5	OVERFLOW	10.0	2229.	.0173	20.0	20.0	.020	20.00	0	
359	356	0	3	CHANNEL	10.0	2788.	.0217	20.0	20.0	.035	10.00	0	
356	1343	0	5	PIPE	2.0	3762.	.0121	.0	.0	.020	2.00	0	
		0	3	OVERFLOW	1.0	3762.	.0121	5.0	20.0	.020	10.00	0	
		0	3	PIPE	.0	1.	.0010	.0	.0	.001	10.00	0	
		10	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0	
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW													
		.0	.0	.3	14.0	3.4	138.0	5.3	200.0	6.6	210.0	7.7	233.0
1343	343	9.7	332.0	14.5	1712.0	18.2	2617.0	23.4	5064.0				
343	1342	0	3										
		7	3										
DIVERSION TO GUTTER NUMBER1362 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	230.0	229.0	332.0	260.0	1712.0	360.0	2617.0	510.0	5064.0	393.0
1342	342	9890.0	1680.0										
342	1335	0	3										
		6	3										
DIVERSION TO GUTTER NUMBER1341 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	72.0	71.0	1352.0	1120.0	2107.0	1616.0	4171.0	2776.0	8280.0	5110.0
1341	341	0	3										
1335	335	0	3										
335	1301	0	1	CHANNEL	10.0	3343.	.0047	18.0	5.0	.045	20.00	0	
1301	1302	0	3										
1302	1303	0	3										
		4	3										
DIVERSION TO GUTTER NUMBER1304 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	585.0	1.0	1973.0	1149.0	3964.0	2984.0				
1303	330	0	3										
1304	1305	0	3										
1305	1599	0	3										
330	329	0	3										
329	328	0	1	CHANNEL	8.0	1804.	.0012	3.5	3.5	.024	20.00	0	
1309	1311	0	3										
		6	3										
DIVERSION TO GUTTER NUMBER1312 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	725.2	.1	824.2	.2	981.0	51.0	3918.0	1261.0	6125.0	2046.0
1311	327	0	3										
368	1330	0	3										
1312	1330	0	3										
1330	1332	0	5	PIPE	1.5	3079.	.0078	10.0	10.0	.025	1.50	0	
				OVERFLOW	28.0	3079.	.0078	5.0	5.0	.040	5.00	0	
1332	1368	0	3										
1368	1369	0	3										
		3	3										
DIVERSION TO GUTTER NUMBER1371 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	245.0	.1	3280.0	418.6						
1369	1370	0	3										
1370	1365	0	5	PIPE	1.5	1286.	.0030	.0	.0	.025	1.50	0	
				OVERFLOW	30.0	1286.	.0030	10.0	10.0	.025	15.00	0	
1371	1372	0	3										
1372	1599	0	3										
328	1309	0	3										
327	326	0	4	CHANNEL	8.0	1305.	.0008	3.5	3.5	.024	4.00	0	
				OVERFLOW	40.0	1305.	.0008	5.7	7.5	.028	20.00	0	
1409	310	0	3										
1336	336	0	3										
336	1310	0	3										
		4	3										
DIVERSION TO GUTTER NUMBER1942 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	20.0	10.0	200.0	100.0	2000.0	1000.0				
1942	1940	0	3										
1310	310	0	3										
310	315	0	3										
315	317	0	4	CHANNEL	.5	3664.	.0088	12.0	12.0	.016	.50	0	
				OVERFLOW	10.0	3664.	.0088	20.0	20.0	.020	10.00	0	
316	317	0	4	CHANNEL	.5	2903.	.0079	12.0	12.0	.016	.50	0	
				OVERFLOW	10.0	2903.	.0079	20.0	20.0	.020	10.00	0	
317	326	0	3										
326	325	0	4	CHANNEL	8.0	458.	.0008	3.5	3.5	.024	4.00	0	
				OVERFLOW	40.0	458.	.0008	5.7	7.5	.028	20.00	0	
325	324	0	3										
324	1392	0	3										
		7	3										
DIVERSION TO GUTTER NUMBER1402 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	725.1	.1	824.0	98.0	930.0	180.0	2657.0	1833.0	4077.0	3077.0
1402	1323	10000.0	8800.0										
1323	323	0	3										
323	1321	0	3										
		7	3										
DIVERSION TO GUTTER NUMBER1387 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	50.0	49.9	254.0	60.0	1565.0	100.0	2841.0	150.0	4250.0	200.0
1392	392	8900.0	400.0										
392	391	0	3										
391	1911	0	4	CHANNEL	15.0	1048.	.0012	3.5	3.5	.045	5.00	0	
				OVERFLOW	55.0	1048.	.0012	4.0	7.5	.055	20.00	0	
338	318	0	4	CHANNEL	1.0	2263.	.0089	1.0	1.0	.045	1.00	0	
				OVERFLOW	10.0	2263.	.0089	50.0	50.0	.035	10.00	0	
318	1911	0	4	CHANNEL	8.0	2821.	.0012	3.0	3.0	.045	1.50	0	

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Node	Node	Flow	Flow	Structure	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow
1911	1912	0	3	OVERFLOW	10.0	2821.	.0012	20.0	20.0	.035	10.00									
1912	390	0	4	CHANNEL	15.0	1048.	.0012	3.5	3.5	.045	4.00									0
390	1238	7	3	OVERFLOW	70.0	1048.	.0012	7.5	5.0	.055	20.00									
		.0	.0		.0	1.	.0010	.0	.0	.001	10.00									388
DIVERSION TO GUTTER NUMBER 398 - TOTAL Q VS DIVERTED Q IN CFS																				
		5000.0	4795.0		200.0	1.0	205.0	5.0	274.0	73.0	431.0	229.0	726.0	523.0						
398	1907	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1907	1320	0	4	CHANNEL	4.0	2175.	.0064	3.0	3.0	.025	2.00									0
				OVERFLOW	300.0	2175.	.0064	80.0	80.0	.025	15.00									
1320	320	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
320	1909	0	4	CHANNEL	6.0	1412.	.0087	3.0	3.0	.035	2.00									0
				OVERFLOW	700.0	1412.	.0087	100.0	100.0	.035	10.00									
1909	322	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1321	321	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
321	1337	0	1	CHANNEL	10.0	1092.	.0080	50.0	50.0	.045	15.00									0
1337	1338	3	3		.0	1.	.0010	.0	.0	.001	10.00									1363
DIVERSION TO GUTTER NUMBER 1363 - TOTAL Q VS DIVERTED Q IN CFS																				
		.0	.0		10.0	.1	3500.0	1910.4												
1338	1361	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1361	1320	0	5	PIPE	1.5	823.	.0100	.0	.0	.025	1.50									0
				OVERFLOW	50.0	823.	.0100	20.0	20.0	.045	15.00									
361	1364	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1363	1364	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1364	1365	0	5	PIPE	1.5	1547.	.0078	.0	.0	.025	1.50									0
				OVERFLOW	10.0	1547.	.0078	50.0	50.0	.045	20.00									
1365	1944	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
370	1944	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1944	1945	0	5	PIPE	4.5	1283.	.0109	.0	.0	.025	4.50									0
				OVERFLOW	10.0	1283.	.0109	50.0	50.0	.035	20.00									
1945	1373	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1373	1375	3	3		.0	1.	.0010	.0	.0	.001	10.00									1377
DIVERSION TO GUTTER NUMBER 1377 - TOTAL Q VS DIVERTED Q IN CFS																				
		.0	.0		195.7	.1	5200.0	3985.2												
1377	1372	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1375	1376	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1376	1946	0	4	CHANNEL	8.0	750.	.0100	3.0	3.0	.045	6.00									0
				OVERFLOW	50.0	750.	.0100	20.0	20.0	.050	5.00									
322	1943	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1943	1946	0	4	CHANNEL	20.0	1443.	.0083	4.0	4.0	.045	6.00									0
				OVERFLOW	400.0	1443.	.0083	50.0	50.0	.060	10.00									
1946	319	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
319	271	0	4	CHANNEL	30.0	4190.	.0086	4.0	4.0	.065	7.00									0
				OVERFLOW	500.0	4190.	.0086	50.0	50.0	.060	10.00									
231	271	0	4	CHANNEL	130.0	5118.	.0074	4.0	4.0	.055	8.00									0
				OVERFLOW	600.0	5118.	.0074	50.0	50.0	.050	20.00									
271	270	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
270	399	0	4	CHANNEL	70.0	2605.	.0074	3.0	3.0	.055	8.00									0
				OVERFLOW	700.0	2605.	.0074	100.0	100.0	.040	20.00									
399	1599	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1599	1947	0	3		.0	1.	.0010	.0	.0	.001	10.00									0
1947	0	0	3		.0	1.	.0010	.0	.0	.001	10.00									0

TOTAL NUMBER OF GUTTERS/PIPES, 610

1

SBC CHANGES FROM DRAFT REPORT MODEL SBC.IN.SWI - ASSORTED MODIFICATIONS
 model sbct_ltc.swi with narrowing of conveyance 1330 overflow channel from 50' to

ARRANGEMENT OF SUBCATCHMENTS AND GUTTERS/PIPES

GUTTER	TRIBUTARY GUTTER/PIPE										TRIBUTARY SUBAREA										D.A. (AC)	
1	2	5	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	64741.0
2	3	4	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0	0	0	2408.0
3	0	0	0	0	0	0	0	0	0	0	3	0	0	0	0	0	0	0	0	0	0	929.0
4	0	0	0	0	0	0	0	0	0	0	4	0	0	0	0	0	0	0	0	0	0	960.0
5	7	6	13	0	0	0	0	0	0	0	5	0	0	0	0	0	0	0	0	0	0	61766.0
6	397	0	0	0	0	0	0	0	0	0	6	0	0	0	0	0	0	0	0	0	0	59943.0
7	9	10	0	0	0	0	0	0	0	0	7	0	0	0	0	0	0	0	0	0	0	986.0
8	15	22	0	0	0	0	0	0	0	0	8	0	0	0	0	0	0	0	0	0	0	59647.0
9	0	0	0	0	0	0	0	0	0	0	9	0	0	0	0	0	0	0	0	0	0	411.0
10	0	0	0	0	0	0	0	0	0	0	10	0	0	0	0	0	0	0	0	0	0	202.0
11	0	0	0	0	0	0	0	0	0	0	11	0	0	0	0	0	0	0	0	0	0	113.0
12	0	0	0	0	0	0	0	0	0	0	12	0	0	0	0	0	0	0	0	0	0	159.0
13	11	12	0	0	0	0	0	0	0	0	13	0	0	0	0	0	0	0	0	0	0	501.0
14	0	0	0	0	0	0	0	0	0	0	14	0	0	0	0	0	0	0	0	0	0	132.0
15	14	16	0	0	0	0	0	0	0	0	15	0	0	0	0	0	0	0	0	0	0	53636.0
16	40	17	0	0	0	0	0	0	0	0	16	0	0	0	0	0	0	0	0	0	0	53468.0
17	18	21	0	0	0	0	0	0	0	0	17	0	0	0	0	0	0	0	0	0	0	1706.0
18	20	0	0	0	0	0	0	0	0	0	18	0	0	0	0	0	0	0	0	0	0	1171.0

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20	0	0	0	0	0	0	0	0	0	0	19	0	0	0	0	0	0	0	0	0	606.0
21	0	0	0	0	0	0	0	0	0	0	20	0	0	0	0	0	0	0	0	0	379.0
22	23	24	0	0	0	0	0	0	0	0	21	0	0	0	0	0	0	0	0	0	4784.0
23	37	34	31	0	0	0	0	0	0	0	22	0	0	0	0	0	0	0	0	0	2671.0
24	25	26	0	0	0	0	0	0	0	0	23	0	0	0	0	0	0	0	0	0	1666.0
25	0	0	0	0	0	0	0	0	0	0	24	0	0	0	0	0	0	0	0	0	363.0
26	27	28	0	0	0	0	0	0	0	0	25	0	0	0	0	0	0	0	0	0	1199.0
27	0	0	0	0	0	0	0	0	0	0	26	0	0	0	0	0	0	0	0	0	107.0
28	29	30	0	0	0	0	0	0	0	0	27	0	0	0	0	0	0	0	0	0	998.0
29	0	0	0	0	0	0	0	0	0	0	28	0	0	0	0	0	0	0	0	0	152.0
30	0	0	0	0	0	0	0	0	0	0	29	0	0	0	0	0	0	0	0	0	546.0
31	32	33	0	0	0	0	0	0	0	0	30	0	0	0	0	0	0	0	0	0	508.0
32	0	0	0	0	0	0	0	0	0	0	31	0	0	0	0	0	0	0	0	0	144.0
33	0	0	0	0	0	0	0	0	0	0	32	0	0	0	0	0	0	0	0	0	257.0
34	35	36	0	0	0	0	0	0	0	0	33	0	0	0	0	0	0	0	0	0	844.0
35	0	0	0	0	0	0	0	0	0	0	34	0	0	0	0	0	0	0	0	0	148.0
36	0	0	0	0	0	0	0	0	0	0	35	0	0	0	0	0	0	0	0	0	251.0
37	38	39	0	0	0	0	0	0	0	0	36	0	0	0	0	0	0	0	0	0	1124.0
38	0	0	0	0	0	0	0	0	0	0	37	0	0	0	0	0	0	0	0	0	368.0
39	0	0	0	0	0	0	0	0	0	0	38	0	0	0	0	0	0	0	0	0	290.0
40	41	42	0	0	0	0	0	0	0	0	39	0	0	0	0	0	0	0	0	0	51645.0
41	0	0	0	0	0	0	0	0	0	0	40	0	0	0	0	0	0	0	0	0	205.0
42	46	62	68	0	0	0	0	0	0	0	41	0	0	0	0	0	0	0	0	0	51084.0
44	1512	1501	0	0	0	0	0	0	0	0	42	0	0	0	0	0	0	0	0	0	30179.0
46	59	60	0	0	0	0	0	0	0	0	43	0	0	0	0	0	0	0	0	0	47929.0
48	50	49	0	0	0	0	0	0	0	0	44	0	0	0	0	0	0	0	0	0	72077.0
49	0	0	0	0	0	0	0	0	0	0	45	0	0	0	0	0	0	0	0	0	220.0
50	51	52	56	0	0	0	0	0	0	0	46	0	0	0	0	0	0	0	0	0	11466.0
51	0	0	0	0	0	0	0	0	0	0	47	0	0	0	0	0	0	0	0	0	362.0
52	244	245	53	0	0	0	0	0	0	0	48	0	0	0	0	0	0	0	0	0	69055.0
53	54	55	0	0	0	0	0	0	0	0	49	0	0	0	0	0	0	0	0	0	536.0
54	0	0	0	0	0	0	0	0	0	0	50	0	0	0	0	0	0	0	0	0	213.0
55	0	0	0	0	0	0	0	0	0	0	51	0	0	0	0	0	0	0	0	0	297.0
56	57	58	0	0	0	0	0	0	0	0	52	0	0	0	0	0	0	0	0	0	1842.0
57	0	0	0	0	0	0	0	0	0	0	53	0	0	0	0	0	0	0	0	0	776.0
58	0	0	0	0	0	0	0	0	0	0	54	0	0	0	0	0	0	0	0	0	220.0
59	74	71	0	0	0	0	0	0	0	0	55	0	0	0	0	0	0	0	0	0	47507.0
60	0	0	0	0	0	0	0	0	0	0	56	0	0	0	0	0	0	0	0	0	225.0
61	63	64	0	0	0	0	0	0	0	0	57	0	0	0	0	0	0	0	0	0	1044.0
62	61	65	0	0	0	0	0	0	0	0	58	0	0	0	0	0	0	0	0	0	2039.0
63	0	0	0	0	0	0	0	0	0	0	59	0	0	0	0	0	0	0	0	0	234.0
64	0	0	0	0	0	0	0	0	0	0	60	0	0	0	0	0	0	0	0	0	258.0
65	66	67	0	0	0	0	0	0	0	0	61	0	0	0	0	0	0	0	0	0	956.0
66	0	0	0	0	0	0	0	0	0	0	62	0	0	0	0	0	0	0	0	0	108.0
67	0	0	0	0	0	0	0	0	0	0	63	0	0	0	0	0	0	0	0	0	636.0
68	69	70	0	0	0	0	0	0	0	0	64	0	0	0	0	0	0	0	0	0	523.0
69	0	0	0	0	0	0	0	0	0	0	65	0	0	0	0	0	0	0	0	0	197.0
70	0	0	0	0	0	0	0	0	0	0	66	0	0	0	0	0	0	0	0	0	246.0
71	72	73	0	0	0	0	0	0	0	0	67	0	0	0	0	0	0	0	0	0	1094.0
72	0	0	0	0	0	0	0	0	0	0	68	0	0	0	0	0	0	0	0	0	197.0
73	0	0	0	0	0	0	0	0	0	0	69	0	0	0	0	0	0	0	0	0	636.0

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74	77	76	94	0	0	0	0	0	0	0	58	0	0	0	0	0	0	0	0	46117.0
75	79	78	0	0	0	0	0	0	0	0	61	0	0	0	0	0	0	0	0	3945.0
76	0	0	0	0	0	0	0	0	0	0	63	0	0	0	0	0	0	0	0	379.0
77	75	88	0	0	0	0	0	0	0	0	65	0	0	0	0	0	0	0	0	4793.0
78	0	0	0	0	0	0	0	0	0	0	66	0	0	0	0	0	0	0	0	256.0
79	80	121	0	0	0	0	0	0	0	0	70	0	0	0	0	0	0	0	0	3627.0
80	82	81	0	0	0	0	0	0	0	0	83	0	0	0	0	0	0	0	0	2668.0
81	87	0	0	0	0	0	0	0	0	0	84	0	0	0	0	0	0	0	0	958.0
82	84	83	0	0	0	0	0	0	0	0	85	0	0	0	0	0	0	0	0	848.0
83	0	0	0	0	0	0	0	0	0	0	86	0	0	0	0	0	0	0	0	197.0
84	85	86	0	0	0	0	0	0	0	0	87	0	0	0	0	0	0	0	0	555.0
85	0	0	0	0	0	0	0	0	0	0	88	0	0	0	0	0	0	0	0	118.0
86	0	0	0	0	0	0	0	0	0	0	89	0	0	0	0	0	0	0	0	331.0
87	0	0	0	0	0	0	0	0	0	0	90	0	0	0	0	0	0	0	0	655.0
88	89	93	0	0	0	0	0	0	0	0	91	0	0	0	0	0	0	0	0	782.0
89	0	0	0	0	0	0	0	0	0	0	228	0	0	0	0	0	0	0	0	319.0
93	0	0	0	0	0	0	0	0	0	0	229	0	0	0	0	0	0	0	0	111.0
94	95	97	0	0	0	0	0	0	0	0	92	0	0	0	0	0	0	0	0	40534.0
95	96	116	0	0	0	0	0	0	0	0	230	0	0	0	0	0	0	0	0	34430.0
96	129	122	0	0	0	0	0	0	0	0	93	0	0	0	0	0	0	0	0	33528.0
97	99	98	0	0	0	0	0	0	0	0	94	0	0	0	0	0	0	0	0	5629.0
98	0	0	0	0	0	0	0	0	0	0	95	0	0	0	0	0	0	0	0	309.0
99	101	100	0	0	0	0	0	0	0	0	96	0	0	0	0	0	0	0	0	4848.0
100	0	0	0	0	0	0	0	0	0	0	97	0	0	0	0	0	0	0	0	458.0
101	102	107	0	0	0	0	0	0	0	0	98	0	0	0	0	0	0	0	0	4335.0
102	106	103	0	0	0	0	0	0	0	0	99	0	0	0	0	0	0	0	0	2382.0
103	104	105	0	0	0	0	0	0	0	0	100	0	0	0	0	0	0	0	0	1795.0
104	119	117	0	0	0	0	0	0	0	0	101	0	0	0	0	0	0	0	0	1302.0
105	0	0	0	0	0	0	0	0	0	0	102	0	0	0	0	0	0	0	0	343.0
106	0	0	0	0	0	0	0	0	0	0	103	0	0	0	0	0	0	0	0	273.0
107	108	109	0	0	0	0	0	0	0	0	104	0	0	0	0	0	0	0	0	1871.0
108	0	0	0	0	0	0	0	0	0	0	105	0	0	0	0	0	0	0	0	202.0
109	110	111	0	0	0	0	0	0	0	0	106	0	0	0	0	0	0	0	0	1563.0
110	112	113	0	0	0	0	0	0	0	0	107	0	0	0	0	0	0	0	0	1148.0
111	0	0	0	0	0	0	0	0	0	0	108	0	0	0	0	0	0	0	0	199.0
112	114	115	0	0	0	0	0	0	0	0	109	0	0	0	0	0	0	0	0	540.0
113	0	0	0	0	0	0	0	0	0	0	110	0	0	0	0	0	0	0	0	209.0
114	0	0	0	0	0	0	0	0	0	0	111	0	0	0	0	0	0	0	0	230.0
115	0	0	0	0	0	0	0	0	0	0	112	0	0	0	0	0	0	0	0	102.0
116	0	0	0	0	0	0	0	0	0	0	113	0	0	0	0	0	0	0	0	702.0
117	0	0	0	0	0	0	0	0	0	0	114	0	0	0	0	0	0	0	0	390.0
118	0	0	0	0	0	0	0	0	0	0	115	0	0	0	0	0	0	0	0	453.0
119	120	118	0	0	0	0	0	0	0	0	116	0	0	0	0	0	0	0	0	707.0
120	0	0	0	0	0	0	0	0	0	0	117	0	0	0	0	0	0	0	0	220.0
121	0	0	0	0	0	0	0	0	0	0	74	0	0	0	0	0	0	0	0	326.0
122	124	123	0	0	0	0	0	0	0	0	118	0	0	0	0	0	0	0	0	2595.0
123	127	128	0	0	0	0	0	0	0	0	119	0	0	0	0	0	0	0	0	1409.0
124	125	126	0	0	0	0	0	0	0	0	120	0	0	0	0	0	0	0	0	705.0
125	0	0	0	0	0	0	0	0	0	0	124	0	0	0	0	0	0	0	0	220.0
126	0	0	0	0	0	0	0	0	0	0	125	0	0	0	0	0	0	0	0	88.0
127	0	0	0	0	0	0	0	0	0	0	126	0	0	0	0	0	0	0	0	548.0

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128	0	0	0	0	0	0	0	0	0	0	127	0	0	0	0	0	0	0	0	0	472.0
129	137	130	0	0	0	0	0	0	0	0	128	0	0	0	0	0	0	0	0	0	30354.0
130	133	131	132	0	0	0	0	0	0	0	129	0	0	0	0	0	0	0	0	0	2081.0
131	0	0	0	0	0	0	0	0	0	0	130	0	0	0	0	0	0	0	0	0	290.0
132	0	0	0	0	0	0	0	0	0	0	131	0	0	0	0	0	0	0	0	0	213.0
133	134	0	0	0	0	0	0	0	0	0	132	0	0	0	0	0	0	0	0	0	1468.0
134	135	136	0	0	0	0	0	0	0	0	133	0	0	0	0	0	0	0	0	0	972.0
135	0	0	0	0	0	0	0	0	0	0	134	0	0	0	0	0	0	0	0	0	160.0
136	0	0	0	0	0	0	0	0	0	0	135	0	0	0	0	0	0	0	0	0	282.0
137	138	139	0	0	0	0	0	0	0	0	136	0	0	0	0	0	0	0	0	0	28122.0
138	0	0	0	0	0	0	0	0	0	0	137	0	0	0	0	0	0	0	0	0	383.0
139	149	140	0	0	0	0	0	0	0	0	138	0	0	0	0	0	0	0	0	0	27597.0
140	142	141	0	0	0	0	0	0	0	0	139	0	0	0	0	0	0	0	0	0	2013.0
141	0	0	0	0	0	0	0	0	0	0	140	0	0	0	0	0	0	0	0	0	132.0
142	146	143	0	0	0	0	0	0	0	0	141	0	0	0	0	0	0	0	0	0	1697.0
143	144	145	0	0	0	0	0	0	0	0	142	0	0	0	0	0	0	0	0	0	540.0
144	0	0	0	0	0	0	0	0	0	0	143	0	0	0	0	0	0	0	0	0	274.0
145	0	0	0	0	0	0	0	0	0	0	144	0	0	0	0	0	0	0	0	0	79.0
146	147	148	0	0	0	0	0	0	0	0	145	0	0	0	0	0	0	0	0	0	1054.0
147	0	0	0	0	0	0	0	0	0	0	146	0	0	0	0	0	0	0	0	0	283.0
148	0	0	0	0	0	0	0	0	0	0	147	0	0	0	0	0	0	0	0	0	453.0
149	152	150	151	0	0	0	0	0	0	0	148	0	0	0	0	0	0	0	0	0	15514.0
150	0	0	0	0	0	0	0	0	0	0	149	0	0	0	0	0	0	0	0	0	58.0
151	0	0	0	0	0	0	0	0	0	0	150	0	0	0	0	0	0	0	0	0	189.0
152	153	154	0	0	0	0	0	0	0	0	151	0	0	0	0	0	0	0	0	0	25053.0
153	0	0	0	0	0	0	0	0	0	0	152	0	0	0	0	0	0	0	0	0	249.0
154	156	155	0	0	0	0	0	0	0	0	153	0	0	0	0	0	0	0	0	0	24303.0
155	0	0	0	0	0	0	0	0	0	0	154	0	0	0	0	0	0	0	0	0	161.0
156	157	158	0	0	0	0	0	0	0	0	155	0	0	0	0	0	0	0	0	0	23893.0
157	172	163	170	171	0	0	0	0	0	0	156	0	0	0	0	0	0	0	0	0	21505.0
158	160	159	0	0	0	0	0	0	0	0	157	0	0	0	0	0	0	0	0	0	1865.0
159	0	0	0	0	0	0	0	0	0	0	158	0	0	0	0	0	0	0	0	0	476.0
160	161	162	0	0	0	0	0	0	0	0	159	0	0	0	0	0	0	0	0	0	1045.0
161	0	0	0	0	0	0	0	0	0	0	160	0	0	0	0	0	0	0	0	0	341.0
162	0	0	0	0	0	0	0	0	0	0	161	0	0	0	0	0	0	0	0	0	362.0
163	166	164	0	0	0	0	0	0	0	0	162	0	0	0	0	0	0	0	0	0	1286.0
164	0	0	0	0	0	0	0	0	0	0	163	0	0	0	0	0	0	0	0	0	76.0
165	168	169	0	0	0	0	0	0	0	0	164	0	0	0	0	0	0	0	0	0	784.0
166	165	167	0	0	0	0	0	0	0	0	165	0	0	0	0	0	0	0	0	0	1098.0
167	0	0	0	0	0	0	0	0	0	0	166	0	0	0	0	0	0	0	0	0	215.0
168	0	0	0	0	0	0	0	0	0	0	167	0	0	0	0	0	0	0	0	0	259.0
169	0	0	0	0	0	0	0	0	0	0	168	0	0	0	0	0	0	0	0	0	175.0
170	0	0	0	0	0	0	0	0	0	0	169	0	0	0	0	0	0	0	0	0	332.0
171	0	0	0	0	0	0	0	0	0	0	170	0	0	0	0	0	0	0	0	0	139.0
172	187	173	0	0	0	0	0	0	0	0	171	0	0	0	0	0	0	0	0	0	19645.0
173	174	175	0	0	0	0	0	0	0	0	172	0	0	0	0	0	0	0	0	0	5003.0
174	0	0	0	0	0	0	0	0	0	0	173	0	0	0	0	0	0	0	0	0	188.0
175	177	176	0	0	0	0	0	0	0	0	174	0	0	0	0	0	0	0	0	0	4585.0
176	180	179	0	0	0	0	0	0	0	0	175	0	0	0	0	0	0	0	0	0	3882.0
177	178	0	0	0	0	0	0	0	0	0	176	0	0	0	0	0	0	0	0	0	625.0
178	0	0	0	0	0	0	0	0	0	0	177	0	0	0	0	0	0	0	0	0	392.0

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179	0	0	0	0	0	0	0	0	0	0	178	0	0	0	0	0	0	0	0	0	211.0
180	181	182	0	0	0	0	0	0	0	0	179	0	0	0	0	0	0	0	0	0	2955.0
181	0	0	0	0	0	0	0	0	0	0	180	0	0	0	0	0	0	0	0	0	438.0
182	183	184	0	0	0	0	0	0	0	0	181	0	0	0	0	0	0	0	0	0	2016.0
183	0	0	0	0	0	0	0	0	0	0	182	0	0	0	0	0	0	0	0	0	599.0
184	186	185	0	0	0	0	0	0	0	0	183	0	0	0	0	0	0	0	0	0	910.0
185	0	0	0	0	0	0	0	0	0	0	184	0	0	0	0	0	0	0	0	0	232.0
186	0	0	0	0	0	0	0	0	0	0	185	0	0	0	0	0	0	0	0	0	461.0
187	192	193	0	0	0	0	0	0	0	0	186	0	0	0	0	0	0	0	0	0	14569.0
192	194	205	0	0	0	0	0	0	0	0	187	0	0	0	0	0	0	0	0	0	13278.0
193	0	0	0	0	0	0	0	0	0	0	188	0	0	0	0	0	0	0	0	0	273.0
194	198	199	196	195	0	0	0	0	0	0	189	0	0	0	0	0	0	0	0	0	5663.0
195	0	0	0	0	0	0	0	0	0	0	190	0	0	0	0	0	0	0	0	0	251.0
196	0	0	0	0	0	0	0	0	0	0	195	0	0	0	0	0	0	0	0	0	387.0
198	201	200	202	0	0	0	0	0	0	0	196	0	0	0	0	0	0	0	0	0	3544.0
199	0	0	0	0	0	0	0	0	0	0	197	0	0	0	0	0	0	0	0	0	634.0
200	0	0	0	0	0	0	0	0	0	0	198	0	0	0	0	0	0	0	0	0	542.0
201	204	203	0	0	0	0	0	0	0	0	199	0	0	0	0	0	0	0	0	0	1955.0
202	0	0	0	0	0	0	0	0	0	0	200	0	0	0	0	0	0	0	0	0	250.0
203	0	0	0	0	0	0	0	0	0	0	203	0	0	0	0	0	0	0	0	0	258.0
204	0	0	0	0	0	0	0	0	0	0	204	0	0	0	0	0	0	0	0	0	854.0
205	207	206	0	0	0	0	0	0	0	0	205	0	0	0	0	0	0	0	0	0	7500.0
206	0	0	0	0	0	0	0	0	0	0	206	0	0	0	0	0	0	0	0	0	250.0
207	211	208	0	0	0	0	0	0	0	0	207	0	0	0	0	0	0	0	0	0	6855.0
208	0	0	0	0	0	0	0	0	0	0	208	0	0	0	0	0	0	0	0	0	275.0
211	212	215	0	0	0	0	0	0	0	0	209	0	0	0	0	0	0	0	0	0	5808.0
212	214	213	0	0	0	0	0	0	0	0	210	0	0	0	0	0	0	0	0	0	1581.0
213	0	0	0	0	0	0	0	0	0	0	211	0	0	0	0	0	0	0	0	0	511.0
214	0	0	0	0	0	0	0	0	0	0	212	0	0	0	0	0	0	0	0	0	482.0
215	219	216	217	0	0	0	0	0	0	0	213	0	0	0	0	0	0	0	0	0	3943.0
216	0	0	0	0	0	0	0	0	0	0	214	0	0	0	0	0	0	0	0	0	505.0
217	0	0	0	0	0	0	0	0	0	0	215	0	0	0	0	0	0	0	0	0	245.0
218	222	221	0	0	0	0	0	0	0	0	219	0	0	0	0	0	0	0	0	0	1711.0
219	220	218	0	0	0	0	0	0	0	0	220	0	0	0	0	0	0	0	0	0	2654.0
220	0	0	0	0	0	0	0	0	0	0	221	0	0	0	0	0	0	0	0	0	506.0
221	0	0	0	0	0	0	0	0	0	0	222	0	0	0	0	0	0	0	0	0	250.0
222	224	223	0	0	0	0	0	0	0	0	223	0	0	0	0	0	0	0	0	0	1417.0
223	0	0	0	0	0	0	0	0	0	0	224	0	0	0	0	0	0	0	0	0	309.0
224	226	225	0	0	0	0	0	0	0	0	225	0	0	0	0	0	0	0	0	0	926.0
225	0	0	0	0	0	0	0	0	0	0	226	0	0	0	0	0	0	0	0	0	152.0
226	0	0	0	0	0	0	0	0	0	0	227	0	0	0	0	0	0	0	0	0	286.0
231	252	0	0	0	0	0	0	0	0	0	231	0	0	0	0	0	0	0	0	0	86054.0
232	234	233	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
233	251	0	0	0	0	0	0	0	0	0	233	0	0	0	0	0	0	0	0	0	85477.0
234	239	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	187.0
235	0	0	0	0	0	0	0	0	0	0	235	0	0	0	0	0	0	0	0	0	187.0
236	232	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
237	238	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
238	1927	240	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
239	235	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	187.0
240	241	0	0	0	0	0	0	0	0	0	240	0	0	0	0	0	0	0	0	0	84397.0

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241	242	0	0	0	0	0	0	0	0	0	241	0	0	0	0	0	0	0	0	84351.0
242	377	289	243	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	84008.0
243	1427	0	0	0	0	0	0	0	0	0	243	0	0	0	0	0	0	0	0	80261.0
244	0	0	0	0	0	0	0	0	0	0	253	0	0	0	0	0	0	0	0	848.0
245	1	246	0	0	0	0	0	0	0	0	254	0	0	0	0	0	0	0	0	67230.0
246	247	250	0	0	0	0	0	0	0	0	255	0	0	0	0	0	0	0	0	2389.0
247	0	0	0	0	0	0	0	0	0	0	256	0	0	0	0	0	0	0	0	809.0
248	0	0	0	0	0	0	0	0	0	0	257	0	0	0	0	0	0	0	0	645.0
249	0	0	0	0	0	0	0	0	0	0	258	0	0	0	0	0	0	0	0	377.0
250	248	249	0	0	0	0	0	0	0	0	259	0	0	0	0	0	0	0	0	1131.0
251	237	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
252	236	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
261	44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	80179.0
262	1935	0	0	0	0	0	0	0	0	0	262	0	0	0	0	0	0	0	0	2758.0
263	262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2758.0
264	1905	0	0	0	0	0	0	0	0	0	264	0	0	0	0	0	0	0	0	2784.0
265	264	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
266	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
267	293	1267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
268	267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
269	265	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
270	271	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86842.0
271	319	231	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86842.0
280	294	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
289	1924	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3653.0
290	1290	0	0	0	0	0	0	0	0	0	290	0	0	0	0	0	0	0	0	3653.0
291	1291	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
292	1923	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
293	1293	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
294	1294	304	1920	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
295	1295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
296	1296	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
297	298	0	0	0	0	0	0	0	0	0	297	0	0	0	0	0	0	0	0	587.0
298	303	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	249.0
299	0	0	0	0	0	0	0	0	0	0	299	0	0	0	0	0	0	0	0	72.0
300	301	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	177.0
301	0	0	0	0	0	0	0	0	0	0	301	0	0	0	0	0	0	0	0	177.0
303	299	1922	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	249.0
304	0	0	0	0	0	0	0	0	0	0	304	0	0	0	0	0	0	0	0	150.0
308	396	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
310	1409	1310	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
311	371	312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	247.0
312	1940	0	0	0	0	0	0	0	0	0	312	0	0	0	0	0	0	0	0	100.0
313	1939	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
314	308	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
315	310	0	0	0	0	0	0	0	0	0	315	0	0	0	0	0	0	0	0	28.0
316	0	0	0	0	0	0	0	0	0	0	316	0	0	0	0	0	0	0	0	43.0
317	315	316	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	71.0
318	338	0	0	0	0	0	0	0	0	0	318	0	0	0	0	0	0	0	0	230.0
319	1946	0	0	0	0	0	0	0	0	0	319	0	0	0	0	0	0	0	0	788.0
320	1320	0	0	0	0	0	0	0	0	0	320	0	0	0	0	0	0	0	0	454.0

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321	1321	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
322	1909	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
323	1323	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9.0
324	325	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
325	1325	326	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
326	327	317	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
327	1311	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
328	337	1329	329	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
329	330	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
330	1306	1303	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
331	1331	1407	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
332	333	334	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
333	1333	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.0
334	1334	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.0
335	1335	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
336	1336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
337	331	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	50.0
338	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73.0
339	1822	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
340	1340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
341	1341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
342	1342	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
343	1343	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
344	366	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
345	346	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	149.0
346	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	71.0
347	1915	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	212.0
348	1348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
349	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	13.0
350	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	51.0
351	1814	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	100.0
352	1919	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
353	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
354	1817	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.0
355	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
356	359	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
357	1357	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
358	311	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
359	345	347	349	355	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
360	1360	292	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
361	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30.0
362	1362	363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
366	1366	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
367	1367	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	23.0
368	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
369	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	17.0
370	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
371	372	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	147.0
372	374	373	367	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	64.0
373	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	38.0

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374	1374	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
375	376	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
376	266	0	0	0	0	0	0	0	0	0	376	0	0	0	0	0	0	0	0	3.0
377	1925	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
378	1378	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
379	380	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
380	1821	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
381	382	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
382	1381	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
383	1820	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
384	0	0	0	0	0	0	0	0	0	0	384	0	0	0	0	0	0	0	0	77.0
385	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
386	1386	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
387	1387	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
388	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
389	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
390	1912	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
391	392	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
392	1941 1392	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
393	358	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
394	395	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
395	386	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
396	1396	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
397	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	39647.0
398	362	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
399	270	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	36842.0
1238	390	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1289	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1290	291	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
1291	268	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
1293	280	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
1294	269	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
1295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1296	295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1301	335	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
1302	1301	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
1303	1302	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
1304	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1305	1307 1304	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
1306	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1307	1308	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
1308	332	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
1309	328	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
1310	336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1311	1309	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
1312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1313	339	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1320	1908 1907 1361	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	293.0
1321	323	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9.0

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1323	1402	0	0	0	0	0	0	0	0	0	1323	0	0	0	0	0	0	0	0	0	9.0
1325	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1329	0	0	0	0	0	0	0	0	0	0	336	0	0	0	0	0	0	0	0	0	31.0
1330	368 1312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1331	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1332	1330	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1333	340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1334	341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1335	342	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
1336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1337	321	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
1338	1337	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
1339	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1342	343	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
1343	356	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
1348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1357	393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1360	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1361	1338	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
1362	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1364	361 1363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30.0
1365	1370 1364	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	129.0
1366	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1367	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1368	1332	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1369	1368	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1370	1369	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1371	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1372	1371 1377	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1373	1945	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1374	375	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
1375	1373	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1376	1375	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1377	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1378	1406 1404	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1381	1382 1405	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1382	296	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1386	1937 385	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1387	1401	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1392	324	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
1393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1396	398	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1401	357	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1402	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1403	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1404	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1405	383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0

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1406	379	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1407	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1408	344	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
1409	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1410	0	0	0	0	0	0	0	0	0	0	1410	0	0	0	0	0	0	0	195.0
1411	1410	1424	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1412	1411	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1413	1412	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1414	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1415	0	0	0	0	0	0	0	0	0	0	1415	0	0	0	0	0	0	0	307.0
1416	1415	1553	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1203.0
1420	0	0	0	0	0	0	0	0	0	0	1420	0	0	0	0	0	0	0	59.0
1421	1420	1426	1441	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1423	1421	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1424	1423	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1425	0	0	0	0	0	0	0	0	0	0	1425	0	0	0	0	0	0	0	68.0
1426	1438	1425	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	382.0
1427	261	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	83179.0
1428	1528	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1429	1428	1416	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1203.0
1430	0	0	0	0	0	0	0	0	0	0	1430	0	0	0	0	0	0	0	82.0
1431	1430	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	82.0
1435	0	0	0	0	0	0	0	0	0	0	1435	0	0	0	0	0	0	0	232.0
1436	1435	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	232.0
1438	1436	1431	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	314.0
1440	0	0	0	0	0	0	0	0	0	0	1440	0	0	0	0	0	0	0	66.0
1441	1453	1440	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76465.0
1442	1514	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2719.0
1445	0	0	0	0	0	0	0	0	0	0	1445	0	0	0	0	0	0	0	164.0
1446	1445	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	164.0
1450	0	0	0	0	0	0	0	0	0	0	1450	0	0	0	0	0	0	0	198.0
1451	1603	1450	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76235.0
1453	1446	1451	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76399.0
1455	0	0	0	0	0	0	0	0	0	0	1455	0	0	0	0	0	0	0	542.0
1456	1455	1482	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1274.0
1457	1456	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1274.0
1460	0	0	0	0	0	0	0	0	0	0	1460	0	0	0	0	0	0	0	286.0
1461	1460	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	286.0
1465	0	0	0	0	0	0	0	0	0	0	1465	0	0	0	0	0	0	0	93.0
1467	1933	1932	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2351.0
1468	1467	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2351.0
1480	1938	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1481	1480	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1482	1481	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1490	0	0	0	0	0	0	0	0	0	0	1490	0	0	0	0	0	0	0	698.0
1491	1490	1457	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1372.0
1500	0	0	0	0	0	0	0	0	0	0	1500	0	0	0	0	0	0	0	465.0
1501	1500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	465.0
1505	0	0	0	0	0	0	0	0	0	0	1505	0	0	0	0	0	0	0	262.0
1506	1505	1800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79714.0
1507	1506	1508	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79714.0

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1620	0	0	0	0	0	0	0	0	0	0	1620	0	0	0	0	0	0	0	0	0	324.0
1621	1653	1620	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1816.0
1623	1616	1621	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2044.0
1624	1623	1705	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2111.0
1625	0	0	0	0	0	0	0	0	0	0	1625	0	0	0	0	0	0	0	0	0	197.0
1626	48	1625	1636	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	72591.0
1628	1631	1626	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73076.0
1630	0	0	0	0	0	0	0	0	0	0	1630	0	0	0	0	0	0	0	0	0	159.0
1631	1643	1630	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	485.0
1635	0	0	0	0	0	0	0	0	0	0	1635	0	0	0	0	0	0	0	0	0	317.0
1636	1635	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	317.0
1640	0	0	0	0	0	0	0	0	0	0	1640	0	0	0	0	0	0	0	0	0	200.0
1641	1640	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	200.0
1643	1646	1641	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	326.0
1645	0	0	0	0	0	0	0	0	0	0	1645	0	0	0	0	0	0	0	0	0	126.0
1646	1645	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	126.0
1650	0	0	0	0	0	0	0	0	0	0	1650	0	0	0	0	0	0	0	0	0	382.0
1651	1661	1650	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	934.0
1653	1651	1656	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1492.0
1655	0	0	0	0	0	0	0	0	0	0	1655	0	0	0	0	0	0	0	0	0	558.0
1656	1655	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	558.0
1660	0	0	0	0	0	0	0	0	0	0	1660	0	0	0	0	0	0	0	0	0	552.0
1661	1660	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	552.0
1665	0	0	0	0	0	0	0	0	0	0	1665	0	0	0	0	0	0	0	0	0	390.0
1666	1665	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	390.0
1705	0	0	0	0	0	0	0	0	0	0	1705	0	0	0	0	0	0	0	0	0	67.0
1710	0	0	0	0	0	0	0	0	0	0	1710	0	0	0	0	0	0	0	0	0	245.0
1711	1710	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	245.0
1712	1711	1624	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2356.0
1715	0	0	0	0	0	0	0	0	0	0	1715	0	0	0	0	0	0	0	0	0	115.0
1716	1715	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	115.0
1800	1509	1468	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79452.0
1812	352	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1813	1812	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1814	1813	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1815	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1816	1815	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1817	1818	1816	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.0
1818	0	0	0	0	0	0	0	0	0	0	354	0	0	0	0	0	0	0	0	0	6.0
1820	384	1383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1821	369	1926	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1822	1339	394	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1905	263	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2758.0
1906	389	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1907	388	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1908	387	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1909	1906	320	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
1910	313	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1911	391	318	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1912	1911	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1913	351	354	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	106.0

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1914	1913	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	106.0
1915	350	1914	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	157.0
1916	1262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1917	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	103.0
1919	1934	353	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1920	1921	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	690.0
1921	297	1917	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	690.0
1922	300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	177.0
1923	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1924	290	1289	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3653.0
1925	378	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1926	381	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1927	1238	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1928	1611	1606	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73656.0
1929	1712	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2356.0
1931	1491	1461	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2258.0
1932	1465	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	93.0
1933	1931	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2258.0
1934	360	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1935	2442	1916	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2719.0
1937	348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1938	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1939	1313	314	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1940	1910	1408	1942	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	88.0
1941	1393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1942	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1943	322	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
1944	1365	370	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1945	1944	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1946	1376	1943	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	624.0
1947	1599	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86952.0

ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER 359 TO GUTTER 266 COMP THROUGH DIVERSION WILL LAG ONE TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.
 ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER 428 TO GUTTER 385 COMP THROUGH DIVERSION WILL LAG ONE TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.
 ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER 541 TO GUTTER 388 COMP THROUGH DIVERSION WILL LAG ONE TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.
 ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER 565 TO GUTTER 389 COMP THROUGH DIVERSION WILL LAG ONE TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.

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SBC CHANGES FROM DRAFT REPORT MODEL SBC_1N.SWI - ASSORTED MODIFICATIONS
 model sbc_1tc.swi with narrowing of conveyance 1330 overflow channel from 50' to

*** PEAK FLOWS, STAGES AND STORAGES OF GUTTERS AND DETENTION DAMS ***

CONVEYANCE ELEMENT	PEAK (CFS)	STAGE (FT)	STORAGE (AC-FT)	TIME (HR/MIN)				
1	4277.	6.4		12 30.	99	1317.	4.0	8 40.
2	1975.	5.5		8 35.	100	300.	2.0	8 30.
3	788.	1.9		8 30.	101	1001.	3.7	8 40.
4	790.	1.7		8 30.	102	601.	2.6	8 35.
5	4099.	6.3		12 30.	103	518.	1.9	8 25.
6	4036.	5.5		12 25.	104	408.	2.6	8 25.
7	615.	3.6		8 30.	105	79.	1.2	8 15.
8	9148.	(DIRECT FLOW)		9 25.	106	55.	1.0	8 25.
9	303.	2.3		8 30.	107	378.	2.4	8 35.
10	157.	.8		8 20.	108	58.	.8	8 30.
11	159.	1.0		8 10.	109	300.	1.9	8 35.
12	137.	.9		8 20.	110	211.	1.7	8 30.
13	458.	1.5		8 20.	111	60.	.8	8 30.
14	160.	.9		8 10.	112	105.	1.2	8 30.
15	7524.	(DIRECT FLOW)		10 0.	113	51.	.8	8 30.
16	7499.	(DIRECT FLOW)		10 0.	114	20.	.5	8 20.
17	755.	2.2		8 30.	115	35.	.7	8 25.
18	478.	2.5		8 30.	116	80.	1.2	8 35.
20	114.	2.1		8 20.	117	132.	1.7	8 20.
21	147.	1.2		8 30.	118	85.	1.2	8 30.
22	1730.	4.0		8 45.	119	165.	2.1	8 25.
23	825.	3.5		8 50.	120	78.	1.2	8 15.
24	660.	3.1		8 40.	121	151.	1.5	8 35.
25	178.	1.2		8 30.	122	477.	2.0	8 50.
26	452.	2.8		8 30.	123	266.	1.5	8 40.
27	44.	.4		8 25.	124	141.	1.3	8 35.
28	347.	1.5		8 30.	125	34.	.6	8 30.
29	87.	1.0		8 25.	126	24.	.5	8 30.
30	192.	1.2		8 35.	127	104.	.9	8 30.
31	198.	1.5		8 35.	128	95.	.8	8 35.
32	40.	.6		8 30.	129	4091.	6.1	9 50.
33	141.	1.2		8 30.	130	367.	1.7	8 40.
34	278.	1.9		8 45.	131	85.	.8	8 15.
35	93.	.8		8 25.	132	49.	.8	8 30.
36	119.	.9		8 40.	133	225.	1.5	8 45.
37	265.	2.0		8 45.	134	157.	1.3	8 35.
38	59.	.5		8 25.	135	15.	.4	8 25.
39	162.	1.1		8 30.	136	25.	.6	8 10.
40	7225.	7.8		10 5.	137	3876.	4.7	9 45.
41	119.	.8		8 25.	138	128.	1.2	8 40.
42	7156.	7.1		10 0.	139	3761.	4.6	9 40.
44	8238.	(DIRECT FLOW)		10 30.	140	378.	1.9	8 45.
46	6679.	7.7		10 0.	141	83.	1.1	8 30.
48	7915.	9.0		9 5.	142	268.	1.8	8 40.
49	380.	1.6		8 10.	143	102.	1.1	8 30.
50	7883.	6.2		8 55.	144	39.	.7	8 15.
51	701.	3.1		8 15.	145	17.	.6	8 30.
52	6888.	7.3		8 50.	146	146.	1.2	8 40.
53	182.	1.9		8 10.	147	53.	.7	8 35.
54	59.	1.0		8 10.	148	59.	.8	8 15.
55	73.	1.1		8 15.	149	3534.	4.3	9 40.
56	1033.	2.7		8 25.	150	50.	.8	8 20.
57	497.	1.5		8 20.	151	113.	1.2	8 30.
58	51.	.9		8 10.	152	3439.	4.5	9 35.
59	6609.	7.6		10 0.	153	43.	.5	8 30.
60	116.	1.0		8 30.	154	3466.	4.8	9 20.
61	304.	2.1		8 45.	155	51.	.4	8 30.
62	642.	2.1		8 45.	156	3406.	4.8	9 15.
63	47.	.8		8 40.	157	3188.	4.8	9 10.
64	49.	1.2		8 30.	158	231.	1.2	8 35.
65	317.	2.9		8 45.	159	37.	.5	8 20.
66	32.	.5		8 25.	160	138.	1.1	8 30.
67	263.	1.7		8 35.	161	57.	.9	8 30.
68	358.	1.8		8 30.	162	31.	.6	8 15.
69	123.	1.0		8 25.	163	216.	1.1	8 35.
70	184.	1.2		8 25.	164	30.	.4	8 30.
71	335.	2.0		8 40.	165	105.	1.0	8 30.
72	117.	1.1		8 30.	166	162.	1.1	8 35.
73	103.	1.2		8 35.	167	48.	.7	8 30.
74	6431.	7.4		9 55.	168	22.	.5	8 10.
75	1217.	4.2		9 5.	169	15.	.4	8 10.
76	192.	1.4		8 35.	170	160.	1.4	8 30.
77	1406.	3.8		9 10.	171	100.	1.0	8 25.
78	37.	.6		8 35.	172	2831.	5.3	9 10.
79	1179.	3.4		9 5.	173	1054.	2.1	8 45.
80	903.	1.9		8 45.	174	59.	.8	8 25.
81	357.	1.8		8 50.	175	878.	2.0	8 40.
82	185.	1.2		8 40.	176	766.	2.6	8 40.
83	31.	.6		8 30.	177	98.	1.0	8 35.
84	127.	1.1		8 35.	178	43.	.8	8 20.
85	26.	.9		8 30.	179	76.	.4	8 30.
86	76.	.9		8 35.	180	411.	2.2	8 30.
87	221.	1.7		8 50.	181	38.	.7	8 10.
88	195.	1.1		8 45.	182	226.	1.3	8 25.
89	127.	1.5		8 45.	183	45.	.7	8 15.
93	12.	.4		8 10.	184	150.	.9	8 20.
94	5203.	5.7		10 0.	185	34.	.8	8 20.
95	4447.	5.2		10 0.	186	97.	.9	8 15.
96	4412.	7.3		9 55.	187	1984.	3.8	9 20.
97	1517.	3.9		8 45.	192	1972.	3.7	9 0.
98	200.	1.5		8 25.	193	182.	.6	8 20.

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194	656.	2.1	8	40.	331	869.	(DIRECT FLOW)	11	35.	
195	21.	.4	8	25.	332	1074.	(DIRECT FLOW)	11	40.	
196	27.	.6	8	10.	333	511.	1.9	11	40.	
198	507.	2.0	8	35.	334	568.	2.0	11	35.	
199	49.	.8	8	30.	335	866.	4.0	11	40.	
200	44.	.7	8	20.	336	414.	(DIRECT FLOW)	11	40.	
201	431.	1.8	8	25.	337	859.	2.3	11	40.	
202	22.	.5	8	10.	338	103.	1.8	8	25.	
203	105.	1.0	8	10.	339	621.	(DIRECT FLOW)	11	35.	
204	318.	1.4	8	20.	340	1621.	(DIRECT FLOW)	11	30.	
205	1354.	3.4	9	0.	341	2203.	(DIRECT FLOW)	11	25.	
206	23.	.2	8	10.	342	3152.	(DIRECT FLOW)	11	25.	
207	1332.	2.8	8	50.	343	3856.	(DIRECT FLOW)	11	25.	
208	25.	.4	8	20.	344	170.	(DIRECT FLOW)	8	15.	
211	1320.	3.7	8	35.	345	377.	1.6	8	10.	
212	327.	1.4	8	30.	346	210.	1.1	8	5.	
213	208.	1.2	8	25.	347	3857.	7.3	11	25.	
214	111.	.8	8	15.	348	1098.	(DIRECT FLOW)	11	35.	
215	981.	2.9	8	30.	349	12.	.3	8	25.	
216	148.	.7	8	15.	350	147.	3.2	8	10.	
217	22.	.2	8	5.	351	2281.	5.7	11	20.	
218	578.	3.0	8	20.	352	3872.	.1	23.0	11	15.
219	825.	2.6	8	25.	353	89.	1.1	8	10.	
220	238.	1.2	8	20.	354	1584.	3.0	11	25.	
221	84.	1.0	8	15.	355	19.	2.2	8	10.	
222	490.	2.7	8	20.	356	3856.	.1	20.8	11	25.
223	148.	.8	8	20.	357	583.	(DIRECT FLOW)	8	25.	
224	341.	2.4	8	15.	358	687.	4.6	8	25.	
225	79.	1.0	8	10.	359	3868.	(DIRECT FLOW)	11	25.	
226	130.	.6	8	10.	360	3887.	(DIRECT FLOW)	11	10.	
231	2378.	3.4	8	35.	361	79.	(DIRECT FLOW)	8	5.	
232	2406.	(DIRECT FLOW)	12	10.	362	704.	(DIRECT FLOW)	11	25.	
233	2396.	4.3	12	10.	363	15.	.5	8	10.	
234	208.	2.8	8	35.	366	170.	1.2	8	15.	
235	245.	1.1	8	20.	367	69.	.8	8	10.	
236	2406.	(DIRECT FLOW)	12	10.	368	167.	(DIRECT FLOW)	8	10.	
237	4972.	(DIRECT FLOW)	11	40.	369	57.	.8	8	5.	
238	4972.	(DIRECT FLOW)	11	40.	370	158.	(DIRECT FLOW)	8	5.	
239	245.	(DIRECT FLOW)	8	20.	371	254.	2.0	8	20.	
240	4769.	4.0	11	40.	372	112.	(DIRECT FLOW)	8	15.	
241	4835.	3.8	11	20.	373	26.	1.2	8	30.	
242	5049.	(DIRECT FLOW)	10	55.	374	36.	1.4	10	55.	
243	3929.	3.5	10	40.	375	231.	(DIRECT FLOW)	10	45.	
244	1385.	3.1	8	20.	376	231.	3.8	10	45.	
245	5962.	7.4	8	45.	377	109.	3.1	11	30.	
246	2497.	4.4	8	30.	378	353.	(DIRECT FLOW)	11	5.	
247	842.	2.3	8	25.	379	198.	(DIRECT FLOW)	8	15.	
248	704.	2.0	8	25.	380	198.	4.0	8	15.	
249	457.	1.8	8	20.	381	285.	(DIRECT FLOW)	11	10.	
250	1192.	3.2	8	25.	382	285.	5.9	11	10.	
251	2399.	(DIRECT FLOW)	11	40.	383	1757.	(DIRECT FLOW)	11	10.	
252	2303.	(DIRECT FLOW)	12	10.	384	187.	4.0	8	10.	
261	8238.	(DIRECT FLOW)	10	30.	385	369.	(DIRECT FLOW)	11	35.	
262	5374.	2.9	10	40.	386	850.	(DIRECT FLOW)	11	35.	
263	5374.	(DIRECT FLOW)	10	40.	387	127.	(DIRECT FLOW)	11	50.	
264	5119.	2.9	10	45.	388	848.	(DIRECT FLOW)	8	45.	
265	5119.	(DIRECT FLOW)	10	45.	389	2573.	(DIRECT FLOW)	11	40.	
266	231.	(DIRECT FLOW)	10	40.	390	1051.	(DIRECT FLOW)	8	45.	
267	3347.	(DIRECT FLOW)	10	45.	391	894.	6.6	12	0.	
268	3294.	.1	53.3	10	392	895.	(DIRECT FLOW)	11	55.	
269	2237.	(DIRECT FLOW)	10	45.	393	687.	(DIRECT FLOW)	8	25.	
270	6320.	8.2	12	50.	394	596.	2.1	11	35.	
271	6390.	(DIRECT FLOW)	12	35.	395	598.	(DIRECT FLOW)	11	35.	
280	2312.	(DIRECT FLOW)	10	45.	396	703.	(DIRECT FLOW)	11	30.	
289	1113.	6.0	11	20.	397	4029.	.1	1783.9	12	20.
290	872.	5.3	11	0.	398	703.	.1	3.7	11	30.
291	3294.	(DIRECT FLOW)	10	55.	399	6320.	(DIRECT FLOW)	12	50.	
292	2420.	3.3	11	0.	1238	203.	(DIRECT FLOW)	8	45.	
293	467.	9.2	10	50.	1262	4259.	(DIRECT FLOW)	10	35.	
294	2312.	(DIRECT FLOW)	10	45.	1267	2881.	(DIRECT FLOW)	10	45.	
295	1783.	.1	89.2	11	5.	1289	243.	(DIRECT FLOW)	11	10.
296	1783.	(DIRECT FLOW)	11	5.	1290	870.	(DIRECT FLOW)	10	55.	
297	902.	4.6	8	10.	1291	3294.	(DIRECT FLOW)	10	55.	
298	127.	.1	2.8	8	25.	1293	467.	(DIRECT FLOW)	10	45.
299	191.	.9	8	10.	1294	2225.	2.7	10	45.	
300	11.	.1	24.6	10	35.	1295	1845.	(DIRECT FLOW)	10	50.
301	435.	1.0	8	10.	1296	1783.	(DIRECT FLOW)	11	5.	
303	201.	(DIRECT FLOW)	8	10.	1301	866.	(DIRECT FLOW)	11	40.	
304	78.	1.5	8	25.	1302	866.	(DIRECT FLOW)	11	40.	
308	334.	(DIRECT FLOW)	11	30.	1303	633.	(DIRECT FLOW)	11	40.	
310	467.	(DIRECT FLOW)	11	40.	1304	233.	(DIRECT FLOW)	11	40.	
311	681.	(DIRECT FLOW)	8	20.	1305	1247.	(DIRECT FLOW)	11	40.	
312	587.	5.6	11	45.	1306	60.	(DIRECT FLOW)	11	45.	
313	541.	(DIRECT FLOW)	11	35.	1307	1014.	(DIRECT FLOW)	11	40.	
314	334.	5.7	11	30.	1308	1074.	(DIRECT FLOW)	11	40.	
315	458.	1.7	11	50.	1309	1548.	(DIRECT FLOW)	11	40.	
316	103.	1.0	8	10.	1310	207.	(DIRECT FLOW)	11	40.	
317	461.	(DIRECT FLOW)	11	50.	1311	1264.	(DIRECT FLOW)	11	40.	
318	211.	3.2	8	35.	1312	285.	(DIRECT FLOW)	11	40.	
319	4066.	7.9	12	35.	1313	207.	(DIRECT FLOW)	11	35.	
320	1406.	2.6	12	10.	1320	1404.	(DIRECT FLOW)	12	5.	
321	1322.	2.6	11	55.	1321	1329.	(DIRECT FLOW)	11	50.	
322	3924.	(DIRECT FLOW)	12	5.	1323	1424.	(DIRECT FLOW)	11	50.	
323	1424.	(DIRECT FLOW)	11	50.	1325	552.	(DIRECT FLOW)	8	30.	
324	2229.	(DIRECT FLOW)	11	50.	1329	80.	.9	8	10.	
325	2229.	(DIRECT FLOW)	11	50.	1330	277.	3.3	11	55.	
326	1719.	7.3	11	50.	1331	618.	(DIRECT FLOW)	11	35.	
327	1257.	6.6	11	45.	1332	277.	(DIRECT FLOW)	11	55.	
328	1548.	(DIRECT FLOW)	11	40.	1333	523.	(DIRECT FLOW)	11	30.	
329	690.	5.5	11	45.	1334	583.	(DIRECT FLOW)	11	25.	
330	693.	(DIRECT FLOW)	11	40.	1335	949.	(DIRECT FLOW)	11	25.	

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1336	414.	(DIRECT FLOW)	11	40.	1517	64.	1.1	8	55.
1337	1322.	(DIRECT FLOW)	11	55.	1520	176.	(DIRECT FLOW)	8	10.
1338	604.	(DIRECT FLOW)	11	55.	1521	7373.	4.9	10	5.
1339	26.	(DIRECT FLOW)	8	20.	1522	7468.	(DIRECT FLOW)	10	10.
1340	1621.	(DIRECT FLOW)	11	30.	1525	98.	(DIRECT FLOW)	8	10.
1341	2203.	(DIRECT FLOW)	11	25.	1526	2790.	3.6	9	50.
1342	3152.	(DIRECT FLOW)	11	25.	1528	2332.	(DIRECT FLOW)	9	45.
1343	3856.	(DIRECT FLOW)	11	25.	1530	187.	(DIRECT FLOW)	8	10.
1348	1098.	(DIRECT FLOW)	11	35.	1531	522.	2.3	8	40.
1357	583.	(DIRECT FLOW)	8	25.	1532	2999.	(DIRECT FLOW)	9	45.
1360	1503.	(DIRECT FLOW)	11	15.	1533	7442.	(DIRECT FLOW)	10	0.
1361	601.	3.3	11	55.	1534	4537.	3.5	10	5.
1362	704.	(DIRECT FLOW)	11	25.	1537	2991.	3.8	9	50.
1363	718.	(DIRECT FLOW)	11	55.	1541	303.	(DIRECT FLOW)	8	10.
1364	705.	3.5	12	5.	1542	204.	2.1	8	30.
1365	974.	(DIRECT FLOW)	12	0.	1544	7443.	(DIRECT FLOW)	10	5.
1366	128.	(DIRECT FLOW)	11	15.	1545	216.	(DIRECT FLOW)	8	15.
1367	14.	(DIRECT FLOW)	8	20.	1546	392.	2.3	8	35.
1368	277.	(DIRECT FLOW)	11	55.	1548	7431.	3.1	10	10.
1369	272.	(DIRECT FLOW)	11	55.	1550	534.	(DIRECT FLOW)	8	15.
1370	269.	3.1	12	0.	1551	671.	2.6	8	35.
1371	4.	(DIRECT FLOW)	11	55.	1553	852.	(DIRECT FLOW)	8	35.
1372	620.	(DIRECT FLOW)	12	5.	1556	89.	(DIRECT FLOW)	8	15.
1373	972.	(DIRECT FLOW)	12	5.	1557	181.	2.1	8	35.
1374	36.	(DIRECT FLOW)	10	45.	1560	178.	(DIRECT FLOW)	8	10.
1375	354.	(DIRECT FLOW)	12	5.	1561	178.	1.6	8	15.
1376	353.	3.5	12	5.	1563	304.	(DIRECT FLOW)	8	15.
1377	618.	(DIRECT FLOW)	12	5.	1565	126.	(DIRECT FLOW)	8	10.
1378	353.	(DIRECT FLOW)	11	5.	1566	126.	1.3	8	15.
1381	285.	(DIRECT FLOW)	11	10.	1570	134.	(DIRECT FLOW)	8	15.
1382	31.	(DIRECT FLOW)	11	5.	1571	133.	.6	8	20.
1383	1752.	(DIRECT FLOW)	11	10.	1575	340.	(DIRECT FLOW)	8	10.
1386	850.	(DIRECT FLOW)	11	35.	1576	274.	2.5	8	25.
1387	127.	(DIRECT FLOW)	11	50.	1599	7517.	(DIRECT FLOW)	12	30.
1392	806.	(DIRECT FLOW)	11	50.	1600	8.	(DIRECT FLOW)	8	0.
1393	104.	(DIRECT FLOW)	8	30.	1601	8487.	5.5	9	20.
1396	703.	(DIRECT FLOW)	11	30.	1603	9605.	(DIRECT FLOW)	9	15.
1401	32.	(DIRECT FLOW)	8	25.	1605	93.	(DIRECT FLOW)	8	15.
1402	1424.	(DIRECT FLOW)	11	50.	1606	723.	2.7	8	20.
1403	103.	(DIRECT FLOW)	12	10.	1610	66.	(DIRECT FLOW)	8	15.
1404	195.	(DIRECT FLOW)	10	45.	1611	8277.	5.3	9	15.
1405	253.	(DIRECT FLOW)	11	10.	1615	123.	(DIRECT FLOW)	8	15.
1406	184.	(DIRECT FLOW)	8	15.	1616	103.	1.7	8	25.
1407	251.	(DIRECT FLOW)	11	35.	1620	155.	(DIRECT FLOW)	8	15.
1408	144.	(DIRECT FLOW)	8	15.	1621	1278.	4.0	8	40.
1409	260.	(DIRECT FLOW)	11	40.	1623	1363.	(DIRECT FLOW)	8	40.
1410	57.	(DIRECT FLOW)	8	10.	1624	1369.	4.0	8	45.
1411	6698.	5.9	9	50.	1625	373.	(DIRECT FLOW)	8	10.
1412	6698.	(DIRECT FLOW)	9	50.	1626	8141.	5.6	9	10.
1413	6698.	(DIRECT FLOW)	9	50.	1628	8482.	(DIRECT FLOW)	9	5.
1414	4577.	(DIRECT FLOW)	9	55.	1630	185.	(DIRECT FLOW)	9	15.
1415	94.	(DIRECT FLOW)	8	10.	1631	506.	2.1	8	35.
1416	867.	3.4	8	45.	1635	433.	(DIRECT FLOW)	8	10.
1420	103.	(DIRECT FLOW)	8	15.	1636	414.	2.0	8	15.
1421	9200.	6.8	9	40.	1640	335.	(DIRECT FLOW)	8	10.
1423	9200.	(DIRECT FLOW)	9	40.	1641	225.	3.4	8	30.
1424	6868.	(DIRECT FLOW)	9	40.	1643	367.	(DIRECT FLOW)	8	25.
1425	18.	(DIRECT FLOW)	8	0.	1645	161.	(DIRECT FLOW)	8	15.
1426	75.	1.2	8	20.	1646	146.	1.5	8	25.
1427	3979.	(DIRECT FLOW)	10	30.	1650	644.	(DIRECT FLOW)	8	10.
1428	2321.	3.0	9	50.	1651	898.	3.4	8	20.
1429	2798.	(DIRECT FLOW)	9	45.	1653	1379.	(DIRECT FLOW)	8	25.
1430	28.	(DIRECT FLOW)	8	10.	1655	568.	(DIRECT FLOW)	8	15.
1431	25.	.8	8	15.	1656	501.	2.7	8	30.
1435	56.	(DIRECT FLOW)	8	10.	1660	427.	(DIRECT FLOW)	8	15.
1436	46.	1.3	8	15.	1661	363.	2.4	8	25.
1438	71.	(DIRECT FLOW)	8	15.	1665	795.	(DIRECT FLOW)	8	5.
1440	60.	(DIRECT FLOW)	8	15.	1666	719.	2.7	8	15.
1441	9176.	6.9	9	35.	1705	20.	(DIRECT FLOW)	8	10.
1442	1127.	2.1	10	35.	1710	106.	(DIRECT FLOW)	8	15.
1445	52.	(DIRECT FLOW)	8	5.	1711	95.	1.1	8	35.
1446	41.	1.1	8	20.	1712	1462.	(DIRECT FLOW)	8	45.
1450	58.	(DIRECT FLOW)	8	15.	1715	91.	(DIRECT FLOW)	8	15.
1451	9435.	6.5	9	25.	1716	60.	.9	8	50.
1453	9455.	(DIRECT FLOW)	9	25.	1800	2413.	(DIRECT FLOW)	9	50.
1455	230.	(DIRECT FLOW)	8	10.	1812	3872.	(DIRECT FLOW)	11	15.
1456	195.	.7	8	25.	1813	3872.	(DIRECT FLOW)	11	15.
1457	195.	(DIRECT FLOW)	8	25.	1814	2286.	(DIRECT FLOW)	11	15.
1460	135.	(DIRECT FLOW)	8	5.	1815	1586.	(DIRECT FLOW)	11	20.
1461	118.	2.0	8	10.	1816	1579.	3.4	11	25.
1465	117.	(DIRECT FLOW)	8	10.	1817	1579.	(DIRECT FLOW)	11	25.
1467	382.	(DIRECT FLOW)	8	20.	1818	25.	.9	8	0.
1468	379.	2.4	8	25.	1820	1757.	(DIRECT FLOW)	11	10.
1480	1021.	3.5	8	15.	1821	204.	(DIRECT FLOW)	8	10.
1481	8.	.0	24	40.	1822	621.	(DIRECT FLOW)	11	35.
1482	8.	(DIRECT FLOW)	24	20.	1905	5142.	(DIRECT FLOW)	10	40.
1490	314.	(DIRECT FLOW)	8	10.	1906	2536.	1.2	11	55.
1491	264.	2.8	9	10.	1907	824.	2.6	8	55.
1500	440.	(DIRECT FLOW)	8	10.	1908	120.	2.1	12	20.
1501	338.	2.8	8	35.	1909	3924.	(DIRECT FLOW)	12	5.
1505	429.	(DIRECT FLOW)	8	10.	1910	281.	(DIRECT FLOW)	11	35.
1506	2123.	3.6	10	45.	1911	1061.	(DIRECT FLOW)	8	40.
1507	8173.	(DIRECT FLOW)	10	25.	1912	1051.	6.4	8	45.
1508	6106.	(DIRECT FLOW)	10	20.	1913	3850.	(DIRECT FLOW)	11	20.
1509	2121.	(DIRECT FLOW)	9	50.	1914	3845.	6.3	11	25.
1510	93.	(DIRECT FLOW)	8	15.	1915	3850.	(DIRECT FLOW)	11	25.
1511	7257.	5.1	10	20.	1916	4248.	3.0	10	35.
1512	8139.	5.9	10	30.	1917	48.	1.1	8	25.
1513	7257.	(DIRECT FLOW)	10	20.	1919	3880.	(DIRECT FLOW)	11	15.
1514	1151.	(DIRECT FLOW)	10	20.	1920	922.	5.4	8	15.
1515	31.	(DIRECT FLOW)	8	5.	1921	942.	(DIRECT FLOW)	8	10.

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1922	11.	.3	10	30.
1923	2424.	(DIRECT FLOW)	11	0.
1924	1115.	(DIRECT FLOW)	11	5.
1925	109.	(DIRECT FLOW)	11	5.
1926	157.	(DIRECT FLOW)	11	10.
1927	203.	3.6	8	55.
1928	8509.	(DIRECT FLOW)	9	15.
1929	1448.	3.1	8	45.
1931	308.	(DIRECT FLOW)	9	0.
1932	113.	1.0	8	15.
1933	308.	2.5	9	0.
1934	3877.	4.1	11	15.
1935	5375.	(DIRECT FLOW)	10	35.
1937	480.	(DIRECT FLOW)	11	35.
1938	1035.	(DIRECT FLOW)	8	10.
1939	541.	(DIRECT FLOW)	11	35.
1940	587.	(DIRECT FLOW)	11	40.
1941	103.	1.0	8	30.
1942	207.	(DIRECT FLOW)	11	40.
1943	3907.	7.0	12	10.
1944	972.	6.4	12	5.
1945	972.	(DIRECT FLOW)	12	5.
1946	4260.	(DIRECT FLOW)	12	10.
1947	7517.	(DIRECT FLOW)	12	30.

UDSWMM

500-YEAR MODEL

500_ltd.wpd July 12, 2000 500-YR SWMM MODEL

URBAN DRAINAGE STORM WATER MANAGEMENT MODEL - 32 BIT VERSION 1998
 REVISED BY UNIVERSITY OF COLORADO AT DENVER

*** ENTRY MADE TO RUNOFF MODEL ***

sbc_ltd.swi
 500-year model

NUMBER OF TIME STEPS 855
 OINTEGRATION TIME INTERVAL (MINUTES) 5.00

1.0 PERCENT OF IMPERVIOUS AREA HAS ZERO DETENTION DEPTH
 OFOR 288 RAINFALL STEPS, THE TIME INTERVAL IS 5.00 MINUTES
 OFOR RAINGAGE NUMBER 1 RAINFALL HISTORY IN INCHES PER HOUR

.05	.05	.05	.05	.05	.05	.05	.06	.06	.06
.06	.06	.06	.06	.06	.06	.06	.06	.06	.07
.07	.07	.07	.07	.07	.07	.07	.07	.07	.08
.08	.08	.08	.08	.08	.08	.09	.09	.09	.09
.09	.10	.10	.10	.10	.10	.11	.11	.11	.11
.12	.12	.12	.12	.13	.13	.13	.14	.14	.15
.15	.15	.16	.16	.17	.18	.18	.19	.20	.20
.21	.22	.23	.24	.25	.27	.28	.30	.32	.34
.37	.40	.44	.48	.53	.59	.67	.78	.91	1.08
1.33	1.68	2.21	3.04	4.35	5.46	5.14	3.63	2.58	1.92
1.49	1.20	.99	.84	.72	.63	.56	.50	.46	.42
.38	.36	.33	.31	.29	.28	.26	.25	.24	.23
.22	.21	.20	.19	.18	.18	.17	.17	.16	.16
.15	.15	.14	.14	.14	.13	.13	.13	.12	.12
.12	.11	.11	.11	.11	.10	.10	.10	.10	.10
.09	.09	.09	.09	.09	.09	.08	.08	.08	.08
.08	.08	.08	.08	.07	.07	.07	.07	.07	.07
.07	.07	.07	.06	.06	.06	.06	.06	.06	.06
.06	.06	.06	.06	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.05
.05	.05	.05	.05	.05	.05	.05	.05	.05	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03

OFOR RAINGAGE NUMBER 2 RAINFALL HISTORY IN INCHES PER HOUR

.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.09	.09	.09	.09
.09	.09	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.09	.09	.09	.09	.09	.09
.10	.10	.10	.10	.10	.10	.10	.10	.10	.10
.11	.11	.11	.11	.11	.11	.11	.12	.12	.12
.12	.13	.13	.13	.14	.14	.14	.15	.15	.16
.16	.17	.18	.19	.20	.21	.22	.24	.25	.27
.29	.32	.35	.39	.44	.50	.57	.66	.78	.95
1.18	1.50	1.99	2.75	3.91	4.78	4.58	3.28	2.33	1.72
1.33	1.05	.86	.72	.61	.53	.46	.41	.37	.34
.31	.28	.26	.24	.23	.21	.20	.19	.18	.18
.17	.16	.16	.15	.15	.14	.14	.13	.13	.13
.12	.12	.12	.12	.12	.11	.11	.11	.11	.11
.11	.10	.10	.10	.10	.10	.10	.10	.10	.10
.10	.10	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.09	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08

OFOR RAINGAGE NUMBER 3 RAINFALL HISTORY IN INCHES PER HOUR

.08	.08	.08	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.09	.09	.09	.09	.09	.10
.10	.10	.10	.10	.10	.10	.10	.10	.10	.10
.10	.11	.11	.11	.11	.11	.11	.11	.11	.12
.12	.12	.12	.12	.13	.13	.13	.13	.14	.14
.14	.15	.15	.15	.16	.16	.17	.17	.18	.19
.20	.20	.21	.22	.24	.25	.26	.28	.30	.32
.34	.37	.41	.45	.49	.55	.62	.70	.81	.95
1.12	1.36	1.69	2.17	2.92	4.23	3.47	2.51	1.91	1.51
1.23	1.03	.87	.75	.66	.58	.52	.47	.43	.39
.36	.33	.31	.29	.27	.26	.24	.23	.22	.21
.20	.19	.18	.18	.17	.17	.16	.16	.15	.15
.14	.14	.14	.13	.13	.13	.13	.12	.12	.12
.12	.12	.12	.11	.11	.11	.11	.11	.11	.11
.10	.10	.10	.10	.10	.10	.10	.10	.10	.10
.10	.10	.10	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.09	.09	.09	.09	.09	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08

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193	184	7080.	217.0	6.0	.2820	.300	.500	.300	.400	3.90	.50	.00024	5
181	192	9200.	507.0	7.0	.2836	.300	.500	.300	.450	4.50	.60	.00010	5
179	180	9040.	501.0	5.0	.2840	.250	.450	.300	.500	3.50	.20	.00100	4
204	204	13440.	854.0	30.0	.3985	.300	.500	.300	.470	3.90	.50	.00024	5
203	203	7000.	258.0	25.0	.4793	.300	.500	.300	.470	3.90	.50	.00024	5
199	201	15400.	843.0	5.0	.3343	.300	.500	.300	.470	4.50	.60	.00010	5
198	200	14440.	542.0	5.0	.2842	.300	.500	.300	.450	3.90	.50	.00024	5
200	202	7640.	250.0	5.0	.2900	.300	.500	.300	.500	4.80	.50	.00010	5
196	198	14440.	797.0	5.0	.4198	.250	.450	.300	.450	3.90	.50	.00024	5
195	196	14640.	387.0	5.0	.2370	.250	.450	.300	.500	4.50	.60	.00010	5
197	199	18040.	634.0	5.0	.2744	.250	.450	.300	.450	3.90	.50	.00024	5
190	195	9520.	251.0	5.0	.2833	.250	.450	.300	.470	3.90	.50	.00024	5
189	194	15120.	847.0	9.0	.3487	.150	.400	.300	.500	4.50	.50	.00010	4
208	208	8520.	275.0	5.0	.3120	.250	.450	.300	.450	3.90	.50	.00024	5
207	207	8560.	772.0	6.0	.4592	.150	.400	.300	.430	3.50	.20	.00100	5
206	206	7720.	250.0	5.0	.3693	.250	.450	.300	.470	3.90	.50	.00024	5
205	205	9800.	395.0	7.0	.4113	.150	.400	.300	.450	3.90	.50	.00024	4
187	192	1540.	115.0	6.0	.5495	.150	.400	.300	.430	3.50	.20	.00100	4
188	193	8960.	273.0	9.0	.3629	.150	.400	.300	.400	3.50	.20	.00100	4
186	187	19200.	1018.0	8.0	.3200	.150	.400	.300	.450	3.90	.50	.00024	4
177	178	13000.	392.0	7.0	.2685	.150	.400	.300	.450	3.90	.50	.00024	5
178	179	7720.	211.0	5.0	.3191	.250	.450	.300	.420	3.50	.20	.00100	5
175	176	15040.	716.0	5.0	.3492	.250	.450	.300	.400	3.50	.20	.00100	4
176	177	12040.	233.0	6.0	.2396	.250	.450	.300	.450	3.90	.50	.00024	4
174	175	3800.	78.0	5.0	.2684	.250	.450	.300	.450	3.90	.50	.00024	4
173	174	8120.	188.0	8.0	.3071	.150	.400	.300	.430	3.90	.50	.00024	4
172	173	11520.	230.0	5.0	.3401	.250	.450	.300	.400	3.50	.20	.00100	4
171	172	3720.	73.0	7.0	.2083	.150	.400	.300	.450	3.90	.50	.00024	4
167	168	7240.	259.0	5.0	.2386	.300	.500	.300	.500	3.90	.50	.00024	5
168	169	6280.	175.0	5.0	.2720	.300	.500	.300	.500	3.90	.50	.00024	5
164	165	13840.	350.0	6.0	.3519	.300	.500	.300	.470	3.90	.50	.00024	4
166	167	10720.	215.0	6.0	.3188	.300	.500	.300	.500	3.90	.50	.00024	4
165	166	1040.	99.0	5.0	.2782	.300	.500	.300	.500	3.90	.50	.00024	4
170	171	8840.	139.0	5.0	.2244	.250	.450	.300	.400	3.50	.20	.00100	4
169	170	9680.	332.0	5.0	.2538	.250	.450	.300	.400	3.50	.20	.00100	4
162	163	5280.	112.0	5.0	.2935	.250	.450	.300	.470	3.90	.50	.00100	4
163	164	8000.	76.0	5.0	.3938	.300	.500	.300	.450	3.90	.50	.00024	4
156	157	1660.	103.0	7.0	.3821	.250	.450	.300	.460	3.50	.20	.00100	4
160	161	8760.	341.0	5.0	.3148	.300	.500	.300	.470	3.90	.50	.00100	4
161	162	11600.	362.0	5.0	.3269	.300	.500	.300	.470	3.90	.50	.00100	5
158	159	12760.	476.0	5.0	.2852	.300	.500	.300	.470	3.90	.50	.00100	5
159	160	6720.	342.0	6.0	.3021	.300	.500	.300	.470	3.90	.50	.00100	4
155	156	9960.	523.0	6.0	.3280	.250	.450	.300	.400	3.90	.50	.00024	4
157	158	11400.	344.0	5.0	.2728	.250	.450	.300	.460	3.90	.50	.00024	4
152	153	8760.	249.0	5.0	.2831	.300	.500	.300	.500	3.90	.50	.00024	4
153	154	5760.	249.0	6.0	.3299	.250	.450	.300	.450	3.90	.50	.00024	4
154	155	2180.	161.0	5.0	.3792	.300	.500	.300	.400	3.50	.20	.00100	4
148	149	6440.	214.0	6.0	.3001	.250	.450	.300	.400	3.50	.20	.00100	4
149	150	5560.	58.0	6.0	.1610	.250	.450	.300	.400	3.50	.20	.00100	4
150	151	8240.	189.0	5.0	.2338	.250	.450	.300	.400	3.50	.20	.00100	4
151	152	13960.	501.0	8.0	.3572	.250	.450	.300	.450	3.90	.50	.00024	4
145	146	6930.	318.0	5.0	.2782	.300	.500	.300	.460	3.90	.50	.00024	4
146	147	11200.	283.0	5.0	.2727	.250	.450	.300	.500	3.90	.50	.00024	4
147	148	5440.	453.0	5.0	.3306	.250	.450	.300	.470	3.90	.50	.00024	4
141	142	4160.	103.0	6.0	.2843	.250	.450	.300	.450	3.90	.50	.00024	4
142	143	9680.	187.0	5.0	.3565	.250	.450	.300	.470	3.90	.50	.00024	4
143	144	4400.	274.0	5.0	.3218	.300	.500	.300	.460	3.90	.50	.00024	4
144	145	4320.	79.0	5.0	.2164	.300	.500	.300	.500	3.90	.50	.00024	4
139	140	8640.	184.0	6.0	.3125	.250	.450	.300	.460	3.90	.50	.00024	4
140	141	7600.	132.0	5.0	.2104	.250	.450	.300	.450	3.50	.20	.00100	4
136	137	6200.	142.0	15.0	.2104	.150	.400	.150	.470	3.50	.20	.00100	4
137	138	8780.	383.0	10.0	.0823	.150	.400	.150	.420	3.50	.20	.00100	4
138	139	3760.	70.0	15.0	.1898	.250	.450	.150	.450	3.90	.50	.00024	4
133	134	20040.	530.0	8.0	.3229	.250	.450	.300	.460	3.90	.50	.00024	4
134	135	8160.	160.0	5.0	.2440	.250	.450	.300	.450	3.90	.50	.00024	5
135	136	6000.	282.0	5.0	.2300	.250	.450	.300	.460	3.90	.50	.00024	5
130	131	9720.	290.0	12.0	.3042	.150	.400	.150	.500	3.90	.50	.00024	4
131	132	9120.	213.0	8.0	.1964	.250	.450	.300	.470	3.90	.50	.00024	4
132	133	15440.	496.0	7.0	.1806	.250	.450	.300	.470	3.90	.50	.00024	4
128	129	7040.	151.0	12.0	.5988	.300	.500	.200	.450	3.90	.50	.00024	4
129	130	6720.	110.0	15.0	.2077	.150	.400	.150	.450	3.90	.50	.00024	4
124	125	7600.	220.0	5.0	.1948	.300	.500	.300	.500	3.90	.50	.00024	4
125	126	8840.	88.0	5.0	.2679	.300	.500	.300	.500	3.90	.50	.00024	4
126	127	16000.	548.0	8.0	.2341	.250	.450	.300	.480	3.90	.50	.00024	4
120	124	15040.	397.0	13.0	.1127	.150	.400	.150	.500	3.90	.50	.00024	4
127	128	17320.	472.0	8.0	.2160	.250	.450	.300	.470	3.90	.50	.00024	4
118	122	18880.	481.0	8.0	.2138	.150	.400	.200	.450	3.90	.50	.00024	4
119	123	8320.	389.0	12.0	.1613	.150	.400	.200	.450	3.90	.50	.00024	4
113	116	19040.	702.0	5.0	.1137	.300	.500	.300	.500	3.90	.50	.00024	4
93	96	12640.	579.0	5.0	.2560	.250	.450	.300	.460	3.90	.50	.00024	4
230	95	8000.	200.0	5.0	.2312	.250	.450	.300	.450	3.90	.50	.00024	4
88	85	3840.	118.0	5.0	.2369	.250	.450	.300	.400	3.90	.50	.00024	4
89	86	11760.	331.0	5.0	.2521	.250	.450	.300	.400	3.90	.50	.00024	4
90	87	16080.	655.0	5.0	.1364	.250	.450	.300	.400	3.50	.20	.00100	4
84	81	12440.	303.0	5.0	.2148	.250	.450	.300	.400	3.50	.20	.00100	4
85	82	2220.	96.0	5.0	.1143	.250	.450	.300	.400	3.50	.20	.00100	4
86	83	4760.	197.0	5.0	.1438	.250	.450	.300	.400	3.90	.50	.00024	4
87	84	5440.	106.0	5.0	.1919	.250	.450	.300	.400	3.90	.50	.00024	4
83	80	31300.	862.0	9.0	.1050	.150	.400	.200	.400	3.50	.20	.00100	4
74	121	9400.	326.0	6.0	.1923	.150	.400	.200	.400	3.50	.20	.00024	4
70	79	16040.	633.0	7.0	.1589	.250	.450	.300	.400	3.50	.20	.00100	4
61	75	3200.	62.0	5.0	.3363	.250	.450	.300	.400	3.90	.50	.00024	4
63	76	12840.	379.0	8.0	.1972	.250	.450	.300	.400	3.50	.20	.00100	4
65	77	4040.	66.0	8.0	.2100	.250	.450	.300	.430	3.90	.50	.00024	4
66	78	7560.	256.0	5.0	.1250	.250	.450	.300	.450	3.90	.50	.00024	4
58	74	9400.	411.0	8.0	.3384	.250	.450	.300	.400	3.50	.20	.00100	4
228	89	8480.	319.0	8.0	.1659	.150	.400	.150	.450	3.50	.20	.00100	4
229	93	4880.	111.0	5.0	.2059	.250	.450	.300	.450	4.50	.60	.00010	4
91	88	16520.	352.0	6.0	.1576	.250	.450	.300	.450	3.90	.50	.00024	4
114	117	12000.	390.0	15.0	.1571	.150	.400	.150	.430	3.90	.50	.00024	4
115	118	16440.	453.0	6.0	.1736	.250	.450	.300	.460	3.90	.50	.00024	4

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116	119	2600.	34.0	15.0	.1472	.150	.400	.150	.500	3.90	.50	.00024	4
117	120	7960.	220.0	15.0	.1331	.150	.400	.150	.470	3.90	.50	.00024	4
101	104	6880.	205.0	15.0	.1564	.150	.400	.150	.450	3.50	.20	.00100	4
102	105	9120.	343.0	10.0	.1175	.150	.400	.150	.500	3.90	.50	.00024	4
103	106	12760.	273.0	8.0	.1121	.250	.450	.300	.500	3.90	.50	.00024	4
99	102	10440.	314.0	10.0	.1275	.150	.400	.150	.480	3.90	.50	.00024	4
100	103	8170.	150.0	8.0	.1343	.150	.400	.150	.450	3.90	.50	.00100	4
109	112	7280.	208.0	7.0	.4086	.250	.450	.300	.470	3.90	.50	.00024	4
110	113	10120.	209.0	7.0	.2899	.250	.450	.300	.500	3.90	.50	.00024	4
111	114	9000.	230.0	5.0	.2973	.300	.500	.300	.470	3.90	.50	.00024	5
112	115	6480.	102.0	6.0	.4123	.250	.450	.300	.460	3.90	.50	.00024	4
107	110	4140.	399.0	8.0	.3550	.250	.450	.300	.470	3.90	.50	.00024	4
105	108	12480.	202.0	5.0	.3863	.300	.500	.300	.470	3.90	.50	.00024	4
106	109	5520.	216.0	7.0	.1680	.250	.450	.300	.500	3.90	.50	.00024	4
108	111	11200.	199.0	5.0	.4732	.300	.500	.300	.460	3.90	.50	.00024	4
104	107	5440.	106.0	8.0	.2557	.250	.450	.300	.480	3.90	.50	.00024	4
97	100	19960.	458.0	7.0	.5159	.250	.450	.300	.480	3.50	.20	.00100	4
95	98	14000.	309.0	18.0	.1544	.250	.450	.200	.470	3.50	.20	.00100	4
96	99	2880.	55.0	10.0	.3003	.250	.450	.300	.480	3.50	.20	.00100	4
98	101	1380.	82.0	8.0	.1629	.250	.450	.200	.470	3.50	.20	.00100	4
94	97	11440.	472.0	8.0	.3012	.250	.450	.300	.470	3.90	.50	.00024	4
92	94	5120.	475.0	7.0	.1426	.250	.450	.300	.500	3.90	.50	.00024	4
56	72	8960.	197.0	7.0	.1792	.150	.400	.150	.420	3.50	.20	.00100	4
57	73	16000.	636.0	8.0	.1300	.150	.400	.150	.440	3.90	.50	.00024	4
55	71	9640.	261.0	7.0	.1967	.250	.450	.300	.470	3.50	.50	.00100	4
43	59	8040.	296.0	9.0	.1912	.150	.400	.150	.400	3.90	.50	.00024	4
47	63	7960.	234.0	6.0	.4083	.250	.450	.300	.470	3.90	.50	.00024	4
48	64	7480.	258.0	6.0	.3750	.250	.450	.300	.500	3.90	.50	.00024	4
45	61	15000.	552.0	8.0	.2077	.250	.450	.200	.470	3.50	.20	.00100	4
42	46	6440.	197.0	7.0	.3799	.250	.450	.200	.400	3.50	.20	.00100	4
44	60	8160.	225.0	7.0	.2515	.250	.450	.200	.470	3.50	.20	.00100	4
46	62	2800.	39.0	5.0	.3963	.250	.450	.300	.470	3.50	.20	.00100	4
50	66	6120.	108.0	6.0	.4444	.250	.450	.300	.500	3.90	.50	.00024	4
51	67	13240.	636.0	7.0	.3651	.250	.450	.300	.470	3.50	.20	.00100	4
53	69	7480.	197.0	12.0	.2552	.150	.400	.150	.470	3.50	.20	.00100	4
54	70	13920.	246.0	12.0	.2827	.150	.400	.150	.420	3.50	.20	.00100	4
49	65	7920.	212.0	5.0	.3375	.250	.450	.300	.480	3.90	.50	.00024	4
52	68	4240.	80.0	7.0	.3917	.250	.450	.300	.500	3.50	.20	.00100	4
41	42	15160.	593.0	8.0	.4922	.250	.450	.200	.450	3.90	.50	.00024	4
39	40	13160.	356.0	20.0	.4570	.250	.450	.100	.450	3.90	.50	.00024	3
40	41	6200.	205.0	9.0	.5172	.250	.450	.200	.500	3.50	.20	.00100	4
18	18	15200.	565.0	7.0	.3792	.250	.450	.200	.420	3.50	.20	.00100	3
19	20	10680.	606.0	9.0	.1670	.150	.400	.150	.470	3.90	.50	.00024	4
20	21	13920.	379.0	6.0	.3275	.250	.450	.300	.400	3.90	.50	.00024	3
14	14	6160.	132.0	25.0	.4006	.250	.450	.100	.500	3.50	.20	.00100	3
15	15	3000.	36.0	25.0	.3169	.250	.450	.100	.450	3.50	.20	.00100	3
16	16	3840.	117.0	25.0	.2094	.250	.450	.100	.400	3.50	.20	.00100	3
17	17	5640.	156.0	20.0	.3423	.250	.450	.100	.400	3.50	.20	.00100	3
8	8	14200.	1227.0	67.0	.2919	.250	.450	.050	.450	3.50	.20	.00100	3
37	38	5060.	368.0	7.0	.2400	.250	.450	.200	.420	3.90	.50	.00024	4
38	39	10280.	290.0	7.0	.3153	.250	.450	.300	.420	3.50	.50	.00100	4
36	37	16320.	466.0	5.0	.1439	.250	.450	.300	.480	3.90	.50	.00024	4
33	34	13680.	445.0	8.0	.1186	.150	.400	.200	.410	3.90	.50	.00024	4
34	35	6280.	148.0	7.0	.2940	.250	.450	.300	.420	3.50	.20	.00100	4
35	36	10680.	251.0	6.0	.1368	.250	.450	.300	.400	3.50	.20	.00100	4
31	32	6520.	144.0	6.0	.2938	.250	.450	.300	.420	3.90	.50	.00024	4
32	33	10360.	257.0	12.0	.1275	.150	.400	.150	.420	3.50	.20	.00100	4
30	31	5440.	107.0	7.0	.2363	.150	.400	.150	.450	4.50	.60	.00010	3
22	23	9840.	195.0	8.0	.1920	.250	.450	.200	.460	3.50	.20	.00100	3
29	30	11560.	546.0	12.0	.0980	.150	.400	.150	.450	3.50	.20	.00100	4
26	27	5080.	107.0	5.0	.2510	.250	.450	.300	.450	3.90	.50	.00024	3
27	28	5040.	300.0	9.0	.1461	.150	.400	.150	.430	3.90	.50	.00024	3
28	29	6120.	152.0	7.0	.2020	.150	.400	.150	.450	3.50	.20	.00100	4
24	25	5920.	363.0	9.0	.3292	.250	.450	.300	.450	3.50	.20	.00100	3
25	26	3720.	94.0	8.0	.1772	.150	.400	.150	.450	3.50	.20	.00100	3
23	24	1740.	104.0	7.0	.1530	.250	.450	.300	.450	3.50	.20	.00100	3
21	22	12000.	447.0	20.0	.2822	.150	.400	.200	.400	3.50	.20	.00100	3
9	9	20640.	411.0	8.0	.2894	.250	.450	.300	.470	3.90	.50	.00024	2
10	10	7520.	202.0	6.0	.3773	.250	.450	.300	.480	3.90	.50	.00024	2
7	7	9980.	373.0	7.0	.2911	.300	.500	.300	.500	3.90	.50	.00024	2
3	3	22000.	929.0	8.0	.3243	.250	.450	.200	.450	3.50	.20	.00100	2
4	4	25560.	960.0	8.0	.2675	.250	.450	.200	.500	3.50	.20	.00100	2
2	2	14480.	519.0	7.0	.4504	.300	.500	.300	.420	3.50	.20	.00100	2
6	6	16100.	296.0	10.0	.4790	.300	.500	.300	.450	3.50	.20	.00100	2
5	5	18300.	336.0	6.0	.2506	.300	.500	.300	.420	5.00	.60	.00006	2
1	1	30900.	567.0	7.0	.5000	.300	.500	.300	.420	3.50	.20	.00100	2
11	11	6000.	113.0	25.0	.3243	.250	.450	.200	.500	3.90	.50	.00024	2
12	12	8360.	159.0	6.0	.3715	.300	.500	.300	.500	3.90	.50	.00024	2
13	13	10480.	229.0	7.0	.3542	.300	.500	.300	.500	3.90	.50	.00024	2
256	247	39100.	808.0	7.0	.1652	.250	.450	.200	.450	3.50	.20	.00100	2
257	248	31200.	645.0	8.0	.2217	.250	.450	.200	.450	3.50	.20	.00100	2
258	249	18300.	377.0	7.0	.1984	.250	.450	.300	.420	3.50	.20	.00100	2
259	250	5300.	109.0	5.0	.1627	.250	.450	.300	.450	4.80	.50	.00010	2
253	244	36900.	848.0	50.0	.2354	.300	.500	.300	.350	3.90	.50	.00024	2
254	245	7300.	100.0	7.0	.2934	.250	.450	.200	.450	3.50	.20	.00100	2
255	246	21800.	450.0	8.0	.2396	.250	.450	.300	.450	3.50	.20	.00100	2
76	54	10300.	213.0	8.0	.3735	.300	.500	.300	.500	5.00	.60	.00006	2
77	55	25900.	297.0	7.0	.4316	.300	.500	.300	.500	5.00	.60	.00006	2
75	53	2400.	26.0	6.0	.4875	.300	.500	.300	.460	3.50	.20	.00024	2
73	52	38400.	441.0	18.0	.3662	.300	.500	.300	.400	3.50	.20	.00100	2
82	51	19700.	362.0	25.0	.3938	.250	.450	.300	.400	3.50	.20	.00100	2
71	50	11300.	207.0	25.0	.4627	.300	.500	.400	.450	3.50	.20	.00100	2
80	58	12000.	220.0	6.0	.3854	.300	.500	.300	.480	5.00	.60	.00006	2
81	57	42200.	776.0	8.0	.5226	.250	.450	.200	.470	4.50	.60	.00010	2
78	56	22000.	404.0	18.0	.4013	.250	.450	.300	.500	4.80	.50	.00010	2
79	56	21400.	442.0	15.0	.3303	.300	.500	.300	.450	4.50	.60	.00010	2
72	49	16000.	220.0	35.0	.5698	.300	.500	.300	.500	4.50	.50	.00010	2
69	48	9400.	391.0	35.0	.2301	.250	.450	.300	.400	3.90	.50	.00024	2
1635	1635	12865.	317.0	12.0	.3700	.300	.500	.300	.450	3.50	.20	.00100	2
1645	1645	5640.	126.0	5.0	.2900	.250	.450	.150	.450	3.50	.20	.00100	2
1640	1640	8667.	200.0	10.0	.2900	.300	.300	.320	.450	3.50	.20	.00100	2

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1630	1630	8660.	159.0	6.0	.1300	.400	.450	.150	.450	3.50	.20	.00100	2
1625	1625	10700.	197.0	9.0	.2100	.200	.400	.150	.450	3.50	.20	.00100	1
1610	1610	6780.	109.0	9.0	.0200	.200	.400	.150	.450	4.80	.50	.00010	1
1665	1665	14692.	390.0	35.0	.2870	.200	.400	.150	.450	3.50	.20	.00100	2
1605	1605	7689.	81.0	6.0	.1100	.200	.400	.150	.450	4.80	.50	.00010	1
1660	1660	23764.	552.0	7.0	.2000	.200	.450	.150	.460	3.90	.50	.00024	2
1650	1650	13676.	382.0	7.0	.2300	.200	.200	.150	.450	3.50	.20	.00100	2
1655	1655	22832.	558.0	6.0	.1600	.200	.450	.150	.460	3.50	.20	.00100	2
1620	1620	17977.	324.0	7.0	.0500	.200	.400	.150	.470	4.80	.50	.00010	2
1615	1615	11967.	228.0	7.0	.1200	.200	.400	.150	.470	4.50	.60	.00010	2
1710	1710	9974.	245.0	5.0	.0100	.200	.400	.150	.350	3.90	.50	.00024	1
1600	1600	3273.	25.0	7.0	.0500	.200	.450	.150	.600	5.00	.70	.00002	1
1705	1705	2245.	67.0	5.0	.0100	.200	.400	.150	.350	3.90	.50	.00024	2
1450	1450	4800.	198.0	5.0	.0200	.150	.450	.150	.600	3.90	.50	.00024	1
1445	1445	6714.	164.0	5.0	.0800	.200	.400	.150	.350	5.00	.60	.00006	1
1440	1440	12663.	66.0	7.0	.0100	.150	.450	.150	.600	3.90	.50	.00024	1
1480	1938	34034.	732.0	35.0	.0200	.200	.400	.150	.300	3.90	.50	.00024	1
1435	1435	6984.	232.0	5.0	.0800	.200	.400	.150	.460	5.00	.60	.00006	1
1430	1430	6338.	82.0	5.0	.0700	.200	.400	.150	.460	5.00	.60	.00006	1
1425	1425	4940.	68.0	6.0	.0400	.200	.400	.150	.600	5.00	.70	.00002	1
1420	1420	26178.	59.0	9.0	.0220	.200	.450	.150	.600	3.90	.50	.00024	1
1570	1570	3089.	171.0	6.0	.3540	.200	.450	.150	.450	3.50	.20	.00100	2
1555	1556	7055.	83.0	7.0	.1300	.200	.450	.150	.450	4.80	.50	.00010	1
1565	1565	4112.	95.0	9.0	.3200	.200	.450	.150	.470	3.50	.20	.00100	2
1560	1560	5353.	123.0	8.0	.4400	.200	.450	.150	.450	3.50	.20	.00100	2
1550	1550	20321.	424.0	7.0	.0700	.200	.400	.150	.450	3.50	.20	.00100	1
1415	1415	5148.	307.0	5.0	.0260	.200	.400	.150	.500	3.90	.50	.00024	1
1410	1410	5300.	195.0	5.0	.0100	.150	.450	.150	.500	3.90	.50	.00024	1
1455	1455	19899.	542.0	11.0	.0037	.200	.400	.150	.350	4.80	.50	.00010	1
1490	1490	8100.	698.0	10.0	.0620	.200	.400	.150	.350	4.50	.50	.00010	1
1465	1465	19569.	93.0	10.0	.0348	.150	.500	.150	.350	4.50	.60	.00010	2
1460	1460	12745.	286.0	9.0	.0603	.200	.400	.150	.350	5.00	.60	.00006	1
1575	1575	10554.	222.0	10.0	.4060	.200	.450	.150	.450	3.50	.20	.00100	2
1545	1545	15603.	253.0	7.0	.0890	.200	.400	.150	.450	4.80	.50	.00010	1
1530	1530	8269.	345.0	6.0	.1080	.200	.400	.150	.350	4.80	.50	.00010	1
1525	1525	14343.	53.0	10.0	.0200	.150	.400	.150	.350	3.90	.50	.00024	1
1505	1505	49306.	262.0	10.0	.0100	.150	.450	.150	.350	3.50	.20	.00100	1
1520	1520	21460.	99.0	10.0	.0100	.200	.450	.150	.350	3.50	.20	.00100	1
1715	1715	3131.	115.0	7.0	.1200	.150	.400	.150	.350	3.90	.50	.00024	1
1515	1515	3666.	8.0	60.0	.0200	.150	.400	.150	.350	3.50	.20	.00100	1
1540	1541	19881.	345.0	15.0	.0300	.200	.400	.150	.350	4.50	.60	.00010	1
1510	1510	16588.	76.0	3.0	.0100	.150	.400	.150	.350	3.90	.50	.00024	1
1500	1500	21483.	465.0	10.0	.0400	.200	.400	.150	.250	3.90	.50	.00024	1
299	299	20092.	72.0	40.0	.1300	.150	.500	.150	.350	4.80	.50	.00010	1
301	301	38137.	177.0	31.0	.1600	.150	.500	.150	.350	4.80	.50	.00010	1
297	297	84806.	338.0	40.0	.1200	.150	.500	.150	.350	4.80	.50	.00010	1
305	1917	1795.	103.0	10.0	.0240	.150	.350	.150	.250	3.90	.50	.00024	1
304	304	2970.	150.0	10.0	.0240	.150	.350	.150	.250	3.90	.50	.00024	1
262	262	3964.	39.0	5.0	.0200	.200	.400	.150	.250	3.90	.50	.00024	1
264	264	1734.	26.0	5.0	.0200	.200	.400	.150	.250	3.90	.50	.00024	1
243	243	46293.	82.0	7.0	.0200	.200	.350	.150	.350	3.90	.50	.00024	1
384	384	27915.	77.0	45.0	.0900	.150	.500	.150	.350	4.80	.50	.00010	1
290	290	4748.	29.0	5.0	.0250	.300	.400	.150	.400	3.90	.50	.00024	1
353	353	12867.	41.0	50.0	.0700	.150	.500	.150	.350	5.00	.60	.00006	1
350	350	13939.	51.0	70.0	.0550	.150	.400	.150	.350	4.80	.50	.00010	1
351	351	17043.	59.0	70.0	.0600	.150	.450	.150	.350	5.00	.60	.00006	1
376	376	1390.	3.0	10.0	.0100	.150	.450	.150	.350	4.80	.50	.00010	1
368	368	7225.	99.0	50.0	.0070	.150	.450	.150	.350	3.90	.50	.00024	1
361	361	6400.	30.0	60.0	.0060	.150	.450	.150	.350	3.90	.50	.00024	1
369	369	7449.	17.0	60.0	.0400	.150	.450	.150	.350	4.80	.50	.00010	1
354	1818	6326.	6.0	95.0	.0400	.150	.350	.150	.250	4.80	.50	.00010	2
355	355	9583.	7.0	65.0	.0400	.150	.350	.150	.250	4.80	.50	.00010	1
363	363	9583.	7.0	33.0	.0550	.150	.350	.150	.250	4.80	.50	.00010	1
366	366	26706.	81.0	45.0	.0550	.150	.500	.150	.350	4.80	.50	.00010	1
367	367	9047.	23.0	65.0	.0450	.150	.500	.150	.350	4.80	.50	.00010	1
373	373	4140.	38.0	6.0	.0200	.150	.400	.150	.350	4.80	.50	.00010	1
241	241	45665.	343.0	45.0	.0200	.150	.400	.150	.450	3.90	.50	.00024	1
346	346	21083.	71.0	40.0	.0600	.150	.450	.150	.350	3.90	.50	.00024	1
345	345	20528.	78.0	50.0	.0600	.150	.450	.150	.350	4.80	.50	.00010	1
349	349	1951.	13.0	15.0	.0200	.150	.450	.150	.350	4.80	.50	.00010	1
347	347	11476.	55.0	65.0	.0500	.150	.400	.150	.350	4.80	.50	.00010	1
371	371	12050.	83.0	50.0	.0500	.150	.450	.150	.250	4.80	.50	.00010	1
338	338	14259.	73.0	8.0	.0250	.150	.350	.150	.250	3.90	.50	.00024	1
333	333	6300.	5.0	60.0	.0400	.200	.450	.150	.550	3.50	.20	.00100	1
334	334	6300.	5.0	60.0	.0400	.150	.350	.150	.250	3.50	.20	.00100	1
240	240	2500.	46.0	25.0	.1100	.150	.450	.150	.600	3.90	.50	.00024	1
318	318	20255.	157.0	20.0	.0300	.150	.550	.150	.500	3.90	.50	.00024	1
335	335	8868.	36.0	45.0	.0500	.150	.450	.150	.450	3.90	.50	.00024	1
336	1329	10002.	31.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
337	337	14520.	50.0	50.0	.0350	.150	.450	.150	.450	3.90	.50	.00024	1
312	312	7094.	12.0	70.0	.0400	.150	.450	.150	.250	3.90	.50	.00024	1
315	315	8712.	28.0	45.0	.0400	.150	.450	.150	.450	3.90	.50	.00024	1
316	316	12777.	43.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
358	358	4084.	12.0	45.0	.0300	.150	.450	.150	.450	3.90	.50	.00024	1
320	320	22099.	161.0	50.0	.0250	.250	.450	.150	.600	3.90	.50	.00024	1
1323	1323	2406.	9.0	50.0	.0080	.150	.450	.150	.450	3.90	.50	.00024	1
321	321	47509.	25.0	60.0	.0450	.150	.450	.150	.350	3.90	.50	.00024	1
319	319	43000.	164.0	70.0	.0250	.150	.400	.150	.250	3.90	.50	.00024	1
370	370	14400.	41.0	70.0	.0250	.150	.400	.150	.250	3.90	.50	.00024	1
233	233	42776.	281.0	25.0	.0500	.150	.500	.150	.500	3.90	.50	.00024	1
235	235	20400.	187.0	20.0	.1100	.150	.500	.150	.500	3.90	.50	.00024	1
231	231	58487.	390.0	55.0	.0200	.150	.400	.150	.250	3.90	.50	.00024	1

OTOTAL NUMBER OF SUBCATCHMENTS, 314
 OTOTAL TRIBUTARY AREA (ACRES), 86852.00
 1

sbc_ltd.swi
 500-year model

500_ltd.wpd July 12, 2000 500-YR SWMM MODEL

*** CONTINUITY CHECK FOR SUBCATCHMENT ROUTING IN UDSWM386 MODEL ***

WATERSHED AREA (ACRES) 86852.000
 TOTAL RAINFALL (INCHES) 4.898
 TOTAL INFILTRATION (INCHES) 3.209
 TOTAL WATERSHED OUTFLOW (INCHES) 1.662
 TOTAL SURFACE STORAGE AT END OF STORM (INCHES) .028
 ERROR IN CONTINUITY, PERCENTAGE OF RAINFALL -.025

1

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 500-year model

GUTTER NUMBER	GUTTER CONNECTION	NDP	NP		WIDTH OR DIAM (FT)	LENGTH (FT)	INVERT SLOPE (FT/FT)	SIDE SLOPES		MANNING N	OVERBANK/SURCHARGE		JK
								HORIZ L	TO VERT R		DEPTH (FT)		
226	224	0	1	CHANNEL	20.0	3740.	.1337	4.0	4.0	.040	15.00	0	
225	224	0	1	CHANNEL	5.0	1862.	.0600	10.0	10.0	.045	15.00	0	
224	222	0	1	CHANNEL	4.0	4220.	.1300	3.0	3.0	.055	15.00	0	
223	222	0	1	CHANNEL	10.0	5960.	.1406	10.0	10.0	.040	15.00	0	
222	218	0	1	CHANNEL	5.0	2280.	.1000	4.0	4.0	.055	15.00	0	
221	218	0	1	CHANNEL	5.0	6520.	.1992	5.0	5.0	.055	15.00	0	
220	219	0	1	CHANNEL	8.0	7580.	.2107	7.0	7.0	.050	15.00	0	
218	219	0	1	CHANNEL	5.0	1660.	.0900	4.0	4.0	.055	15.00	0	
219	215	0	1	CHANNEL	10.0	2531.	.1000	7.0	7.0	.055	15.00	0	
216	215	0	1	CHANNEL	20.0	8160.	.1875	10.0	10.0	.055	15.00	0	
214	212	0	1	CHANNEL	10.0	6880.	.1727	10.0	10.0	.055	15.00	0	
213	212	0	1	CHANNEL	10.0	5900.	.1268	10.0	10.0	.055	15.00	0	
212	211	0	1	CHANNEL	15.0	6100.	.1511	7.0	7.0	.060	15.00	0	
215	211	0	4	CHANNEL	10.0	5210.	.0600	4.0	4.0	.050	2.00	0	
				OVERFLOW	50.0	5210.	.0600	6.0	6.0	.055	25.00	0	
217	215	0	1	CHANNEL	20.0	4860.	.3560	5.0	5.0	.040	15.00	0	
211	207	0	4	CHANNEL	8.0	2390.	.0500	3.0	3.0	.050	2.00	0	
				OVERFLOW	25.0	2390.	.0500	5.0	5.0	.055	25.00	0	
186	184	0	1	CHANNEL	10.0	4260.	.1002	9.0	9.0	.060	15.00	0	
185	184	0	1	CHANNEL	5.0	3720.	.0594	6.0	6.0	.060	15.00	0	
183	182	0	1	CHANNEL	10.0	8000.	.1050	6.0	6.0	.060	15.00	0	
181	180	0	1	CHANNEL	5.0	6640.	.1583	7.0	7.0	.060	15.00	0	
184	182	0	1	CHANNEL	15.0	3540.	.1158	8.0	8.0	.055	15.00	0	
182	180	0	4	CHANNEL	15.0	4600.	.0720	4.0	4.0	.050	2.50	0	
				OVERFLOW	100.0	4370.	.0758	15.0	15.0	.055	20.00	0	
180	176	0	4	CHANNEL	10.0	4520.	.0507	4.0	4.0	.045	3.00	0	
				OVERFLOW	35.0	4294.	.0534	3.0	3.0	.060	20.00	0	
204	201	0	1	CHANNEL	15.0	6720.	.0911	6.0	6.0	.050	15.00	0	
203	201	0	1	CHANNEL	5.0	3500.	.2286	5.0	5.0	.055	15.00	0	
201	198	0	4	CHANNEL	15.0	7700.	.0835	4.0	4.0	.050	3.00	0	
				OVERFLOW	50.0	7315.	.0879	7.0	7.0	.060	20.00	0	
200	198	0	1	CHANNEL	5.0	7220.	.1722	7.0	7.0	.055	15.00	0	
202	198	0	1	CHANNEL	5.0	3820.	.1971	5.0	5.0	.060	15.00	0	
198	194	0	4	CHANNEL	25.0	7220.	.0370	4.0	4.0	.050	3.00	0	
				OVERFLOW	200.0	6860.	.0389	7.0	7.0	.060	20.00	0	
199	194	0	1	CHANNEL	5.0	9020.	.1233	6.0	6.0	.060	15.00	0	
196	194	0	1	CHANNEL	5.0	7320.	.1243	5.0	5.0	.060	15.00	0	
195	194	0	1	CHANNEL	10.0	4760.	.1513	5.0	5.0	.060	15.00	0	
194	192	0	4	CHANNEL	20.0	7560.	.0921	4.0	4.0	.055	3.00	0	
				OVERFLOW	80.0	7182.	.0969	10.0	10.0	.060	20.00	0	
208	207	0	1	CHANNEL	10.0	4260.	.2230	8.0	8.0	.060	15.00	0	
207	205	0	4	CHANNEL	25.0	5000.	.0150	4.0	4.0	.040	2.00	0	
				OVERFLOW	200.0	5000.	.0150	10.0	10.0	.050	25.00	0	
206	205	0	1	CHANNEL	25.0	3860.	.2591	5.0	5.0	.040	15.00	0	
205	192	0	4	CHANNEL	20.0	4900.	.0349	4.0	4.0	.045	3.00	0	
				OVERFLOW	100.0	4900.	.0349	8.0	8.0	.055	25.00	0	
192	187	0	4	CHANNEL	32.0	1540.	.0120	4.0	4.0	.040	3.00	0	
				OVERFLOW	250.0	1540.	.0120	20.0	20.0	.050	25.00	0	
193	187	0	1	CHANNEL	25.0	4480.	.1897	4.0	4.0	.040	15.00	0	
187	172	0	4	CHANNEL	32.0	7388.	.0100	4.0	4.0	.040	3.00	0	
				OVERFLOW	250.0	7388.	.0100	20.0	20.0	.050	25.00	0	
178	177	0	1	CHANNEL	5.0	6500.	.1186	8.0	8.0	.060	15.00	0	
177	175	0	1	CHANNEL	8.0	6020.	.0862	7.0	7.0	.055	15.00	0	
179	176	0	1	CHANNEL	20.0	3860.	.2383	5.0	5.0	.045	16.00	0	
176	175	0	4	CHANNEL	20.0	7520.	.0386	4.0	4.0	.045	3.00	0	
				OVERFLOW	100.0	7144.	.0406	5.0	5.0	.060	20.00	0	
174	173	0	1	CHANNEL	5.0	4060.	.1421	6.0	6.0	.055	15.00	0	
175	173	0	4	CHANNEL	30.0	1900.	.0353	4.0	4.0	.035	3.00	0	
				OVERFLOW	150.0	1805.	.0372	15.0	15.0	.045	20.00	0	
173	172	0	4	CHANNEL	25.0	5760.	.0587	4.0	4.0	.035	3.00	0	
				OVERFLOW	200.0	5472.	.0618	15.0	15.0	.045	20.00	0	
172	157	0	4	CHANNEL	25.0	1860.	.0100	3.0	3.0	.045	3.00	0	
				OVERFLOW	75.0	1860.	.0100	5.0	5.0	.050	25.00	0	
168	165	0	1	CHANNEL	5.0	3620.	.1740	7.0	7.0	.060	15.00	0	
169	165	0	1	CHANNEL	5.0	3140.	.1720	7.0	7.0	.060	15.00	0	
165	166	0	1	CHANNEL	10.0	6920.	.1026	5.0	5.0	.060	15.00	0	
167	166	0	1	CHANNEL	5.0	5360.	.1940	6.0	6.0	.060	15.00	0	
166	163	0	1	CHANNEL	15.0	1040.	.0673	10.0	10.0	.055	15.00	0	
164	163	0	1	CHANNEL	10.0	4000.	.1263	8.0	8.0	.050	15.00	0	
163	157	0	1	CHANNEL	25.0	2640.	.0568	5.0	5.0	.050	15.00	0	
170	157	0	1	CHANNEL	5.0	4840.	.1543	5.0	5.0	.055	15.00	0	
171	157	0	1	CHANNEL	5.0	4420.	.1837	7.0	7.0	.055	15.00	0	
157	156	0	4	CHANNEL	25.0	1660.	.0220	3.0	3.0	.045	3.00	0	
				OVERFLOW	75.0	1660.	.0220	4.0	4.0	.050	25.00	0	
161	160	0	1	CHANNEL	5.0	4380.	.1667	5.0	5.0	.060	15.00	0	

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162	160	0	1	CHANNEL	5.0	5800.	.2121	5.0	5.0	.060	15.00	0
160	158	0	1	CHANNEL	10.0	3360.	.0908	10.0	10.0	.055	15.00	0
159	158	0	1	CHANNEL	10.0	6380.	.1293	6.0	6.0	.060	15.00	0
158	156	0	1	CHANNEL	20.0	5700.	.0619	5.0	5.0	.050	15.00	0
156	154	0	4	CHANNEL	35.0	4980.	.0190	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	4980.	.0190	3.0	3.0	.055	25.00	0
155	154	0	1	CHANNEL	12.0	2180.	.2683	4.0	4.0	.050	15.00	0
153	152	0	1	CHANNEL	12.0	4380.	.1530	4.0	4.0	.060	15.00	0
154	152	0	4	CHANNEL	35.0	2880.	.0200	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	2880.	.0200	3.0	3.0	.055	25.00	0
152	149	0	4	CHANNEL	30.0	6980.	.0150	4.0	4.0	.045	3.00	0
				OVERFLOW	200.0	6980.	.0150	5.0	5.0	.050	25.00	0
150	149	0	1	CHANNEL	5.0	2780.	.1691	4.0	4.0	.055	15.00	0
151	149	0	1	CHANNEL	6.0	4120.	.1286	4.0	4.0	.055	15.00	0
149	139	0	4	CHANNEL	35.0	3220.	.0140	4.0	4.0	.045	3.00	0
				OVERFLOW	300.0	3220.	.0140	5.0	5.0	.050	25.00	0
147	146	0	1	CHANNEL	8.0	5600.	.1625	6.0	6.0	.060	15.00	0
148	146	0	1	CHANNEL	8.0	2720.	.1048	8.0	8.0	.060	15.00	0
146	142	0	1	CHANNEL	10.0	5540.	.0727	8.0	8.0	.055	15.00	0
144	143	0	1	CHANNEL	5.0	2200.	.1568	8.0	8.0	.060	15.00	0
145	143	0	1	CHANNEL	3.0	2160.	.1574	5.0	5.0	.060	15.00	0
143	142	0	1	CHANNEL	8.0	4840.	.1184	5.0	5.0	.060	15.00	0
142	140	0	1	CHANNEL	10.0	2080.	.0514	8.0	5.0	.055	15.00	0
141	140	0	1	CHANNEL	5.0	3800.	.1237	5.0	5.0	.060	15.00	0
140	139	0	1	CHANNEL	15.0	4320.	.0505	8.0	7.0	.055	15.00	0
138	137	0	1	CHANNEL	10.0	5440.	.0432	10.0	10.0	.055	15.00	0
139	137	0	4	CHANNEL	30.0	1880.	.0160	4.0	4.0	.045	3.00	0
				OVERFLOW	200.0	1880.	.0160	5.0	5.0	.050	25.00	0
137	129	0	4	CHANNEL	30.0	2009.	.0130	4.0	4.0	.040	3.00	0
				OVERFLOW	200.0	2009.	.0130	5.0	5.0	.050	25.00	0
135	134	0	1	CHANNEL	5.0	4080.	.1716	5.0	5.0	.060	15.00	0
136	134	0	1	CHANNEL	5.0	3000.	.1433	6.0	6.0	.060	15.00	0
134	133	0	1	CHANNEL	10.0	10020.	.0868	5.0	5.0	.055	15.00	0
133	130	0	1	CHANNEL	15.0	7720.	.0505	5.0	5.0	.055	15.00	0
131	130	0	4	CHANNEL	15.0	4860.	.1008	3.0	3.0	.055	3.00	0
				OVERFLOW	100.0	4617.	.1061	10.0	10.0	.060	20.00	0
132	130	0	1	CHANNEL	8.0	4560.	.0789	6.0	6.0	.060	15.00	0
130	129	0	1	CHANNEL	25.0	3360.	.0363	7.0	7.0	.055	15.00	0
129	96	0	4	CHANNEL	30.0	3520.	.0160	3.5	3.5	.055	4.00	0
				OVERFLOW	100.0	3520.	.0160	4.0	4.0	.060	25.00	0
125	124	0	1	CHANNEL	5.0	3800.	.1842	8.0	8.0	.055	15.00	0
126	124	0	1	CHANNEL	5.0	3420.	.1871	6.0	6.0	.060	15.00	0
124	122	0	1	CHANNEL	10.0	7520.	.0535	8.0	8.0	.055	15.00	0
127	123	0	1	CHANNEL	10.0	8000.	.1056	10.0	10.0	.055	15.00	0
128	123	0	1	CHANNEL	10.0	8660.	.1236	15.0	15.0	.055	15.00	0
123	122	0	1	CHANNEL	15.0	4160.	.0317	15.0	15.0	.055	15.00	0
122	96	0	1	CHANNEL	20.0	9440.	.0607	5.0	5.0	.060	15.00	0
96	95	0	4	CHANNEL	25.0	6320.	.0170	2.0	2.0	.055	4.00	0
				OVERFLOW	50.0	6320.	.0170	2.0	2.0	.060	25.00	0
116	95	0	4	CHANNEL	5.0	9520.	.0772	3.0	3.0	.050	2.50	0
				OVERFLOW	70.0	9044.	.0813	8.0	8.0	.055	20.00	0
95	94	0	4	CHANNEL	30.0	4000.	.0120	3.0	3.0	.040	3.00	0
				OVERFLOW	150.0	4000.	.0120	5.0	5.0	.050	25.00	0
85	84	0	1	CHANNEL	5.0	2220.	.0396	4.0	4.0	.060	15.00	0
86	84	0	1	CHANNEL	8.0	5880.	.1259	4.0	4.0	.060	15.00	0
84	82	0	1	CHANNEL	10.0	2720.	.0890	10.0	10.0	.060	15.00	0
83	82	0	1	CHANNEL	10.0	2380.	.0450	12.0	12.0	.060	15.00	0
82	80	0	1	CHANNEL	20.0	2220.	.0396	12.0	12.0	.060	15.00	0
87	81	0	1	CHANNEL	10.0	8040.	.0796	5.0	5.0	.065	15.00	0
81	80	0	1	CHANNEL	15.0	6220.	.0691	7.0	7.0	.065	15.00	0
80	79	0	1	CHANNEL	20.0	6380.	.1993	10.0	10.0	.065	15.00	0
121	79	0	4	CHANNEL	8.0	4700.	.0660	4.0	4.0	.055	2.50	0
				OVERFLOW	60.0	4465.	.0695	12.0	12.0	.057	20.00	0
79	75	0	1	CHANNEL	25.0	8020.	.0212	10.0	10.0	.060	15.00	0
78	75	0	1	CHANNEL	8.0	3780.	.0688	20.0	20.0	.060	15.00	0
75	77	0	1	CHANNEL	25.0	1600.	.0188	3.0	5.0	.060	15.00	0
77	74	0	1	CHANNEL	40.0	2020.	.0198	3.0	3.0	.060	15.00	0
76	74	0	4	CHANNEL	10.0	6420.	.0779	4.0	4.0	.050	2.00	0
				OVERFLOW	60.0	6420.	.0779	8.0	8.0	.055	20.00	0
74	59	0	4	CHANNEL	30.0	4700.	.0130	4.0	4.0	.050	4.00	0
				OVERFLOW	75.0	4700.	.0130	4.0	3.0	.055	25.00	0
89	88	0	1	CHANNEL	8.0	4240.	.0217	10.0	10.0	.055	15.00	0
93	88	0	1	CHANNEL	5.0	2440.	.0984	10.0	10.0	.055	15.00	0
86	77	0	4	CHANNEL	11.0	7200.	.1380	10.0	10.0	.060	3.00	0
				OVERFLOW	100.0	7200.	.1380	50.0	50.0	.045	20.00	0
120	119	0	4	CHANNEL	5.0	3980.	.0879	3.0	3.0	.050	3.00	0
				OVERFLOW	200.0	3781.	.0925	10.0	10.0	.055	20.00	0
118	119	0	4	CHANNEL	5.0	8220.	.1095	3.0	3.0	.050	3.00	0
				OVERFLOW	150.0	7809.	.1153	10.0	10.0	.055	20.00	0
119	104	0	4	CHANNEL	5.0	1300.	.0400	3.0	3.0	.050	3.00	0
				OVERFLOW	150.0	1235.	.0421	10.0	10.0	.055	20.00	0
117	104	0	4	CHANNEL	5.0	6000.	.0587	3.0	3.0	.050	3.00	0
				OVERFLOW	100.0	5700.	.0618	10.0	10.0	.055	20.00	0
104	103	0	4	CHANNEL	10.0	3440.	.0343	3.0	3.0	.045	3.00	0
				OVERFLOW	150.0	3268.	.0361	10.0	10.0	.050	20.00	0
105	103	0	4	CHANNEL	5.0	4560.	.0811	3.0	3.0	.045	3.00	0
				OVERFLOW	100.0	4332.	.0854	10.0	10.0	.050	20.00	0
106	102	0	4	CHANNEL	5.0	6380.	.0690	3.0	3.0	.045	3.00	0
				OVERFLOW	70.0	6061.	.0726	10.0	10.0	.050	20.00	0
103	102	0	4	CHANNEL	8.0	1380.	.0362	4.0	40.0	.050	3.00	0
				OVERFLOW	68.0	1311.	.0381	25.0	25.0	.055	20.00	0
102	101	0	4	CHANNEL	11.0	5220.	.0383	8.0	8.0	.055	3.00	0
				OVERFLOW	100.0	4959.	.0403	5.0	5.0	.060	20.00	0
114	112	0	1	CHANNEL	5.0	4500.	.1467	5.0	5.0	.060	8.00	0
115	112	0	1	CHANNEL	5.0	3240.	.1759	5.0	5.0	.060	8.00	0
112	110	0	4	CHANNEL	5.0	3640.	.1745	3.0	3.0	.055	2.50	0
				OVERFLOW	40.0	3458.	.1837	10.0	8.0	.060	20.00	0
113	110	0	4	CHANNEL	5.0	5060.	.1690	3.0	3.0	.055	3.00	0
				OVERFLOW	40.0	4807.	.1779	10.0	10.0	.060	20.00	0
110	109	0	4	CHANNEL	11.0	4140.	.0531	4.0	4.0	.055	3.00	0
				OVERFLOW	60.0	3933.	.0559	50.0	50.0	.060	20.00	0

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111	109	0	4	CHANNEL	5.0	5600.	.2348	3.0	3.0	.050	2.00	0				
				OVERFLOW	20.0	5320.	.2472	6.0	6.0	.055	20.00					
108	107	0	4	CHANNEL	5.0	6240.	.1875	3.0	3.0	.050	2.00	0				
				OVERFLOW	20.0	5928.	.1974	6.0	6.0	.055	20.00					
109	107	0	4	CHANNEL	11.0	2760.	.0525	4.0	4.0	.050	3.00	0				
				OVERFLOW	60.0	2622.	.0553	6.0	6.0	.055	20.00					
107	101	0	4	CHANNEL	11.0	2720.	.0368	4.0	4.0	.050	3.00	0				
				OVERFLOW	45.0	2584.	.0387	6.0	6.0	.055	20.00					
101	99	0	4	CHANNEL	11.0	1380.	.0268	4.0	4.0	.050	3.00	0				
				OVERFLOW	50.0	1311.	.0282	5.0	5.0	.055	20.00					
100	99	0	4	CHANNEL	5.0	9980.	.1735	3.0	3.0	.050	2.00	0				
				OVERFLOW	25.0	9481.	.1826	5.0	5.0	.055	20.00					
99	97	0	4	CHANNEL	11.0	1440.	.0299	4.0	4.0	.050	3.00	0				
				OVERFLOW	50.0	1368.	.0315	5.0	5.0	.055	20.00					
98	97	0	4	CHANNEL	8.0	7000.	.1179	3.0	3.0	.050	2.00	0				
				OVERFLOW	35.0	6650.	.1241	6.0	6.0	.055	20.00					
97	94	0	4	CHANNEL	11.0	5720.	.0332	4.0	4.0	.050	2.50	0				
				OVERFLOW	50.0	5434.	.0349	4.0	4.0	.055	20.00					
94	74	0	4	CHANNEL	32.0	2560.	.0120	4.0	4.0	.040	3.50	0				
				OVERFLOW	150.0	2560.	.0120	8.0	8.0	.050	25.00					
72	71	0	1	CHANNEL	10.0	4480.	.0808	5.0	5.0	.055	15.00	0				
73	71	0	1	CHANNEL	10.0	8000.	.0303	8.0	8.0	.055	15.00	0				
71	59	0	1	CHANNEL	12.0	4820.	.0664	5.0	5.0	.060	15.00	0				
59	46	0	4	CHANNEL	30.0	4020.	.0140	4.0	4.0	.050	4.00	0				
				OVERFLOW	60.0	4020.	.0140	3.0	3.0	.055	25.00					
63	61	0	1	CHANNEL	9.0	6420.	.0779	5.0	5.0	.070	20.00	0				
64	61	0	1	CHANNEL	9.0	2020.	.0198	5.0	5.0	.070	20.00	0				
61	62	0	1	CHANNEL	12.0	7500.	.0633	5.0	5.0	.070	20.00	0				
60	46	0	1	CHANNEL	12.0	4080.	.1262	5.0	5.0	.060	20.00	0				
46	42	0	4	CHANNEL	25.0	3220.	.0300	3.0	3.0	.055	5.00	0				
				OVERFLOW	50.0	3220.	.0300	4.0	4.0	.060	25.00					
66	65	0	1	CHANNEL	9.0	3060.	.2026	4.0	4.0	.060	15.00	0				
67	65	0	4	CHANNEL	10.0	6620.	.0853	3.0	3.0	.050	4.00	0				
				OVERFLOW	45.0	6289.	.0898	3.0	3.0	.060	25.00					
65	62	0	4	CHANNEL	15.0	3960.	.0088	3.0	3.0	.050	4.00	0				
				OVERFLOW	50.0	3762.	.0093	3.0	3.0	.060	25.00					
62	42	0	1	CHANNEL	12.0	1400.	.2629	5.0	5.0	.070	20.00	0				
69	68	0	1	CHANNEL	10.0	3740.	.1056	6.0	6.0	.055	15.00	0				
70	68	0	1	CHANNEL	12.0	6960.	.0912	6.0	6.0	.055	15.00	0				
68	42	0	1	CHANNEL	12.0	2120.	.1203	5.0	5.0	.060	15.00	0				
41	40	0	1	CHANNEL	12.0	3100.	.2423	5.0	5.0	.060	20.00	0				
42	40	0	4	CHANNEL	20.0	7580.	.0500	3.0	3.0	.055	4.00	0				
				OVERFLOW	50.0	7580.	.0500	2.0	2.0	.060	25.00					
40	16	0	4	CHANNEL	20.0	3000.	.0330	3.0	3.0	.055	4.00	0				
				OVERFLOW	50.0	3000.	.0330	2.0	2.0	.060	25.00					
20	18	0	1	CHANNEL	10.0	5340.	.0534	8.0	8.0	.050	15.00	0				
18	17	0	4	CHANNEL	11.0	7600.	.0605	3.0	3.0	.050	3.00	0				
				OVERFLOW	40.0	7220.	.0637	5.0	5.0	.055	20.00					
21	17	0	1	CHANNEL	10.0	6960.	.1042	5.0	5.0	.060	15.00	0				
17	16	0	4	CHANNEL	11.0	1000.	.0493	10.0	10.0	.040	3.00	0				
				OVERFLOW	40.0	1000.	.0493	8.0	8.0	.055	20.00					
14	15	0	1	CHANNEL	15.0	3080.	.2662	3.0	3.0	.060	15.00	0				
15	8	0	3		.0	1.	.0010	.0	.0	.001	10.00	0				
16	15	0	3		.0	1.	.0010	.0	.0	.001	10.00	0				
8	397	0	3		.0	1.	.0010	.0	.0	.001	10.00	0				
397	6	14	2	PIPE	.1	1.	.0050	.0	.0	.013	.10	0				
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW																
					.0	.0	207.0	170.0	415.0	476.0	833.0	1330.0	1254.0	2417.0	1677.0	3673.0
					2104.0	5078.0	2535.0	6591.0	2968.0	8200.0	3405.0	9896.0	3847.0	12853.0	4292.0	16870.0
					6098.0	37861.0	7880.0	91713.0								
38	37	0	1	CHANNEL	12.0	5060.	.1146	15.0	15.0	.050	15.00	0				
39	37	0	1	CHANNEL	10.0	5140.	.0807	10.0	10.0	.050	20.00	0				
37	23	0	4	CHANNEL	11.0	8160.	.0386	4.0	4.0	.050	3.00	0				
				OVERFLOW	60.0	7752.	.0406	25.0	25.0	.055	20.00					
35	34	0	1	CHANNEL	10.0	3140.	.0930	10.0	10.0	.050	15.00	0				
36	34	0	1	CHANNEL	12.0	5340.	.0549	15.0	15.0	.050	15.00	0				
34	23	0	4	CHANNEL	11.0	6840.	.0450	4.0	4.0	.050	3.00	0				
				OVERFLOW	50.0	6498.	.0474	25.0	25.0	.055	20.00					
32	31	0	1	CHANNEL	8.0	3260.	.0883	8.0	8.0	.055	15.00	0				
33	31	0	1	CHANNEL	8.0	5180.	.0788	8.0	8.0	.055	15.00	0				
31	23	0	1	CHANNEL	12.0	2720.	.0393	10.0	10.0	.055	15.00	0				
23	22	0	4	CHANNEL	11.0	4920.	.0315	3.0	3.0	.050	3.00	0				
				OVERFLOW	50.0	4674.	.0332	10.0	10.0	.055	20.00					
29	28	0	1	CHANNEL	5.0	3060.	.1471	6.0	6.0	.055	15.00	0				
30	28	0	1	CHANNEL	12.0	5780.	.0484	15.0	15.0	.050	15.00	0				
27	26	0	1	CHANNEL	10.0	2540.	.1693	10.0	10.0	.040	15.00	0				
28	26	0	4	CHANNEL	11.0	2520.	.0595	10.0	10.0	.040	3.00	0				
				OVERFLOW	80.0	2394.	.0626	25.0	25.0	.045	15.00					
25	24	0	1	CHANNEL	6.0	5920.	.1309	8.0	8.0	.050	15.00	0				
26	24	0	4	CHANNEL	12.0	1860.	.0242	4.0	4.0	.050	3.00	0				
				OVERFLOW	80.0	1767.	.0255	10.0	10.0	.055	15.00					
24	22	0	4	CHANNEL	12.0	1740.	.0287	4.0	4.0	.050	3.00	0				
				OVERFLOW	100.0	1653.	.0302	10.0	10.0	.055	20.00					
22	8	0	4	CHANNEL	11.0	3600.	.0658	3.0	3.0	.050	3.00	0				
				OVERFLOW	40.0	3600.	.0658	6.0	6.0	.055	20.00					
9	7	0	4	CHANNEL	3.0	10320.	.1556	3.0	3.0	.060	2.00	0				
				OVERFLOW	20.0	9804.	.1638	2.0	2.0	.080	25.00					
10	7	0	1	CHANNEL	15.0	3760.	.1293	3.0	3.0	.040	15.00	0				
7	5	0	4	CHANNEL	5.0	4940.	.0656	2.0	2.0	.060	2.50	0				
				OVERFLOW	25.0	4693.	.0691	2.0	2.0	.080	20.00					
3	2	0	1	CHANNEL	25.0	11000.	.0682	4.0	4.0	.040	15.00	0				
4	2	0	1	CHANNEL	25.0	12780.	.1033	4.0	4.0	.040	15.00	0				
2	1	0	4	CHANNEL	8.0	7240.	.0631	2.0	2.0	.070	3.00	0				
				OVERFLOW	30.0	6878.	.0664	2.0	2.0	.080	20.00					
6	5	0	4	CHANNEL	35.0	4840.	.0340	2.0	2.0	.055	4.00	0				
				OVERFLOW	60.0	4840.	.0340	2.0	2.0	.065	25.00					
5	1	0	4	CHANNEL	30.0	4960.	.0240	2.0	2.0	.055	4.00	0				
				OVERFLOW	55.0	4960.	.0240	2.0	2.0	.065	25.00					
1	245	0	4	CHANNEL	30.0	10240.	.0240	2.0	2.0	.055	4.00	0				
				OVERFLOW	55.0	10240.	.0240	2.0	2.0	.065	25.00					
11	13	0	1	CHANNEL	12.0	3000.	.1200	3.0	3.0	.040	15.00	0				

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12	13	0	1	CHANNEL	12.0	4180.	.1340	3.0	3.0	.040	15.00	0	
13	5	0	4	CHANNEL	15.0	5240.	.1202	4.0	4.0	.040	5.00	0	
				OVERFLOW	100.0	4978.	.1265	40.0	40.0	.045	20.00	0	
248	250	0	4	CHANNEL	25.0	9340.	.0931	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	8973.	.0980	40.0	40.0	.080	20.00	0	
249	250	0	4	CHANNEL	20.0	3940.	.0964	4.0	4.0	.060	5.00	0	
				OVERFLOW	90.0	3743.	.1015	40.0	40.0	.080	20.00	0	
247	246	0	4	CHANNEL	25.0	8120.	.0924	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	7714.	.0973	40.0	40.0	.080	20.00	0	
250	246	0	4	CHANNEL	25.0	2060.	.0485	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	1957.	.0511	40.0	40.0	.080	20.00	0	
246	245	0	4	CHANNEL	25.0	4660.	.0676	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	4427.	.0712	40.0	40.0	.080	20.00	0	
244	52	0	4	CHANNEL	25.0	8700.	.0989	4.0	4.0	.070	5.00	0	
				OVERFLOW	100.0	8265.	.1041	40.0	40.0	.080	20.00	0	
245	52	0	4	CHANNEL	30.0	3060.	.0300	3.0	3.0	.070	4.00	0	
				OVERFLOW	60.0	3060.	.0300	2.0	2.0	.080	20.00	0	
54	53	0	1	CHANNEL	5.0	4000.	.1500	3.0	3.0	.060	15.00	0	
55	53	0	1	CHANNEL	5.0	5500.	.1382	3.0	3.0	.060	15.00	0	
53	52	0	1	CHANNEL	5.0	1200.	.1083	3.0	3.0	.060	15.00	0	
51	50	0	4	CHANNEL	5.0	5200.	.1327	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	4940.	.1397	40.0	40.0	.080	20.00	0	
52	50	0	4	CHANNEL	35.0	9160.	.0218	3.0	3.0	.055	4.00	0	
				OVERFLOW	65.0	9160.	.0218	2.0	2.0	.065	25.00	0	
50	48	0	4	CHANNEL	40.0	3400.	.0294	5.0	5.0	.060	4.00	0	
				OVERFLOW	150.0	3400.	.0294	75.0	75.0	.080	25.00	0	
57	56	0	4	CHANNEL	25.0	8400.	.1262	4.0	4.0	.060	5.00	0	
				OVERFLOW	100.0	7980.	.1328	40.0	40.0	.080	20.00	0	
58	56	0	1	CHANNEL	5.0	2200.	.1636	3.0	3.0	.060	15.00	0	
56	50	0	4	CHANNEL	25.0	10000.	.0930	4.0	4.0	.070	5.00	0	
				OVERFLOW	100.0	9500.	.0979	40.0	40.0	.080	20.00	0	
49	48	0	1	CHANNEL	12.0	3200.	.2594	3.0	3.0	.060	8.00	0	
48	1626	0	4	CHANNEL	30.0	4700.	.0133	2.0	2.0	.070	5.00	0	
				OVERFLOW	200.0	4700.	.0133	2.0	2.0	.085	25.00	0	
1238	1927	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1927	238	0	4	CHANNEL	15.0	964.	.0012	3.5	3.5	.045	4.00	0	
				OVERFLOW	70.0	964.	.0012	7.5	5.0	.055	20.00	0	
1295	295	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
295	1296	10	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0	
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW													
		.0	.0	8.3	.5	17.8	1.0	28.1	10.5	39.4	18.2	52.5	23.5
		68.3	278.0	86.7	1321.5	107.1	5035.0	150.0	10000.0				
1296	296	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
296	1382	6	3		.0	1.	.0010	.0	.0	.001	10.00	1383	
DIVERSION TO GUTTER NUMBER1383 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	24.0	.1	278.0	250.0	1321.0	1290.0	5035.0	5000.0	10000.0	9964.0
1382	1381	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
384	1820	0	5	PIPE	3.0	4047.	.0176	.0	.0	.020	3.00	0	
				OVERFLOW	1.0	4047.	.0176	20.0	20.0	.020	50.00	0	
1820	383	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1383	1820	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
383	1405	8	3		.0	1.	.0010	.0	.0	.001	10.00	1360	
DIVERSION TO GUTTER NUMBER1360 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	150.0	1.0	223.0	23.0	285.0	75.0	426.0	201.0	1592.0	1342.0
		3953.0	3653.0	10000.0	9680.0								
1405	1381	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1381	382	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
382	381	0	5	PIPE	7.5	1142.	.0020	.0	.0	.015	7.50	0	
				OVERFLOW	7.5	1142.	.0020	20.0	20.0	.015	50.00	0	
381	1926	4	3		.0	1.	.0010	.0	.0	.001	10.00	1366	
DIVERSION TO GUTTER NUMBER1366 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	150.0	1.0	342.0	182.0	2438.0	2050.0				
369	1821	0	4	CHANNEL	.5	1030.	.0089	12.0	12.0	.016	.50	0	
				OVERFLOW	10.0	1030.	.0089	20.0	20.0	.020	10.00	0	
1926	1821	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1821	380	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
380	379	0	1	CHANNEL	8.0	754.	.0040	1.5	1.5	.050	10.00	0	
379	1406	4	3		.0	1.	.0010	.0	.0	.001	10.00	1367	
DIVERSION TO GUTTER NUMBER1367 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	180.0	.1	629.0	354.0	3656.0	3293.0				
1406	1378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1404	1378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1378	378	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
378	1925	5	3		.0	1.	.0010	.0	.0	.001	10.00	1289	
DIVERSION TO GUTTER NUMBER1289 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	90.0	1.0	95.0	5.0	363.0	253.0	528.0	390.0		
1925	377	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
377	242	0	1	CHANNEL	8.0	2090.	.0040	1.5	1.5	.055	10.00	0	
1715	1716	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1716	1517	0	4	CHANNEL	10.0	3321.	.0032	8.0	8.0	.035	.50	0	
				OVERFLOW	30.0	3321.	.0032	80.0	80.0	.035	15.00	0	
1515	1517	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1517	1522	0	4	CHANNEL	4.0	851.	.0035	8.0	8.0	.035	.50	0	
				OVERFLOW	20.0	851.	.0035	60.0	60.0	.035	15.00	0	
1541	1542	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1542	1544	0	4	CHANNEL	5.0	10122.	.0260	4.0	4.0	.040	2.00	0	
				OVERFLOW	30.0	10122.	.0260	80.0	80.0	.045	15.00	0	
1520	1521	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1525	1526	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1528	1428	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1428	1429	0	4	CHANNEL	4.0	1682.	.0131	2.0	2.0	.025	2.00	0	
				OVERFLOW	400.0	1682.	.0131	40.0	40.0	.035	15.00	0	
1415	1416	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1550	1551	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1560	1561	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1561	1563	0	4	CHANNEL	3.0	2480.	.1940	4.0	4.0	.050	2.00	0	
				OVERFLOW	25.0	2480.	.1940	50.0	50.0	.055	15.00	0	
1565	1566	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	
1566	1563	0	4	CHANNEL	3.0	2240.	.2140	4.0	4.0	.050	2.00	0	
				OVERFLOW	25.0	2240.	.2140	6.0	6.0	.055	15.00	0	
1563	1551	0	3		.0	1.	.0010	.0	.0	.001	10.00	0	

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1551	1553	0	4	CHANNEL	3.0	8900.	.0560	5.0	5.0	.040	2.00	0
				OVERFLOW	30.0	8900.	.0560	50.0	50.0	.045	10.00	0
1570	1571	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1571	1557	0	1	CHANNEL	5.0	1200.	.2670	40.0	40.0	.055	10.00	0
1556	1557	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1557	1553	0	4	CHANNEL	3.0	5620.	.0240	5.0	5.0	.040	2.00	0
				OVERFLOW	25.0	5620.	.0240	40.0	40.0	.045	15.00	0
1553	1416	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1416	1429	0	4	CHANNEL	5.0	4085.	.0225	4.0	4.0	.050	2.00	0
				OVERFLOW	25.0	4085.	.0225	40.0	40.0	.055	15.00	0
1429	1526	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1526	1532	0	4	CHANNEL	2.0	1410.	.0136	2.0	2.0	.055	2.00	0
				OVERFLOW	400.0	1410.	.0136	40.0	40.0	.065	15.00	0
1530	1531	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1545	1546	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1575	1576	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1576	1546	0	4	CHANNEL	2.0	3500.	.0229	5.0	5.0	.050	2.00	0
				OVERFLOW	30.0	3500.	.0229	50.0	50.0	.055	15.00	0
1546	1531	0	4	CHANNEL	5.0	7763.	.0840	4.0	4.0	.050	2.00	0
				OVERFLOW	30.0	7763.	.0840	75.0	75.0	.055	15.00	0
1531	1532	0	4	CHANNEL	5.0	5288.	.0872	4.0	4.0	.040	2.00	0
				OVERFLOW	30.0	5288.	.0872	80.0	80.0	.045	15.00	0
1532	1537	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1537	1533	0	4	CHANNEL	2.0	1127.	.0035	2.0	2.0	.035	2.00	0
				OVERFLOW	400.0	1127.	.0035	5.0	40.0	.035	15.00	0
1414	1534	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1534	1533	0	4	CHANNEL	10.0	1966.	.0080	5.0	5.0	.050	1.00	0
				OVERFLOW	400.0	1966.	.0080	50.0	3.0	.065	15.00	0
1533	1521	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1521	1544	0	4	CHANNEL	4.0	2633.	.0093	2.0	2.0	.050	2.00	0
				OVERFLOW	500.0	2633.	.0093	25.0	25.0	.065	10.00	0
1544	1548	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1548	1522	0	4	CHANNEL	4.0	1054.	.0038	8.0	8.0	.035	.50	0
				OVERFLOW	500.0	1054.	.0038	60.0	60.0	.035	15.00	0
1522	1511	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1510	1511	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1511	1513	0	4	CHANNEL	4.0	3213.	.0057	2.0	2.0	.050	2.00	0
				OVERFLOW	512.0	3213.	.0057	50.0	50.0	.060	10.00	0
1513	1514	8	3		.0	1.	.0010	.0	.0	.001	10.00	1508
DIVERSION TO GUTTER NUMBER1508 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	50.0	.1	140.0	48.0	415.0	192.0	1791.0	1299.0	3930.0 3176.0
		7762.0	6551.0	15011.0	13210.0							
1514	1442	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1442	1935	0	4	CHANNEL	2.0	2252.	.0097	4.0	4.0	.040	1.00	0
				OVERFLOW	300.0	2252.	.0097	80.0	80.0	.060	15.00	0
1262	1916	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1916	1935	0	4	CHANNEL	2.0	1211.	.0046	5.0	3.0	.035	1.00	0
				OVERFLOW	400.0	1211.	.0046	100.0	3.0	.035	20.00	0
1935	262	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
262	263	0	4	CHANNEL	2.0	529.	.0058	5.0	3.0	.035	1.00	0
				OVERFLOW	500.0	529.	.0058	150.0	3.0	.035	20.00	0
263	1905	8	3		.0	1.	.0010	.0	.0	.001	10.00	266
DIVERSION TO GUTTER NUMBER266 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	175.0	174.9	412.0	185.0	908.0	198.0	1902.0	212.0	3161.0 228.0
		6477.0	233.0	13854.0	256.0							
1905	264	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
264	265	0	4	CHANNEL	2.0	1138.	.0017	5.0	3.0	.035	.50	0
				OVERFLOW	600.0	1138.	.0017	150.0	3.0	.035	20.00	0
265	269	8	3		.0	1.	.0010	.0	.0	.001	10.00	1267
DIVERSION TO GUTTER NUMBER1267 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	170.0	169.9	227.0	195.0	710.0	516.0	1689.0	1249.0	2933.0 1956.0
		6244.0	3358.0	13598.0	6585.0							
269	1294	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1294	294	0	4	CHANNEL	2.0	1043.	.0027	4.0	4.0	.025	1.00	0
				OVERFLOW	375.0	1043.	.0027	80.0	3.0	.035	15.00	0
304	294	0	1	CHANNEL	8.0	2370.	.0060	5.0	5.0	.035	10.00	0
299	303	0	4	CHANNEL	.5	3612.	.0400	12.0	12.0	.016	.50	0
				OVERFLOW	24.0	3612.	.0400	20.0	20.0	.020	10.00	0
301	300	0	4	CHANNEL	.5	3743.	.0800	12.0	12.0	.016	.50	0
				OVERFLOW	24.0	3743.	.0800	20.0	20.0	.020	10.00	0
300	1922	5	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	5.4	10.0	28.7	11.0	36.6	32.0	39.3	468.0	
1922	303	0	4	CHANNEL	.5	899.	.0667	12.0	12.0	.016	.50	0
				OVERFLOW	10.0	899.	.0667	20.0	20.0	.020	10.00	0
303	298	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
298	297	11	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	.1	15.0	.5	45.0	1.4	94.0	2.9	130.0	5.3 158.0
		9.3	182.0	12.2	192.0	15.9	225.0	20.4	286.0	25.0	827.0	
297	1921	0	4	CHANNEL	6.0	5106.	.0250	3.0	3.0	.045	6.00	0
				OVERFLOW	50.0	6800.	.0188	3.0	3.0	.035	10.00	0
1917	1921	0	4	CHANNEL	5.0	1894.	.0079	8.0	8.0	.035	1.00	0
				OVERFLOW	40.0	1894.	.0079	80.0	80.0	.035	15.00	0
1921	1920	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
1920	294	0	4	CHANNEL	18.0	785.	.0013	6.0	6.0	.035	6.00	0
				OVERFLOW	100.0	785.	.0013	12.0	12.0	.035	15.00	0
294	280	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
280	1293	6	3		.0	1.	.0010	.0	.0	.001	10.00	1295
DIVERSION TO GUTTER NUMBER1295 - TOTAL Q VS DIVERTED Q IN CFS												
		.0	.0	295.0	1.0	370.0	42.0	1046.0	661.0	2827.0	2327.0	8734.0 8169.0
1293	293	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
293	267	0	5	PIPE	8.5	757.	.0020	.0	.0	.015	8.50	0
				OVERFLOW	8.5	757.	.0020	.0	.0	.015	20.00	0
1267	267	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
267	268	0	3		.0	1.	.0010	.0	.0	.001	10.00	0
268	1291	8	2	PIPE	.1	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW												
		.0	.0	1.4	81.0	5.0	267.0	10.4	465.0	16.9	632.0	25.0 1145.0
		35.1	1888.0	140.0	10000.0							
1291	291	0	3		.0	1.	.0010	.0	.0	.001	10.00	0

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291	1290	6	3	.0	1.	.0010	.0	.0	.001	10.00	1923
DIVERSION TO GUTTER NUMBER1923 - TOTAL Q VS DIVERTED Q IN CFS											
.0 .0 515.0 1.0 1249.0 471.0 1956.0 1098.0 6585.0 5685.0 10000.0 9000.0											
1290	290	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1290	1924	0	4	CHANNEL	30.0	1375.	.0017	4.0	4.0	.045	6.00
				OVERFLOW	100.0	1375.	.0017	20.0	20.0	.050	15.00
1289	1924	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1924	289	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
289	242	0	4	CHANNEL	30.0	1962.	.0017	4.0	4.0	.045	6.00
				OVERFLOW	100.0	1962.	.0017	20.0	20.0	.050	15.00
1505	1506	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1410	1411	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1420	1421	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1435	1436	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1436	1438	0	4	CHANNEL	2.0	3730.	.0350	4.0	4.0	.050	3.00
				OVERFLOW	30.0	3730.	.0350	16.0	16.0	.055	15.00
1430	1431	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1431	1438	0	4	CHANNEL	2.0	1670.	.0820	4.0	4.0	.040	1.00
				OVERFLOW	12.0	1670.	.0820	15.0	15.0	.045	15.00
1438	1426	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1425	1426	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1426	1421	0	4	CHANNEL	5.0	2319.	.0190	8.0	8.0	.040	2.00
				OVERFLOW	40.0	2319.	.0190	75.0	75.0	.045	15.00
1445	1446	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1446	1453	0	4	CHANNEL	2.0	6667.	.0606	3.0	3.0	.040	3.00
				OVERFLOW	25.0	6667.	.0606	6.0	6.0	.045	15.00
1645	1646	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1646	1643	0	4	CHANNEL	5.0	5300.	.1450	4.0	4.0	.060	2.00
				OVERFLOW	25.0	5300.	.1450	15.0	15.0	.065	15.00
1640	1641	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1641	1643	0	4	CHANNEL	2.0	5800.	.0160	3.0	3.0	.060	3.00
				OVERFLOW	25.0	5800.	.0160	8.0	8.0	.065	15.00
1643	1631	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1630	1631	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1631	1628	0	4	CHANNEL	10.0	7611.	.0730	4.0	4.0	.040	3.00
				OVERFLOW	40.0	7611.	.0730	10.0	10.0	.045	15.00
1625	1626	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1635	1636	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1636	1626	0	1	CHANNEL	2.0	4200.	.0840	8.0	8.0	.040	10.00
1626	1628	0	4	CHANNEL	25.0	1908.	.0205	4.0	4.0	.070	2.00
				OVERFLOW	100.0	1908.	.0205	75.0	75.0	.075	15.00
1628	1611	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1610	1611	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1611	1928	0	4	CHANNEL	30.0	4400.	.0290	4.0	4.0	.060	2.50
				OVERFLOW	150.0	4400.	.0290	75.0	75.0	.070	15.00
1605	1606	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1665	1666	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1666	1606	0	4	CHANNEL	3.0	6900.	.2130	3.0	3.0	.050	2.00
				OVERFLOW	20.0	6900.	.2130	2.0	2.0	.055	10.00
1606	1928	0	4	CHANNEL	5.0	5987.	.0812	4.0	4.0	.045	2.00
				OVERFLOW	25.0	5987.	.0812	3.0	3.0	.060	15.00
1928	1601	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1600	1601	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1601	1603	0	4	CHANNEL	25.0	1264.	.0290	6.0	6.0	.060	2.50
				OVERFLOW	85.0	1264.	.0290	80.0	80.0	.070	15.00
1710	1711	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1711	1712	0	4	CHANNEL	5.0	5430.	.0479	4.0	4.0	.035	1.00
				OVERFLOW	30.0	5430.	.0479	5.0	5.0	.035	15.00
1615	1616	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1616	1623	0	4	CHANNEL	2.0	6409.	.0620	3.0	3.0	.040	3.00
				OVERFLOW	20.0	6409.	.0620	5.0	5.0	.045	15.00
1660	1661	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1661	1651	0	4	CHANNEL	3.0	9600.	.1670	4.0	4.0	.060	3.00
				OVERFLOW	25.0	9600.	.1670	3.0	3.0	.065	15.00
1650	1651	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1651	1653	0	4	CHANNEL	5.0	4100.	.0860	4.0	4.0	.050	3.00
				OVERFLOW	25.0	4100.	.0860	3.0	3.0	.055	15.00
1655	1656	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1656	1653	0	4	CHANNEL	3.0	10800.	.1170	4.0	4.0	.050	3.00
				OVERFLOW	25.0	10800.	.1170	3.0	3.0	.055	15.00
1653	1621	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1620	1621	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1621	1623	0	4	CHANNEL	5.0	10100.	.0320	5.0	5.0	.045	3.00
				OVERFLOW	35.0	10100.	.0320	2.0	2.0	.060	15.00
1623	1624	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1705	1624	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1624	1712	0	4	CHANNEL	2.0	2490.	.0380	5.0	5.0	.050	2.00
				OVERFLOW	25.0	2490.	.0380	5.0	5.0	.050	10.00
1712	1929	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1929	1603	0	4	CHANNEL	10.0	1172.	.0043	10.0	10.0	.035	.50
				OVERFLOW	20.0	1172.	.0043	40.0	40.0	.035	15.00
1603	1451	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1450	1451	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1451	1453	0	4	CHANNEL	30.0	2963.	.0110	6.0	6.0	.060	2.50
				OVERFLOW	110.0	2963.	.0110	80.0	80.0	.070	15.00
1453	1441	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1440	1441	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1441	1421	0	4	CHANNEL	30.0	3235.	.0078	4.0	4.0	.060	2.50
				OVERFLOW	110.0	3235.	.0078	75.0	75.0	.070	15.00
1421	1423	0	4	CHANNEL	30.0	800.	.0120	4.0	4.0	.060	2.50
				OVERFLOW	120.0	800.	.0120	75.0	75.0	.090	15.00
1423	1424	8	3	.0	1.	.0010	.0	.0	.001	10.00	1528
DIVERSION TO GUTTER NUMBER1528 - TOTAL Q VS DIVERTED Q IN CFS											
.0 .0 1000.0 1.0 2000.0 114.0 3100.0 335.0 4000.0 597.0 5683.0 1262.0											
1424	1411	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1411	1412	0	4	CHANNEL	30.0	3369.	.0084	4.0	4.0	.060	2.50
				OVERFLOW	160.0	3369.	.0084	75.0	75.0	.065	15.00
1412	1413	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1413	1509	9	3	.0	1.	.0010	.0	.0	.001	10.00	1414
DIVERSION TO GUTTER NUMBER1414 - TOTAL Q VS DIVERTED Q IN CFS											

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		.0	.0	500.0	1.0	999.0	125.0	1886.0	841.0	2765.0	1456.0	3403.0	1937.0
1509	1800	4421.0	2668.0	7425.0	5187.0	13357.0	10368.0	.0010	.0	.0	.001	10.00	0
1490	1491	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1455	1456	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1938	1480	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1480	1481	0	4	CHANNEL		5.0	2400.	.0500	2.0	2.0	.040	2.00	0
				OVERFLOW		20.0	2400.	.0500	10.0	10.0	.045	10.00	0
1481	1482	7	2	PIPE		.0	1.	.0010	.0	.0	.030	.10	0
RESERVOIR STORAGE IN ACRE-FEET VS SPILLWAY OUTFLOW													
		.0	.0	308.0	18.0	624.0	76.0	947.0	179.0	1279.0	318.0	1618.0	1676.0
		1965.0	4700.0										
1482	1456	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1456	1457	0	1	CHANNEL		2.0	4450.	.0363	80.0	80.0	.030	20.00	0
1457	1491	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1491	1931	0	4	CHANNEL		5.0	10236.	.0090	4.0	4.0	.050	2.00	0
				OVERFLOW		25.0	10236.	.0090	60.0	60.0	.065	15.00	0
1460	1461	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1461	1931	0	4	CHANNEL		3.0	2286.	.0280	4.0	4.0	.050	2.00	0
				OVERFLOW		20.0	2286.	.0280	24.0	24.0	.055	15.00	0
1931	1933	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1933	1467	0	4	CHANNEL		5.0	403.	.0099	2.0	2.0	.020	2.00	0
				OVERFLOW		25.0	403.	.0099	10.0	10.0	.025	15.00	0
1465	1932	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1932	1467	0	4	CHANNEL		4.0	1591.	.0289	8.0	8.0	.035	.50	0
				OVERFLOW		25.0	1591.	.0289	4.0	4.0	.035	15.00	0
1467	1468	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1468	1800	0	4	CHANNEL		5.0	2357.	.0180	2.0	2.0	.020	2.00	0
				OVERFLOW		25.0	2357.	.0180	10.0	10.0	.025	15.00	0
1800	1506	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1506	1507	0	4	CHANNEL		33.0	8099.	.0054	4.0	4.0	.060	2.50	0
				OVERFLOW		800.0	8099.	.0054	10.0	10.0	.065	15.00	0
1508	1507	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1507	1512	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1512	44	0	4	CHANNEL		33.0	1367.	.0064	4.0	4.0	.060	2.50	0
				OVERFLOW		308.0	1367.	.0064	80.0	80.0	.065	15.00	0
1500	1501	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1501	44	0	4	CHANNEL		5.0	8609.	.0212	2.0	2.0	.040	2.00	0
				OVERFLOW		20.0	8609.	.0212	10.0	10.0	.045	15.00	0
44	261	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
261	1427	9	3			.0	1.	.0010	.0	.0	.001	10.00	1262
DIVERSION TO GUTTER NUMBER1262 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	500.0	1.0	875.0	35.0	1920.0	315.0	2709.0	660.0	3916.0	1323.0
		5586.0	2377.0	9768.0	5344.0	18394.0	11928.0						
1427	243	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
243	242	0	4	CHANNEL		65.0	2991.	.0112	2.0	2.0	.043	2.50	0
				OVERFLOW		650.0	2991.	.0112	100.0	100.0	.055	15.00	0
242	241	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
241	240	0	4	CHANNEL		65.0	5732.	.0100	2.0	2.0	.043	3.00	0
				OVERFLOW		1200.0	5732.	.0100	200.0	200.0	.055	20.00	0
240	238	0	4	CHANNEL		65.0	2861.	.0100	2.0	2.0	.050	3.00	0
				OVERFLOW		1200.0	2861.	.0100	200.0	200.0	.075	20.00	0
238	237	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
237	251	5	3			.0	1.	.0010	.0	.0	.001	10.00	389
DIVERSION TO GUTTER NUMBER389 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	2060.0	1.0	4980.0	2580.0	6630.0	3530.0	11150.0	7500.0		
		389	1906	0	3	.0	1.	.0010	.0	.0	.001	10.00	0
1906	1909	0	4	CHANNEL		10.0	3340.	.0042	8.0	8.0	.025	.50	0
				OVERFLOW		1200.0	3340.	.0042	80.0	80.0	.025	15.00	0
251	233	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
235	239	0	1	CHANNEL		1.0	3509.	.0050	50.0	50.0	.020	10.00	0
239	234	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
234	232	0	4	CHANNEL		2.0	2072.	.0044	3.0	3.0	.050	2.00	0
				OVERFLOW		50.0	2072.	.0044	50.0	50.0	.035	10.00	0
233	232	0	4	CHANNEL		65.0	3076.	.0100	2.0	2.0	.050	4.00	0
				OVERFLOW		600.0	3076.	.0100	200.0	200.0	.080	20.00	0
232	236	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
236	252	5	3			.0	1.	.0010	.0	.0	.001	10.00	1403
DIVERSION TO GUTTER NUMBER1403 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	2060.0	1.0	2400.0	100.0	3100.0	500.0	10000.0	2500.0		
1403	1599	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
252	231	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1357	357	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
357	1401	6	3			.0	1.	.0010	.0	.0	.001	10.00	1325
DIVERSION TO GUTTER NUMBER1325 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	26.0	.1	263.0	235.0	391.0	361.0	995.0	960.0	5000.0	4950.0
1401	1387	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1387	387	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
387	1908	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1908	1320	0	4	CHANNEL		2.0	1718.	.0076	3.0	3.0	.025	2.00	0
				OVERFLOW		600.0	1718.	.0076	80.0	80.0	.025	10.00	0
266	376	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
376	375	0	1	CHANNEL		4.0	1569.	.0041	4.0	4.0	.050	10.00	0
375	1374	4	3			.0	1.	.0010	.0	.0	.001	10.00	1404
DIVERSION TO GUTTER NUMBER1404 - TOTAL Q VS DIVERTED Q IN CFS													
		.0	.0	24.0	.1	135.0	100.0	540.0	500.0				
1374	374	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
374	372	0	4	CHANNEL		4.0	2538.	.0115	3.0	3.0	.045	2.00	0
				OVERFLOW		20.0	2538.	.0115	20.0	20.0	.035	10.00	0
373	372	0	4	CHANNEL		3.0	1779.	.0075	4.0	4.0	.045	1.00	0
				OVERFLOW		20.0	1779.	.0075	20.0	20.0	.035	10.00	0
1367	367	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
367	372	0	4	CHANNEL		.5	2663.	.0103	12.0	12.0	.016	.50	0
				OVERFLOW		10.0	2663.	.0103	20.0	20.0	.020	10.00	0
372	371	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
371	311	0	4	CHANNEL		10.0	2893.	.0078	2.0	2.0	.045	1.00	0
				OVERFLOW		10.0	2893.	.0078	50.0	50.0	.035	10.00	0
1339	1822	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
1348	348	0	3			.0	1.	.0010	.0	.0	.001	10.00	0
348	1937	5	3			.0	1.	.0010	.0	.0	.001	10.00	1331
DIVERSION TO GUTTER NUMBER1331 - TOTAL Q VS DIVERTED Q IN CFS													

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		.0	.0	40.0	.1	314.0	77.0	1075.0	357.0	2228.0	783.0	4144.0	1719.0	
1814	351	6379.0	2711.0											
351	1913	0	3											
				PIPE		2.0	2056.	.0117	.0	.0	.001	10.00	0	
				OVERFLOW		40.0	2056.	.0117	8.0	8.0	.035	15.00	0	
1815	1816	0	3											
1818	1817	0	4	CHANNEL		2.0	354.	.0100	4.0	4.0	.020	1.00	0	
				OVERFLOW		12.0	354.	.0100	10.0	10.0	.030	10.00	0	
1816	1817	0	4	CHANNEL		6.0	837.	.0037	12.0	12.0	.015	1.00	0	
				OVERFLOW		30.0	837.	.0037	8.0	3.0	.030	15.00	0	
1817	354	0	3											
354	1913	0	5	PIPE		1.5	1345.	.2800	.0	.0	.015	1.50	0	
				OVERFLOW		24.0	1345.	.2800	20.0	5.0	.035	15.00	0	
1913	1914	0	3											
1914	1915	0	5	PIPE		2.0	756.	.0066	.0	.0	.016	2.00	0	
				OVERFLOW		1.0	756.	.0066	20.0	20.0	.020	15.00	0	
1915	347	0	3											
347	359	0	5	PIPE		4.0	2229.	.0173	.0	.0	.015	4.00	0	
				OVERFLOW		10.0	2229.	.0173	20.0	20.0	.020	20.00	0	
349	359	0	1	CHANNEL		10.0	2788.	.0217	20.0	20.0	.035	10.00	0	
355	359	0	5	PIPE		2.0	3762.	.0121	.0	.0	.020	2.00	0	
				OVERFLOW		1.0	3762.	.0121	5.0	20.0	.020	10.00	0	
359	356	0	3											
356	1343	10	2	PIPE		.1	1.	.0010	.0	.0	.030	10.00	0	
				RESERVOIR STORAGE IN ACRE- FEET VS SPILLWAY OUTFLOW										
		.0	.0	.3	14.0	3.4	138.0	5.3	200.0	6.6	210.0	7.7	230.0	
		9.7	332.0	14.5	1712.0	18.2	2617.0	23.4	5064.0					
1343	343	0	3											
343	1342	7	3											
				DIVERSION TO GUTTER NUMBER1362 - TOTAL Q VS DIVERTED Q IN CFS										
		.0	.0	230.0	229.0	332.0	260.0	1712.0	360.0	2617.0	510.0	5064.0	893.0	
		9890.0	1680.0											
1342	342	0	3											
342	1335	6	3											
				DIVERSION TO GUTTER NUMBER1341 - TOTAL Q VS DIVERTED Q IN CFS										
		.0	.0	72.0	71.0	1352.0	1120.0	2107.0	1616.0	4171.0	2776.0	8280.0	5110.0	
1341	341	0	3											
1335	335	0	3											
335	1301	0	1	CHANNEL		10.0	3343.	.0047	18.0	5.0	.045	20.00	0	
1301	1302	0	3											
1302	1303	4	3											
				DIVERSION TO GUTTER NUMBER1304 - TOTAL Q VS DIVERTED Q IN CFS										
		.0	.0	585.0	1.0	1973.0	1149.0	3964.0	2984.0					
1303	330	0	3											
1304	1305	0	3											
1305	1599	0	3											
330	329	0	3											
329	328	0	1	CHANNEL		8.0	1804.	.0012	3.5	3.5	.024	20.00	0	
1309	1311	6	3											
				DIVERSION TO GUTTER NUMBER1312 - TOTAL Q VS DIVERTED Q IN CFS										
		.0	.0	725.2	.1	824.2	.2	981.0	51.0	3918.0	1261.0	6125.0	2048.0	
1311	327	0	3											
368	1330	0	3											
1312	1330	0	3											
1330	1332	0	5	PIPE		1.5	3079.	.0078	10.0	10.0	.025	1.50	0	
				OVERFLOW		28.0	3079.	.0078	5.0	5.0	.040	5.00	0	
1332	1368	0	3											
1368	1369	3	3											
				DIVERSION TO GUTTER NUMBER1371 - TOTAL Q VS DIVERTED Q IN CFS										
		.0	.0	245.0	.1	3280.0	418.6							
1369	1370	0	3											
1370	1365	0	5	PIPE		1.5	1286.	.0030	.0	.0	.025	1.50	0	
				OVERFLOW		30.0	1286.	.0030	10.0	10.0	.025	15.00	0	
1371	1372	0	3											
1372	1599	0	3											
328	1309	0	3											
327	326	0	4	CHANNEL		8.0	1305.	.0008	3.5	3.5	.024	4.00	0	
				OVERFLOW		40.0	1305.	.0008	5.7	7.5	.028	20.00	0	
1409	310	0	3											
1336	336	0	3											
336	1310	4	3											
				DIVERSION TO GUTTER NUMBER1942 - TOTAL Q VS DIVERTED Q IN CFS										
		.0	.0	20.0	10.0	200.0	100.0	2000.0	1000.0					
1942	1940	0	3											
1310	310	0	3											
310	315	0	3											
315	317	0	4	CHANNEL		.5	3664.	.0088	12.0	12.0	.016	.50	0	
				OVERFLOW		10.0	3664.	.0088	20.0	20.0	.020	10.00	0	
316	317	0	4	CHANNEL		.5	2903.	.0079	12.0	12.0	.016	.50	0	
				OVERFLOW		10.0	2903.	.0079	20.0	20.0	.020	10.00	0	
317	326	0	3											
326	325	0	4	CHANNEL		8.0	458.	.0008	3.5	3.5	.024	4.00	0	
				OVERFLOW		40.0	458.	.0008	5.7	7.5	.028	20.00	0	
325	324	0	3											
324	1392	7	3											
				DIVERSION TO GUTTER NUMBER1402 - TOTAL Q VS DIVERTED Q IN CFS										
		.0	.0	725.1	.1	824.0	98.0	930.0	180.0	2657.0	1833.0	4077.0	3077.0	
		10000.0	8800.0											
1402	1323	0	3											
1323	323	0	3											
323	1321	7	3											
				DIVERSION TO GUTTER NUMBER1387 - TOTAL Q VS DIVERTED Q IN CFS										
		.0	.0	50.0	49.9	254.0	60.0	1565.0	100.0	2841.0	150.0	4250.0	200.0	
		8800.0	400.0											
1392	392	0	3											
392	391	0	3											
391	1911	0	4	CHANNEL		15.0	1048.	.0012	3.5	3.5	.045	5.00	0	
				OVERFLOW		55.0	1048.	.0012	4.0	7.5	.055	20.00	0	
338	318	0	4	CHANNEL		1.0	2263.	.0089	1.0	1.0	.045	1.00	0	
				OVERFLOW		10.0	2263.	.0089	50.0	50.0	.035	10.00	0	
318	1911	0	4	CHANNEL		8.0	2821.	.0012	3.0	3.0	.045	1.50	0	

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20	0	0	0	0	0	0	0	0	0	0	19	0	0	0	0	0	0	0	0	0	606.0
21	0	0	0	0	0	0	0	0	0	0	20	0	0	0	0	0	0	0	0	0	379.0
22	23	24	0	0	0	0	0	0	0	0	21	0	0	0	0	0	0	0	0	0	4784.0
23	37	34	31	0	0	0	0	0	0	0	22	0	0	0	0	0	0	0	0	0	2671.0
24	25	26	0	0	0	0	0	0	0	0	23	0	0	0	0	0	0	0	0	0	1666.0
25	0	0	0	0	0	0	0	0	0	0	24	0	0	0	0	0	0	0	0	0	363.0
26	27	28	0	0	0	0	0	0	0	0	25	0	0	0	0	0	0	0	0	0	1199.0
27	0	0	0	0	0	0	0	0	0	0	26	0	0	0	0	0	0	0	0	0	107.0
28	29	30	0	0	0	0	0	0	0	0	27	0	0	0	0	0	0	0	0	0	998.0
29	0	0	0	0	0	0	0	0	0	0	28	0	0	0	0	0	0	0	0	0	152.0
30	0	0	0	0	0	0	0	0	0	0	29	0	0	0	0	0	0	0	0	0	546.0
31	32	33	0	0	0	0	0	0	0	0	30	0	0	0	0	0	0	0	0	0	508.0
32	0	0	0	0	0	0	0	0	0	0	31	0	0	0	0	0	0	0	0	0	144.0
33	0	0	0	0	0	0	0	0	0	0	32	0	0	0	0	0	0	0	0	0	257.0
34	35	36	0	0	0	0	0	0	0	0	33	0	0	0	0	0	0	0	0	0	844.0
35	0	0	0	0	0	0	0	0	0	0	34	0	0	0	0	0	0	0	0	0	148.0
36	0	0	0	0	0	0	0	0	0	0	35	0	0	0	0	0	0	0	0	0	251.0
37	38	39	0	0	0	0	0	0	0	0	36	0	0	0	0	0	0	0	0	0	1124.0
38	0	0	0	0	0	0	0	0	0	0	37	0	0	0	0	0	0	0	0	0	368.0
39	0	0	0	0	0	0	0	0	0	0	38	0	0	0	0	0	0	0	0	0	290.0
40	41	42	0	0	0	0	0	0	0	0	39	0	0	0	0	0	0	0	0	0	51645.0
41	0	0	0	0	0	0	0	0	0	0	40	0	0	0	0	0	0	0	0	0	205.0
42	46	62	68	0	0	0	0	0	0	0	41	0	0	0	0	0	0	0	0	0	51084.0
44	1512	1501	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30179.0
46	59	60	0	0	0	0	0	0	0	0	42	0	0	0	0	0	0	0	0	0	17929.0
48	50	49	0	0	0	0	0	0	0	0	69	0	0	0	0	0	0	0	0	0	12077.0
49	0	0	0	0	0	0	0	0	0	0	72	0	0	0	0	0	0	0	0	0	220.0
50	51	52	56	0	0	0	0	0	0	0	71	0	0	0	0	0	0	0	0	0	71466.0
51	0	0	0	0	0	0	0	0	0	0	82	0	0	0	0	0	0	0	0	0	362.0
52	244	245	53	0	0	0	0	0	0	0	73	0	0	0	0	0	0	0	0	0	69055.0
53	54	55	0	0	0	0	0	0	0	0	75	0	0	0	0	0	0	0	0	0	536.0
54	0	0	0	0	0	0	0	0	0	0	76	0	0	0	0	0	0	0	0	0	213.0
55	0	0	0	0	0	0	0	0	0	0	77	0	0	0	0	0	0	0	0	0	297.0
56	57	58	0	0	0	0	0	0	0	0	78	79	0	0	0	0	0	0	0	0	1842.0
57	0	0	0	0	0	0	0	0	0	0	81	0	0	0	0	0	0	0	0	0	776.0
58	0	0	0	0	0	0	0	0	0	0	80	0	0	0	0	0	0	0	0	0	220.0
59	74	71	0	0	0	0	0	0	0	0	43	0	0	0	0	0	0	0	0	0	47507.0
60	0	0	0	0	0	0	0	0	0	0	44	0	0	0	0	0	0	0	0	0	225.0
61	63	64	0	0	0	0	0	0	0	0	45	0	0	0	0	0	0	0	0	0	1044.0
62	61	65	0	0	0	0	0	0	0	0	46	0	0	0	0	0	0	0	0	0	2039.0
63	0	0	0	0	0	0	0	0	0	0	47	0	0	0	0	0	0	0	0	0	234.0
64	0	0	0	0	0	0	0	0	0	0	48	0	0	0	0	0	0	0	0	0	258.0
65	66	67	0	0	0	0	0	0	0	0	49	0	0	0	0	0	0	0	0	0	956.0
66	0	0	0	0	0	0	0	0	0	0	50	0	0	0	0	0	0	0	0	0	108.0
67	0	0	0	0	0	0	0	0	0	0	51	0	0	0	0	0	0	0	0	0	636.0
68	69	70	0	0	0	0	0	0	0	0	52	0	0	0	0	0	0	0	0	0	523.0
69	0	0	0	0	0	0	0	0	0	0	53	0	0	0	0	0	0	0	0	0	197.0
70	0	0	0	0	0	0	0	0	0	0	54	0	0	0	0	0	0	0	0	0	246.0
71	72	73	0	0	0	0	0	0	0	0	55	0	0	0	0	0	0	0	0	0	1094.0
72	0	0	0	0	0	0	0	0	0	0	56	0	0	0	0	0	0	0	0	0	197.0
73	0	0	0	0	0	0	0	0	0	0	57	0	0	0	0	0	0	0	0	0	636.0

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74	77	76	94	0	0	0	0	0	0	0	58	0	0	0	0	0	0	0	0	46117.0
75	79	78	0	0	0	0	0	0	0	0	61	0	0	0	0	0	0	0	0	3945.0
76	0	0	0	0	0	0	0	0	0	0	63	0	0	0	0	0	0	0	0	379.0
77	75	88	0	0	0	0	0	0	0	0	65	0	0	0	0	0	0	0	0	4793.0
78	0	0	0	0	0	0	0	0	0	0	66	0	0	0	0	0	0	0	0	256.0
79	80	121	0	0	0	0	0	0	0	0	70	0	0	0	0	0	0	0	0	3627.0
80	82	81	0	0	0	0	0	0	0	0	83	0	0	0	0	0	0	0	0	2668.0
81	87	0	0	0	0	0	0	0	0	0	84	0	0	0	0	0	0	0	0	958.0
82	84	83	0	0	0	0	0	0	0	0	85	0	0	0	0	0	0	0	0	848.0
83	0	0	0	0	0	0	0	0	0	0	86	0	0	0	0	0	0	0	0	197.0
84	85	86	0	0	0	0	0	0	0	0	87	0	0	0	0	0	0	0	0	555.0
85	0	0	0	0	0	0	0	0	0	0	88	0	0	0	0	0	0	0	0	118.0
86	0	0	0	0	0	0	0	0	0	0	89	0	0	0	0	0	0	0	0	331.0
87	0	0	0	0	0	0	0	0	0	0	90	0	0	0	0	0	0	0	0	655.0
88	89	93	0	0	0	0	0	0	0	0	91	0	0	0	0	0	0	0	0	782.0
89	0	0	0	0	0	0	0	0	0	0	228	0	0	0	0	0	0	0	0	319.0
93	0	0	0	0	0	0	0	0	0	0	229	0	0	0	0	0	0	0	0	111.0
94	95	97	0	0	0	0	0	0	0	0	92	0	0	0	0	0	0	0	0	40534.0
95	96	116	0	0	0	0	0	0	0	0	230	0	0	0	0	0	0	0	0	34430.0
96	129	122	0	0	0	0	0	0	0	0	93	0	0	0	0	0	0	0	0	33528.0
97	99	98	0	0	0	0	0	0	0	0	94	0	0	0	0	0	0	0	0	5629.0
98	0	0	0	0	0	0	0	0	0	0	95	0	0	0	0	0	0	0	0	309.0
99	101	100	0	0	0	0	0	0	0	0	96	0	0	0	0	0	0	0	0	4848.0
100	0	0	0	0	0	0	0	0	0	0	97	0	0	0	0	0	0	0	0	458.0
101	102	107	0	0	0	0	0	0	0	0	98	0	0	0	0	0	0	0	0	4335.0
102	106	103	0	0	0	0	0	0	0	0	99	0	0	0	0	0	0	0	0	2382.0
103	104	105	0	0	0	0	0	0	0	0	100	0	0	0	0	0	0	0	0	1795.0
104	119	117	0	0	0	0	0	0	0	0	101	0	0	0	0	0	0	0	0	1302.0
105	0	0	0	0	0	0	0	0	0	0	102	0	0	0	0	0	0	0	0	343.0
106	0	0	0	0	0	0	0	0	0	0	103	0	0	0	0	0	0	0	0	273.0
107	108	109	0	0	0	0	0	0	0	0	104	0	0	0	0	0	0	0	0	1871.0
108	0	0	0	0	0	0	0	0	0	0	105	0	0	0	0	0	0	0	0	202.0
109	110	111	0	0	0	0	0	0	0	0	106	0	0	0	0	0	0	0	0	1563.0
110	112	113	0	0	0	0	0	0	0	0	107	0	0	0	0	0	0	0	0	1148.0
111	0	0	0	0	0	0	0	0	0	0	108	0	0	0	0	0	0	0	0	199.0
112	114	115	0	0	0	0	0	0	0	0	109	0	0	0	0	0	0	0	0	540.0
113	0	0	0	0	0	0	0	0	0	0	110	0	0	0	0	0	0	0	0	209.0
114	0	0	0	0	0	0	0	0	0	0	111	0	0	0	0	0	0	0	0	230.0
115	0	0	0	0	0	0	0	0	0	0	112	0	0	0	0	0	0	0	0	102.0
116	0	0	0	0	0	0	0	0	0	0	113	0	0	0	0	0	0	0	0	702.0
117	0	0	0	0	0	0	0	0	0	0	114	0	0	0	0	0	0	0	0	390.0
118	0	0	0	0	0	0	0	0	0	0	115	0	0	0	0	0	0	0	0	453.0
119	120	118	0	0	0	0	0	0	0	0	116	0	0	0	0	0	0	0	0	707.0
120	0	0	0	0	0	0	0	0	0	0	117	0	0	0	0	0	0	0	0	220.0
121	0	0	0	0	0	0	0	0	0	0	74	0	0	0	0	0	0	0	0	326.0
122	124	123	0	0	0	0	0	0	0	0	118	0	0	0	0	0	0	0	0	2595.0
123	127	128	0	0	0	0	0	0	0	0	119	0	0	0	0	0	0	0	0	1409.0
124	125	126	0	0	0	0	0	0	0	0	120	0	0	0	0	0	0	0	0	705.0
125	0	0	0	0	0	0	0	0	0	0	124	0	0	0	0	0	0	0	0	220.0
126	0	0	0	0	0	0	0	0	0	0	125	0	0	0	0	0	0	0	0	88.0
127	0	0	0	0	0	0	0	0	0	0	126	0	0	0	0	0	0	0	0	548.0

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128	0	0	0	0	0	0	0	0	0	0	127	0	0	0	0	0	0	0	0	0	0	472.0
129	137	130	0	0	0	0	0	0	0	0	128	0	0	0	0	0	0	0	0	0	0	30354.0
130	133	131	132	0	0	0	0	0	0	0	129	0	0	0	0	0	0	0	0	0	0	2081.0
131	0	0	0	0	0	0	0	0	0	0	130	0	0	0	0	0	0	0	0	0	0	290.0
132	0	0	0	0	0	0	0	0	0	0	131	0	0	0	0	0	0	0	0	0	0	213.0
133	134	0	0	0	0	0	0	0	0	0	132	0	0	0	0	0	0	0	0	0	0	1468.0
134	135	136	0	0	0	0	0	0	0	0	133	0	0	0	0	0	0	0	0	0	0	972.0
135	0	0	0	0	0	0	0	0	0	0	134	0	0	0	0	0	0	0	0	0	0	160.0
136	0	0	0	0	0	0	0	0	0	0	135	0	0	0	0	0	0	0	0	0	0	282.0
137	138	139	0	0	0	0	0	0	0	0	136	0	0	0	0	0	0	0	0	0	0	28122.0
138	0	0	0	0	0	0	0	0	0	0	137	0	0	0	0	0	0	0	0	0	0	383.0
139	149	140	0	0	0	0	0	0	0	0	138	0	0	0	0	0	0	0	0	0	0	27597.0
140	142	141	0	0	0	0	0	0	0	0	139	0	0	0	0	0	0	0	0	0	0	2013.0
141	0	0	0	0	0	0	0	0	0	0	140	0	0	0	0	0	0	0	0	0	0	132.0
142	146	143	0	0	0	0	0	0	0	0	141	0	0	0	0	0	0	0	0	0	0	1697.0
143	144	145	0	0	0	0	0	0	0	0	142	0	0	0	0	0	0	0	0	0	0	540.0
144	0	0	0	0	0	0	0	0	0	0	143	0	0	0	0	0	0	0	0	0	0	274.0
145	0	0	0	0	0	0	0	0	0	0	144	0	0	0	0	0	0	0	0	0	0	79.0
146	147	148	0	0	0	0	0	0	0	0	145	0	0	0	0	0	0	0	0	0	0	1054.0
147	0	0	0	0	0	0	0	0	0	0	146	0	0	0	0	0	0	0	0	0	0	283.0
148	0	0	0	0	0	0	0	0	0	0	147	0	0	0	0	0	0	0	0	0	0	453.0
149	152	150	151	0	0	0	0	0	0	0	148	0	0	0	0	0	0	0	0	0	0	25514.0
150	0	0	0	0	0	0	0	0	0	0	149	0	0	0	0	0	0	0	0	0	0	58.0
151	0	0	0	0	0	0	0	0	0	0	150	0	0	0	0	0	0	0	0	0	0	189.0
152	153	154	0	0	0	0	0	0	0	0	151	0	0	0	0	0	0	0	0	0	0	25053.0
153	0	0	0	0	0	0	0	0	0	0	152	0	0	0	0	0	0	0	0	0	0	249.0
154	156	155	0	0	0	0	0	0	0	0	153	0	0	0	0	0	0	0	0	0	0	24303.0
155	0	0	0	0	0	0	0	0	0	0	154	0	0	0	0	0	0	0	0	0	0	161.0
156	157	158	0	0	0	0	0	0	0	0	155	0	0	0	0	0	0	0	0	0	0	23893.0
157	172	163	170	171	0	0	0	0	0	0	156	0	0	0	0	0	0	0	0	0	0	21505.0
158	160	159	0	0	0	0	0	0	0	0	157	0	0	0	0	0	0	0	0	0	0	1865.0
159	0	0	0	0	0	0	0	0	0	0	158	0	0	0	0	0	0	0	0	0	0	476.0
160	161	162	0	0	0	0	0	0	0	0	159	0	0	0	0	0	0	0	0	0	0	1045.0
161	0	0	0	0	0	0	0	0	0	0	160	0	0	0	0	0	0	0	0	0	0	341.0
162	0	0	0	0	0	0	0	0	0	0	161	0	0	0	0	0	0	0	0	0	0	362.0
163	166	164	0	0	0	0	0	0	0	0	162	0	0	0	0	0	0	0	0	0	0	1286.0
164	0	0	0	0	0	0	0	0	0	0	163	0	0	0	0	0	0	0	0	0	0	76.0
165	168	169	0	0	0	0	0	0	0	0	164	0	0	0	0	0	0	0	0	0	0	784.0
166	165	167	0	0	0	0	0	0	0	0	165	0	0	0	0	0	0	0	0	0	0	1098.0
167	0	0	0	0	0	0	0	0	0	0	166	0	0	0	0	0	0	0	0	0	0	215.0
168	0	0	0	0	0	0	0	0	0	0	167	0	0	0	0	0	0	0	0	0	0	259.0
169	0	0	0	0	0	0	0	0	0	0	168	0	0	0	0	0	0	0	0	0	0	175.0
170	0	0	0	0	0	0	0	0	0	0	169	0	0	0	0	0	0	0	0	0	0	332.0
171	0	0	0	0	0	0	0	0	0	0	170	0	0	0	0	0	0	0	0	0	0	139.0
172	187	173	0	0	0	0	0	0	0	0	171	0	0	0	0	0	0	0	0	0	0	19645.0
173	174	175	0	0	0	0	0	0	0	0	172	0	0	0	0	0	0	0	0	0	0	5003.0
174	0	0	0	0	0	0	0	0	0	0	173	0	0	0	0	0	0	0	0	0	0	188.0
175	177	176	0	0	0	0	0	0	0	0	174	0	0	0	0	0	0	0	0	0	0	4585.0
176	180	179	0	0	0	0	0	0	0	0	175	0	0	0	0	0	0	0	0	0	0	3882.0
177	178	0	0	0	0	0	0	0	0	0	176	0	0	0	0	0	0	0	0	0	0	625.0
178	0	0	0	0	0	0	0	0	0	0	177	0	0	0	0	0	0	0	0	0	0	392.0

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179	0	0	0	0	0	0	0	0	0	0	178	0	0	0	0	0	0	0	0	211.0
180	181	182	0	0	0	0	0	0	0	0	179	0	0	0	0	0	0	0	0	2955.0
181	0	0	0	0	0	0	0	0	0	0	180	0	0	0	0	0	0	0	0	438.0
182	183	184	0	0	0	0	0	0	0	0	181	0	0	0	0	0	0	0	0	2016.0
183	0	0	0	0	0	0	0	0	0	0	182	0	0	0	0	0	0	0	0	599.0
184	186	185	0	0	0	0	0	0	0	0	183	0	0	0	0	0	0	0	0	910.0
185	0	0	0	0	0	0	0	0	0	0	184	0	0	0	0	0	0	0	0	232.0
186	0	0	0	0	0	0	0	0	0	0	185	0	0	0	0	0	0	0	0	461.0
187	192	193	0	0	0	0	0	0	0	0	186	0	0	0	0	0	0	0	0	14569.0
192	194	205	0	0	0	0	0	0	0	0	187	0	0	0	0	0	0	0	0	13278.0
193	0	0	0	0	0	0	0	0	0	0	188	0	0	0	0	0	0	0	0	273.0
194	198	199	196	195	0	0	0	0	0	0	189	0	0	0	0	0	0	0	0	5663.0
195	0	0	0	0	0	0	0	0	0	0	190	0	0	0	0	0	0	0	0	251.0
196	0	0	0	0	0	0	0	0	0	0	195	0	0	0	0	0	0	0	0	387.0
198	201	200	202	0	0	0	0	0	0	0	196	0	0	0	0	0	0	0	0	3544.0
199	0	0	0	0	0	0	0	0	0	0	197	0	0	0	0	0	0	0	0	634.0
200	0	0	0	0	0	0	0	0	0	0	198	0	0	0	0	0	0	0	0	542.0
201	204	203	0	0	0	0	0	0	0	0	199	0	0	0	0	0	0	0	0	1955.0
202	0	0	0	0	0	0	0	0	0	0	200	0	0	0	0	0	0	0	0	250.0
203	0	0	0	0	0	0	0	0	0	0	203	0	0	0	0	0	0	0	0	258.0
204	0	0	0	0	0	0	0	0	0	0	204	0	0	0	0	0	0	0	0	854.0
205	207	206	0	0	0	0	0	0	0	0	205	0	0	0	0	0	0	0	0	7500.0
206	0	0	0	0	0	0	0	0	0	0	206	0	0	0	0	0	0	0	0	250.0
207	211	208	0	0	0	0	0	0	0	0	207	0	0	0	0	0	0	0	0	6855.0
208	0	0	0	0	0	0	0	0	0	0	208	0	0	0	0	0	0	0	0	275.0
211	212	215	0	0	0	0	0	0	0	0	209	0	0	0	0	0	0	0	0	5808.0
212	214	213	0	0	0	0	0	0	0	0	210	0	0	0	0	0	0	0	0	1581.0
213	0	0	0	0	0	0	0	0	0	0	211	0	0	0	0	0	0	0	0	511.0
214	0	0	0	0	0	0	0	0	0	0	212	0	0	0	0	0	0	0	0	482.0
215	219	216	217	0	0	0	0	0	0	0	213	0	0	0	0	0	0	0	0	3943.0
216	0	0	0	0	0	0	0	0	0	0	214	0	0	0	0	0	0	0	0	505.0
217	0	0	0	0	0	0	0	0	0	0	215	0	0	0	0	0	0	0	0	245.0
218	222	221	0	0	0	0	0	0	0	0	219	0	0	0	0	0	0	0	0	1711.0
219	220	218	0	0	0	0	0	0	0	0	220	0	0	0	0	0	0	0	0	2654.0
220	0	0	0	0	0	0	0	0	0	0	221	0	0	0	0	0	0	0	0	506.0
221	0	0	0	0	0	0	0	0	0	0	222	0	0	0	0	0	0	0	0	250.0
222	224	223	0	0	0	0	0	0	0	0	223	0	0	0	0	0	0	0	0	1417.0
223	0	0	0	0	0	0	0	0	0	0	224	0	0	0	0	0	0	0	0	309.0
224	226	225	0	0	0	0	0	0	0	0	225	0	0	0	0	0	0	0	0	926.0
225	0	0	0	0	0	0	0	0	0	0	226	0	0	0	0	0	0	0	0	152.0
226	0	0	0	0	0	0	0	0	0	0	227	0	0	0	0	0	0	0	0	286.0
231	252	0	0	0	0	0	0	0	0	0	231	0	0	0	0	0	0	0	0	86054.0
232	234	233	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
233	251	0	0	0	0	0	0	0	0	0	233	0	0	0	0	0	0	0	0	85477.0
234	239	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	187.0
235	0	0	0	0	0	0	0	0	0	0	235	0	0	0	0	0	0	0	0	187.0
236	232	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85664.0
237	238	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
238	1927	240	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	85196.0
239	235	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	187.0
240	241	0	0	0	0	0	0	0	0	0	240	0	0	0	0	0	0	0	0	84397.0

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241	242	0	0	0	0	0	0	0	0	0	241	0	0	0	0	0	0	0	0	84351.0
242	377	289	243	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	84008.0
243	1427	0	0	0	0	0	0	0	0	0	243	0	0	0	0	0	0	0	0	80261.0
244	0	0	0	0	0	0	0	0	0	0	253	0	0	0	0	0	0	0	0	848.0
245	1	246	0	0	0	0	0	0	0	0	254	0	0	0	0	0	0	0	0	67230.0
246	247	250	0	0	0	0	0	0	0	0	255	0	0	0	0	0	0	0	0	2389.0
247	0	0	0	0	0	0	0	0	0	0	256	0	0	0	0	0	0	0	0	808.0
248	0	0	0	0	0	0	0	0	0	0	257	0	0	0	0	0	0	0	0	645.0
249	0	0	0	0	0	0	0	0	0	0	258	0	0	0	0	0	0	0	0	377.0
250	248	249	0	0	0	0	0	0	0	0	259	0	0	0	0	0	0	0	0	1131.0
251	237	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	35196.0
252	236	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	35664.0
261	44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30179.0
262	1935	0	0	0	0	0	0	0	0	0	262	0	0	0	0	0	0	0	0	2758.0
263	262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2758.0
264	1905	0	0	0	0	0	0	0	0	0	264	0	0	0	0	0	0	0	0	2784.0
265	264	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
266	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
267	293	1267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
268	267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
269	265	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
270	271	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86842.0
271	319	231	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86842.0
280	294	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
289	1924	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3653.0
290	1290	0	0	0	0	0	0	0	0	0	290	0	0	0	0	0	0	0	0	3653.0
291	1291	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
292	1923	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
293	1293	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
294	1294	304	1920	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
295	1295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
296	1296	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
297	298	0	0	0	0	0	0	0	0	0	297	0	0	0	0	0	0	0	0	587.0
298	303	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	249.0
299	0	0	0	0	0	0	0	0	0	0	299	0	0	0	0	0	0	0	0	72.0
300	301	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	177.0
301	0	0	0	0	0	0	0	0	0	0	301	0	0	0	0	0	0	0	0	177.0
303	299	1922	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	249.0
304	0	0	0	0	0	0	0	0	0	0	304	0	0	0	0	0	0	0	0	150.0
308	396	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
310	1409	1310	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
311	371	312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	247.0
312	1940	0	0	0	0	0	0	0	0	0	312	0	0	0	0	0	0	0	0	100.0
313	1939	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
314	308	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
315	310	0	0	0	0	0	0	0	0	0	315	0	0	0	0	0	0	0	0	28.0
316	0	0	0	0	0	0	0	0	0	0	316	0	0	0	0	0	0	0	0	43.0
317	315	316	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	71.0
318	338	0	0	0	0	0	0	0	0	0	318	0	0	0	0	0	0	0	0	230.0
319	1946	0	0	0	0	0	0	0	0	0	319	0	0	0	0	0	0	0	0	788.0
320	1320	0	0	0	0	0	0	0	0	0	320	0	0	0	0	0	0	0	0	454.0

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321	1321	0	0	0	0	0	0	0	0	0	321	0	0	0	0	0	0	0	0	0	34.0
322	1909	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
323	1323	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9.0
324	325	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
325	1325	326	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
326	327	317	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
327	1311	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
328	337	1329	329	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
329	330	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
330	1306	1303	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
331	1331	1407	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
332	333	334	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
333	1333	0	0	0	0	0	0	0	0	0	333	0	0	0	0	0	0	0	0	0	5.0
334	1334	0	0	0	0	0	0	0	0	0	334	0	0	0	0	0	0	0	0	0	5.0
335	1335	0	0	0	0	0	0	0	0	0	335	0	0	0	0	0	0	0	0	0	417.0
336	1336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
337	331	0	0	0	0	0	0	0	0	0	337	0	0	0	0	0	0	0	0	0	50.0
338	0	0	0	0	0	0	0	0	0	0	338	0	0	0	0	0	0	0	0	0	73.0
339	1822	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
340	1340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
341	1341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
342	1342	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
343	1343	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
344	366	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
345	346	0	0	0	0	0	0	0	0	0	345	0	0	0	0	0	0	0	0	0	149.0
346	0	0	0	0	0	0	0	0	0	0	346	0	0	0	0	0	0	0	0	0	71.0
347	1915	0	0	0	0	0	0	0	0	0	347	0	0	0	0	0	0	0	0	0	212.0
348	1348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
349	0	0	0	0	0	0	0	0	0	0	349	0	0	0	0	0	0	0	0	0	13.0
350	0	0	0	0	0	0	0	0	0	0	350	0	0	0	0	0	0	0	0	0	51.0
351	1814	0	0	0	0	0	0	0	0	0	351	0	0	0	0	0	0	0	0	0	100.0
352	1919	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
353	0	0	0	0	0	0	0	0	0	0	353	0	0	0	0	0	0	0	0	0	41.0
354	1817	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.0
355	0	0	0	0	0	0	0	0	0	0	355	0	0	0	0	0	0	0	0	0	7.0
356	359	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
357	1357	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
358	311	0	0	0	0	0	0	0	0	0	358	0	0	0	0	0	0	0	0	0	259.0
359	345	347	349	355	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
360	1360	292	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
361	0	0	0	0	0	0	0	0	0	0	361	0	0	0	0	0	0	0	0	0	30.0
362	1362	363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
363	0	0	0	0	0	0	0	0	0	0	363	0	0	0	0	0	0	0	0	0	7.0
366	1366	0	0	0	0	0	0	0	0	0	366	0	0	0	0	0	0	0	0	0	81.0
367	1367	0	0	0	0	0	0	0	0	0	367	0	0	0	0	0	0	0	0	0	23.0
368	0	0	0	0	0	0	0	0	0	0	368	0	0	0	0	0	0	0	0	0	99.0
369	0	0	0	0	0	0	0	0	0	0	369	0	0	0	0	0	0	0	0	0	17.0
370	0	0	0	0	0	0	0	0	0	0	370	0	0	0	0	0	0	0	0	0	41.0
371	372	0	0	0	0	0	0	0	0	0	371	0	0	0	0	0	0	0	0	0	147.0
372	374	373	367	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	64.0
373	0	0	0	0	0	0	0	0	0	0	373	0	0	0	0	0	0	0	0	0	38.0

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374	1374	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
375	376	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
376	266	0	0	0	0	0	0	0	0	0	376	0	0	0	0	0	0	0	0	3.0
377	1925	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
378	1378	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
379	380	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
380	1821	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
381	382	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
382	1381	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
383	1820	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
384	0	0	0	0	0	0	0	0	0	0	384	0	0	0	0	0	0	0	0	77.0
385	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
386	1386	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
387	1387	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
388	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
389	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
390	1912	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
391	392	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
392	1941 1392	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
393	358	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
394	395	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
395	386	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
396	1396	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
397	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	59647.0
398	362	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
399	270	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	36842.0
1238	390	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1267	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1289	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1290	291	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
1291	268	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
1293	280	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3624.0
1294	269	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2784.0
1295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1296	295	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1301	335	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
1302	1301	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
1303	1302	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	417.0
1304	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1305	1307 1304	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
1306	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1307	1308	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
1308	332	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10.0
1309	328	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
1310	336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1311	1309	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	498.0
1312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1313	339	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1320	1908 1907 1361	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	293.0
1321	323	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9.0

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1323	1402	0	0	0	0	0	0	0	0	0	1323	0	0	0	0	0	0	0	0	0	9.0
1325	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1329	0	0	0	0	0	0	0	0	0	0	336	0	0	0	0	0	0	0	0	0	31.0
1330	368	1312	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1331	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1332	1330	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1333	340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1334	341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1335	342	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
1336	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1337	321	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
1338	1337	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
1339	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1341	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1342	343	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
1343	356	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	381.0
1348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1357	393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1360	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1361	1338	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	34.0
1362	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1364	361	1363	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30.0
1365	1370	1364	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	129.0
1366	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1367	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1368	1332	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1369	1368	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1370	1369	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	99.0
1371	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1372	1371	1377	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1373	1945	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1374	375	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3.0
1375	1373	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1376	1375	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1377	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1378	1406	1404	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1381	1382	1405	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1382	296	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1386	1937	385	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1387	1401	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1392	324	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	569.0
1393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1396	398	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1401	357	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1402	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1403	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1404	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1405	383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0

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1406	379	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1407	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1408	344	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	81.0
1409	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1410	0	0	0	0	0	0	0	0	0	0	1410	0	0	0	0	0	0	0	195.0
1411	1410	1424	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1412	1411	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1413	1412	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77101.0
1414	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1415	0	0	0	0	0	0	0	0	0	0	1415	0	0	0	0	0	0	0	307.0
1416	1415	1553	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1203.0
1420	0	0	0	0	0	0	0	0	0	0	1420	0	0	0	0	0	0	0	59.0
1421	1420	1426	1441	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1423	1421	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1424	1423	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76906.0
1425	0	0	0	0	0	0	0	0	0	0	1425	0	0	0	0	0	0	0	68.0
1426	1438	1425	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	382.0
1427	261	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	80179.0
1428	1528	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1429	1428	1416	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1203.0
1430	0	0	0	0	0	0	0	0	0	0	1430	0	0	0	0	0	0	0	82.0
1431	1430	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	82.0
1435	0	0	0	0	0	0	0	0	0	0	1435	0	0	0	0	0	0	0	232.0
1436	1435	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	232.0
1438	1436	1431	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	314.0
1440	0	0	0	0	0	0	0	0	0	0	1440	0	0	0	0	0	0	0	66.0
1441	1453	1440	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76465.0
1442	1514	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2719.0
1445	0	0	0	0	0	0	0	0	0	0	1445	0	0	0	0	0	0	0	164.0
1446	1445	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	164.0
1450	0	0	0	0	0	0	0	0	0	0	1450	0	0	0	0	0	0	0	198.0
1451	1603	1450	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76235.0
1453	1446	1451	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	76399.0
1455	0	0	0	0	0	0	0	0	0	0	1455	0	0	0	0	0	0	0	542.0
1456	1455	1482	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1274.0
1457	1456	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1274.0
1460	0	0	0	0	0	0	0	0	0	0	1460	0	0	0	0	0	0	0	286.0
1461	1460	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	286.0
1465	0	0	0	0	0	0	0	0	0	0	1465	0	0	0	0	0	0	0	93.0
1467	1933	1932	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2351.0
1468	1467	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2351.0
1480	1938	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1481	1480	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1482	1481	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1490	0	0	0	0	0	0	0	0	0	0	1490	0	0	0	0	0	0	0	698.0
1491	1490	1457	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1972.0
1500	0	0	0	0	0	0	0	0	0	0	1500	0	0	0	0	0	0	0	465.0
1501	1500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	465.0
1505	0	0	0	0	0	0	0	0	0	0	1505	0	0	0	0	0	0	0	262.0
1506	1505	1800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79714.0
1507	1506	1508	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	79714.0

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1620	0	0	0	0	0	0	0	0	0	0	1620	0	0	0	0	0	0	0	0	0	324.0
1621	1653	1620	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1816.0
1623	1616	1621	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2044.0
1624	1623	1705	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2111.0
1625	0	0	0	0	0	0	0	0	0	0	1625	0	0	0	0	0	0	0	0	0	197.0
1626	48	1625	1636	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	72591.0
1628	1631	1626	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73076.0
1630	0	0	0	0	0	0	0	0	0	0	1630	0	0	0	0	0	0	0	0	0	159.0
1631	1643	1630	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	485.0
1635	0	0	0	0	0	0	0	0	0	0	1635	0	0	0	0	0	0	0	0	0	317.0
1636	1635	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	317.0
1640	0	0	0	0	0	0	0	0	0	0	1640	0	0	0	0	0	0	0	0	0	200.0
1641	1640	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	200.0
1643	1646	1641	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	326.0
1645	0	0	0	0	0	0	0	0	0	0	1645	0	0	0	0	0	0	0	0	0	126.0
1646	1645	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	126.0
1650	0	0	0	0	0	0	0	0	0	0	1650	0	0	0	0	0	0	0	0	0	382.0
1651	1661	1650	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	934.0
1653	1651	1656	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1492.0
1655	0	0	0	0	0	0	0	0	0	0	1655	0	0	0	0	0	0	0	0	0	558.0
1656	1655	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	558.0
1660	0	0	0	0	0	0	0	0	0	0	1660	0	0	0	0	0	0	0	0	0	552.0
1661	1660	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	552.0
1665	0	0	0	0	0	0	0	0	0	0	1665	0	0	0	0	0	0	0	0	0	390.0
1666	1665	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	390.0
1705	0	0	0	0	0	0	0	0	0	0	1705	0	0	0	0	0	0	0	0	0	67.0
1710	0	0	0	0	0	0	0	0	0	0	1710	0	0	0	0	0	0	0	0	0	245.0
1711	1710	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	245.0
1712	1711	1624	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2356.0
1715	0	0	0	0	0	0	0	0	0	0	1715	0	0	0	0	0	0	0	0	0	115.0
1716	1715	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	115.0
1800	1509	1468	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9452.0
1812	352	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1813	1812	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1814	1813	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1815	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1816	1815	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1817	1818	1816	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6.0
1818	0	0	0	0	0	0	0	0	0	0	354	0	0	0	0	0	0	0	0	0	6.0
1820	384	1383	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1821	369	1926	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1822	1339	394	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1905	263	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2758.0
1906	389	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1907	388	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1908	387	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	259.0
1909	1906	320	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
1910	313	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1911	391	318	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1912	1911	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1913	351	354	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	106.0

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1914	1913	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	106.0
1915	350 1914	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	157.0
1916	1262	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1917	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	103.0
1919	1934 353	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41.0
1920	1921	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	690.0
1921	297 1917	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	690.0
1922	300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	177.0
1923	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1924	290 1289	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3653.0
1925	378	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	94.0
1926	381	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	77.0
1927	1238	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	799.0
1928	1611 1606	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	73656.0
1929	1712	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2356.0
1931	1491 1461	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2258.0
1932	1465	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	93.0
1933	1931	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2258.0
1934	360	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1935	1442 1916	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2719.0
1937	348	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1938	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	732.0
1939	1313 314	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.0
1940	1910 1408 1942	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	88.0
1941	1393	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1942	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.0
1943	322	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	454.0
1944	1365 370	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1945	1944	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	170.0
1946	1376 1943	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	624.0
1947	1599	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	86852.0
ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER											359	TO GUTTER	266	COMP	THROUGH DIVERSION WILL LAG ONE					
TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.																				
ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER											426	TO GUTTER	385	COMP	THROUGH DIVERSION WILL LAG ONE					
TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.																				
ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER											541	TO GUTTER	388	COMP	THROUGH DIVERSION WILL LAG ONE					
TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.																				
ORDER OF TREE STRUCTURE (NGUT VALUE) DECREASES THROUGH DIVERSION FROM GUTTER											565	TO GUTTER	389	COMP	THROUGH DIVERSION WILL LAG ONE					
TIME STEP UNLESS GUTTER CARDS ARE MODIFIED TO REVERSE DIVERSION.																				
1																				

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*** PEAK FLOWS, STAGES AND STORAGES OF GUTTERS AND DETENTION DAMS ***

CONVEYANCE ELEMENT	PEAK (CFS)	STAGE (FT)	STORAGE (AC-FT)	TIME (HR/MIN)				
1	8302.	8.5		11 30.	104	806.	3.3	8 35.
2	3430.	6.8		8 30.	105	161.	1.6	8 20.
3	1354.	2.5		8 25.	106	142.	1.6	8 30.
4	1378.	2.3		8 25.	107	957.	3.5	8 35.
5	7926.	8.3		11 30.	108	162.	1.4	8 25.
6	7805.	7.3		11 30.	109	748.	3.0	8 30.
7	1213.	4.5		8 30.	110	514.	2.6	8 30.
8	19411.	(DIRECT FLOW)		9 15.	111	166.	1.4	8 20.
9	585.	2.8		8 25.	112	248.	1.9	8 20.
10	300.	1.2		8 15.	113	145.	1.4	8 25.
11	263.	1.3		8 10.	114	16.	.5	8 15.
12	262.	1.2		8 15.	115	95.	1.1	8 20.
13	847.	2.1		8 20.	116	217.	2.0	8 40.
14	282.	1.2		8 10.	117	261.	2.4	8 20.
15	16157.	(DIRECT FLOW)		9 25.	118	228.	1.9	8 30.
16	16088.	(DIRECT FLOW)		9 25.	119	388.	3.1	8 30.
17	1466.	3.0		8 30.	120	154.	1.7	8 15.
18	904.	3.3		8 30.	121	294.	2.1	8 25.
20	238.	1.6		8 25.	122	1189.	3.2	8 45.
21	348.	1.9		8 30.	123	655.	2.3	8 40.
22	3551.	5.2		8 40.	124	355.	2.0	8 35.
23	1775.	4.5		8 40.	125	100.	1.0	8 30.
24	1317.	3.8		8 35.	126	70.	.9	8 20.
25	346.	1.7		8 25.	127	263.	1.4	8 35.
26	903.	3.5		8 30.	128	246.	1.2	8 35.
27	108.	.7		8 20.	129	7199.	7.5	9 20.
28	686.	2.1		8 30.	130	887.	2.6	8 40.
29	171.	1.4		8 20.	131	201.	1.2	8 20.
30	363.	1.6		8 30.	132	127.	1.3	8 30.
31	433.	2.1		8 30.	133	535.	2.4	8 40.
32	104.	1.0		8 25.	134	343.	1.9	8 30.
33	267.	1.6		8 25.	135	11.	.4	8 15.
34	589.	2.8		8 35.	136	21.	.5	8 15.
35	180.	1.1		8 20.	137	6579.	5.6	9 15.
36	228.	1.3		8 30.	138	245.	1.6	8 35.
37	598.	2.9		8 40.	139	6336.	5.4	9 15.
38	128.	.8		8 30.	140	967.	2.9	8 40.
39	314.	1.5		8 25.	141	163.	1.5	8 20.
40	15373.	10.8		9 30.	142	734.	2.9	8 35.
41	240.	1.2		8 15.	143	278.	1.8	8 25.
42	15201.	9.8		9 30.	144	97.	1.0	8 25.
44	15451.	(DIRECT FLOW)		10 10.	145	50.	.9	8 25.
46	13993.	10.4		9 30.	146	407.	1.9	8 35.
48	14371.	11.2		8 55.	147	160.	1.2	8 30.
49	609.	2.0		8 10.	148	140.	1.2	8 25.
50	14253.	7.3		8 50.	149	5657.	4.9	9 15.
51	1055.	3.7		8 10.	150	93.	1.1	8 15.
52	12290.	9.4		8 45.	151	218.	1.7	8 20.
53	433.	2.8		8 20.	152	5442.	5.2	9 10.
54	133.	1.5		8 15.	153	127.	1.0	8 30.
55	237.	2.0		8 20.	154	5369.	5.7	8 55.
56	2174.	4.0		8 25.	155	101.	.7	8 25.
57	1081.	2.4		8 20.	156	5212.	5.6	8 55.
58	147.	1.5		8 15.	157	4597.	5.5	8 50.
59	13833.	10.4		9 25.	158	508.	1.9	8 35.
60	231.	1.4		8 20.	159	29.	.5	8 20.
61	672.	3.0		8 40.	160	312.	1.5	8 30.
62	1388.	3.0		8 40.	161	157.	1.4	8 30.
63	132.	1.4		8 35.	162	25.	.5	8 15.
64	138.	2.0		8 30.	163	536.	1.8	8 30.
65	680.	4.2		8 40.	164	80.	.7	8 20.
66	92.	.9		8 20.	165	232.	1.6	8 30.
67	527.	2.5		8 25.	166	395.	1.7	8 30.
68	686.	2.4		8 20.	167	141.	1.2	8 25.
69	238.	1.5		8 20.	168	18.	.5	8 15.
70	344.	1.7		8 20.	169	13.	.4	8 15.
71	679.	2.8		8 35.	170	312.	1.9	8 25.
72	225.	1.6		8 20.	171	190.	1.3	8 20.
73	246.	1.9		8 40.	172	3785.	6.0	9 .5.
74	13360.	10.1		9 25.	173	1705.	2.8	8 35.
75	2464.	6.0		8 55.	174	148.	1.3	8 20.
76	367.	2.0		8 25.	175	1351.	2.6	8 40.
77	2908.	5.6		8 55.	176	1135.	3.1	8 45.
78	99.	.9		8 35.	177	186.	1.4	8 30.
79	2351.	4.6		8 55.	178	34.	.7	8 20.
80	1835.	2.7		8 40.	179	75.	.4	8 40.
81	690.	2.5		8 40.	180	551.	2.6	8 30.
82	460.	1.9		8 35.	181	33.	.6	8 20.
83	78.	1.0		8 30.	182	192.	1.2	8 30.
84	329.	1.7		8 30.	183	40.	.6	8 20.
85	67.	1.4		8 25.	184	122.	.8	8 30.
86	196.	1.5		8 30.	185	26.	.7	8 25.
87	433.	2.4		8 40.	186	83.	.8	8 20.
88	459.	1.7		8 40.	187	2337.	4.0	9 15.
89	250.	2.0		8 35.	192	1993.	3.7	9 .5.
93	38.	.7		8 25.	193	347.	.9	8 15.
94	10515.	7.3		9 25.	194	720.	2.2	8 40.
95	8338.	6.7		9 30.	195	17.	.3	8 15.
96	8188.	9.5		9 25.	196	23.	.6	8 20.
97	3234.	5.1		8 45.	198	435.	1.8	8 40.
98	365.	2.0		8 20.	199	37.	.7	8 25.
99	2780.	5.1		8 40.	200	34.	.6	8 20.
100	565.	2.4		8 25.	201	376.	1.7	8 30.
101	2237.	4.8		8 40.	202	18.	.5	8 15.
102	1263.	3.4		8 45.	203	87.	.9	8 15.
103	1044.	2.5		8 35.	204	275.	1.3	8 25.

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205	1304.	3.3	9	5.	341	5011.	(DIRECT FLOW)	10	55.	
206	19.	.1	8	15.	342	8105.	(DIRECT FLOW)	10	55.	
207	1199.	2.7	9	0.	343	9765.	(DIRECT FLOW)	10	55.	
208	19.	.3	8	15.	344	266.	(DIRECT FLOW)	8	15.	
211	1152.	3.6	8	40.	345	557.	1.8	8	10.	
212	292.	1.3	8	35.	346	306.	1.3	8	5.	
213	195.	1.1	8	35.	347	9748.	8.9	10	55.	
214	91.	.7	8	20.	348	2510.	(DIRECT FLOW)	11	5.	
215	849.	2.7	8	40.	349	20.	.4	8	25.	
216	122.	.6	8	25.	350	205.	3.3	8	10.	
217	18.	.1	8	15.	351	5546.	7.8	10	50.	
218	492.	2.8	8	25.	352	9746.	.1	48.9	10	45.
219	728.	2.4	8	30.	353	136.	1.3	8	10.	
220	223.	1.2	8	30.	354	4208.	4.0	10	55.	
221	68.	.9	8	15.	355	25.	2.4	8	10.	
222	427.	2.5	8	25.	356	9765.	.1	33.4	10	55.
223	139.	.8	8	30.	357	923.	(DIRECT FLOW)	11	20.	
224	288.	2.3	8	20.	358	1141.	5.3	11	20.	
225	66.	.9	8	15.	359	9764.	(DIRECT FLOW)	10	55.	
226	108.	.6	8	20.	360	9768.	(DIRECT FLOW)	10	40.	
231	3055.	3.9	8	25.	361	112.	(DIRECT FLOW)	8	5.	
232	3073.	(DIRECT FLOW)	11	30.	362	1660.	(DIRECT FLOW)	10	55.	
233	3057.	4.6	11	30.	363	23.	.6	8	10.	
234	349.	3.1	8	30.	366	266.	1.4	8	15.	
235	409.	1.4	8	20.	367	103.	1.0	8	15.	
236	3073.	(DIRECT FLOW)	11	30.	368	242.	(DIRECT FLOW)	8	10.	
237	6652.	(DIRECT FLOW)	11	5.	369	80.	.9	8	5.	
238	6652.	(DIRECT FLOW)	11	5.	370	204.	(DIRECT FLOW)	8	5.	
239	409.	(DIRECT FLOW)	8	20.	371	370.	2.2	8	20.	
240	6449.	4.3	11	5.	372	172.	(DIRECT FLOW)	8	15.	
241	6557.	4.1	10	50.	373	48.	1.4	8	25.	
242	6934.	(DIRECT FLOW)	10	20.	374	36.	1.4	10	35.	
243	5687.	3.8	10	20.	375	248.	(DIRECT FLOW)	10	25.	
244	2068.	3.9	8	15.	376	248.	4.0	10	25.	
245	10684.	9.6	8	40.	377	111.	3.2	10	40.	
246	4112.	5.4	8	30.	378	373.	(DIRECT FLOW)	10	25.	
247	1419.	3.0	8	20.	379	227.	(DIRECT FLOW)	8	10.	
248	1185.	2.7	8	25.	380	227.	4.3	8	10.	
249	752.	2.3	8	15.	381	338.	(DIRECT FLOW)	10	50.	
250	2021.	4.3	8	25.	382	338.	8.0	10	50.	
251	3103.	(DIRECT FLOW)	11	5.	383	5125.	(DIRECT FLOW)	10	40.	
252	2588.	(DIRECT FLOW)	11	30.	384	281.	4.2	8	10.	
261	15451.	(DIRECT FLOW)	10	10.	385	1251.	(DIRECT FLOW)	11	0.	
262	11362.	3.8	10	15.	386	2430.	(DIRECT FLOW)	11	5.	
263	11362.	(DIRECT FLOW)	10	15.	387	199.	(DIRECT FLOW)	11	15.	
264	11079.	4.1	10	20.	388	1064.	(DIRECT FLOW)	8	40.	
265	11079.	(DIRECT FLOW)	10	20.	389	3550.	(DIRECT FLOW)	11	5.	
266	248.	(DIRECT FLOW)	10	15.	390	1267.	(DIRECT FLOW)	8	40.	
267	6011.	(DIRECT FLOW)	10	20.	391	1221.	7.3	11	30.	
268	5870.	.1	86.6	10	30.	392	1224.	(DIRECT FLOW)	11	20.
269	5599.	(DIRECT FLOW)	10	20.	393	1141.	(DIRECT FLOW)	11	20.	
270	9057.	8.8	12	5.	394	1892.	3.2	11	5.	
271	9123.	(DIRECT FLOW)	11	50.	395	1891.	(DIRECT FLOW)	11	5.	
280	5735.	(DIRECT FLOW)	10	25.	396	1660.	(DIRECT FLOW)	10	55.	
289	1154.	6.1	10	50.	397	7792.	.1	2858.3	11	25.
290	896.	5.3	10	35.	398	1660.	.1	4.8	10	55.
291	5870.	(DIRECT FLOW)	10	30.	399	9057.	(DIRECT FLOW)	12	5.	
292	4979.	4.7	10	40.	1238	203.	(DIRECT FLOW)	8	40.	
293	532.	10.4	10	25.	1262	9682.	(DIRECT FLOW)	10	15.	
294	5735.	(DIRECT FLOW)	10	25.	1267	5479.	(DIRECT FLOW)	10	20.	
295	5153.	.1	108.1	10	35.	1289	261.	(DIRECT FLOW)	10	30.
296	5153.	(DIRECT FLOW)	10	35.	1290	894.	(DIRECT FLOW)	10	30.	
297	1336.	5.5	8	10.	1291	5870.	(DIRECT FLOW)	10	30.	
298	153.	.1	4.9	8	25.	1293	532.	(DIRECT FLOW)	10	25.
299	278.	1.0	8	10.	1294	5585.	3.8	10	25.	
300	26.	.1	34.5	9	40.	1295	5203.	(DIRECT FLOW)	10	30.
301	655.	1.2	8	5.	1296	5153.	(DIRECT FLOW)	10	35.	
303	289.	(DIRECT FLOW)	8	10.	1301	3015.	(DIRECT FLOW)	11	5.	
304	126.	1.9	8	25.	1302	3015.	(DIRECT FLOW)	11	5.	
308	409.	(DIRECT FLOW)	10	55.	1303	906.	(DIRECT FLOW)	11	5.	
310	1387.	(DIRECT FLOW)	11	10.	1304	2109.	(DIRECT FLOW)	11	5.	
311	1145.	(DIRECT FLOW)	11	10.	1305	4513.	(DIRECT FLOW)	11	5.	
312	1093.	7.5	11	15.	1306	65.	(DIRECT FLOW)	11	10.	
313	1047.	(DIRECT FLOW)	11	5.	1307	2404.	(DIRECT FLOW)	11	5.	
314	409.	6.3	11	0.	1308	2469.	(DIRECT FLOW)	11	5.	
315	1377.	2.7	11	15.	1309	2832.	(DIRECT FLOW)	11	10.	
316	154.	1.2	8	10.	1310	639.	(DIRECT FLOW)	11	10.	
317	1380.	(DIRECT FLOW)	11	15.	1311	2018.	(DIRECT FLOW)	11	10.	
318	354.	3.8	8	35.	1312	814.	(DIRECT FLOW)	11	10.	
319	6516.	8.6	11	55.	1313	639.	(DIRECT FLOW)	11	5.	
320	2602.	2.9	11	35.	1320	2599.	(DIRECT FLOW)	11	30.	
321	3097.	3.6	11	20.	1321	3100.	(DIRECT FLOW)	11	15.	
322	6086.	(DIRECT FLOW)	11	30.	1323	3265.	(DIRECT FLOW)	11	15.	
323	3265.	(DIRECT FLOW)	11	15.	1325	889.	(DIRECT FLOW)	11	25.	
324	4271.	(DIRECT FLOW)	11	15.	1329	118.	1.1	8	10.	
325	4271.	(DIRECT FLOW)	11	15.	1330	818.	4.7	11	15.	
326	3393.	9.4	11	15.	1331	1325.	(DIRECT FLOW)	11	5.	
327	2013.	7.8	11	15.	1332	818.	(DIRECT FLOW)	11	15.	
328	2832.	(DIRECT FLOW)	11	10.	1333	1148.	(DIRECT FLOW)	11	0.	
329	969.	6.4	11	10.	1334	1353.	(DIRECT FLOW)	10	55.	
330	970.	(DIRECT FLOW)	11	5.	1335	3095.	(DIRECT FLOW)	10	55.	
331	1865.	(DIRECT FLOW)	11	5.	1336	1278.	(DIRECT FLOW)	11	10.	
332	2469.	(DIRECT FLOW)	11	5.	1337	3097.	(DIRECT FLOW)	11	20.	
333	1133.	2.6	11	10.	1338	1407.	(DIRECT FLOW)	11	20.	
334	1337.	2.8	11	0.	1339	26.	(DIRECT FLOW)	8	20.	
335	3015.	6.7	11	5.	1340	3658.	(DIRECT FLOW)	11	0.	
336	1278.	(DIRECT FLOW)	11	10.	1341	5011.	(DIRECT FLOW)	10	55.	
337	1861.	3.2	11	10.	1342	8105.	(DIRECT FLOW)	10	55.	
338	168.	2.0	8	20.	1343	9765.	(DIRECT FLOW)	10	55.	
339	1917.	(DIRECT FLOW)	11	5.	1348	2510.	(DIRECT FLOW)	11	5.	
340	3658.	(DIRECT FLOW)	11	0.	1357	923.	(DIRECT FLOW)	11	20.	

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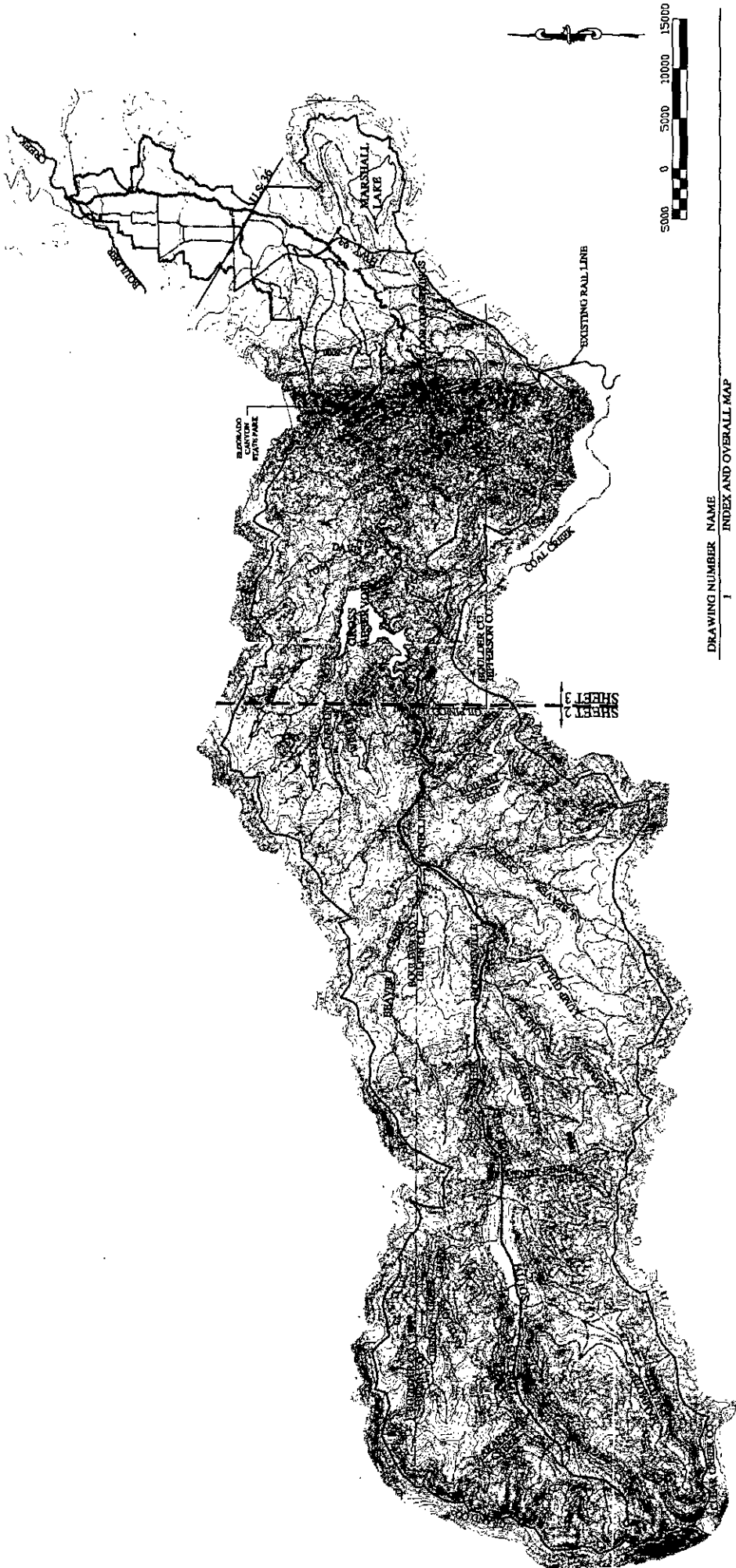
1360	4821.	(DIRECT FLOW)	10	45.	1533	14551.	(DIRECT FLOW)	9	45.
1361	1404.	4.2	11	25.	1534	8820.	4.7	9	50.
1362	1660.	(DIRECT FLOW)	10	55.	1537	5892.	4.7	9	35.
1363	1690.	(DIRECT FLOW)	11	20.	1541	495.	(DIRECT FLOW)	8	10.
1364	1679.	4.4	11	25.	1542	317.	2.4	8	35.
1365	2413.	(DIRECT FLOW)	11	25.	1544	14582.	(DIRECT FLOW)	9	50.
1366	179.	(DIRECT FLOW)	10	55.	1545	397.	(DIRECT FLOW)	8	10.
1367	37.	(DIRECT FLOW)	8	15.	1546	664.	2.6	8	35.
1368	818.	(DIRECT FLOW)	11	15.	1548	14537.	4.2	9	55.
1369	739.	(DIRECT FLOW)	11	15.	1550	861.	(DIRECT FLOW)	8	10.
1370	738.	4.2	11	20.	1551	1089.	3.0	8	30.
1371	79.	(DIRECT FLOW)	11	15.	1553	1399.	(DIRECT FLOW)	8	30.
1372	1838.	(DIRECT FLOW)	11	25.	1556	163.	(DIRECT FLOW)	8	10.
1373	2408.	(DIRECT FLOW)	11	30.	1557	310.	2.4	8	30.
1374	36.	(DIRECT FLOW)	10	25.	1560	294.	(DIRECT FLOW)	8	10.
1375	646.	(DIRECT FLOW)	11	30.	1561	288.	1.9	8	10.
1376	647.	4.6	11	30.	1563	494.	(DIRECT FLOW)	8	10.
1377	1762.	(DIRECT FLOW)	11	30.	1565	210.	(DIRECT FLOW)	8	10.
1378	373.	(DIRECT FLOW)	10	25.	1566	206.	1.6	8	15.
1381	339.	(DIRECT FLOW)	10	40.	1570	230.	(DIRECT FLOW)	8	15.
1382	35.	(DIRECT FLOW)	10	35.	1571	229.	.8	8	20.
1383	5118.	(DIRECT FLOW)	10	40.	1575	553.	(DIRECT FLOW)	8	10.
1386	2430.	(DIRECT FLOW)	11	5.	1576	441.	2.8	8	25.
1387	199.	(DIRECT FLOW)	11	15.	1599	14267.	(DIRECT FLOW)	11	40.
1392	1007.	(DIRECT FLOW)	11	15.	1600	10.	(DIRECT FLOW)	8	0.
1393	218.	(DIRECT FLOW)	11	25.	1601	15296.	6.6	9	10.
1396	1660.	(DIRECT FLOW)	10	55.	1603	17323.	(DIRECT FLOW)	9	5.
1401	34.	(DIRECT FLOW)	11	20.	1605	170.	(DIRECT FLOW)	8	10.
1402	3264.	(DIRECT FLOW)	11	15.	1606	1148.	3.2	8	20.
1403	484.	(DIRECT FLOW)	11	30.	1610	118.	(DIRECT FLOW)	8	10.
1404	212.	(DIRECT FLOW)	10	25.	1611	14904.	6.4	9	5.
1405	304.	(DIRECT FLOW)	10	40.	1615	247.	(DIRECT FLOW)	8	10.
1406	190.	(DIRECT FLOW)	8	10.	1616	226.	2.3	8	25.
1407	540.	(DIRECT FLOW)	11	5.	1620	299.	(DIRECT FLOW)	8	10.
1408	240.	(DIRECT FLOW)	8	15.	1621	2305.	5.0	8	35.
1409	748.	(DIRECT FLOW)	11	10.	1623	2505.	(DIRECT FLOW)	8	35.
1410	95.	(DIRECT FLOW)	8	15.	1624	2515.	5.0	8	40.
1411	11667.	7.0	9	40.	1625	575.	(DIRECT FLOW)	8	10.
1412	11667.	(DIRECT FLOW)	9	40.	1626	14754.	6.8	9	0.
1413	11667.	(DIRECT FLOW)	9	40.	1628	15311.	(DIRECT FLOW)	9	0.
1414	8892.	(DIRECT FLOW)	9	45.	1630	304.	(DIRECT FLOW)	8	10.
1415	162.	(DIRECT FLOW)	8	15.	1631	845.	2.7	8	30.
1416	1448.	3.9	8	45.	1635	706.	(DIRECT FLOW)	8	10.
1420	181.	(DIRECT FLOW)	8	10.	1636	678.	2.5	8	15.
1421	16586.	8.2	9	25.	1640	535.	(DIRECT FLOW)	8	10.
1423	16586.	(DIRECT FLOW)	9	25.	1641	366.	3.9	8	25.
1424	11968.	(DIRECT FLOW)	9	25.	1643	606.	(DIRECT FLOW)	8	25.
1425	22.	(DIRECT FLOW)	8	0.	1645	265.	(DIRECT FLOW)	8	10.
1426	170.	1.8	8	25.	1646	246.	1.9	8	20.
1427	5769.	(DIRECT FLOW)	10	10.	1650	1034.	(DIRECT FLOW)	8	10.
1428	4611.	3.5	9	35.	1651	1538.	4.0	8	20.
1429	5442.	(DIRECT FLOW)	9	30.	1653	2334.	(DIRECT FLOW)	8	20.
1430	73.	(DIRECT FLOW)	8	15.	1655	954.	(DIRECT FLOW)	8	15.
1431	67.	1.1	8	15.	1656	836.	3.3	8	30.
1435	119.	(DIRECT FLOW)	8	15.	1660	779.	(DIRECT FLOW)	8	15.
1436	104.	1.9	8	20.	1661	689.	3.1	8	25.
1438	170.	(DIRECT FLOW)	8	20.	1665	1150.	(DIRECT FLOW)	8	5.
1440	108.	(DIRECT FLOW)	8	10.	1666	1070.	3.1	8	15.
1441	16557.	8.3	9	25.	1705	35.	(DIRECT FLOW)	8	15.
1442	1703.	2.4	10	15.	1710	184.	(DIRECT FLOW)	8	20.
1445	113.	(DIRECT FLOW)	8	15.	1711	172.	1.3	8	35.
1446	97.	1.6	8	25.	1712	2687.	(DIRECT FLOW)	8	35.
1450	103.	(DIRECT FLOW)	8	20.	1715	156.	(DIRECT FLOW)	8	15.
1451	17027.	7.8	9	15.	1716	107.	1.1	8	45.
1453	17076.	(DIRECT FLOW)	9	15.	1800	3298.	(DIRECT FLOW)	9	35.
1455	351.	(DIRECT FLOW)	8	10.	1812	9746.	(DIRECT FLOW)	10	45.
1456	311.	.8	8	25.	1813	9746.	(DIRECT FLOW)	10	45.
1457	311.	(DIRECT FLOW)	8	25.	1814	5540.	(DIRECT FLOW)	10	45.
1460	234.	(DIRECT FLOW)	8	10.	1815	4205.	(DIRECT FLOW)	10	50.
1461	214.	2.4	8	20.	1816	4205.	5.4	10	55.
1465	205.	(DIRECT FLOW)	8	10.	1817	4206.	(DIRECT FLOW)	10	55.
1467	645.	(DIRECT FLOW)	8	25.	1918	32.	1.0	8	0.
1468	642.	2.8	8	30.	1820	5125.	(DIRECT FLOW)	10	40.
1480	1513.	4.0	8	15.	1821	231.	(DIRECT FLOW)	8	5.
1481	11.	.0	23	35.	1822	1917.	(DIRECT FLOW)	11	5.
1482	11.	(DIRECT FLOW)	22	30.	1905	11114.	(DIRECT FLOW)	10	15.
1490	486.	(DIRECT FLOW)	8	10.	1906	3509.	1.3	11	20.
1491	444.	3.2	9	15.	1907	1038.	2.7	8	50.
1500	715.	(DIRECT FLOW)	8	10.	1908	191.	2.1	11	35.
1501	564.	3.3	8	35.	1909	6086.	(DIRECT FLOW)	11	30.
1505	664.	(DIRECT FLOW)	8	10.	1910	299.	(DIRECT FLOW)	11	5.
1506	2919.	3.8	10	25.	1911	1281.	(DIRECT FLOW)	8	35.
1507	15351.	(DIRECT FLOW)	10	5.	1912	1267.	6.9	8	40.
1508	12489.	(DIRECT FLOW)	10	5.	1913	9741.	(DIRECT FLOW)	10	50.
1509	2775.	(DIRECT FLOW)	9	40.	1914	9733.	8.1	10	50.
1510	159.	(DIRECT FLOW)	8	10.	1915	9740.	(DIRECT FLOW)	10	50.
1511	14226.	6.4	10	5.	1916	9666.	4.2	10	15.
1512	15278.	7.3	10	10.	1917	76.	1.2	8	30.
1513	14226.	(DIRECT FLOW)	10	5.	1919	9774.	(DIRECT FLOW)	10	45.
1514	1737.	(DIRECT FLOW)	10	5.	1920	1330.	6.3	8	15.
1515	41.	(DIRECT FLOW)	8	5.	1921	1393.	(DIRECT FLOW)	8	10.
1517	112.	1.3	8	50.	1922	26.	.5	9	40.
1520	269.	(DIRECT FLOW)	8	10.	1923	4976.	(DIRECT FLOW)	10	35.
1521	14432.	6.3	9	50.	1924	1157.	(DIRECT FLOW)	10	35.
1522	14602.	(DIRECT FLOW)	9	55.	1925	112.	(DIRECT FLOW)	10	25.
1525	156.	(DIRECT FLOW)	8	5.	1926	160.	(DIRECT FLOW)	10	50.
1526	5434.	4.4	9	35.	1927	203.	3.6	8	50.
1528	4618.	(DIRECT FLOW)	9	30.	1928	15313.	(DIRECT FLOW)	9	5.
1530	340.	(DIRECT FLOW)	8	15.	1929	2673.	3.9	8	40.
1531	913.	2.6	8	40.	1931	541.	(DIRECT FLOW)	8	55.
1532	5907.	(DIRECT FLOW)	9	35.	1932	198.	1.2	8	10.

500_ltd.wpd July 12, 2000 500-YR SWMM MODEL

1933	541.	3.0	8	55.
1934	9770.	6.6	10	45.
1935	11369.	(DIRECT FLOW)	10	15.
1937	1185.	(DIRECT FLOW)	11	5.
1938	1541.	(DIRECT FLOW)	8	10.
1939	1047.	(DIRECT FLOW)	11	5.
1940	1094.	(DIRECT FLOW)	11	10.
1941	218.	1.4	11	25.
1942	639.	(DIRECT FLOW)	11	10.
1943	6071.	7.7	11	35.
1944	2408.	7.3	11	30.
1945	2408.	(DIRECT FLOW)	11	30.
1946	6713.	(DIRECT FLOW)	11	35.
1947	14267.	(DIRECT FLOW)	11	40.

APPENDIX B

Drawing No. 1	Index and Overall Watershed Map
Drawing No. 2	Upper Watershed and Model
Drawing No. 3	Upper Watershed and Model
Drawing No. 4	Enlarged Watershed and Model - Highway 93
Drawing No. 5	Enlarged Watershed and Model - Highway 93 and Highway 36
Drawing No. 6	Enlarged Watershed and Model - Highway 36
Drawing No. 7	Enlarged Watershed and Model - Foothills Pkwy., Wellman, and Baseline Rd.
Drawing No. 8	Enlarged Watershed and Model - Highway 93
Drawing No. 9	Model Detail - Highway 93 and Baseline Splits
Drawing No. 10.	Model Detail - Highway 36 Splits
Drawing No. 11.	Model Detail - Wellman Splits



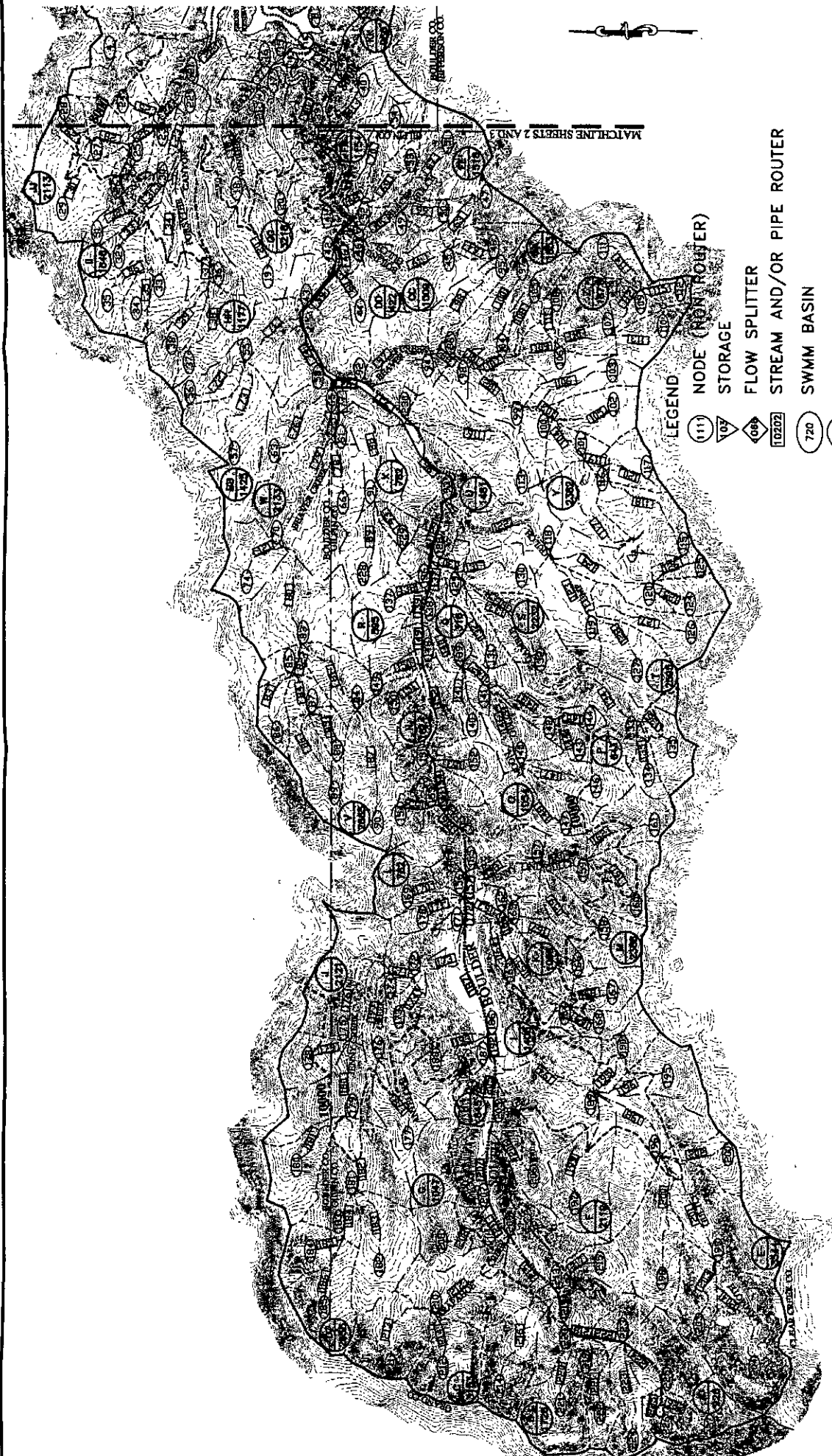
DRAWING NUMBER	NAME
1	INDEX AND OVERALL MAP
2	UPPER WATERSHED AND MODEL
3	LOWER WATERSHED AND MODEL
4	ENLARGED WATERSHED AND MODEL - HIGHWAY 93
5	ENLARGED WATERSHED AND MODEL - HIGHWAY 93 AND HIGHWAY 36
6	ENLARGED WATERSHED AND MODEL - HIGHWAY 36
7	ENLARGED WATERSHED AND MODEL - FOOTHILLS PKWY., WELLMAN, AND BASELINE RD.
8	ENLARGED WATERSHED AND MODEL - ARAPAHOE RD.
9	MODEL DETAIL - HIGHWAY 93 AND BASELINE SPLITS
10	MODEL DETAIL - HIGHWAY 36 SPLITS
11	MODEL DETAIL - WELLMAN SPLITS

PROJECT: SOUTH BOULDER CREEK HYDROLOGY STUDY
 SHEET: 3
 INDEX AND OVERALL WATERSHED MAP

URBAN DRAINAGE AND FLOOD CONTROL DISTRICT
 CITY OF BOULDER
 UNIVERSITY OF COLORADO

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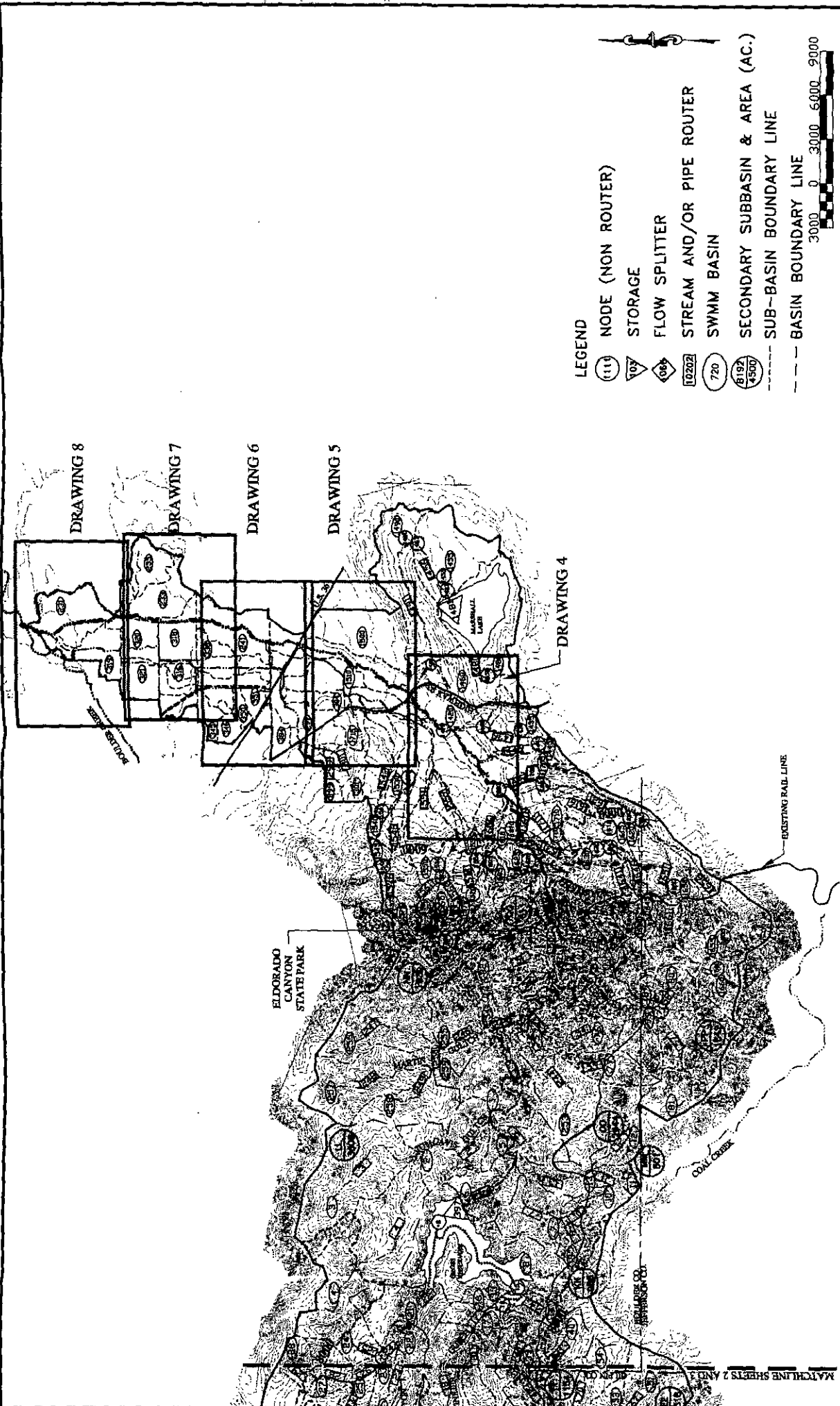
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 DRAWING NO. _____
 SHEET NO. _____
 DATE: _____
 BY: _____
 CHECKED BY: _____



- LEGEND
- (111) NODE (NON-ROUTER)
 - ▽ STORAGE
 - ◇ FLOW SPLITTER
 - ▭ STREAM AND/OR PIPE ROUTER
 - 720 SWMM BASIN
 - 5192 4500 SECONDARY SUBBASIN & AREA (AC.)
 - SUB-BASIN BOUNDARY LINE
 - · - · - BASIN BOUNDARY LINE



	PROJECT NO. _____ DRAWING NO. _____ DATE _____ BY _____ CHECKED BY _____	URBAN DRAINAGE AND FLOOD CONTROL DISTRICT SOUTH BOULDER CREEK SOUTH BOULDER COUNTY UNIVERSITY OF COLORADO	SOUTH BOULDER CREEK HYDROLOGY STUDY	UPPER WATERSHED AND MODEL	2
	MATCHLINE SHEETS 2 AND 3				



LEGEND

- (111) NODE (NON ROUTER)
- ▽ STORAGE
- ◇ FLOW SPLITTER
- 10202 STREAM AND/OR PIPE ROUTER
- 720 SWMM BASIN
- 8192 4500 SECONDARY SUBBASIN & AREA (AC.)
- - - SUB-BASIN BOUNDARY LINE
- - - BASIN BOUNDARY LINE

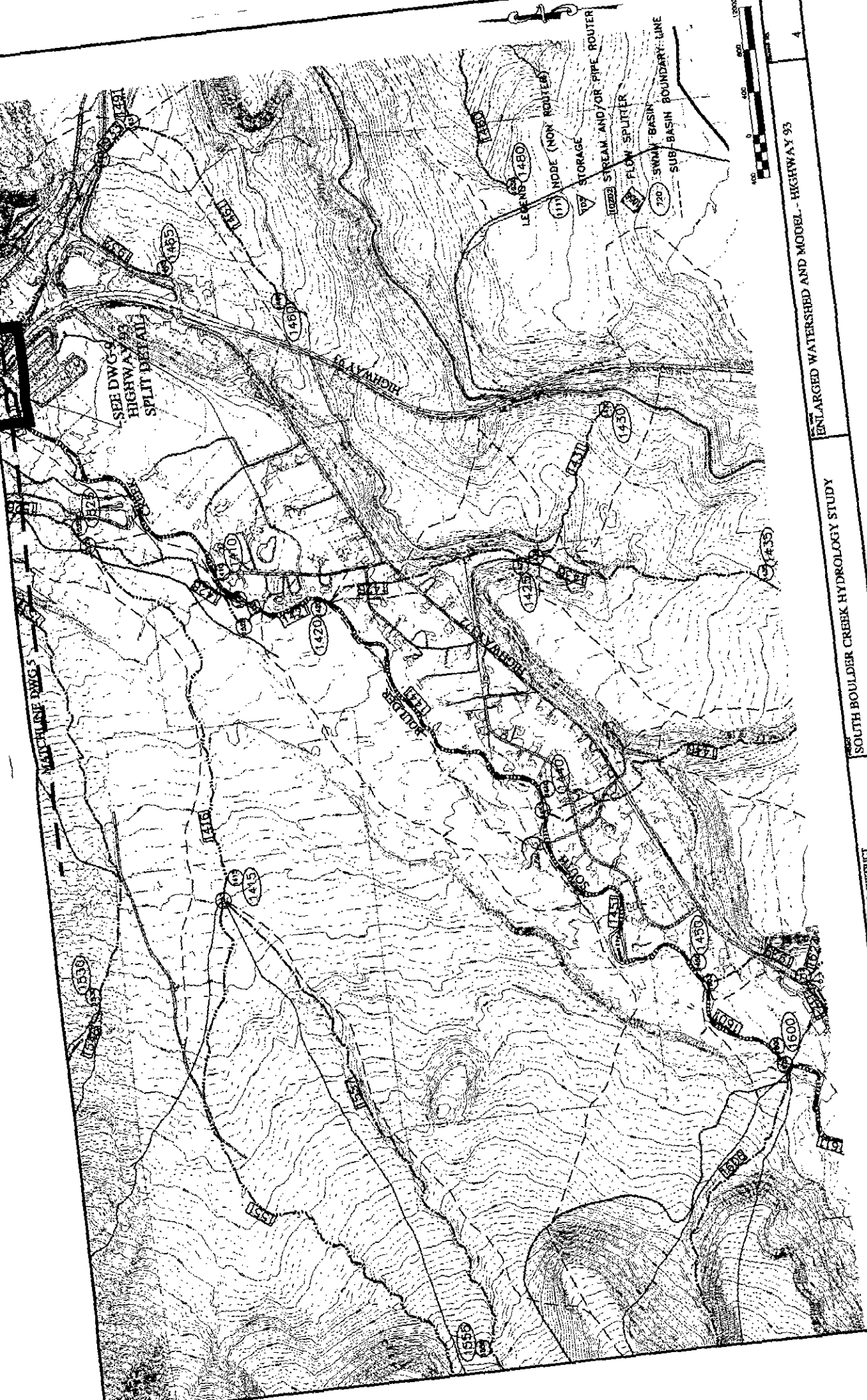


TAGGART
 PROFESSIONAL ENGINEERS
 1000 SOUTH BOULDER CREEK HYDROLOGY STUDY
 UPPER WATERSHED AND MODEL
 3

PREPARED BY: DR. JAMES P. LEE
 REVIEWED BY: J. L. HARRIS
 DATE: JANUARY 28, 1978

USED IN DRAINAGE AND FLOOD CONTROL DISTRICT
 CITY OF BOULDER
 BOULDER COUNTY
 UNIVERSITY OF COLORADO

MATCHLINE SHEETS 2 AND 3



ENLARGED WATERSHED AND MODEL - HIGHWAY 95

SOUTH BOULDER CREEK HYDROLOGY STUDY

SOUTH BOULDER CREEK AND FLOOD CONTROL DISTRICT

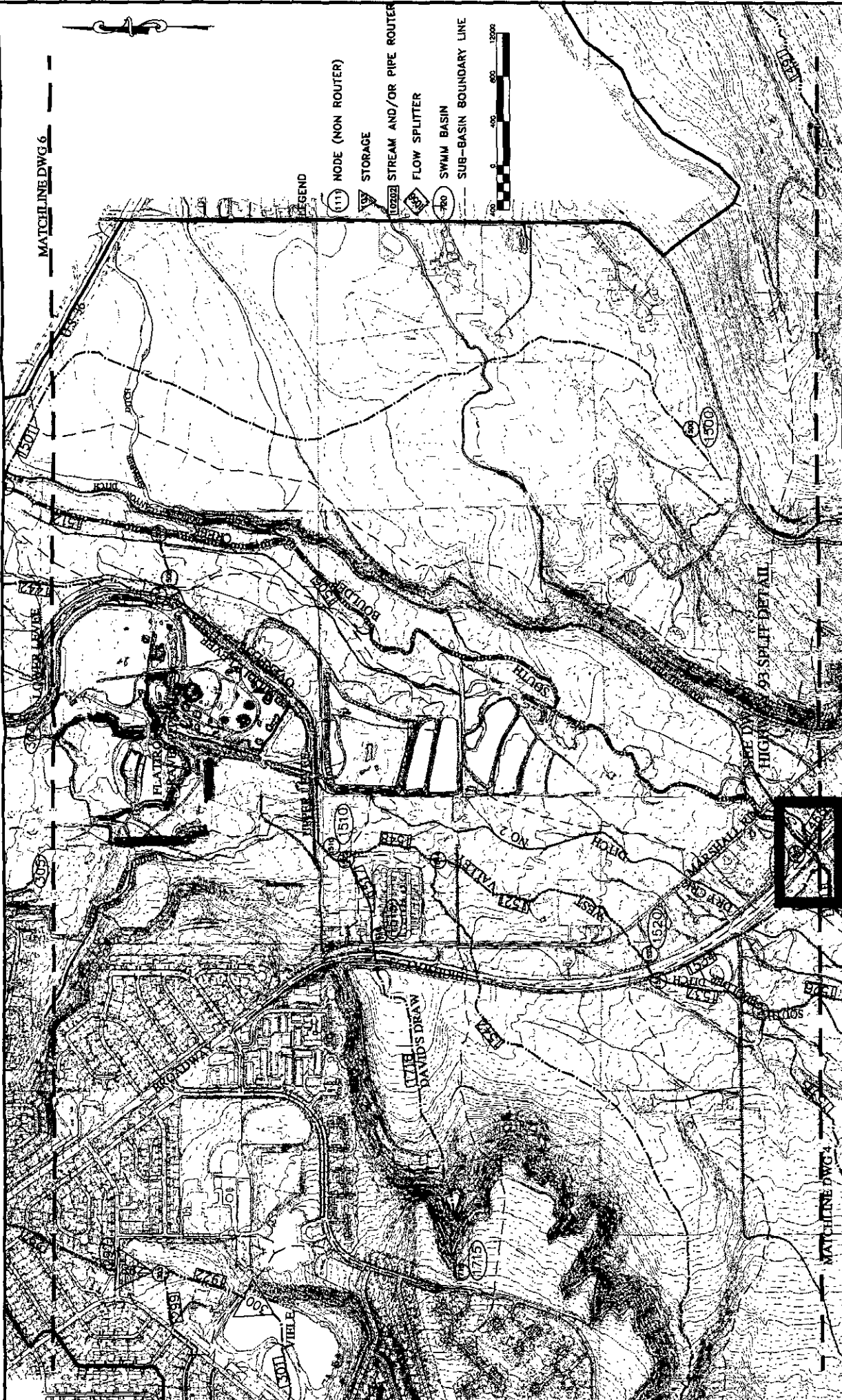
URBAN DRAINAGE AND FLOOD CONTROL DISTRICT
 CITY OF BOULDER
 BOULDER COUNTY
 UNIVERSITY OF COLORADO

DATE: 11-19-88
 SURVEYED BY: J.A.R.
 DRAWN BY: J.A.R.
 SCALE: AS SHOWN



14

MATCHLINE DWG 6

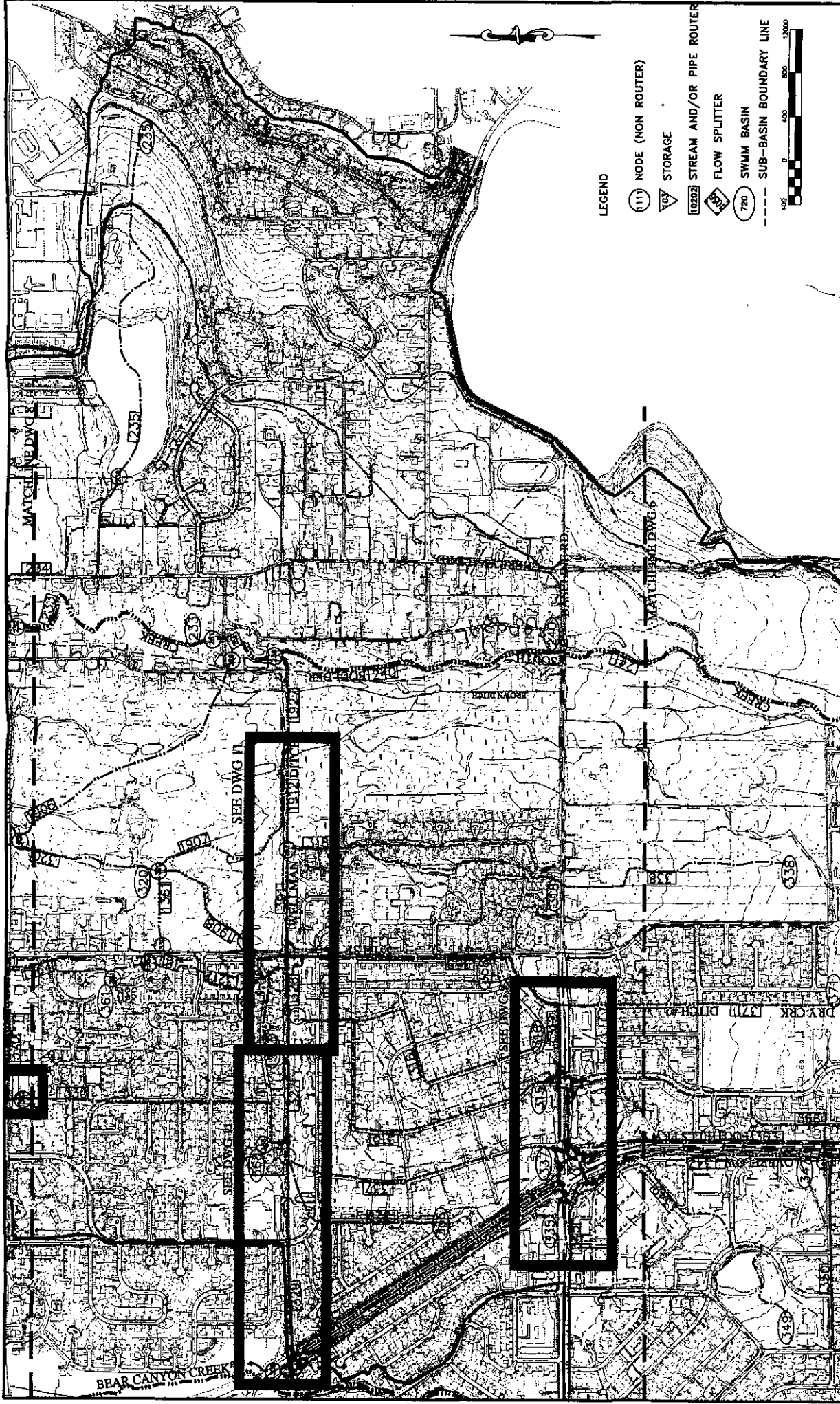


ENLARGED WATERSHED AND MODEL - HIGHWAY 93 AND HIGHWAY 36

SOUTH BOULDER CREEK HYDROLOGY STUDY

URBAN DRAINAGE AND FLOOD CONTROL DISTRICT BOULDER COUNTY UNIVERSITY OF COLORADO


TAGGART
 ENGINEERS ARCHITECTS
 1500 17TH AVENUE, SUITE 100
 BOULDER, COLORADO 80502
 PHONE: 303.440.1000
 FAX: 303.440.1001
 WWW.TAGGART.COM



LEGEND

- (111) NODE (NON ROUTER)
- ▽ STORAGE
- ▭ STREAM AND/OR PIPE ROUTER
- ◇ FLOW SPLITTER
- SWMM BASIN
- - - SUB-BASIN BOUNDARY LINE



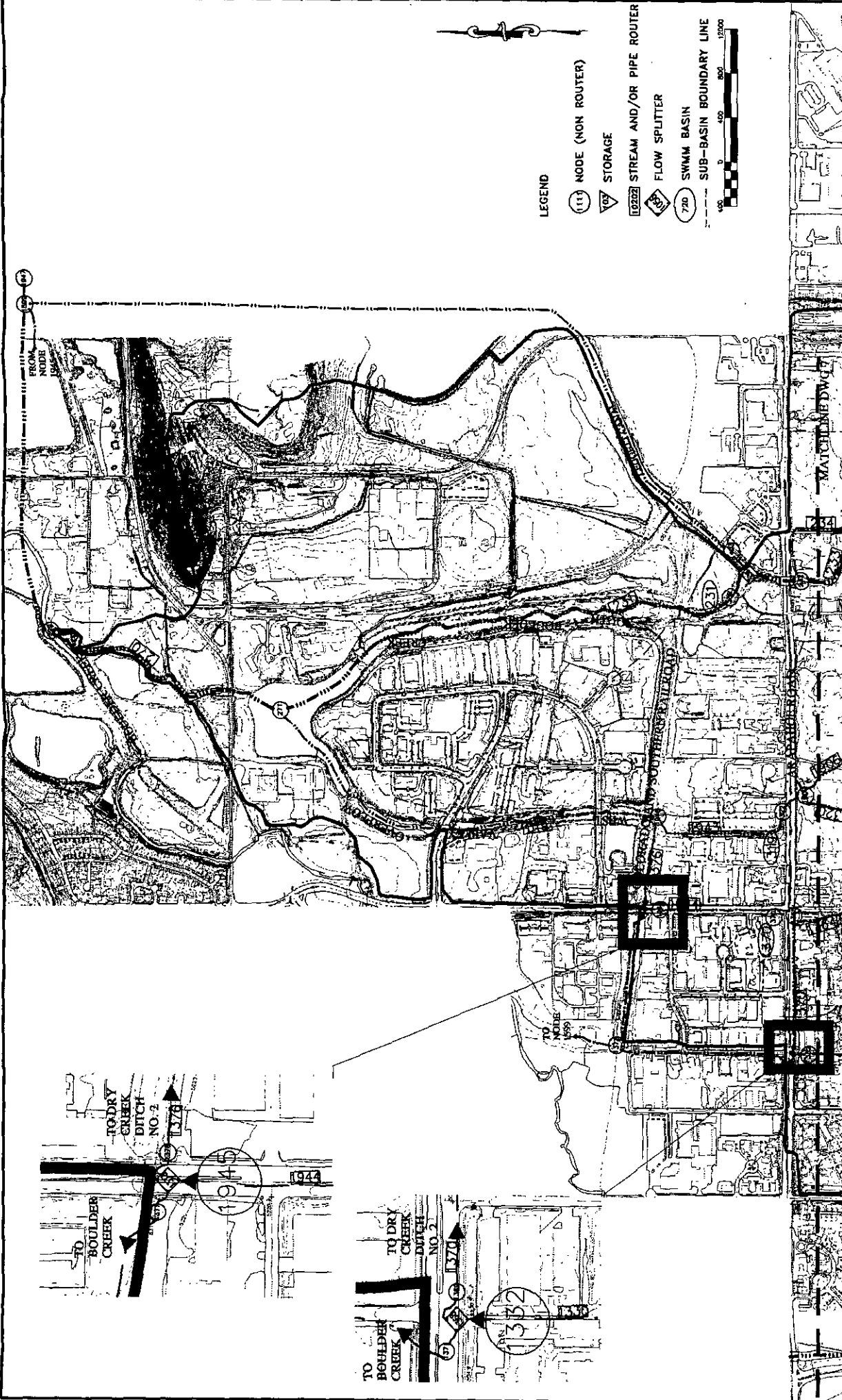
ENLARGED WATERSHED AND MODEL - FOOTHILLS PKWY.,
WELLMAN, AND BASELINE RD.

SOUTH BOULDER CREEK HYDROLOGY STUDY

URBAN DRAINAGE AND FLOOD CONTROL DISTRICT
BOULDER COUNTY
UNIVERSITY OF COLORADO

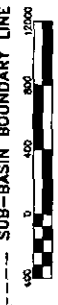
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PROJECT NO. 15-0000-001
SHEET NO. 7
DATE: 12/00



LEGEND

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- ▽ STORAGE
- ▭ STREAM AND/OR PIPE ROUTER
- ◇ FLOW SPLITTER
- SWMM BASIN
- - - SUB-BASIN BOUNDARY LINE



ENLARGED WATERSHED AND MODEL - HIGHWAY 93

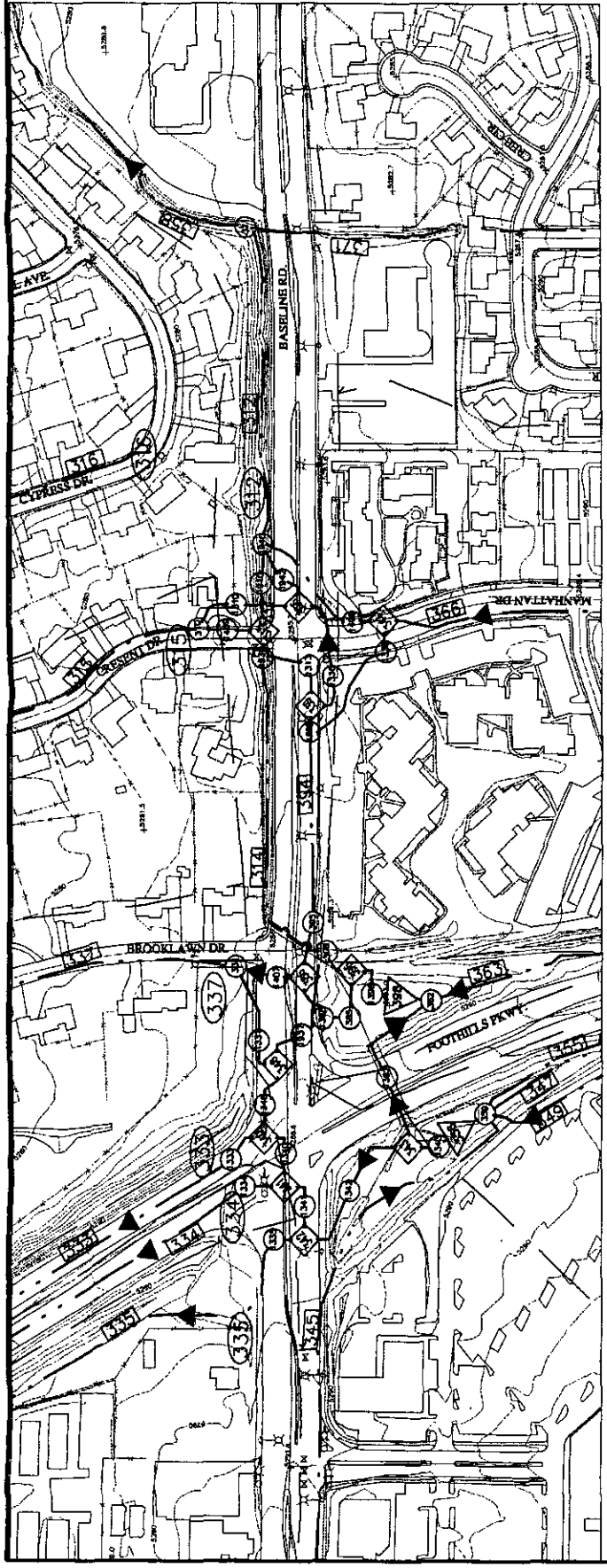
SOUTH BOULDER CREEK HYDROLOGY STUDY

MANAGEMENT AND FLOOD CONTROL DISTRICT

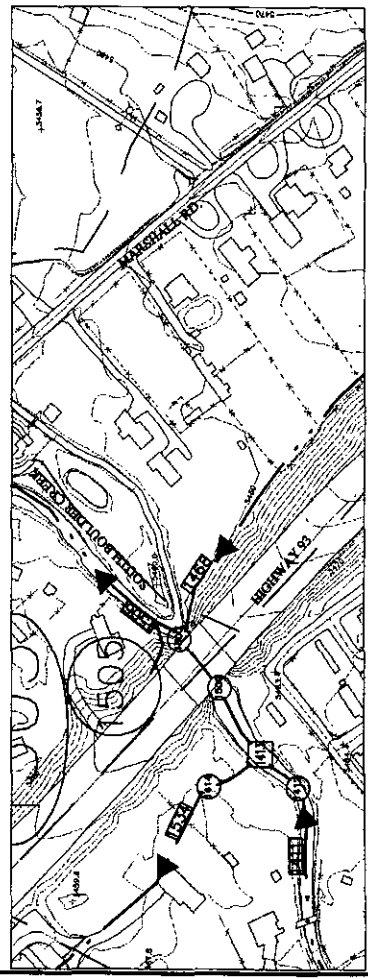
CITY OF BOULDER
BOULDER COUNTY
UNIVERSITY OF COLORADO

DATE: 11/11/88
BY: J. W. B. CUL
PROJECT NO.: 1049
DRAWING NO.: 70





BASELINE SPLITS



HIGHWAY 93 SPLIT

LEGEND

- (11) NODE (NON ROUTER)
- ▽ STORAGE
- ◇ (10/20) STREAM AND/OR PIPE ROUTER
- ◇ (S) FLOW SPLITTER
- (7/0) SHWM BASIN
- - - SUB-BASIN BOUNDARY LINE

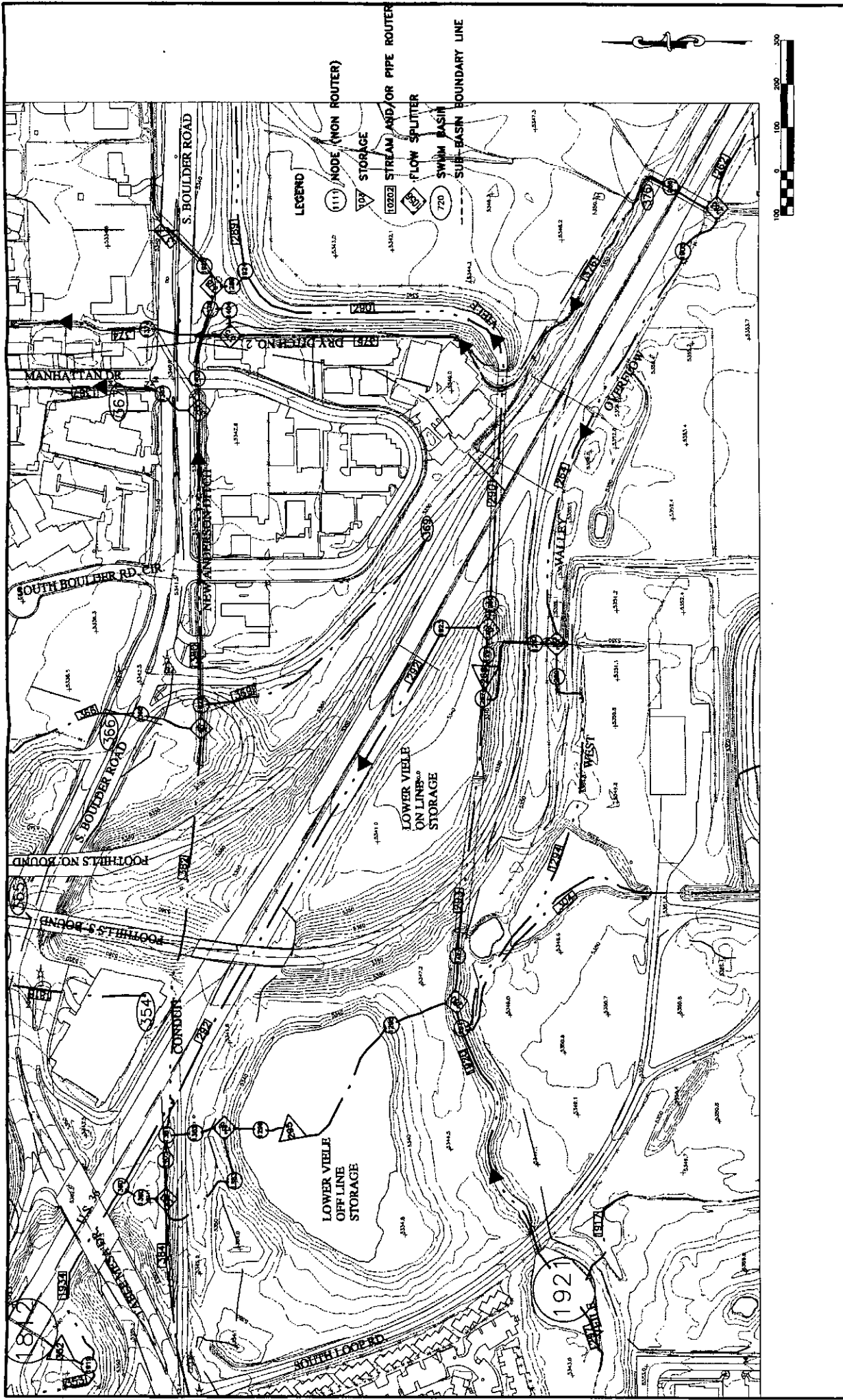


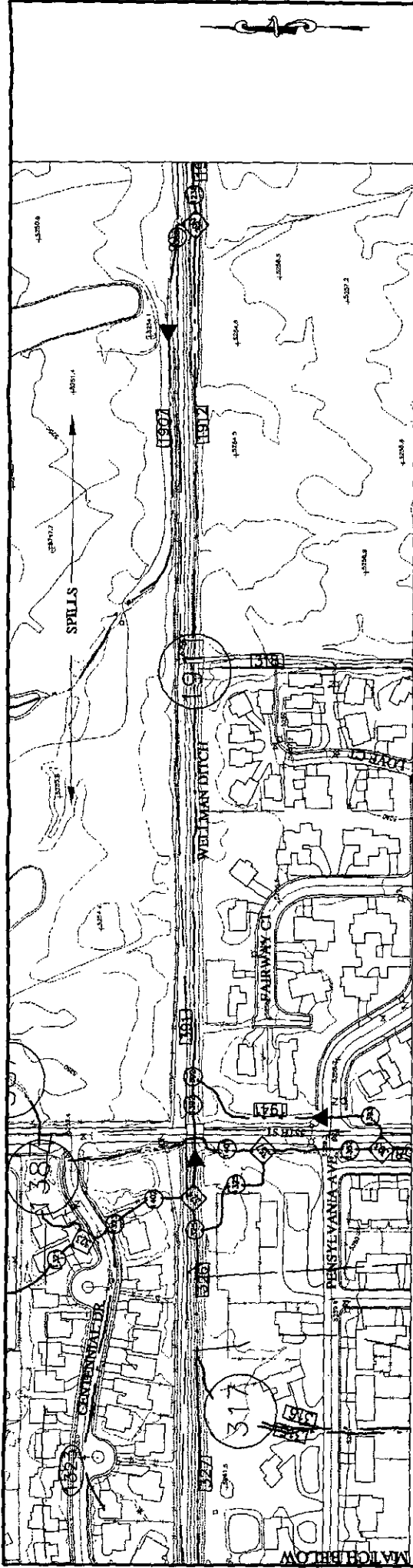
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URBAN DRAINAGE AND FLOOD CONTROL DISTRICT
 CITY OF BOULDER
 UNIVERSITY OF COLORADO

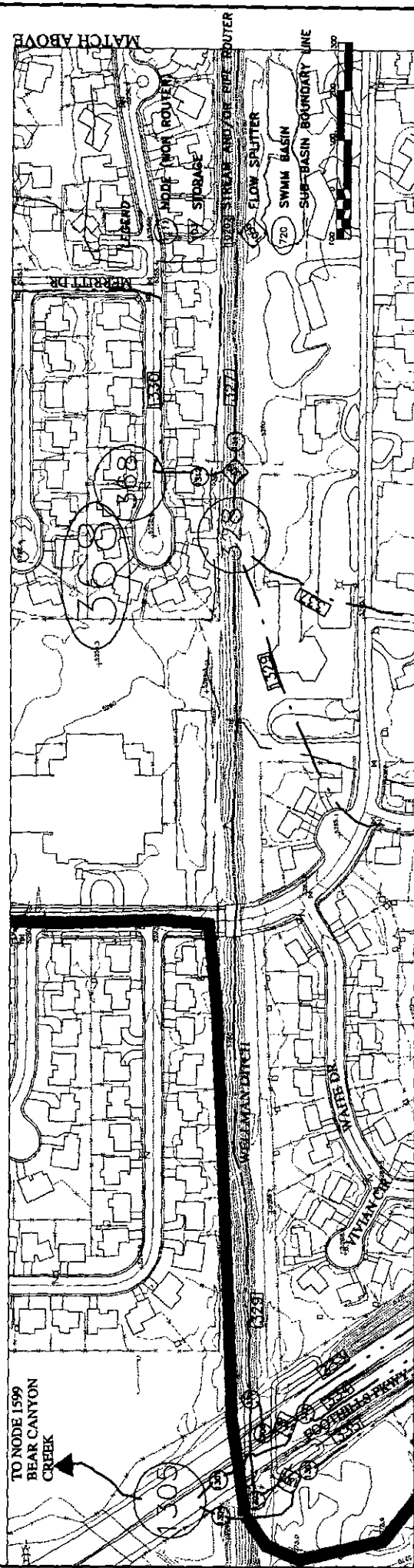
SOUTH BOULDER CREEK HYDROLOGY STUDY
 BASELINE SPLITS

MODEL DETAIL - HIGHWAY 93 AND
 BASELINE SPLITS





WELLMAN SPLITS



ELEMENTS HERE ASSUME NO FLOW ENTERING FROM THE WEST FROM WELLMAN DITCH AND BEAR CANYON CREEK

FOOTHILLS AND WELLMAN ROUTING

	PROJECT NO. 15-0001-01-01 SHEET NO. 11 DATE: 12/20/08 BY: MARGARET M. JEN	URBAN DRAINAGE AND FLOOD CONTROL DISTRICT CITY OF BOULDER BOULDER COUNTY UNIVERSITY OF COLORADO	SOUTH BOULDER CREEK HYDROLOGY STUDY MODEL DETAIL - WELLMAN SPLITS	SHEET NO. 11
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